Large scale Finite Element solvers for the large eddy simulation of incompressible turbulent flows

author:
Oriol Colomés Gené
supervisor:
Santiago Badia

Departament d'Enginyeria Civil i Ambiental

February 25, 2016



Mixed FE VMS

- 1. Motivation
- 2. Residual-based VMS
- 3. Mixed FE VMS
- 4. Segregated Runge-Kutta
- 5. Segregated VMS
- 6. Conclusions

Mixed FE VMS

- 1. Motivation
- 2. Residual-based VMS
- 3. Mixed FE VMS
- 4. Segregated Runge-Kutta
- Segregated VMS
- 6. Conclusions

Segregated VMS

Motivation

Thesis motivation

Highly scalable Finite Element (FE) framework for Large Eddy Simulations (LES) of incompressible turbulent flows

Segregated VMS

Motivation

Thesis motivation

Highly scalable Finite Element (FE) framework for Large Eddy Simulations (LES) of incompressible turbulent flows

How to get there?

Thesis motivation

Residual-based VMS

Highly scalable Finite Element (FE) framework for Large Eddy Simulations (LES) of incompressible turbulent flows

How to get there?

1. Variational MultiScale (VMS) methods as LES models.

Thesis motivation

Highly scalable Finite Element (FE) framework for Large Eddy Simulations (LES) of incompressible turbulent flows

How to get there?

- Variational MultiScale (VMS) methods as LES models.
- 2. Time integration schemes with velocity-pressure segregation.

Thesis motivation

Highly scalable Finite Element (FE) framework for Large Eddy Simulations (LES) of incompressible turbulent flows

How to get there?

- Variational MultiScale (VMS) methods as LES models.
- Time integration schemes with velocity-pressure segregation.
- 3. Highly scalable algorithms based on Domain Decomposition (DD) and block preconditioners.

Step by step...

Residual-based VMS as LES models.

- Residual-based VMS as LES models.
- Mixed FE formulations LES.

- Residual-based VMS as LES models.
- Mixed FE formulations LES.
- High-order FE methods.

- Residual-based VMS as LES models.
- Mixed FE formulations LES.
- High-order FE methods.
- High-order time integration schemes.

Segregated VMS

Motivation

- Residual-based VMS as LES models.
- Mixed FE formulations LES.
- High-order FE methods.
- High-order time integration schemes.
- Adaptive time stepping techniques.

- Residual-based VMS as LES models.
- Mixed FE formulations LES.
- High-order FE methods.
- High-order time integration schemes.
- Adaptive time stepping techniques.
- Velocity-pressure segregation.

- Residual-based VMS as LES models.
- Mixed FE formulations LES.
- High-order FE methods.
- High-order time integration schemes.
- Adaptive time stepping techniques.
- Velocity-pressure segregation.
- Scalable solvers.

- Residual-based VMS as LES models.
- Mixed FE formulations LES.
- High-order FE methods.
- High-order time integration schemes.
- Adaptive time stepping techniques.
- Velocity-pressure segregation.
- Scalable solvers.
- · Application.

- Residual-based VMS as LES models.
- Mixed FE formulations LES.
- High-order FE methods.
- High-order time integration schemes.
- Adaptive time stepping techniques.
- Velocity-pressure segregation.
- Scalable solvers.
- Application.

2. Residual-based VMS Formulation **Energy statements** Numerical experiments Conclusions



Implicit LES

ILES: only numerical dissipation (for stabilization) acts as turbulent model

Not based on filtering of the Navier-Stokes equations

Mixed FE VMS

Rely on numerical artifacts, no modification at the continuous level

Mixed FE VMS

Incomp. Navier Stokes equations

Find \mathbf{u} and p defined in Ω

$$\partial_t \mathbf{u} + \mathbf{u} \cdot \nabla \mathbf{u} + \nabla p - \nu \nabla^2 \mathbf{u} = \mathbf{f}$$
$$\nabla \cdot \mathbf{u} = 0$$

with appropriate boundary conditions on Γ .

Incomp. Navier Stokes equations

Mixed FE VMS

Find **u** and **p** defined in Ω

$$\partial_t \mathbf{u} + \mathbf{u} \cdot \nabla \mathbf{u} + \nabla p - \nu \nabla^2 \mathbf{u} = \mathbf{f}$$
$$\nabla \cdot \mathbf{u} = 0$$

with appropriate boundary conditions on Γ .

The weak problem is: $\forall \mathbf{v} \in \mathcal{V}_0$ and $\forall q \in \mathcal{Q}_0$, find $\mathbf{u} \in \mathcal{V}$ and $p \in \mathcal{Q}$ such that

$$(\mathbf{v}, \partial_t \mathbf{u})_{\Omega} + (\nabla \mathbf{v}, \nu \nabla \mathbf{u})_{\Omega} + b(\mathbf{u}, \mathbf{u}, \mathbf{v}) - (\nabla \cdot \mathbf{v}, p)_{\Omega} = \langle \mathbf{v}, \mathbf{f} \rangle_{\Omega}$$

$$(q, \nabla \cdot \mathbf{u})_{\Omega} = 0$$

Incomp. Navier Stokes equations

Find \mathbf{u} and p defined in Ω

$$\partial_t \mathbf{u} + \mathbf{u} \cdot \nabla \mathbf{u} + \nabla p - \nu \nabla^2 \mathbf{u} = \mathbf{f}$$

 $\nabla \cdot \mathbf{u} = 0$

with appropriate boundary conditions on Γ .

The weak problem is: $\forall \mathbf{v} \in \mathcal{V}_0$ and $\forall q \in \mathcal{Q}_0$, find $\mathbf{u} \in \mathcal{V}$ and $p \in \mathcal{Q}$ such that

$$(\mathbf{v}, \partial_t \mathbf{u})_{\Omega} + (\nabla \mathbf{v}, \nu \nabla \mathbf{u})_{\Omega} + b(\mathbf{u}, \mathbf{u}, \mathbf{v}) - (\nabla \cdot \mathbf{v}, p)_{\Omega} = \langle \mathbf{v}, \mathbf{f} \rangle_{\Omega}$$

$$(q, \nabla \cdot \mathbf{u})_{\Omega} = 0$$

where

Motivation

$$b(\mathbf{a}, \mathbf{u}, \mathbf{v}) = \langle \mathbf{v}, \mathbf{a} \cdot \nabla \mathbf{u} \rangle_{\Omega}$$

Incomp. Navier Stokes equations

Find \mathbf{u} and p defined in Ω

$$\partial_t \mathbf{u} + \mathbf{u} \cdot \nabla \mathbf{u} + \nabla p - \nu \nabla^2 \mathbf{u} = \mathbf{f}$$
$$\nabla \cdot \mathbf{u} = 0$$

with appropriate boundary conditions on Γ .

The weak problem is: $\forall \mathbf{v} \in \mathcal{V}_0$ and $\forall q \in \mathcal{Q}_0$, find $\mathbf{u} \in \mathcal{V}$ and $p \in \mathcal{Q}$ such that

$$(\mathbf{v}, \partial_t \mathbf{u})_{\Omega} + (\nabla \mathbf{v}, \nu \nabla \mathbf{u})_{\Omega} + b (\mathbf{u}, \mathbf{u}, \mathbf{v}) - (\nabla \cdot \mathbf{v}, p)_{\Omega} = \langle \mathbf{v}, \mathbf{f} \rangle_{\Omega}$$

$$(q, \nabla \cdot \mathbf{u})_{\Omega} = 0$$

where

Motivation

$$b\left(\mathbf{a},\mathbf{u},\mathbf{v}\right) = \frac{1}{2} \langle \mathbf{v},\mathbf{a}\cdot\nabla\mathbf{u}\rangle_{\Omega} - \frac{1}{2} \langle \mathbf{a}\cdot\nabla\mathbf{v},\mathbf{u}\rangle_{\Omega} + \frac{1}{2} \langle \mathbf{v},\mathbf{n}\cdot\mathbf{a}\mathbf{u}\rangle_{\Gamma}$$

A decomposition of spaces $\mathcal V$ and $\mathcal Q$ given by

Mixed FE VMS

$$\mathcal{V} = \mathcal{V}_h \oplus \widetilde{\mathcal{V}}, \quad \mathcal{Q} = \mathcal{Q}_h \oplus \widetilde{\mathcal{Q}}$$

A decomposition of spaces $\mathcal V$ and $\mathcal Q$ given by

$$\mathcal{V} = \mathcal{V}_h \oplus \widetilde{\mathcal{V}}, \quad \mathcal{Q} = \mathcal{Q}_h \oplus \widetilde{\mathcal{Q}}$$

is applied to the function and test spaces

$$\mathbf{u} = \mathbf{u}_h + \widetilde{\mathbf{u}}, \quad p = p_h + \widetilde{p}$$

 $\mathbf{v} = \mathbf{v}_h + \widetilde{\mathbf{v}}, \quad q = q_h + \widetilde{q}$

A decomposition of spaces $\mathcal V$ and $\mathcal Q$ given by

Mixed FE VMS

$$\mathcal{V} = \mathcal{V}_h \oplus \widetilde{\mathcal{V}}, \quad \mathcal{Q} = \mathcal{Q}_h \oplus \widetilde{\mathcal{Q}}$$

is applied to the function and test spaces

$$\mathbf{u} = \mathbf{u}_h + \widetilde{\mathbf{u}}, \quad p = p_h + \widetilde{p}$$

 $\mathbf{v} = \mathbf{v}_h + \widetilde{\mathbf{v}}, \quad q = q_h + \widetilde{q}$

We keep all the (eight) contributions from the splitting of the convective term

$$\mathbf{u} \cdot \nabla \mathbf{u} = \mathbf{u}_h \cdot \nabla \mathbf{u}_h + \widetilde{\mathbf{u}} \cdot \nabla \mathbf{u}_h + \mathbf{u}_h \cdot \nabla \widetilde{\mathbf{u}} + \widetilde{\mathbf{u}} \cdot \nabla \widetilde{\mathbf{u}}$$

A decomposition of spaces \mathcal{V} and \mathcal{Q} given by

$$\mathcal{V} = \mathcal{V}_h \oplus \widetilde{\mathcal{V}}, \quad \mathcal{Q} = \mathcal{Q}_h \oplus \widetilde{\mathcal{Q}}$$

is applied to the function and test spaces

$$\mathbf{u} = \mathbf{u}_h + \widetilde{\mathbf{u}}, \quad p = p_h + \widetilde{p}$$

 $\mathbf{v} = \mathbf{v}_h + \widetilde{\mathbf{v}}, \quad q = q_h + \widetilde{q}$

We keep all the (eight) contributions from the splitting of the convective term

$$\mathbf{u} \cdot \nabla \mathbf{u} = \mathbf{u}_h \cdot \nabla \mathbf{u}_h + \mathbf{\tilde{u}} \cdot \nabla \mathbf{u}_h + \mathbf{u}_h \cdot \nabla \mathbf{\tilde{u}} + \mathbf{\tilde{u}} \cdot \nabla \mathbf{\tilde{u}}$$

and all the (four) contributions from the temporal term

$$\partial_t \mathbf{u} = \partial_t \mathbf{u}_h + \frac{\partial_t \widetilde{\mathbf{u}}}{\mathbf{u}}$$

Semidiscrete problem

FEM equations

$$B((\mathbf{u}_h, p_h); (\widetilde{\mathbf{u}}, \widetilde{p}); (\mathbf{v}_h, q_h)) = L(\mathbf{v}_h, q_h)$$

Mixed FE VMS

$$B((\widetilde{\mathbf{u}}, \widetilde{p}); (\mathbf{u}_h, p_h); (\widetilde{\mathbf{v}}, \widetilde{q})) = L(\widetilde{\mathbf{v}}, \widetilde{q})$$

Semidiscrete problem

FEM equations

$$(\mathbf{v}_{h}, \partial_{t}\mathbf{u}_{h})_{\Omega} + b(\mathbf{a}, \mathbf{u}_{h}, \mathbf{v}_{h}) + (\nabla \mathbf{v}_{h}, \nu \nabla \mathbf{u}_{h})_{\Omega} - (\nabla \cdot \mathbf{v}_{h}, p_{h})_{\Omega}$$
$$+ (\mathbf{v}_{h}, \partial_{t}\widetilde{\mathbf{u}})_{\Omega} + (\mathcal{L}^{*}\mathbf{v}_{h}, \widetilde{\mathbf{u}})_{\Omega^{h}} - (\nabla \cdot \mathbf{v}_{h}, \widetilde{p})_{\Omega^{h}} = \langle \mathbf{v}_{h}, \mathbf{f} \rangle_{\Omega}$$
$$(q_{h}, \nabla \cdot \mathbf{u}_{h})_{\Omega} - (\nabla q_{h}, \widetilde{\mathbf{u}})_{\Omega^{h}} = 0$$

Mixed FE VMS

$$\partial_t \widetilde{\mathbf{u}} + \tau_m^{-1} \widetilde{\mathbf{u}} = \mathcal{P} \mathbf{R}_m$$
$$\tau_c^{-1} \widetilde{\mathbf{p}} = \mathcal{P} \mathbf{R}_c$$

$$au_m = \left(\frac{c_1 \nu}{h^2} + \frac{c_2 |\mathbf{a}|}{h}\right)^{-1}, \quad au_c = \frac{h^2}{c_1 au_m}$$

$$\mathbf{a} = \mathbf{u}_h + \widetilde{\mathbf{u}}$$

Semidiscrete problem

FEM equations

$$\begin{aligned} (\mathbf{v}_{h}, \partial_{t}\mathbf{u}_{h})_{\Omega} + b (\mathbf{a}, \mathbf{u}_{h}, \mathbf{v}_{h}) + (\nabla \mathbf{v}_{h}, \nu \nabla \mathbf{u}_{h})_{\Omega} - (\nabla \cdot \mathbf{v}_{h}, p_{h})_{\Omega} \\ + (\mathbf{v}_{h}, \partial_{t}\widetilde{\mathbf{u}})_{\Omega} + (\mathcal{L}^{*}\mathbf{v}_{h}, \widetilde{\mathbf{u}})_{\Omega^{h}} - (\nabla \cdot \mathbf{v}_{h}, \widetilde{p})_{\Omega^{h}} = \langle \mathbf{v}_{h}, \mathbf{f} \rangle_{\Omega} \\ (q_{h}, \nabla \cdot \mathbf{u}_{h})_{\Omega} - (\nabla q_{h}, \widetilde{\mathbf{u}})_{\Omega^{h}} = 0 \end{aligned}$$

Mixed FE VMS

$$\partial_t \tilde{\mathbf{u}} + \tau_m^{-1} \tilde{\mathbf{u}} = \mathcal{P} \mathbf{R}_m$$
$$\tau_c^{-1} \tilde{\mathbf{p}} = \mathcal{P} \mathbf{R}_c$$

$$\mathbf{R}_m := \mathbf{f} - \partial_t \mathbf{u}_h - \mathcal{L} \mathbf{u}_h - \nabla p_h, \quad \mathbf{R}_c := -\nabla \cdot \mathbf{u}_h$$

Semidiscrete problem

FEM equations

$$(\mathbf{v}_{h}, \partial_{t}\mathbf{u}_{h})_{\Omega} + b(\mathbf{a}, \mathbf{u}_{h}, \mathbf{v}_{h}) + (\nabla \mathbf{v}_{h}, \nu \nabla \mathbf{u}_{h})_{\Omega} - (\nabla \cdot \mathbf{v}_{h}, p_{h})_{\Omega}$$
$$+ (\mathbf{v}_{h}, \partial_{t}\widetilde{\mathbf{u}})_{\Omega} + (\mathcal{L}^{*}\mathbf{v}_{h}, \widetilde{\mathbf{u}})_{\Omega^{h}} - (\nabla \cdot \mathbf{v}_{h}, \widetilde{p})_{\Omega^{h}} = \langle \mathbf{v}_{h}, \mathbf{f} \rangle_{\Omega}$$
$$(q_{h}, \nabla \cdot \mathbf{u}_{h})_{\Omega} - (\nabla q_{h}, \widetilde{\mathbf{u}})_{\Omega^{h}} = 0$$

Mixed FE VMS

$$\partial_t \tilde{\mathbf{u}} + \tau_m^{-1} \tilde{\mathbf{u}} = \mathcal{P} \mathbf{R}_m$$
$$\tau_c^{-1} \tilde{\mathbf{p}} = \mathcal{P} \mathbf{R}_c$$

$$\mathcal{P} = I$$
 (ASGS), $\mathcal{P} = P_h^{\perp} = I - P_h$ (OSS)

Semidiscrete problem

FEM equations

$$\begin{aligned} (\mathbf{v}_{h}, \partial_{t}\mathbf{u}_{h})_{\Omega} + b (\mathbf{a}, \mathbf{u}_{h}, \mathbf{v}_{h}) + (\nabla \mathbf{v}_{h}, \nu \nabla \mathbf{u}_{h})_{\Omega} - (\nabla \cdot \mathbf{v}_{h}, p_{h})_{\Omega} \\ + (\mathbf{v}_{h}, \partial_{t}\widetilde{\mathbf{u}})_{\Omega} + (\mathcal{L}^{*}\mathbf{v}_{h}, \widetilde{\mathbf{u}})_{\Omega^{h}} - (\nabla \cdot \mathbf{v}_{h}, \widetilde{p})_{\Omega^{h}} = \langle \mathbf{v}_{h}, \mathbf{f} \rangle_{\Omega} \\ (q_{h}, \nabla \cdot \mathbf{u}_{h})_{\Omega} - (\nabla q_{h}, \widetilde{\mathbf{u}})_{\Omega^{h}} = 0 \end{aligned}$$

Mixed FE VMS

$$\partial_t \tilde{\mathbf{u}} + \tau_m^{-1} \tilde{\mathbf{u}} = \mathcal{P} \mathbf{R}_m$$
$$\tau_c^{-1} \tilde{\mathbf{p}} = \mathcal{P} R_c$$

$$\mathcal{P} = I$$
 (ASGS), $\mathcal{P} = P_h^{\perp} = I - P_h$ (OSS)

$$\mathbf{a} = \mathbf{u}_h + \widetilde{\mathbf{u}}$$

Summary

	Sgs space	Sgs dynamics	Advection
1	ASGS	Static	Linear
2	ASGS	Dynamic	Linear
3	ASGS	Dynamic	Nonlinear
4	OSS	Static	Linear
5	OSS	Dynamic	Linear
6	OSS	Dynamic	Nonlinear

Mixed FE VMS

- 1 It is the most standard method (SUPG for linear elements) up to the choice of the stabilization parameters. Unknown stability properties.
- 4 Strictly pointwise positive for linear elements (no backscatter).
- 5 Convergent to weak solutions of NS equations (Badia & Gutierrez 2012).

Segregated VMS

Energy statements

FE counterpart:

$$B((\mathbf{u}_h, p_h); (\widetilde{\mathbf{u}}, \widetilde{p}); (\mathbf{u}_h, p_h)) = L(\mathbf{u}_h, p_h)$$

SGS counterpart:

$$B((\widetilde{\mathbf{u}},\widetilde{p});(\mathbf{u}_h,p_h);(\widetilde{\mathbf{u}},\widetilde{p}))=L(\widetilde{\mathbf{u}},\widetilde{p})$$

TOTAL:

$$B((\mathbf{u}_h, p_h); (\widetilde{\mathbf{u}}, \widetilde{p}); (\mathbf{u}_h, p_h)) + B((\widetilde{\mathbf{u}}, \widetilde{p}); (\mathbf{u}_h, p_h); (\widetilde{\mathbf{u}}, \widetilde{p})) = L(\mathbf{u}_h, p_h) + L(\widetilde{\mathbf{u}}, \widetilde{p})$$

Energy statements

FE counterpart:

$$\frac{1}{2}d_{t}\|\mathbf{u}_{h}\|^{2} + \nu\|\nabla\mathbf{u}_{h}\|^{2} + b(\mathbf{a}, \mathbf{u}_{h}, \mathbf{u}_{h})
+ (\partial_{t}\widetilde{\mathbf{u}}, \mathbf{u}_{h}) + (\mathcal{L}_{a}^{*}(\mathbf{u}_{h}, \rho_{h}), \widetilde{\mathbf{u}}) - (\nabla \cdot \mathbf{u}_{h}, \widetilde{\rho}) = \langle \mathbf{f}, \mathbf{u}_{h} \rangle$$

Mixed FE VMS

SGS counterpart:

$$\frac{1}{2}d_{t}\|\widetilde{\mathbf{u}}\|^{2} + \tau_{m}^{-1}\|\widetilde{\mathbf{u}}\|^{2} + \tau_{c}^{-1}\|\widetilde{p}\|^{2} \\
+ (\mathcal{P}(\partial_{t}\mathbf{u}_{h}), \widetilde{\mathbf{u}}) + (\mathcal{P}(\mathcal{L}_{a}^{*}(\mathbf{u}_{h}, p_{h})), \widetilde{\mathbf{u}}) - (\mathcal{P}(\nabla \cdot \mathbf{u}_{h}), \widetilde{p}) = \langle \mathcal{P}(\mathbf{f}), \widetilde{\mathbf{u}} \rangle$$

TOTAL:

Energy statements

FE counterpart:

$$\frac{1}{2} d_t ||\mathbf{u}_h||^2 + \nu ||\nabla \mathbf{u}_h||^2 + b(\mathbf{a}, \mathbf{u}_h, \mathbf{u}_h)
+ (\partial_t \widetilde{\mathbf{u}}, \mathbf{u}_h) + (\mathcal{L}_a^*(\mathbf{u}_h, \rho_h), \widetilde{\mathbf{u}}) - (\nabla \cdot \mathbf{u}_h, \widetilde{\rho}) = \langle \mathbf{f}, \mathbf{u}_h \rangle$$

Mixed FE VMS

SGS counterpart:

$$\frac{1}{2} \frac{d_t \|\widetilde{\mathbf{u}}\|^2 + \tau_m^{-1} \|\widetilde{\mathbf{u}}\|^2 + \tau_c^{-1} \|\widetilde{\boldsymbol{p}}\|^2}{+ (\mathcal{P}(\partial_t \mathbf{u}_h), \widetilde{\mathbf{u}}) + (\mathcal{P}(\mathcal{L}_a^*(\mathbf{u}_h, \boldsymbol{p}_h)), \widetilde{\mathbf{u}}) - (\mathcal{P}(\nabla \cdot \mathbf{u}_h), \widetilde{\boldsymbol{p}}) = \langle \mathcal{P}(\mathbf{f}), \widetilde{\mathbf{u}} \rangle}$$

TOTAL:

$$\frac{1}{2}d_t\|\mathbf{u}_h\|^2 + \frac{1}{2}d_t\|\widetilde{\mathbf{u}}\|^2$$

FE counterpart:

$$\frac{1}{2}d_{t}\|\mathbf{u}_{h}\|^{2} + \nu\|\nabla\mathbf{u}_{h}\|^{2} + b(\mathbf{a}, \mathbf{u}_{h}, \mathbf{u}_{h})
+ (\partial_{t}\widetilde{\mathbf{u}}, \mathbf{u}_{h}) + (\mathcal{L}_{a}^{*}(\mathbf{u}_{h}, \rho_{h}), \widetilde{\mathbf{u}}) - (\nabla \cdot \mathbf{u}_{h}, \widetilde{\rho}) = \langle \mathbf{f}, \mathbf{u}_{h} \rangle$$

Mixed FE VMS

SGS counterpart:

$$\frac{1}{2}d_{t}\|\widetilde{\mathbf{u}}\|^{2} + \tau_{m}^{-1}\|\widetilde{\mathbf{u}}\|^{2} + \tau_{c}^{-1}\|\widetilde{p}\|^{2} \\
+ (\mathcal{P}(\partial_{t}\mathbf{u}_{h}), \widetilde{\mathbf{u}}) + (\mathcal{P}(\mathcal{L}_{a}^{*}(\mathbf{u}_{h}, p_{h})), \widetilde{\mathbf{u}}) - (\mathcal{P}(\nabla \cdot \mathbf{u}_{h}), \widetilde{p}) = \langle \mathcal{P}(\mathbf{f}), \widetilde{\mathbf{u}} \rangle$$

$$\frac{1}{2}d_{t}\|\mathbf{u}_{h}\|^{2} + \frac{1}{2}d_{t}\|\widetilde{\mathbf{u}}\|^{2} + \nu\|\nabla\mathbf{u}_{h}\|^{2}$$

FE counterpart:

Motivation

$$\frac{1}{2}d_{t}\|\mathbf{u}_{h}\|^{2} + \nu\|\nabla\mathbf{u}_{h}\|^{2} + b(\mathbf{a}, \mathbf{u}_{h}, \mathbf{u}_{h})
+ (\partial_{t}\widetilde{\mathbf{u}}, \mathbf{u}_{h}) + (\mathcal{L}_{a}^{*}(\mathbf{u}_{h}, p_{h}), \widetilde{\mathbf{u}}) - (\nabla \cdot \mathbf{u}_{h}, \widetilde{p}) = \langle \mathbf{f}, \mathbf{u}_{h} \rangle$$

SGS counterpart:

$$\frac{1}{2}d_{t}\|\widetilde{\mathbf{u}}\|^{2} + \tau_{m}^{-1}\|\widetilde{\mathbf{u}}\|^{2} + \tau_{c}^{-1}\|\widetilde{p}\|^{2} \\
+ (\mathcal{P}(\partial_{t}\mathbf{u}_{h}), \widetilde{\mathbf{u}}) + (\mathcal{P}(\mathcal{L}_{a}^{*}(\mathbf{u}_{h}, p_{h})), \widetilde{\mathbf{u}}) - (\mathcal{P}(\nabla \cdot \mathbf{u}_{h}), \widetilde{p}) = \langle \mathcal{P}(\mathbf{f}), \widetilde{\mathbf{u}} \rangle$$

$$\frac{1}{2}d_{t}\|\mathbf{u}_{h}\|^{2} + \frac{1}{2}d_{t}\|\widetilde{\mathbf{u}}\|^{2} + \nu\|\nabla\mathbf{u}_{h}\|^{2}$$

FE counterpart:

$$\frac{1}{2}d_{t}\|\mathbf{u}_{h}\|^{2} + \nu\|\nabla\mathbf{u}_{h}\|^{2} + b(\mathbf{a}, \mathbf{u}_{h}, \mathbf{u}_{h})
+ (\partial_{t}\widetilde{\mathbf{u}}, \mathbf{u}_{h}) + (\mathcal{L}_{a}^{*}(\mathbf{u}_{h}, \rho_{h}), \widetilde{\mathbf{u}}) - (\nabla \cdot \mathbf{u}_{h}, \widetilde{\rho}) = \langle \mathbf{f}, \mathbf{u}_{h} \rangle$$

Mixed FE VMS

SGS counterpart:

$$\frac{1}{2}d_{t}\|\widetilde{\mathbf{u}}\|^{2} + \tau_{m}^{-1}\|\widetilde{\mathbf{u}}\|^{2} + \tau_{c}^{-1}\|\widetilde{\boldsymbol{p}}\|^{2} + (\mathcal{P}(\partial_{t}\mathbf{u}_{h}), \widetilde{\mathbf{u}}) + (\mathcal{P}(\mathcal{L}_{a}^{*}(\mathbf{u}_{h}, p_{h})), \widetilde{\mathbf{u}}) - (\mathcal{P}(\nabla \cdot \mathbf{u}_{h}), \widetilde{\boldsymbol{p}}) = \langle \mathcal{P}(\mathbf{f}), \widetilde{\mathbf{u}} \rangle$$

$$\frac{1}{2}d_{t}\|\mathbf{u}_{h}\|^{2} + \frac{1}{2}d_{t}\|\widetilde{\mathbf{u}}\|^{2} + \nu\|\nabla\mathbf{u}_{h}\|^{2} + \tau_{m}^{-1}\|\widetilde{\mathbf{u}}\|^{2} + \tau_{c}^{-1}\|\widetilde{\boldsymbol{\rho}}\|^{2}$$

Motivation

Energy statements

FE counterpart:

$$\frac{1}{2}d_{t}\|\mathbf{u}_{h}\|^{2} + \nu\|\nabla\mathbf{u}_{h}\|^{2} + b(\mathbf{a}, \mathbf{u}_{h}, \mathbf{u}_{h})
+ (\partial_{t}\widetilde{\mathbf{u}}, \mathbf{u}_{h}) + (\mathcal{L}_{a}^{*}(\mathbf{u}_{h}, p_{h}), \widetilde{\mathbf{u}}) - (\nabla \cdot \mathbf{u}_{h}, \widetilde{p}) = \langle \mathbf{f}, \mathbf{u}_{h} \rangle$$

SGS counterpart:

$$\frac{1}{2}d_{t}\|\widetilde{\mathbf{u}}\|^{2} + \tau_{m}^{-1}\|\widetilde{\mathbf{u}}\|^{2} + \tau_{c}^{-1}\|\widetilde{p}\|^{2} \\
+ (\mathcal{P}(\partial_{t}\mathbf{u}_{h}),\widetilde{\mathbf{u}}) + (\mathcal{P}(\mathcal{L}_{a}^{*}(\mathbf{u}_{h},p_{h})),\widetilde{\mathbf{u}}) - (\mathcal{P}(\nabla \cdot \mathbf{u}_{h}),\widetilde{p}) = \langle \mathcal{P}(\mathbf{f}),\widetilde{\mathbf{u}} \rangle$$

$$\frac{1}{2}d_{t}\|\mathbf{u}_{h}\|^{2} + \frac{1}{2}d_{t}\|\widetilde{\mathbf{u}}\|^{2} + \nu\|\nabla\mathbf{u}_{h}\|^{2} + \tau_{m}^{-1}\|\widetilde{\mathbf{u}}\|^{2} + \tau_{c}^{-1}\|\widetilde{p}\|^{2} \\
+ (\partial_{t}\widetilde{\mathbf{u}}, \mathbf{u}_{h}) + (\mathcal{P}(\partial_{t}\mathbf{u}_{h}), \widetilde{\mathbf{u}}) + (\mathcal{L}_{a}^{*}(\mathbf{u}_{h}, p_{h}), \widetilde{\mathbf{u}}) + (\mathcal{P}(\mathcal{L}_{a}^{*}(\mathbf{u}_{h}, p_{h})), \widetilde{\mathbf{u}}) \\
- (\nabla \cdot \mathbf{u}_{h}, \widetilde{p}) - (\mathcal{P}(\nabla \cdot \mathbf{u}_{h}), \widetilde{p})$$

FE counterpart:

$$\frac{1}{2}d_{t}\|\mathbf{u}_{h}\|^{2} + \nu\|\nabla\mathbf{u}_{h}\|^{2} + b(\mathbf{a}, \mathbf{u}_{h}, \mathbf{u}_{h})
+ (\partial_{t}\widetilde{\mathbf{u}}, \mathbf{u}_{h}) + (\mathcal{L}_{a}^{*}(\mathbf{u}_{h}, p_{h}), \widetilde{\mathbf{u}}) - (\nabla \cdot \mathbf{u}_{h}, \widetilde{p}) = \langle \mathbf{f}, \mathbf{u}_{h} \rangle$$

Mixed FE VMS

SGS counterpart:

$$\frac{1}{2}d_{t}\|\widetilde{\mathbf{u}}\|^{2} + \tau_{m}^{-1}\|\widetilde{\mathbf{u}}\|^{2} + \tau_{c}^{-1}\|\widetilde{p}\|^{2} \\
+ (\mathcal{P}(\partial_{t}\mathbf{u}_{h}), \widetilde{\mathbf{u}}) + (\mathcal{P}(\mathcal{L}_{a}^{*}(\mathbf{u}_{h}, p_{h})), \widetilde{\mathbf{u}}) - (\mathcal{P}(\nabla \cdot \mathbf{u}_{h}), \widetilde{p}) = \langle \mathcal{P}(\mathbf{f}), \widetilde{\mathbf{u}} \rangle$$

$$\frac{1}{2}d_{t}\|\mathbf{u}_{h}\|^{2} + \frac{1}{2}d_{t}\|\widetilde{\mathbf{u}}\|^{2} + \nu\|\nabla\mathbf{u}_{h}\|^{2} + \tau_{m}^{-1}\|\widetilde{\mathbf{u}}\|^{2} + \tau_{c}^{-1}\|\widetilde{p}\|^{2}
+ (\partial_{t}\widetilde{\mathbf{u}}, \mathbf{u}_{h}) + (\mathcal{P}(\partial_{t}\mathbf{u}_{h}), \widetilde{\mathbf{u}}) + (\mathcal{L}_{a}^{*}(\mathbf{u}_{h}, p_{h}), \widetilde{\mathbf{u}}) + (\mathcal{P}(\mathcal{L}_{a}^{*}(\mathbf{u}_{h}, p_{h})), \widetilde{\mathbf{u}})
- (\nabla \cdot \mathbf{u}_{h}, \widetilde{p}) - (\mathcal{P}(\nabla \cdot \mathbf{u}_{h}), \widetilde{p}) = \langle \mathbf{f}, \mathbf{u}_{h} \rangle + \langle \mathcal{P}(\mathbf{f}), \widetilde{\mathbf{u}} \rangle$$

FE counterpart:

$$\frac{1}{2}d_t \|\mathbf{u}_h\|^2 + \nu \|\nabla \mathbf{u}_h\|^2 + b(\mathbf{a}, \mathbf{u}_h, \mathbf{u}_h)
+ (\partial_t \widetilde{\mathbf{u}}, \mathbf{u}_h) + (\mathcal{L}_a^*(\mathbf{u}_h, p_h), \widetilde{\mathbf{u}}) - (\nabla \cdot \mathbf{u}_h, \widetilde{p}) = \langle \mathbf{f}, \mathbf{u}_h \rangle$$

Mixed FE VMS

SGS counterpart:

$$\frac{1}{2}d_{t}\|\widetilde{\mathbf{u}}\|^{2} + \tau_{m}^{-1}\|\widetilde{\mathbf{u}}\|^{2} + \tau_{c}^{-1}\|\widetilde{p}\|^{2} \\
+ (\mathcal{P}(\partial_{t}\mathbf{u}_{h}), \widetilde{\mathbf{u}}) + (\mathcal{P}(\mathcal{L}_{a}^{*}(\mathbf{u}_{h}, p_{h})), \widetilde{\mathbf{u}}) - (\mathcal{P}(\nabla \cdot \mathbf{u}_{h}), \widetilde{p}) = \langle \mathcal{P}(\mathbf{f}), \widetilde{\mathbf{u}} \rangle$$

TOTAL: Static subscales

$$\frac{1}{2}d_{t}\|\mathbf{u}_{h}\|^{2} + \nu\|\nabla\mathbf{u}_{h}\|^{2} + \tau_{m}^{-1}\|\widetilde{\mathbf{u}}\|^{2} + \tau_{c}^{-1}\|\widetilde{p}\|^{2} \\
+ (\mathcal{P}(\partial_{t}\mathbf{u}_{h}), \widetilde{\mathbf{u}}) + (\mathcal{L}_{a}^{*}(\mathbf{u}_{h}, p_{h}), \widetilde{\mathbf{u}}) + (\mathcal{P}(\mathcal{L}_{a}^{*}(\mathbf{u}_{h}, p_{h})), \widetilde{\mathbf{u}}) \\
- (\nabla \cdot \mathbf{u}_{h}, \widetilde{p}) - (\mathcal{P}(\nabla \cdot \mathbf{u}_{h}), \widetilde{p}) = \langle \mathbf{f}, \mathbf{u}_{h} \rangle + \langle \mathcal{P}(\mathbf{f}), \widetilde{\mathbf{u}} \rangle$$

Segregated VMS

Energy statements

FE counterpart:

$$\frac{1}{2}d_{t}\|\mathbf{u}_{h}\|^{2} + \nu\|\nabla\mathbf{u}_{h}\|^{2} + b(\mathbf{a}, \mathbf{u}_{h}, \mathbf{u}_{h})
+ (\partial_{t}\widetilde{\mathbf{u}}, \mathbf{u}_{h}) + (\mathcal{L}_{a}^{*}(\mathbf{u}_{h}, p_{h}), \widetilde{\mathbf{u}}) - (\nabla \cdot \mathbf{u}_{h}, \widetilde{p}) = \langle \mathbf{f}, \mathbf{u}_{h} \rangle$$

SGS counterpart:

$$\frac{1}{2}d_{t}\|\widetilde{\mathbf{u}}\|^{2} + \tau_{m}^{-1}\|\widetilde{\mathbf{u}}\|^{2} + \tau_{c}^{-1}\|\widetilde{p}\|^{2} \\
+ (\mathcal{P}(\partial_{t}\mathbf{u}_{h}), \widetilde{\mathbf{u}}) + (\mathcal{P}(\mathcal{L}_{a}^{*}(\mathbf{u}_{h}, p_{h})), \widetilde{\mathbf{u}}) - (\mathcal{P}(\nabla \cdot \mathbf{u}_{h}), \widetilde{p}) = \langle \mathcal{P}(\mathbf{f}), \widetilde{\mathbf{u}} \rangle$$

Dynamic subscales - ASGS

$$\frac{1}{2}d_{t}\|\mathbf{u}_{h} + \widetilde{\mathbf{u}}\|^{2} + \nu\|\nabla\mathbf{u}_{h}\|^{2} + \tau_{m}^{-1}\|\widetilde{\mathbf{u}}\|^{2} + \tau_{c}^{-1}\|\widetilde{p}\|^{2} - 2(\nu\Delta\mathbf{u}_{h}, \widetilde{\mathbf{u}})$$

$$= \langle \mathbf{f}, \mathbf{u}_{h} \rangle + \langle \mathbf{f}, \widetilde{\mathbf{u}} \rangle$$

Segregated VMS

Energy statements

FE counterpart:

Motivation

$$\frac{1}{2}d_{t}\|\mathbf{u}_{h}\|^{2} + \nu\|\nabla\mathbf{u}_{h}\|^{2} + b(\mathbf{a}, \mathbf{u}_{h}, \mathbf{u}_{h})
+ (\partial_{t}\widetilde{\mathbf{u}}, \mathbf{u}_{h}) + (\mathcal{L}_{a}^{*}(\mathbf{u}_{h}, \rho_{h}), \widetilde{\mathbf{u}}) - (\nabla \cdot \mathbf{u}_{h}, \widetilde{\rho}) = \langle \mathbf{f}, \mathbf{u}_{h} \rangle$$

Mixed FE VMS

SGS counterpart:

$$\frac{1}{2}d_{t}\|\widetilde{\mathbf{u}}\|^{2} + \tau_{m}^{-1}\|\widetilde{\mathbf{u}}\|^{2} + \tau_{c}^{-1}\|\widetilde{\boldsymbol{\rho}}\|^{2} \\
+ (\mathcal{P}(\partial_{t}\mathbf{u}_{h}), \widetilde{\mathbf{u}}) + (\mathcal{P}(\mathcal{L}_{a}^{*}(\mathbf{u}_{h}, p_{h})), \widetilde{\mathbf{u}}) - (\mathcal{P}(\nabla \cdot \mathbf{u}_{h}), \widetilde{\boldsymbol{\rho}}) = \langle \mathcal{P}(\mathbf{f}), \widetilde{\mathbf{u}} \rangle$$

Dynamic subscales - OSS

$$\frac{1}{2}d_{t}\|\mathbf{u}_{h}\|^{2} + \frac{1}{2}d_{t}\|\widetilde{\mathbf{u}}\|^{2} + \nu\|\nabla\mathbf{u}_{h}\|^{2} + \tau_{m}^{-1}\|\widetilde{\mathbf{u}}\|^{2} + \tau_{c}^{-1}\|\widetilde{\boldsymbol{\rho}}\|^{2}
- 2(\nu\Delta\mathbf{u}_{h},\widetilde{\mathbf{u}})
= \langle \mathbf{f}, \mathbf{u}_{h} \rangle + \langle \mathcal{P}(\mathbf{f}), \widetilde{\mathbf{u}} \rangle$$

Numerical experiments

Three different turbulent benchmarks:

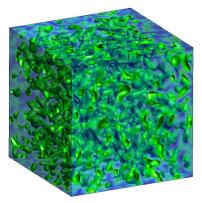
- Decaying of Homogeneous Isotropic Turbulence (DHIT).
- Taylor-Green Vortex (TGV) flow.
- Turbulent Channel Flow (TCF).

Segregated VMS

DHITDecay of Homogeneous Isotropic Turbulence

Problem setting:

- Prescribed initial energy spectra corresponding to $Re_{\lambda} = 952$.
- Setting defined in AGARD database (Mansour & Wray 1993).
- A (very simple) time step adaptation technique is used.
- Different mesh discretizations $(Q_1/Q_1 \text{ and } Q_2/Q_2)$.



Energy espectra (models):

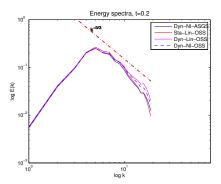


Figure : $32^3 - Q1$, t = 0.2s

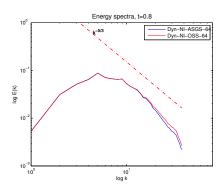


Figure : $64^3 - Q1$, t = 0.8s

Energy espectra (models):

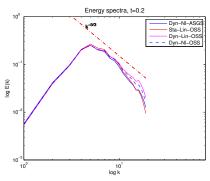


Figure : $32^3 - Q1$, t = 0.2s

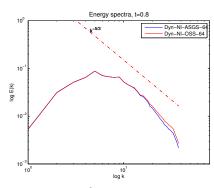


Figure : $64^3 - Q1$, t = 0.8s

Small differences between methods (physical sense).

Energy espectra (models):

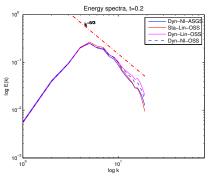


Figure : $32^3 - Q1$, t = 0.2s

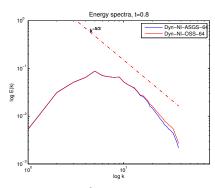


Figure : $64^3 - Q1$, t = 0.8s

- Small differences between methods (physical sense).
- Even more similar when we refine the mesh.

Computational cost (models):

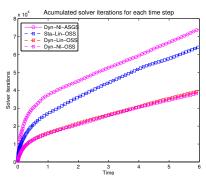


Figure: $32^3 - Q1$

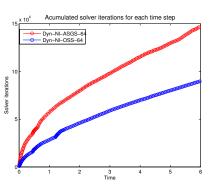


Figure: $64^3 - Q1$

Computational cost (models):

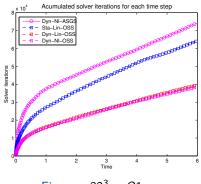


Figure: $32^3 - Q1$

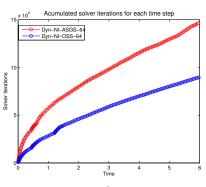


Figure: $64^3 - Q1$

Big differences between methods (computational sense).

Computational cost (models):

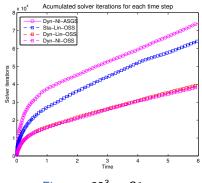


Figure: $32^3 - Q1$

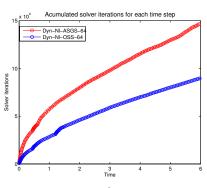


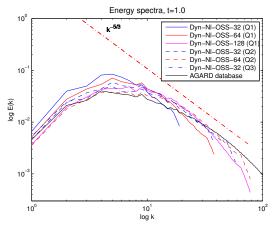
Figure: $64^3 - Q1$

- Big differences between methods (computational sense).
- Dynamic versions of OSS method are the most efficient.

Segregated VMS

DHIT Decay of Homogeneous Isotropic Turbulence

Energy espectra (refinement):



Results become closer to the DNS when we refine the mesh.

Problem setting:

- Prescribed initial condition.
- Re = 1600.
- Different mesh discretizations $(Q_1/Q_1 \text{ and } Q_2/Q_2)$.

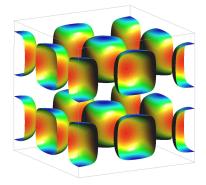


Figure : Initial vorticity isosurface $|\omega|=1$

TGV Taylor-Green Vortex flow

Problem setting:

- Prescribed initial condition.
- Re = 1600.
- Different mesh discretizations $(Q_1/Q_1 \text{ and } Q_2/Q_2)$.

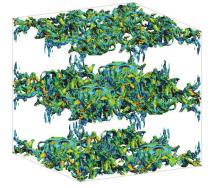


Figure : Vorticity isosurfaces $|\omega| = 9.0$

TGV Taylor-Green Vortex flow

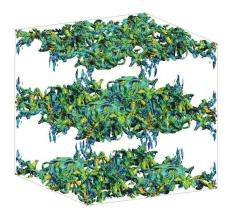


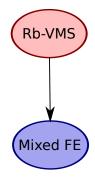




Figure: Velocity isosurface

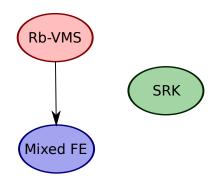
Motivation

- 3. Mixed FE VMS Formulation Block-preconditioning Numerical experiments Conclusions



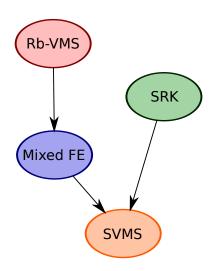
Motivation

- 4. Segregated Runge-Kutta Formulation Numerical experiments Conclusions



- 1. Motivation
- 2. Residual-based VMS
- 3. Mixed FE VMS
- Segregated Runge-Kutta
- 5. Segregated VMS
 Formulation
 Block-preconditioning
 Numerical experiments
 Conclusions

6. Conclusions



- 1. Motivation
- 2. Residual-based VMS
- Mixed FE VMS
- 4. Segregated Runge-Kutta
- 5. Segregated VMS
- 6. Conclusions

Segregated VMS

Outline

• Line 1.

Outline

- Line 1.
- Line 2.
 Less formal

Outline

- Line 1.
- Line 2. Less formal
- Line 3. Less formal, different color.

Blocks

Standard Block

This is a standard block.

Example Block

This is an example block.

Alert Block

This is an alert block.



