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# Lecture15: Impedance

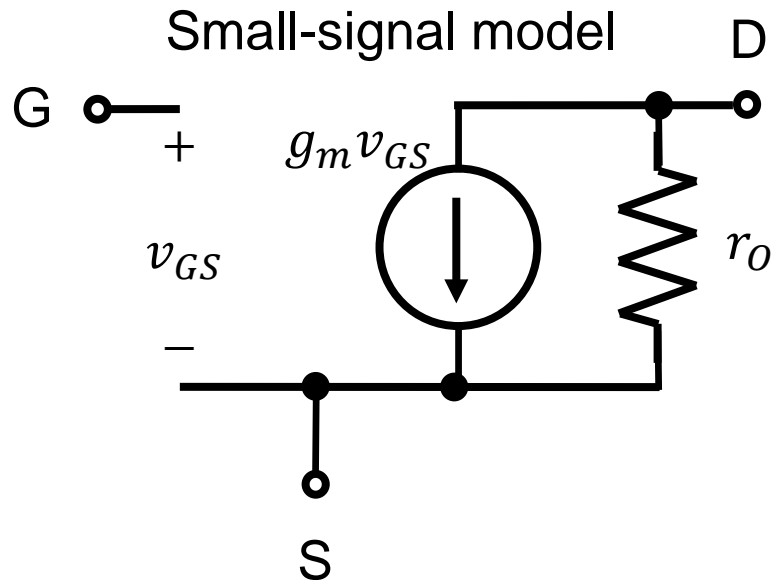
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# Review of previous lecture

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- Small-signal model



# Example 6.14 (Razavi)

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- Assume that  $\mu_n C_{ox} = 100 \mu\text{A V}^{-2}$  and  $\frac{W}{L} = 10$ .
  - When the drain bias current is 0.5 mA, the gate overdrive voltage,  $V_{GS} - V_{TH}$ , is 1 V.
  - Then,

$$g_m = 1 \text{ mS}$$

- Channel-length modulation
  - With the channel-length modulation coefficient,  $\lambda = 0.1 \text{ V}^{-1}$ ,
$$I_D = \frac{1}{2} \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{TH})^2 (1 + \lambda V_{DS})$$
  - Then,

$$r_o = 20 \text{ k}\Omega$$

# Simple math

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- Following relations are useful.
  - Sine and cosine functions can be expanded with  $e^{+j\omega t}$  and  $e^{-j\omega t}$ .

$$\sin \omega t = -\frac{j}{2} e^{+j\omega t} + \frac{j}{2} e^{-j\omega t}$$

$$\cos \omega t = \frac{1}{2} e^{+j\omega t} + \frac{1}{2} e^{-j\omega t}$$

- Therefore, for a function of  $f(t) = f_s \sin \omega t + f_c \cos \omega t$ , the expansion is

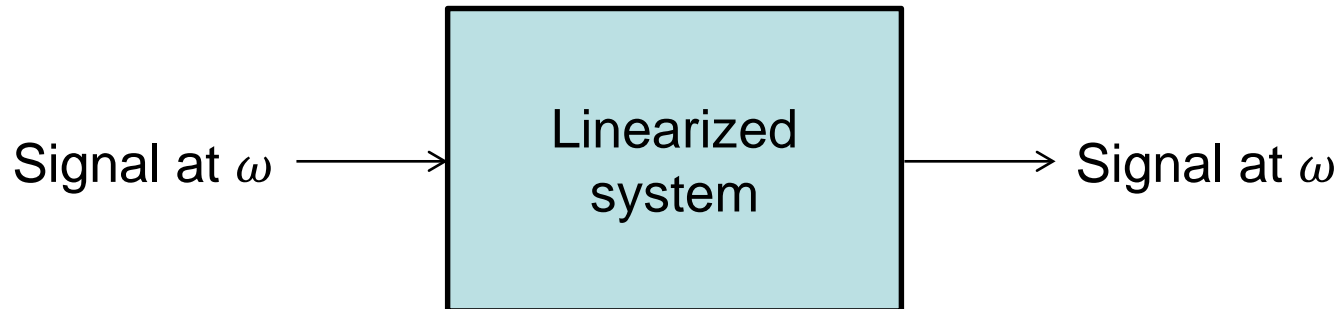
$$f(t) = \left( -j \frac{f_s}{2} + \frac{f_c}{2} \right) e^{+j\omega t} + \left( +j \frac{f_s}{2} + \frac{f_c}{2} \right) e^{-j\omega t}$$

- A single complex number,  $-j \frac{f_s}{2} + \frac{f_c}{2}$ , is enough to represent  $f(t)$ .

# Linearized system

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- Our circuit is nonlinear in general.
- However, we have linearized it.
  - When the input signal has an angular frequency,  $\omega$ , the output signal has the same one.
  - It is sufficient to consider the input-output relation at  $\omega$ .



# Impedance

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- Resistance,  $V(t) = R I(t)$ 
  - It is assumed that  $V(t)$  and  $I(t)$  are in the same phase.
- Impedance,  $V(\omega) = Z(\omega)I(\omega)$ 
  - Consider  $V(t) = V_0 \sin \omega t$  and  $I(t) = I_0 \cos \omega t$ . (Different phases)
  - We introduce a phasor voltage,  $V(\omega)$ , and a phasor current,  $I(\omega)$ .
  - The relation between  $V(t)$  and  $V(\omega)$  is  $V(t) = \text{Re}[V(\omega)e^{j\omega t}]$ .
  - When  $V(t) = V_0 \sin \omega t$ , the phasor voltage is  $V(\omega) = -jV_0$ .
  - When  $I(t) = I_0 \cos \omega t$ , the phasor voltage is  $I(\omega) = I_0$ .
  - In this example,  $Z(\omega) = -j \frac{V_0}{I_0}$ . A purely imaginary number.

# Multi-terminal devices

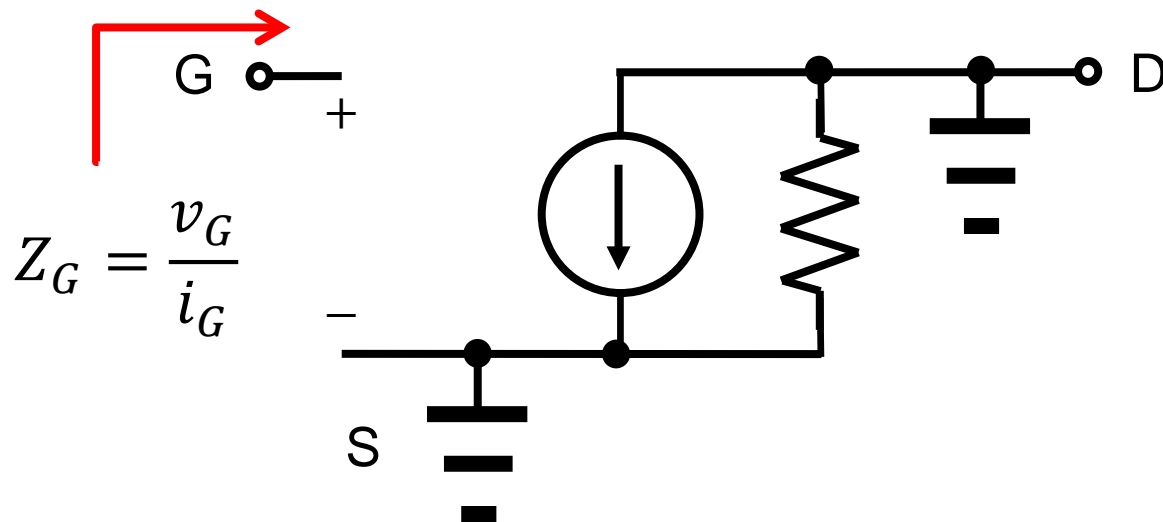
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- When the number of terminals is 3,
  - We can define 9 ( = 3 X 3 ) different impedances.
- Termination condition is important.
  - Depending on the termination condition, the impedance can be heavily changed.
  - In many cases, it is obvious from the problem.

# Impedances of MOSFET

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- “Looking into the TERMINAL,” we see the impedance of the TERMINAL.
  - Example) Looking into the gate. The source and drain are ac-grounded.



- Similar for other terminals



# Input impedance

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- Consider a input signal with a finite internal resistance.
  - Usually, the internal resistance is small, but not zero.
  - The actual small-signal voltage applied to the gate terminal is given by

$$v_G(\omega) = v_{in} \frac{Z_G(\omega)}{r_{int} + Z_G(\omega)}$$

