Lecture14: MOSFET, small-signal model

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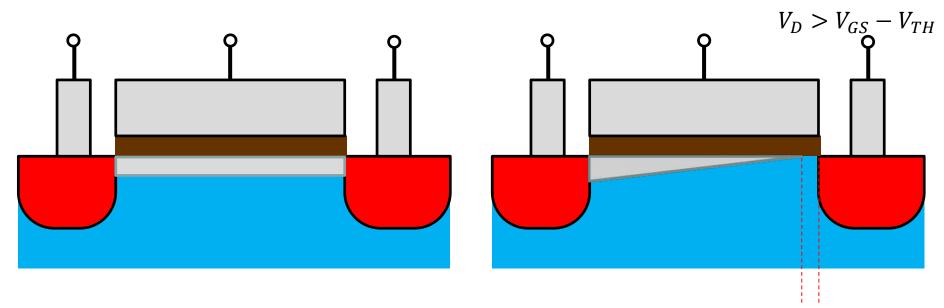
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Review of previous lecture

- How to analyze a circuit with a MOSFET and a resistor
- Transconductance

Channel length modulation

Channel length modulation

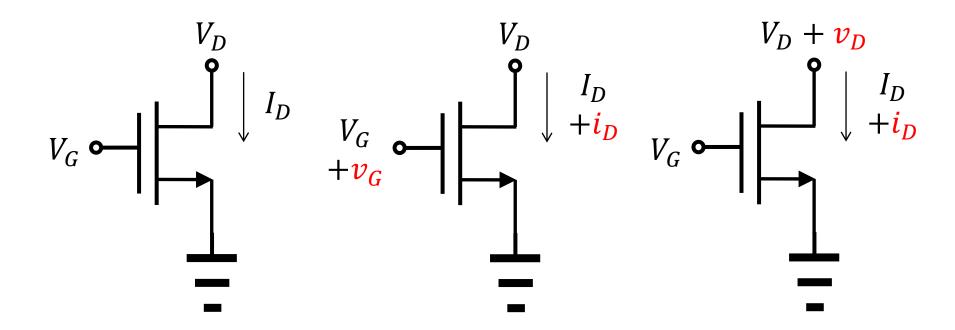


Output resistance?

$$r_O = \frac{\Delta V_{DS}}{\Delta I_D}$$

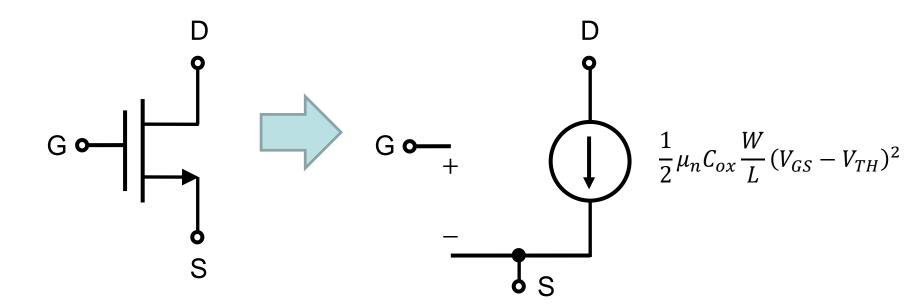
Derivatives

- We can define two derivatives.
 - Transconductance, g_m . Output resistance, r_O .



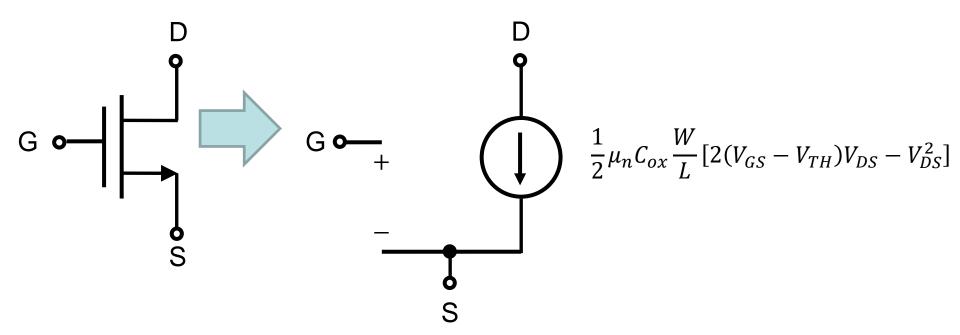
Large-signal model (1/2)

- Saturation region
 - Drain current is determined by gate voltage. (voltage-controlled current source)



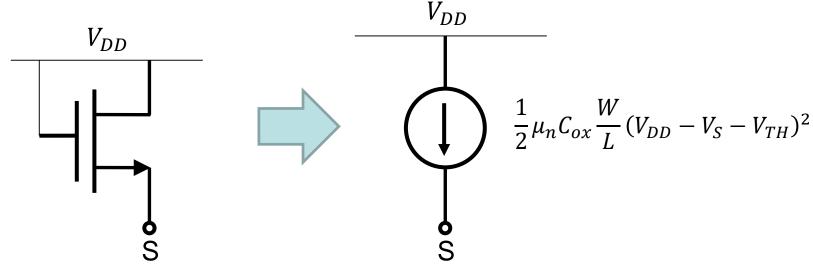
Large-signal model (2/2)

- Triode region
 - Still, it can be described by a voltage-controlled current source.



Example 6.13 (Razavi)

- Always in the saturation region!
 - Any necessary condition?

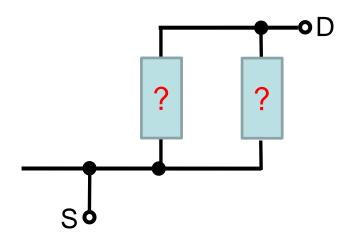


Gate and drain are tied.

They are connected to V_{DD} .

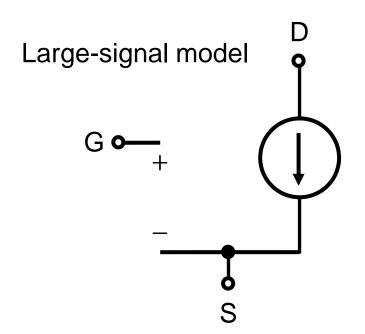
Small-signal current

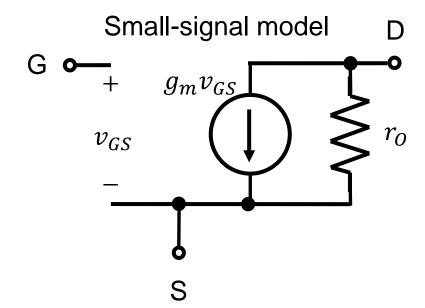
- Using the transconductance (g_m) and the output resistance (r_O) ,
 - The small-signal drain current is given as $i_D = g_m v_G + \frac{v_D}{r_O}$.
 - When we build a small-signal model, two contributions must be separately considered.



Small-signal model

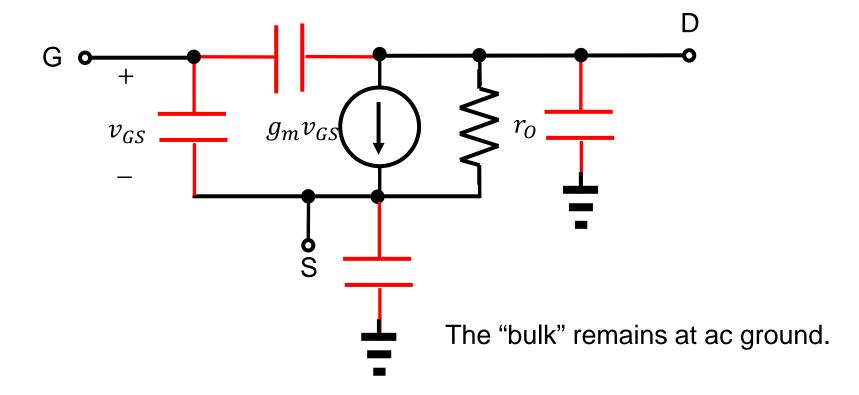
 For small-signal analysis, a small-signal model for the MOSFET is introduced.





Time-dependent one?

In general, capacitive components can be seen.



At low frequencies

- Capacitor current is $I = C \frac{dV}{dt}$.
 - When a sinusoidal dependence, for example $\sin \omega t$, is assumed, the capacitor current is proportional to ω .
 - At low frequencies, ω can be regarded as a small number.
 - In other words, the electric conduction between two nodes becomes rather weak.
 - Therefore, we often neglect the capacitive components in the small-signal model.
 - Of course, at higher frequencies, they become very important.

Simple math

- Following relations are useful.
 - Sine and cosine functions can be expanded with $e^{+j\omega t}$ and $e^{-j\omega t}$.

$$\sin \omega t = -\frac{j}{2}e^{+j\omega t} + \frac{j}{2}e^{-j\omega t}$$
$$\cos \omega t = \frac{1}{2}e^{+j\omega t} + \frac{1}{2}e^{-j\omega t}$$

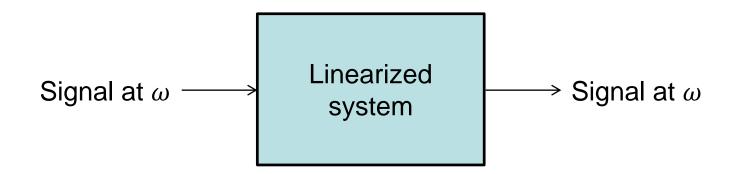
- Therefore, for a function of $f(t) = f_s \sin \omega t + f_c \cos \omega t$, the expansion is

$$f(t) = \left(-j\frac{f_s}{2} + \frac{f_c}{2}\right)e^{+j\omega t} + \left(+j\frac{f_s}{2} + \frac{f_c}{2}\right)e^{-j\omega t}$$

- A single complex number, $-j\frac{f_s}{2} + \frac{f_c}{2}$, is enough to represent f(t).

Linearized system

- Our circuit is nonlinear in general.
- However, we have <u>linearized</u> it.
 - When the input signal has an angluar frequency, ω , the output signal has the same one.
 - It is sufficient to consider the input-output relation at ω .



Impedance

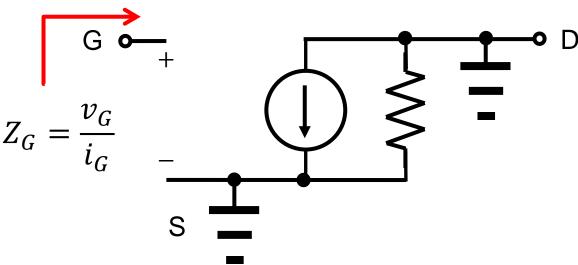
- Resistance, V(t) = R I(t)
 - It is assumed that V(t) and I(t) are in the same phase.
- Impedance, $V(\omega) = Z(\omega)I(\omega)$
 - Consider $V(t) = V_0 \sin \omega t$ and $I(t) = I_0 \cos \omega t$. (Different phases)
 - We introduce a phasor voltage, $V(\omega)$, and a phasor current, $I(\omega)$.
 - The relation between V(t) and $V(\omega)$ is $V(t) = Re[V(\omega)e^{j\omega t}]$.
 - When $V(t) = V_0 \sin \omega t$, the phasor voltage is $V(\omega) = -jV_0$.
 - When $I(t) = I_0 \cos \omega t$, the phasor voltage is $I(\omega) = I_0$.
 - In this example, $Z(\omega) = -j\frac{V_0}{I_0}$. A purely imaginary number.

Multi-terminal devices

- When the number of terminals is 3,
 - We can define $9 (= 3 \times 3)$ different impedances.
- Termination condition is important.
 - Depending on the termination condition, the impedance can be heavily changed.
 - In many cases, it is obvious from the problem.

Impedances of MOSFET

- "Looking into the <u>TERMINAL</u>," we see the impedance of the <u>TERMINAL</u>.
 - Example) Looking into the gate. The source and drain are acgrounded.

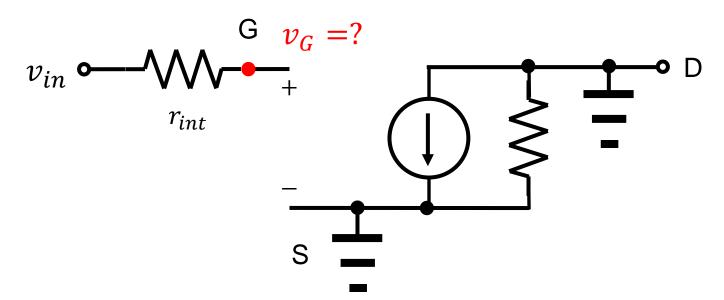


Similar for other terminals

Input impedance

- Consider a input signal with a finite internal resistance.
 - Usually, the internal resistance is small, but not zero.
 - The actual small-signal voltage applied to the gate terminal is given by

$$v_G(\omega) = v_{in} \frac{Z_G(\omega)}{r_{int} + Z_G(\omega)}$$



GIST Lecture on May 6, 2020 (Internal use only)