# VLSI Devices Lecture 13

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#### **Drain current**

- Using the previous approximation,
  - We can obtain the following expression:

$$\begin{split} I_{d} &= \mu_{eff} \frac{W}{L} \bigg\{ C_{ox} \bigg( V_{gs} - V_{fb} + \frac{k_{B}T}{q} \bigg) \phi_{s} - \frac{1}{2} C_{ox} \phi_{s}^{2} - \frac{2}{3} \sqrt{2 \epsilon_{si} q N_{a}} \phi_{s}^{1.5} \\ &+ \frac{k_{B}T}{q} \sqrt{2 \epsilon_{si} q N_{a} \phi_{s}} \bigg\} \bigg|_{\phi_{s,s}}^{\phi_{s,d}} \end{split}$$
 Taur, Eq. (3.21)

–Only with  $\phi_{s,s}$  and  $\phi_{s,d}$ , we can evaluate the drain current.

## Regional approximations

- After the onset of inversion but <u>before saturation</u>,
  - The surface potential,  $\phi_s(y)$ , can be approximated by  $\phi(0,y) = V(y) + 2\phi_B$

- It means that

$$\phi_{s,s} = 2\phi_B$$
$$\phi_{s,d} = 2\phi_B + V_{ds}$$

– In this case,  $rac{dV}{d\phi_{\it S}}=1$  . We must calculate the following term for  $\phi_{\it S,d}$  :

$$C_{ox}(V_{gs} - V_{fb})(2\phi_B + V_{ds}) - \frac{1}{2}C_{ox}(2\phi_B + V_{ds})^2 - \frac{2}{3}\sqrt{2\epsilon_{si}qN_a}(2\phi_B + V_{ds})^{1.5}$$

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Taur, Eq. (3.3)

## A simpler form of $I_d$

• By taking the difference, we can find a simpler form:

$$\begin{split} & I_{d} \\ &= \mu_{eff} \frac{W}{L} \bigg\{ C_{ox} \bigg( V_{gs} - V_{fb} - 2\phi_{B} - \frac{1}{2} V_{ds} \bigg) V_{ds} \\ & - \frac{2}{3} \sqrt{2\epsilon_{si} q N_{a}} \big[ (2\phi_{B} + V_{ds})^{1.5} - (2\phi_{B})^{1.5} \big] \bigg\} \quad \text{Taur, Eq. (3.22)} \end{split}$$

– For a given  $V_{gs}$ ,  $I_d$  first increases linearly with  $V_{ds}$ , then gradually levels off to a saturated value.

## Linear (triode) region

• When  $V_{ds}$  is small, we may keep only up to the first order.

$$\begin{split} & I_{d} \\ & = \mu_{eff} \frac{W}{L} \bigg\{ C_{ox} \big( V_{gs} - V_{fb} - 2\phi_B \big) V_{ds} - \frac{2}{3} \sqrt{2\epsilon_{si}qN_a} \left[ \frac{3}{2} (2\phi_B)^{0.5} V_{ds} \right] \bigg\} \\ & = \mu_{eff} \frac{W}{L} C_{ox} \left( V_{gs} - V_{fb} - 2\phi_B - \frac{\sqrt{4\epsilon_{si}qN_a\phi_B}}{C_{ox}} \right) V_{ds} \\ & = \mu_{eff} \frac{W}{L} C_{ox} \big( V_{gs} - V_t \big) V_{ds} \end{split} \qquad \qquad \text{Taur, Eq. (3.23)}$$

- The threshold voltage,  $V_t$ , is given by

$$V_t = V_{fb} + 2\phi_B + \frac{\sqrt{4\epsilon_{si}qN_a\phi_B}}{C_{ox}}$$
 Taur, Eq. (3.24)

– It is the gate voltage when the surface potential reaches at  $2\phi_B$ .

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### Parabolic region

We must keep up to the second order.

$$\begin{split} I_{d} &= \mu_{eff} \frac{W}{L} \left\{ C_{ox} \left( V_{gs} - V_{fb} - 2\phi_{B} - \frac{1}{2} V_{ds} \right) V_{ds} \right. \\ &- \frac{2}{3} \sqrt{2\epsilon_{si} q N_{a}} \left[ \frac{3}{2} (2\phi_{B})^{0.5} V_{ds} + \frac{3}{8} (2\phi_{B})^{-0.5} V_{ds}^{2} \right] \right\} \\ &= \mu_{eff} \frac{W}{L} \left\{ C_{ox} \left( V_{gs} - V_{t} - \frac{1}{2} V_{ds} \right) V_{ds} - \frac{1}{4} \sqrt{2\epsilon_{si} q N_{a}} \left[ (2\phi_{B})^{-0.5} V_{ds}^{2} \right] \right\} \\ &= \mu_{eff} \frac{W}{L} \left\{ C_{ox} \left( V_{gs} - V_{t} \right) V_{ds} - \frac{1}{2} C_{ox} \left[ 1 + \frac{\sqrt{\epsilon_{si} q N_{a} / (4\phi_{B})}}{C_{ox}} \right] V_{ds}^{2} \right\} \end{split}$$

Taur, Eq. (3.25)

## Let's introduce a factor, m.

• It is given as

$$m = 1 + \frac{\sqrt{\epsilon_{si}qN_a/(4\phi_B)}}{C_{ox}}$$

Taur, Eq. (3.26)

- From the maximum depletion width,

$$W_{dm} = \sqrt{\frac{4\epsilon_{si}\phi_B}{qN_a}}$$

Taur, Eq. (2.190)

- An alternative form is available,

$$m = 1 + \frac{C_{dm}}{C_{ox}} = 1 + \frac{3t_{ox}}{W_{dm}}$$

Taur, Eq. (3.27)

## Its physical meaning

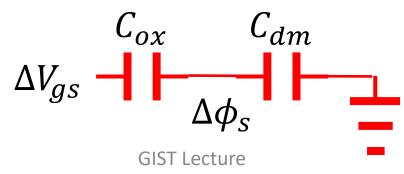
- Serial capacitors give  $\frac{C_{ox}C_{dm}}{C_{ox}+C_{dm}}$ .
  - Charge across the oxide capacitor:

$$\frac{C_{ox}C_{dm}}{C_{ox} + C_{dm}} \Delta V_{gs} = C_{dm} \Delta \phi_s$$

-Therefore,

$$m = \frac{C_{ox} + C_{dm}}{C_{ox}} = \frac{\Delta V_{gs}}{\Delta \phi_s}$$

-m should be kept close to one.



#### **Saturation current**

- Maximum value of  $I_d$  at a given  $V_{gs}$ 
  - Recall that

$$I_{d} = \mu_{eff} \frac{W}{L} \Big\{ C_{ox} \big( V_{gs} - V_{t} \big) V_{ds} - \frac{m}{2} C_{ox} V_{ds}^{2} \Big\} \quad \text{Taur, Eq. (3.25)}$$
 - When  $V_{ds} = V_{dsat} = \frac{V_{gs} - V_{t}}{m}$ ,

$$I_{d} = I_{dsat} = \mu_{eff} C_{ox} \frac{W}{L} \frac{(V_{gs} - V_{t})^{2}}{2m}$$
 Taur, Eq. (3.28)

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#### Pinch-off

• For  $\phi_S = 2\phi_B + V$ , the Tylor expansion gives

$$Q_{i} = -C_{ox}(V_{gs} - V_{fb} - 2\phi_{B} - V) + \sqrt{4\epsilon_{si}qN_{a}\phi_{B}} + \sqrt{\frac{\epsilon_{si}qN_{a}}{4\phi_{B}}}V$$

$$Q_{i} = -C_{ox}\left(V_{gs} - V_{t} - V - \frac{1}{C_{ox}}\sqrt{\frac{\epsilon_{si}qN_{a}}{4\phi_{B}}}V\right) = C_{ox}(V_{gs} - V_{t} - mV)$$
Taur, Eq. (3.29)

-At  $V_{ds} = \frac{V_{gs} - V_t}{m}$  (on-set of saturation), the surface channel vanishes at the drain end of the channel.

## Subthreshold current (1)

- ullet Subthreshold region where  $V_{gs} < V_t$ 
  - Recall that

$$-Q_{S} = \sqrt{2\epsilon_{Si}k_{B}TN_{a}} \left[ \frac{q\phi_{S}}{k_{B}T} + \frac{n_{i}^{2}}{N_{a}^{2}} \exp\left(\frac{q}{k_{B}T}(\phi_{S} - V)\right) \right]^{1/2}$$
Taur, Eq. (3.35)

- Its Taylor expansion

Small in the subthreshold region

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$$-Q_{s} \approx \sqrt{2\epsilon_{si}k_{B}TN_{a}} \left| \sqrt{\frac{q\phi_{s}}{k_{B}T} + \frac{1}{2}} \sqrt{\frac{k_{B}T}{q\phi_{s}} \frac{n_{i}^{2}}{N_{a}^{2}}} \exp\left(\frac{q}{k_{B}T}(\phi_{s} - V)\right) \right|$$

## Subthreshold current (2)

The second term for the inversion charge

$$-Q_i \approx \sqrt{\frac{\epsilon_{si}qN_a}{2\phi_s}\frac{k_BT}{q}\frac{n_i^2}{N_a^2}} \exp\left(\frac{q}{k_BT}(\phi_s - V)\right) \text{ Taur, Eq. (3.36)}$$

- In this case,  $\phi_{S}$  is a function of  $V_{qS}$  only.
- Recall

$$I_d = \mu_{eff} \frac{W}{L} \int_0^{V_{ds}} [-Q_i(V)] dV$$
 Taur, Eq. (3.10)

–Then, we have

$$I_{d} = \mu_{eff} \frac{W}{L} \sqrt{\frac{\epsilon_{si} q N_{a}}{4\phi_{B}}} \left(\frac{k_{B}T}{q}\right)^{2} \left(\frac{n_{i}}{N_{a}}\right)^{2} \exp\left(\frac{q\phi_{s}}{k_{B}T}\right) \left(1 - \exp\left(-\frac{qV_{ds}}{k_{B}T}\right)\right)$$
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Taur, Eq. (3.37)

## Subthreshold current (3)

• Since 
$$m=\frac{\Delta V_{gs}}{\Delta \phi_s}$$
,  $V_{gs}-V_t=m(\phi_s-2\phi_B)$ .

-Then,

$$\exp\left(\frac{q\phi_S}{k_BT}\right) = \exp\left(\frac{q(V_{gs} - V_t)}{mk_BT}\right) \exp\left(2\frac{q\phi_B}{k_BT}\right)$$

- From the above expression,

$$= \mu_{eff} \frac{W}{L} \sqrt{\frac{\epsilon_{si} q N_a}{4\phi_B} \left(\frac{k_B T}{q}\right)^2} \exp\left(\frac{q(V_{gs} - V_t)}{m k_B T}\right) \left(1 - \exp\left(-\frac{q V_{ds}}{k_B T}\right)\right)$$

Taur, Eq. (3.39)

## Subthreshold slope (1)

•  $I_d$  is independent of  $V_{ds}$ , when  $V_{ds} \gg k_B T/q$ .

$$I_{d} = \mu_{eff} \frac{W}{L} \sqrt{\frac{\epsilon_{si} q N_{a}}{2\phi_{s}}} \left(\frac{k_{B}T}{q}\right)^{2} \exp\left(\frac{q(V_{gs} - V_{t})}{mk_{B}T}\right)$$

- Its gate voltage dependence is very important.

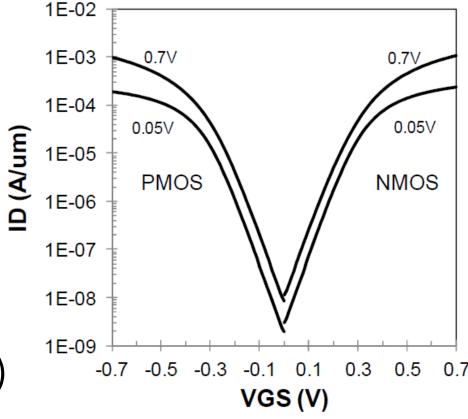
$$\log_{10} I_d = (a \ constant) + \frac{q(V_{gs} - V_t)}{mk_B T} \log_{10} e$$

$$\frac{d(\log_{10} I_d)}{dV_{gs}} = \frac{q}{mk_B T} \log_{10} e$$
Subthreshold slope 
$$S = \left(\frac{d(\log_{10} I_d)}{dV_{gs}}\right)^{-1} = \frac{mk_B T}{q} \ln 10$$
 Taur, Eq. (3.41)

## Subthreshold slope (2)

- At 300 K,  $\frac{k_B T}{q} \ln 10$  is 60 mV/dec.
  - -Note that m is larger than 1.

Subthreshold behavior (Natarajan, IEDM 2024)



## Thank you!