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Introductory Course on Model Reduction of Linear Time Invariant Systems

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- Linear Time Invariant Systems
- Norms of Signals and Systems
- Introduction to Model Reduction
- Model Reduction by Projection
- **Balanced Truncation**



- Fry a steak
- The cook controls the heat at the fireplace
- and observes the process, e.g.
 via measuring the temperature
 in the inner

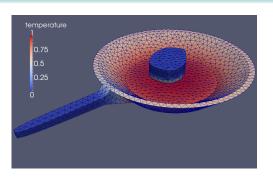


The model

$$\begin{split} \dot{\theta} &= \nabla \cdot \left(\nu \nabla \theta \right) & \text{ in } (0,\infty) \times \Omega, \\ \theta &= u, & \text{ at the plate}, \\ \theta(0) &= 0. \end{split}$$

- The cook controls the heat at. the fireplace, which we denote by u
- and observes the process, e.g. he measures the temperature y in the center: $y = f(\theta)$.

Simulation



The model:

$$\dot{\theta} = \nabla \cdot (\nu \nabla \theta),$$

$$\theta = u,$$

$$\theta(0) = 0.$$

- The cook controls the heat u
- and observes the process via $y = f(\theta)$.
- A Finite Element discretization of the problem leads to the finite dimensional model

$$E\dot{\theta}(t) = A\theta(t) + Bu(t), \quad \theta(0) = 0, \tag{1}$$

$$y(t) = C\theta(t), \tag{2}$$

a linear time invariant system.

$$E\dot{x}(t) = Ax(t) + Bu(t), \quad x(0) = x_0,$$
 (3a)

$$y(t) = Cx(t) + Du(t), \tag{3b}$$

with

- $E \in \mathbb{R}^{n \times n}$: the identity or the mass matrix
- $A \in \mathbb{R}^{n \times n}$: the system matrix
- $B \in \mathbb{R}^{n \times m}$: the input matrix
- $C \in \mathbb{R}^{q \times n}$: the output matrix
- $D \in \mathbb{R}^{q \times n}$: the throughput

- $x(t) \in \mathbb{R}^n$: the system's state
- $u(t) \in \mathbb{R}^m$: the input or control
- $y(t) \in \mathbb{R}^q$: the output or measurements
- n, m, $q \in \mathbb{N}$: the system dimensions

We will assume that E = I and denote the LTI (3) by (A, B, C, D).

Linear State Space System

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Some Preliminary Thoughts

$$E\dot{x}(t) = Ax(t) + Bu(t),$$

$$y(t) = Cx(t) + Du(t)$$

A simple question...

What is x?

- it is a physical state in the model like the temperature
- in practise, we may not access it only the measurement y = Cx
- it is but a mathematical object as a part of a model
- furthermore, as we will see later, the state x can be severely changed e.g. in the course of model reduction

The state x can be seen...

...as nothing but an artificial object of the model for the input to output behavior

$$G: u \mapsto y$$

of an abstract system **P**:



that maps an input u to the corresponding output y.

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...as nothing but an artificial object of the model for the input to output behavior

$$G: u \mapsto y$$

of an abstract system P:

$$y \leftarrow y(t) = Cx(t)$$
 $x(t) = Ax(t) + Bu(t)$

that maps an input u to the corresponding output y.

If **P** is modelled trough an (A, B, C, D) system, then the function **G** can be defined via

$$\mathbf{G}\colon u\mapsto y\colon y(t)=C\big[e^{At}x_0+\int_0^t e^{A(t-s)}Bu(s)\;\mathrm{d} s\big]+Du(t),$$

known as the formula of variation of constants.

This is in time-domain: A function u depending on time $t \in [0, \infty)$ is mapped onto a function y depending on time $t \in [0, \infty)$.

Introducing Frequency-Domain

Through the Laplace transform \mathcal{L} and its inverse \mathcal{L}^{-1} , we can switch between time-domain and frequency-domain representations of the input and output signals:

$$U(s) := \mathcal{L}\{u\}(s) := \int_0^\infty e^{-st} u(t) dt,$$

where $s \in \mathbb{C}$ is the $\mathit{frequency}$ and

$$y(t) := \mathcal{L}^{-1}\{Y\}(t) := \lim_{T \to \infty} \frac{1}{2\pi i} \int_{\gamma - iT}^{\gamma + iT} e^s Y(s) ds$$

where $\gamma \in \mathbb{R}$ is chosen such that the contour path of the integration is the domain of convergence of Y.

$$\dot{x}(t) = Ax(t) + Bu(t)$$

$$y(t) = Cx(t) + Du(t)$$

With the basic properties of the Laplace transform

•
$$\dot{X}(s) := \mathcal{L}\{\dot{x}\}(s) - x(0) = s\mathcal{L}\{x\}(s) = sX(s) - x(0)$$

• and linearity $\mathcal{L}\{Ax\}(s) = AX(s)$

with zero initial value x(0) = 0, the (A, B, C, D) system defines the transfer function

$$G(s) := C(sI - A)^{-1}B + D$$

in frequency domain.

Fact

An LTI (A, B, C, D) always defines a transfer function

$$G(s) = C(sI - A)^{-1}B + D$$

which is a matrix $G \in \mathbb{R}^{q \times m}$ with coefficients that are rational functions of s.

Question

Given a rational matrix function $s \mapsto G(s) \in \mathbb{R}^{q \times m}$, is there an

system, so that $G(s) = C(sI - A)^{-1}B + D$?

given
$$G$$
, find (A, B, C, D) ,

$$G(s) = C(sI - A)^{-1}B + D$$

If there is one such (A, B, C, D), then there are infinitely many:

• For $T \in \mathbb{R}^{n \times n}$ invertible, also $(TAT^{-1}, TB, CT^{-1}, D)$ is a realization:

$$C(sI - A)^{-1}B + D = CT^{-1}(sI - TAT^{-1})^{-1}TB + D.$$

Moreover, also

$$(\begin{bmatrix}A&0\\0&0\end{bmatrix},\begin{bmatrix}B\\0\end{bmatrix},\begin{bmatrix}C&0\end{bmatrix},D)$$

is a realization of G.

Janzations

Facts and Thoughts on Realizations

- If G is *proper*, then there is a realization (A, B, C, D) as a state space system.
- This realization is by no means unique.
- The dimension of the state can be arbitrary large. What is the smallest possible dimension? (cf. model reduction)
- What is a good choice for the state?

Remark: A transfer function $G : s \mapsto G(s) \in \mathbb{R}^{q \times m}$ with coefficients that are rational functions in s, is *proper*, if in each coefficient the polynomial degree of the numerators does not exceed the degree of denominators.

Based on the previous considerations, we can say that

- The states of an LTI system (A, B, C, D) are just a part of a model that realizes a transfer function G
- The transfer function G describes how controls u lead to outputs y
- As seen above in the example, there can be states that are neither affected (controlled) by the inputs nor seen (observed) by the outputs
- These states are obviously not needed to realize the input to output behavior of G

We will give a thorough characterization of the controllable and observable states of an LTI.

Controllability

Definition

The LTI (A, B, C, D) or the pair (A, B) is said to be *controllable* if, for any initial state $x(0) = x_0$, $t_1 > 0$ and final state x_1 , there exists a (piecewise continuous) input u such that the solution of (3) satisfies $x(t_1) = x_1$. Otherwise, the system (A, B, C, D) or the pair (A, B) is said to be uncontrollable.

$\mathsf{Theorem}$

The following statements are equivalent:

- (i.) The pair (A, B) is controllable.
- (ii.) The controllability matrix $C := \begin{bmatrix} B & AB & A^2B & \cdots & A^{n-1}B \end{bmatrix}$ has full rank.
- (iii.) The matrix $\begin{bmatrix} A \lambda I & B \end{bmatrix}$ has full rank for all $\lambda \in \mathbb{C}$.

Observability

Definition

The LTI (A, B, C, D) or the pair (C, A) is said to be *observable* if, for any $t_1 > 0$, the initial state $x(0) = x_0$ can be determined from the time history of the input u and the output y in the interval of $[0, t_1]$. Otherwise, the system (A, B, C, D), or (C, A), is said to be *unobservable*.

Observability is the dual concept of controllability:

$\mathsf{Theorem}$

The pair (C, A) is observable if and only if the pair (A^T, C^T) is controllable.

TI Systems Norms of Signals and Systems Introduction to MOR MOR by Projection Balanced Truncation

Invariance Under State Space Transformation

Theorem

The LTI (A, B, C, D) is controllable (observable) if, and only if, the transformed LTI $(TAT^{-1}, TB, CT^{-1}, D)$ is controllable (observable), where T is a regular matrix.

- Recall that also a transfer function is invariant with respect to state space transformations on its realization.
- Next, we find the states that are at least necessary for the realization of a transfer function...

Given an LTI (A, B, C, D), there is a state space transformation T such that the transformed system $(TAT^{-1}, TB, CT^{-1}, D)$ has the form

$$\begin{split} \frac{\mathrm{d}}{\mathrm{d}t} \begin{bmatrix} x_{co} \\ x_{c\bar{o}} \\ x_{\bar{c}o} \\ x_{\bar{c}o} \end{bmatrix} &= \begin{bmatrix} A_{co} & 0 & A_{13} & 0 \\ A_{21} & A_{c\bar{o}} & A_{23} & A_{24} \\ 0 & 0 & A_{\bar{c}o} & 0 \\ 0 & 0 & A_{43} & A_{\bar{c}\bar{o}} \end{bmatrix} \begin{bmatrix} x_{co} \\ x_{c\bar{o}} \\ x_{\bar{c}o} \\ x_{\bar{c}o} \end{bmatrix} + \begin{bmatrix} B_{co} \\ B_{c\bar{o}} \\ 0 \\ 0 \end{bmatrix} u \\ y &= \begin{bmatrix} C_{co} & 0 & C_{\bar{c}o} & 0 \end{bmatrix} \begin{bmatrix} x_{co} \\ x_{c\bar{o}} \\ x_{\bar{c}o} \\ x_{\bar{c}o} \\ x_{\bar{c}o} \end{bmatrix} + Du, \end{split}$$

with the subsystem $(A_{co}, B_{co}, C_{co}, D)$ being controllable and observable, while the remaining states $x_{\bar{c}o}$, $x_{c\bar{o}}$, or $x_{\bar{c}\bar{o}}$ are not controllable, not observable, or neither of them.

For a constructive proof of the Theorem, see Ch. 3.3 of [Zhou, Doyle, Glover '96]

For any state space system (A, B, C, D), there is a transformation T so that the transformed states $T^{-1}x$ decompose into

- x_{co} controllable and observable
- $x_{c\bar{o}}$ controllable but not observable
- $x_{\bar{c}o}$ observable but not controllable
- $x_{\bar{c}\bar{o}}$ not observable and not controllable

Moreover, for the transfer function, it holds that

$$G(s) = C(sI - A)^{-1}B = C_{co}(sI - A_{co})^{-1}B_{co}.$$

Conclusion from the Kalman Decomposition

What does this mean for us and a transfer function G(s)?

- The minimal dimension of a realization is the dimension of x_{co} in the Kalman Canonical Decomposition
- Such a realization is called minimal realization
- It is the starting point for further model reduction. (Throwing out $x_{\bar{c}o}$ etc. does not effect G(s) and is typically not considered a model reduction)
- There are algorithm to reduce a realization to a minimal one, cf. [VARGA '90].
- In practice, the uncontrolled and unobserved states play a role and they may cause troubles. (check the literature for zero dynamics)

• A system G is stable if all poles of G are located in the left half-plane \mathbb{C}^- .

- If (A, B, C, D) is a minimal realization of a stable system G, then the poles of G are the eigenvalues of A.
- In this case, the system is stable if

 λ is an eigenvalue of A, then $\lambda \in \mathbb{C}^-$.

- Such an A is called stable or Hurwitz.
- A stable system can have a stable realization.

If m=q=1, then $G(s)=\frac{N(s)}{D(s)}$, where N(s) and D(s) are polynomials and the *poles* are the roots of D(s), i.e. those $s \in \mathbb{C}$ for which D(s)=0.

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Linear Time Invariant Systems Stability

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Gramians and Balanced Realizations

If A is stable, then the Lyapunov equations

$$A^*P + PA + BB^* = 0$$

and

$$AQ + Q^*A + C^*C = 0$$

have a unique positive definite solutions P and Q.

- The matrix P is called the the controllability Gramian
- and Q is called the observability Gramian
- and one can show that P and Q fulfill

$$P = \int_0^\infty e^{A\tau} B B^* e^{A^*\tau} d\tau \quad \text{and} \quad Q = \int_0^\infty e^{A^*\tau} C^* C e^{A\tau} d\tau.$$

Linear Time Invariant Systems

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Gramians and Balanced Realizations

$$A^*P + PA + BB^* = 0$$

 $AQ + Q^*A + C^*C = 0$

- If P and Q are the Gramians of a stable realization (A, B, C, D),
- then the transformed system $(\hat{A}, \hat{B}, \hat{C}, \hat{D}) = (TAT^{-1}, TB, CT^{-1}, D)$ has the Gramians

$$\hat{P} = TPT^*$$
 and $\hat{Q} = (T^{-1})^*QT^{-1}$

for any regular transformation T.

Linear Time Invariant Systems

Gramians and Balanced Realizations

- For any minimal and stable system (A, B, C, D),
- there are particular transformations T,
- so that the transformed system has Gramians that are equal and diagonal:

$$\hat{P}=\hat{Q}=egin{bmatrix} \lambda_1 & & & & & \\ & \lambda_2 & & & & \\ & & \ddots & & & \\ & & & \lambda_n \end{bmatrix},$$
 with $\lambda_1\geq\lambda_2\geq\cdots\geq\lambda_n>0.$

These realizations are called Balanced Realizations.

Summary

- LTI as model for physical processes (e.g. heat transfer)
- The input/output behavior is often more important than the state
- Moreover, the state need not have a meaning
- State space systems (A, B, C, D) can be seen as realizations of transfer functions
- A transfer function has multiple realizations
- The minimal realizations are of our interest
- A stable system can have stable realization
- Minimal and stable realization can be balanced



K. Zhou, J. C. Doyle, and K. Glover. Robust and Optimal Control. (Chapter 3 for LTI) Prentice-Hall, Upper Saddle River, NJ, 1996.



A. Varga.

Computation of irreducible generalized state-space realizations. Kybernetika, 26(2):89-106, 1990.



A. Gaul.

Leckerbraten – a lightweight Python toolbox to solve the heat equation on arbitrary domains

https://github.com/andrenarchy/leckerbraten, 2013.



J. Heiland.

The slides, additional material, and information on this course https://github.com/highlando/mor-shortcourse-SH, 2015.

- Norms of Signals and Systems
 - Norms
 - Norms of Signals
 - Norm of a System
 - Defining a Norm for Systems
 - Relation to Model Reduction

Basic Notions of Norms

Ingredients of a normed space $(V, \|\cdot\|)$:

- A linear space V over \mathbb{C} (or \mathbb{R})
- and a functional

$$\|\cdot\|\colon V\to\mathbb{R}$$

that has the following properties:

- i) $\|\alpha v\| = |\alpha| \|v\|$,
- ii) $||v + w|| \le ||v|| + ||w||$, and
- iii) $||v|| \ge 0$ and ||v|| = 0 if, and only if, v = 0,

for any v, $w \in V$ and any $\alpha \in \mathbb{C}$ (or \mathbb{R}).

Norms of Linear Operators

If $(V,\|\cdot\|_V)$ and $(W,\|\cdot\|_W)$, then for the space of linear maps $(V\to W)$ a norm is defined via

$$||G||_* := \sup_{v \in V, v \neq 0} \frac{||Gv||_W}{||v||_V}.$$

This is the norm for $G: V \to W$ that is induced by $\|\cdot\|_V$ and $\|\cdot\|_W$. There can be other norms that are not induced.

Common norms and spaces for the input or output signals

$$u: [0, \infty) \to \mathbb{R}^m$$
 or $y: [0, \infty) \to \mathbb{R}^q$

- All definitions work similar for finite time intervals [0, T] or the whole time axis $(-\infty, \infty)$.
- Where it is clear from the context, we will drop the superscripts p and m that denote the dimension of the signals.

Norms of Signals

Definition

The \mathbf{L}_{1}^{m} norm

$$||u||_{\mathbf{L}_1} := \int_0^\infty \sum_{i=1}^m |u_i(t)| \, dt$$

defines the L_1^m space of integrable (summable) functions

$$\mathbf{L}_1^m := \left\{ u \colon [0, \infty) \to \mathbb{R}^m : \|u\|_{\mathbf{L}_1} < \infty \right\}$$

on the positive time axis.

Definition

The \mathbf{L}_{∞}^{m} norm

$$||u||_{\mathbf{L}_{\infty}} := \max_{i=\{1,\ldots,m\}} \sup_{t>0} |u_i(t)|$$

defines the \mathbf{L}_{∞}^{m} space of bounded functions

$$\mathbf{L}_{\infty}^{m} := \{u \colon [0, \infty) \to \mathbb{R}^{m} : \|u\|_{\mathbf{L}_{\infty}} < \infty\}.$$

Definition

The \mathbf{L}_2^q norm

$$\|y\|_{\mathsf{L}_2} := \left(\int_0^\infty \sum_{i=1}^q |y_i(t)|^2 \ \mathsf{d}t\right)^{\frac{1}{2}}$$

defines the L_2^q space of square integrable functions

$$\mathbf{L}_{2}^{q} := \{ y \colon [0, \infty) \to \mathbb{R}^{q} : ||y||_{\mathbf{L}_{2}} < \infty \}$$

Norms of Signals and Systems Norms of Signals

The L_2 norm can also be evaluated in frequency domain

Theorem

For $u \in \mathbf{L}_2$ it holds that

$$\|u\|_{\mathbf{L}_2} = \left(\frac{1}{2\pi} \int_{-\infty}^{\infty} U(i\omega)^* U(i\omega) \, \mathrm{d}\omega\right)^{\frac{1}{2}},$$

where U is the Fourier transform of u.

The Fourier transform \mathcal{F} and the Laplace transform \mathcal{L} coincide for $s=i\omega,\,\omega\in\mathbb{R}$ and u(t) = 0 for t < 0:

$$\mathcal{F}(u)(i\omega) := \int_{-\infty}^{\infty} u(t)e^{-i\omega t} dt = \int_{0}^{\infty} u(t)e^{-st} dt = \mathcal{L}(u)(s)$$

A system G or (A, B, C, D) transfers inputs to outputs.

Ask yourself...

- What does a norm mean for a system?
- What is a large system, what is a small system?

From the definition of an operator norm:

$$\|G\| = \sup_{u \neq 0} \frac{\|Gu\|}{\|u\|}$$

we derive that for all u:

$$||y|| = ||Gu|| \le ||G|| ||u||.$$

An Answer

For systems, large refers to what extend an input is amplified. Therefore, ||G|| is often called the gain.

Norms of Signals and Systems Norm of a System

From the definition of an operator norm:

$$||G|| = \sup_{u \neq 0} \frac{||Gu||}{||u||}$$

we derive that for all u:

$$||y|| = ||Gu|| \le ||G|| ||u||.$$

With a norm, one can compare two systems G_1 and G_2 via the difference in the output for the same input:

$$||y_1 - y_2|| = ||G_1u - G_2u|| \le ||G_1 - G_2|| ||u||.$$

Defining a Norm for Systems

We consider a SISO system (A, B, C, -), i.e m = q = 1 and D = 0.

Consider (A, B, C, -) a with stable and strictly proper transfer function G is stable. Then the *impulse response* of the system

$$g(t) = C \int_0^t e^{A(t-\tau)} B\delta(\tau) ds = Ce^{At} B$$

decays exponentially and

$$\|g\|_{\mathbf{L}_2} = \left(\frac{1}{2\pi}\int_{-\infty}^{\infty} G(i\omega)^* G(i\omega) d\omega\right)^{\frac{1}{2}} =: \|G\|_2 < \infty.$$

A system (A, B, C, D) or A is stable, if there exists a $\lambda > 0$, such that $||e^A t|| \le e^{-\lambda t}$, for t > 0. This means that all eigenvalues of A must have a negative real part.

Tmpulse response:
$$\delta(\tau) := \begin{cases} 0, & \text{if } t \neq 0, \\ \text{very large, if } t = 0 \end{cases}$$
 so that $\int_{-\infty}^{\infty} u(\tau) \delta(\tau) \ \mathrm{d}\tau = u(0).$

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This defines a norm for systems since (Exercise!)

- $G = C(sI A)^{-1}B$ is indeed the Laplace transform of g
- \bullet the functional $\|\cdot\|_2$ for stable and strictly proper transferfunctions is a norm

Furthermore, $||y||_{\mathbf{L}_{\infty}} \le ||G||_2 ||u||_{\mathbf{L}_{\infty}}$. (Exercise!)

Defining a Norm for Systems

For MIMO systems (A, B, C, -) with $u(t) \in \mathbb{R}^m$ and $y(t) \in \mathbb{R}^q$, with a stable and strictly proper transferfunction $\mathcal{G} : s \to \mathbb{R}^{q \times m}$, the \mathcal{H}_2 norm is defined as

$$\|G\|_2 := \left(\frac{1}{2\pi} \int_{-\infty}^{\infty} \operatorname{tr}\left(G(i\omega)^* G(i\omega)\right) d\omega\right)^{\frac{1}{2}}.$$

Fact

This is the norm of the Hardy space \mathcal{H}_2 of matrix functions that are analytic in the open right half of the complex plane. Stable and strictly proper transfer functions are in \mathcal{H}_2 .

Defining a Norm for Systems

For a stable and proper transfer function one can define the \mathcal{H}_{∞} norm:

$$\|G\|_{\infty} := \sup_{\omega \in \mathbb{R}} \sigma_{\mathsf{max}} (G(i\omega)),$$

where $\sigma_{\text{max}}\left(G(i\omega)\right)$ is the largest singular value of $G(i\omega)$.

Fact 1

This is the norm of the Hardy space \mathcal{H}_{∞} of matrix functions that are analytic in the open right half of the complex plane and bounded on the imaginary axis. Stable and strictly proper transfer functions are in \mathcal{H}_{∞} .

Fact 2

The \mathcal{H}_{∞} -norm is induced by the \mathbf{L}_2 norm:

$$\|G\|_{\infty} = \sup_{u \in \mathbf{L}_2, u \neq 0} \frac{\|Gu\|_{\mathbf{L}_2}}{\|u\|_{\mathbf{L}_2}}.$$

Approximation Problems - Model Reduction

Output errors in time-domain

Comparing the original system G and the reduced system G:

$$\left|\left|y-\hat{y}\right|\right|_2 \ \leq \ \left|\left|G-\hat{G}\right|\right|_{\infty} \left|\left|u\right|\right|_2 \quad \Longrightarrow \left|\left|G-\hat{G}\right|\right|_{\infty} < \mathrm{tol}$$

$$\left|\left|y-\hat{y}\right|\right|_{\infty} \ \leq \ \left|\left|G-\hat{G}\right|\right|_{2}\left|\left|u\right|\right|_{2} \qquad \Longrightarrow \left|\left|G-\hat{G}\right|\right|_{2} < \mathrm{tol}$$

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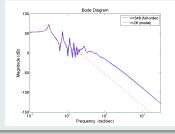
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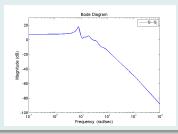
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\mathcal{H}_{∞} -norm	best approximation problem for given reduced order r in general open; balanced truncation yields suboptimal solution with computable \mathcal{H}_{∞} -norm bound.
\mathcal{H}_2 -norm	necessary conditions for best approximation known; (local) optimizer computable with iterative rational Krylov algorithm (IRKA)
Hankel-norm $ G _H := \sigma_{max}$	optimal Hankel norm approximation (AAK theory).

Other measures

- absolute errors $\left\| G(\jmath\omega_j) \hat{G}(\jmath\omega_j) \right\|_2$, $\left\| G(\jmath\omega_j) \hat{G}(\jmath\omega_j) \right\|_{200}$ $(i = 1, ..., N_{\omega});$
- relative errors $\frac{\left|\left|G(\jmath\omega_j)-\hat{G}(\jmath\omega_j)\right|\right|_2}{\left|\left|G(\jmath\omega_j)\right|\right|_2}$, $\frac{\left|\left|G(\jmath\omega_j)-\hat{G}(\jmath\omega_j)\right|\right|_{\infty}}{\left|\left|G(\jmath\omega_j)\right|\right|_{\infty}}$;
- "eyeball norm", i.e. look at frequency response/Bode (magnitude) plot: for SISO system, log-log plot frequency vs. $|G(j\omega)|$ (or $|G(j\omega) - \hat{G}(j\omega)|$) in decibels, 1 dB $\simeq 20 \log_{10}(\text{value})$.





- Introduction to Model Reduction
 - Model Reduction for Dynamical Systems
 - Application Areas
 - Motivating Examples

Model Reduction — Abstract Definition

Problem

Given a model of a physical problem with dynamics described by the states $x(t) \in \mathbb{R}^n$, where n is the dimension of the state space.

The dimension n is large because x(t) typically contains information that

- is (almost) redundant,
- not (really) important,
- or not (really) of interest.

We want to adjust the model such that the new state is of small dimension but still bears all important and interesting information.

This is the task of model reduction (also: dimension reduction, order reduction).

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This is the task of model reduction (also: dimension reduction, order reduction).

Model Reduction for Dynamical Systems

Dynamical Systems

$$\Sigma : \left\{ \begin{array}{lcl} \dot{x}(t) & = & f(t, x(t), u(t)), & x(t_0) = x_0, \\ y(t) & = & g(t, x(t), u(t)) \end{array} \right.$$

with

- states $x(t) \in \mathbb{R}^n$,
- inputs $u(t) \in \mathbb{R}^m$,
- outputs $y(t) \in \mathbb{R}^q$.



Model Reduction for Dynamical Systems

Original System

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Reduced-Order Model (ROM)

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Goal:

 $||y - \hat{y}|| < \text{tolerance} \cdot ||u||$ for all admissible input signals.

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 $||y - \hat{y}|| < \text{tolerance} \cdot ||u||$ for all admissible input signals.

Secondary goal: reconstruct approximation of x from \hat{x} .

Linear, Time-Invariant (LTI) Systems

$$\begin{array}{lcl} E\dot{x} & = & f(t,x,u) & = & Ax+Bu, \quad E,A\in\mathbb{R}^{n\times n}, \\ y & = & g(t,x,u) & = & Cx+Du, \quad C\in\mathbb{R}^{q\times n}, \end{array} \qquad \begin{array}{ll} B\in\mathbb{R}^{n\times m}, \\ D\in\mathbb{R}^{q\times m}. \end{array}$$

Linear, Time-Invariant (LTI) Systems

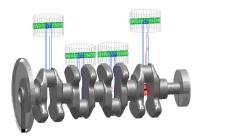
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Linear, Time-Invariant Parametric Systems

$$E(p)\dot{x}(t;p) = A(p)x(t;p) + B(p)u(t),$$

$$y(t;p) = C(p)x(t;p) + D(p)u(t),$$

where $A(p), E(p) \in \mathbb{R}^{n \times n}, B(p) \in \mathbb{R}^{n \times m}, C(p) \in \mathbb{R}^{q \times n}, D(p) \in \mathbb{R}^{q \times m}$.





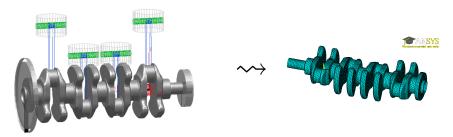
- Resolving complex 3D geometries ⇒ millions of degrees of freedom.
- Analysis of elastic deformations requires many simulation runs for varying external forces.

Standard MOR techniques in structural mechanics: modal truncation,

Application Areas

Structural Mechanics / Finite Element Modeling





- Resolving complex 3D geometries ⇒ millions of degrees of freedom.
- Analysis of elastic deformations requires many simulation runs for varying external forces.

Standard MOR techniques in structural mechanics: modal truncation, combined with Guyan reduction (static condensation) --> Craig-Bampton method.

Application Areas (Optimal) Control

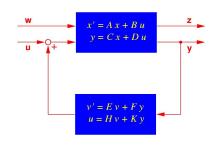
since \sim 1980ies

Feedback Controllers

A feedback controller (dynamic compensator) is a linear system of order N, where

- input = output of plant,
- output = input of plant.

Modern (LQG- $/\mathcal{H}_2$ - $/\mathcal{H}_{\infty}$ -) control design: N > n.



Practical controllers require small N ($N \sim 10$, say) due to

- increasing fragility for larger N.

 \implies reduce order of plant (n) and/or controller (N).

Standard MOR techniques in systems and control: balanced truncation

Application Areas (Optimal) Control

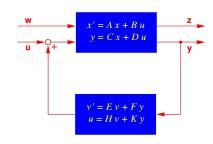
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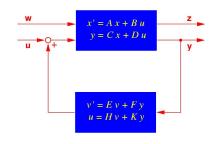
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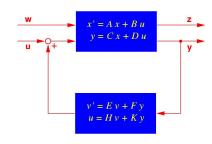
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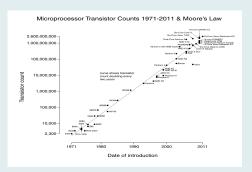
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Progressive miniaturization

- Verification of VLSI/ULSI chip design needs a large number of simulations.
- Moore's Law (1965/75) states that the number of on-chip transistors doubles each 24 months.



Source: http://en.wikipedia.org/wiki/File:Transistor_Count_and_Moore'sLaw_-_2011.svg

since \sim 1990ies

Micro Electronics/Circuit Simulation

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Micro Electronics/Circuit Simulation

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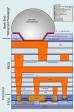
Intel 4004 (1971)	Intel Core 2 Extreme (quad-core) (2007)
1 layer, 10μ technology	9 layers, 45 <i>nm</i> technology
2,300 transistors	> 8, 200, 000 transistors
64 kHz clock speed	> 3 GHz clock speed.

Micro Electronics/Circuit Simulation since \sim 1990ies

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Source: http://en.wikipedia.org/wiki/Image:Silicon_chip_3d.png.

Micro Electronics/Circuit Simulation

since \sim 1990ies

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- Here: mostly MOR for linear systems, they occur in micro electronics through modified nodal analysis (MNA) for RLC networks. e.g., when
 - decoupling large linear subcircuits,
 - modeling transmission lines,
 - modeling pin packages in VLSI chips,
 - modeling circuit elements described by Maxwell's equation using partial element equivalent circuits (PEEC).

Micro Electronics/Circuit Simulation

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Standard MOR techniques in circuit simulation:

Krylov subspace / Padé approximation / rational interpolation methods.

Application Areas

Many other disciplines in computational sciences and engineering like

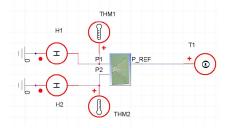
- computational fluid dynamics (CFD),
- computational electromagnetics,
- chemical process engineering,
- design of MEMS/NEMS (micro/nano-electrical-mechanical systems),
- computational acoustics,
- . . .

[Source: Evgenii Rudnyi, CADFEM GmbH]

Motivating Examples

Electro-Thermic Simulation of Integrated Circuit (IC)

SIMPLORER® test circuit with 2 transistors.

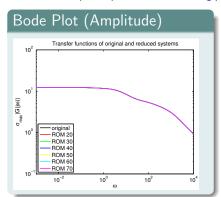


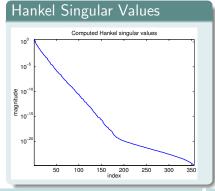
- Conservative thermic sub-system in SIMPLORER: voltage → temperature, current → heat flow.
- Original model: n = 270.593, $m = q = 2 \Rightarrow$ Computing time (on Intel Xeon dualcore 3GHz, 1 Thread):
 - Main computational cost for set-up data $\approx 22min$.
 - Computation of reduced models from set-up data: 44–49sec. (r = 20-70).
 - Bode plot (MATLAB on Intel Core i7, 2,67GHz, 12GB): 7.5h for original system, < 1min for reduced system.
 - Speed-up factor: 18 including / > 450 excluding reduced model generation!

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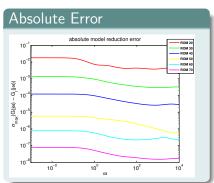
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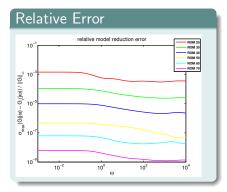




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A Nonlinear Model from Computational Neurosciences: the FitzHugh-Nagumo System

• Simple model for neuron (de-)activation [Chaturantabut/Sorensen 2009]

$$\epsilon v_t(x,t) = \epsilon^2 v_{xx}(x,t) + f(v(x,t)) - w(x,t) + g,$$

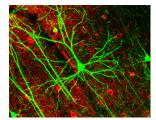
$$w_t(x,t) = hv(x,t) - \gamma w(x,t) + g.$$

with f(v) = v(v - 0.1)(1 - v) and initial and boundary conditions

$$v(x,0) = 0,$$
 $w(x,0) = 0,$ $x \in [0,1]$
 $v_x(0,t) = -i_0(t),$ $v_x(1,t) = 0,$ $t > 0,$

where
$$\epsilon = 0.015$$
, $h = 0.5$, $\gamma = 2$, $g = 0.05$, $i_0(t) = 50000t^3 \exp(-15t)$.





Source: http://en.wikipedia.org/wiki/Neuron

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where
$$\epsilon = 0.015, h = 0.5, \gamma = 2, g = 0.05, i_0(t) = 50000t^3 \exp(-15t)$$
.

- Parameter g handled as an additional input.
- Original state dimension $n = 2 \cdot 400$, QBDAE dimension $N = 3 \cdot 400$, reduced QBDAE dimension r=26, chosen expansion point $\sigma=1$.

Motivating Examples

A Nonlinear Model from Computational Neurosciences: the FitzHugh-Nagumo System

Motivating Examples

Parametric MOR: Applications in Microsystems/MEMS Design

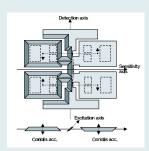
Microgyroscope (butterfly gyro)



- Voltage applied to electrodes induces vibration of wings, resulting rotation due to Coriolis force yields sensor data.
- FF model of second order: $N = 17.361 \rightsquigarrow n = 34.722, m = 1, q = 12.$
- Sensor for position control based on acceleration and rotation.

Source: The Oberwolfach Benchmark Collection http://www.imtek.de/simulation/benchmark

Application: inertial navigation.

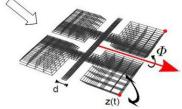


Parametric MOR: Applications in Microsystems/MEMS Design

Microgyroscope (butterfly gyro)

Parametric FE model: $M(d)\ddot{x}(t) + D(\Phi, d, \alpha, \beta)\dot{x}(t) + T(d)x(t) = Bu(t)$.





Microgyroscope (butterfly gyro)

Parametric FF model:

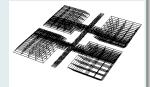
$$M(d)\ddot{x}(t) + D(\Phi, d, \alpha, \beta)\dot{x}(t) + T(d)x(t) = Bu(t),$$

wohei

$$M(d) = M_1 + dM_2,$$

$$D(\Phi, d, \alpha, \beta) = \Phi(D_1 + dD_2) + \alpha M(d) + \beta T(d),$$

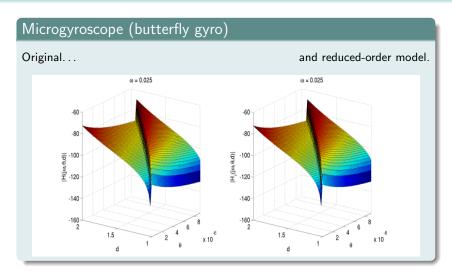
$$T(d) = T_1 + \frac{1}{d}T_2 + dT_3,$$



with

- width of bearing: d,
- angular velocity:
- Rayleigh damping parameters: α, β .

Parametric MOR: Applications in Microsystems/MEMS Design



Outline

- Linear Time Invariant Systems
- 2 Norms of Signals and Systems
- Introduction to Model Reduction
- Model Reduction by ProjectionProjection and Interpolation
 - Projection and interpolation
 - Modal Truncation
 - Rational Interpolation
 - H₂-Optimal Model Reduction
- Balanced Truncation

- Automatically generate compact models \hat{G} from a given model G
- Satisfy desired error tolerance tol for all admissible input signals u

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 - stability

A G is stable, if all poles of G are in \mathbb{C}^- . A system (A, B, C, D) or A is stable, if all eigenvalues of A have a negative real part. Compare: $G(s) = C(sI - A)^{-1}B$

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 - minimum phase
 - passivity

A system G has minimum phase if all zeros of G are in the left half-plane \mathbb{C}^- .

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A system G is passive if, bluntly speaking, it does not generate energy. Condition for passivity:

$$\int_{-\infty}^t u(\tau)^T y(\tau) \, d\tau \ge 0 \quad \text{for all } t \in \mathbb{R}, \quad \text{for all } u \in L_2(\mathbb{R}, \mathbb{R}^m).$$

Projection Basics

Definition

A projector $P \colon \mathcal{X} \to \mathcal{X}$ is a linear map, or a matrix, with $P^2 = P$.

Example

$$\bullet$$
 $\mathcal{X} = \mathbb{R}^2$

•
$$P = \begin{bmatrix} 1 & 1 \\ 0 & 0 \end{bmatrix}$$
 is a projector in \mathcal{X}

Notion and Properties of Projectors

- A projector is a linear map $P: \mathcal{X} \to \mathcal{X}$ with $P^2 = P$.
- If $\mathcal{X} = \mathbb{R}^n$, a projector is a matrix $P \in \mathbb{R}^{n \times n}$ with $P^2 = P$.
- Let V = range(P), then P is called a projector onto V.
- If $\{v_1,\ldots,v_r\}$ is a basis of some $\mathcal{V}\in\mathcal{X}$ and $V=[v_1,\ldots,v_r]$, then

$$P := V(V^T V)^{-1} V^T$$

defines the orthogonal projector onto \mathcal{V} .

• If $W \subset \mathcal{X}$ is another r-dimensional subspace with a basis matrix $W = [w_1, \dots, w_r]$ so that $W^T V$ is not singular, then

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defines the oblique projector onto V along the orthogonal complement W_{\perp} of W.

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Projection and Interpolation

Methods:

- Modal Truncation
- Rational Interpolation (Padé-Approximation and (rational) Krylov Subspace Methods)
- Balanced Truncation
- many more...

Joint feature of these methods: computation of reduced-order model (ROM) by projection!

The ideal model reduction

- There is a space $\mathcal{V} \subset \mathbb{R}^n$ with dim $\mathcal{V} = r < n$, such that $x \in \mathcal{V}$ for all time t and input u.
- Take a space W, so that $W_{\perp} \oplus V = \mathbb{R}^n$.
- Galerkin-type projections: W = V.
- Petrov-Galerkin projections: $W \neq V$.
- ullet Take matrices V and W that form bases of V and W, with

$$W^{\mathsf{T}}V = I_r$$

- Then $V(W^{\mathsf{T}}V)^{-1}W = VW^{\mathsf{T}}$ is a projector onto V
- Define $\hat{x} := W^\mathsf{T} x \in \mathbb{R}^r$ and define $\tilde{x} := V\hat{x} = VW^\mathsf{T} x$
- If everything is exact, then

$$||x - \tilde{x}|| = ||x - VW^{\mathsf{T}}x|| = 0$$

$$\hat{A} := W^T A V, \quad \hat{B} := W^T B, \quad \hat{C} := C V, \quad (\hat{D} := D).$$

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- Define $\hat{x} := W^\mathsf{T} x \in \mathbb{R}^r$ and define $\tilde{x} := V \hat{x} = V W^\mathsf{T} x$
- If everything is exact, then

$$||x - \tilde{x}|| = ||x - VW^{\mathsf{T}}x|| = 0$$

$$\hat{A} := W^T A V, \quad \hat{B} := W^T B, \quad \hat{C} := C V, \quad (\hat{D} := D).$$

Model reduction in practise

- Assume that there is a space $\mathcal{V} \subset \mathbb{R}^n$ with dim $\mathcal{V} = r < n$, such that $x \in \mathcal{V}$ for all time t and input u.
- Take a space W, so that $W_{\perp} \oplus V = \mathbb{R}^n$.
- Galerkin-type projections: W = V.
- Petrov-Galerkin projections: $W \neq V$.
- ullet Find matrices V and W that approximate bases of ${\mathcal V}$ and ${\mathcal W}$, with

$$W^{\mathsf{T}}V = I_r$$

- Then $V(W^{\mathsf{T}}V)^{-1}W = VW^{\mathsf{T}}$ is a projector almost onto \mathcal{V}
- Define $\hat{x} := W^\mathsf{T} x \in \mathbb{R}^r$ and define $\tilde{x} := V \hat{x} = V W^\mathsf{T} x$
- If everything is done well, then

$$||x - \tilde{x}|| = ||x - VW^\mathsf{T}x|| \approx 0$$

$$\hat{A} := W^T A V, \quad \hat{B} := W^T B, \quad \hat{C} := C V, \quad (\hat{D} := D).$$

Definition of the reduced model

... and given an (A, B, C, D) system,

the reduced-order model $(\hat{A}, \hat{B}, \hat{C}, \hat{D})$ is

$$\hat{A} := W^T A V, \quad \hat{B} := W^T B, \quad \hat{C} := C V, \quad (\hat{D} := D).$$

Why is the ROM defined like this:

It is the (Petrov)-Galerkin condition $\dot{\tilde{x}} - A\tilde{x} - Bu \perp \mathcal{W}$:

$$W^{T}(\dot{\tilde{x}} - A\tilde{x} - Bu) = W^{T}(VW^{T}\dot{x} - AVW^{T}x - Bu)$$

is zero, if, and only if,

$$\dot{\hat{x}} - \hat{A}\hat{x} - \hat{B}u = 0.$$

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is zero, if, and only if,

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Model Reduction by Projection

Projection --> Rational Interpolation

A Petrov-Galerkin projected ROM interpolates the transfer function:

Theorem 3.3

[Grimme '97, Villemagne/Skelton '87]

Given the ROM

$$\hat{A} = W^T A V$$
, $\hat{B} = W^T B$, $\hat{C} = C V$, $(\hat{D} = D)$,

and $s_* \in \mathbb{C} \setminus (\Lambda(A) \cup \Lambda(\hat{A}))$, if either

•
$$(s_*I_n - A)^{-1}B \in \text{range}(V)$$
, or

•
$$(s_*I_n - A)^{-*}C^T \in \text{range}(W)$$
,

then the interpolation condition

$$G(s_*) = \hat{G}(s_*).$$

in s* holds.

Note: extension to Hermite interpolation conditions later!

Projection → Rational Interpolation

Given the ROM

$$\hat{A} = W^T A V$$
, $\hat{B} = W^T B$, $\hat{C} = C V$, $(\hat{D} = D)$,

$$G(s) - \hat{G}(s) = (C(sl_n - A)^{-1}B + D) - (\hat{C}(sl_r - \hat{A})^{-1}\hat{B} + \hat{D})$$

Projection → Rational Interpolation

Given the ROM

$$\hat{A} = W^T A V$$
, $\hat{B} = W^T B$, $\hat{C} = C V$, $(\hat{D} = D)$,

$$G(s) - \hat{G}(s) = (C(sI_n - A)^{-1}B + D) - (\hat{C}(sI_r - \hat{A})^{-1}\hat{B} + \hat{D})$$

$$= C((sI_n - A)^{-1} - V(sI_r - \hat{A})^{-1}W^T)B$$

Model Reduction by Projection **Projection** → Rational Interpolation

Given the ROM

$$\hat{A} = W^T A V$$
, $\hat{B} = W^T B$, $\hat{C} = C V$, $(\hat{D} = D)$,

$$G(s) - \hat{G}(s) = (C(sI_n - A)^{-1}B + D) - (\hat{C}(sI_r - \hat{A})^{-1}\hat{B} + \hat{D})$$

$$= C((sI_n - A)^{-1} - V(sI_r - \hat{A})^{-1}W^T)B$$

$$= C(I_n - \underbrace{V(sI_r - \hat{A})^{-1}W^T(sI_n - A)}_{=:P(s)})(sI_n - A)^{-1}B.$$

Projection → Rational Interpolation

Given the ROM

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If
$$s_* \in \mathbb{C} \setminus (\Lambda(A) \cup \Lambda(\hat{A}))$$
, then $P(s_*)$ is a projector onto \mathcal{V} :
range $(P(s_*)) \subset \text{range}(V)$, all matrices have full rank \Rightarrow "=",
$$P(s_*)^2 = V(s_* I_r - \hat{A})^{-1} W^T(s_* I_n - A) V(s_* I_r - \hat{A})^{-1} W^T(s_* I_n - A)$$

Model Reduction by Projection Projection --- Rational Interpolation

Given the ROM

$$\hat{A} = W^T A V, \quad \hat{B} = W^T B, \quad \hat{C} = C V, \quad (\hat{D} = D),$$

$$G(s) - \hat{G}(s) = (C(sI_n - A)^{-1}B + D) - (\hat{C}(sI_r - \hat{A})^{-1}\hat{B} + \hat{D})$$

$$= C(I_n - \underbrace{V(sI_r - \hat{A})^{-1}W^T(sI_n - A)}_{=:P(s)})(sI_n - A)^{-1}B.$$

If
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, then $P(s_*)$ is a projector onto \mathcal{V} :

$$\operatorname{range}(P(s_*)) \subset \operatorname{range}(V), \text{ all matrices have full rank } \Rightarrow "=",$$

$$P(s_*)^2 = V(s_*I_r - \hat{A})^{-1}W^T(s_*I_n - A)V(s_*I_r - \hat{A})^{-1}W^T(s_*I_n - A)$$

$$= V(s_*I_r - \hat{A})^{-1}\underbrace{(s_*I_r - \hat{A})(s_*I_r - \hat{A})^{-1}}W^T(s_*I_n - A) = P(s_*).$$

Projection → Rational Interpolation

Given the ROM

$$\hat{A} = W^T A V, \quad \hat{B} = W^T B, \quad \hat{C} = C V, \quad (\hat{D} = D),$$

the error transfer function can be written as

$$G(s) - \hat{G}(s) = (C(sI_n - A)^{-1}B + D) - (\hat{C}(sI_r - \hat{A})^{-1}\hat{B} + \hat{D})$$

$$= C(I_n - \underbrace{V(sI_r - \hat{A})^{-1}W^T(sI_n - A)}_{=:P(s)})(sI_n - A)^{-1}B.$$

If
$$s_* \in \mathbb{C} \setminus (\Lambda(A) \cup \Lambda(\hat{A}))$$
, then $P(s_*)$ is a projector onto $\mathcal{V} \Longrightarrow$

if
$$(s_*I_n - A)^{-1}B \in \mathcal{V}$$
, then $(I_n - P(s_*))(s_*I_n - A)^{-1}B = 0$,

hence

$$G(s_*) - \hat{G}(s_*) = 0 \Rightarrow G(s_*) = \hat{G}(s_*)$$
, i.e., \hat{G} interpolates G in $s_*!$

Model Reduction by Projection

 $\textbf{Projection} \leadsto \textbf{Rational Interpolation}$

Given the ROM

$$\hat{A} = W^T A V, \quad \hat{B} = W^T B, \quad \hat{C} = C V, \quad (\hat{D} = D),$$

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$$G(s) - \hat{G}(s) = (C(sI_n - A)^{-1}B + D) - (\hat{C}(sI_r - \hat{A})^{-1}\hat{B} + \hat{D})$$

$$= C(I_n - \underbrace{V(sI_r - \hat{A})^{-1}W^T(sI_n - A)}_{=:P(s)})(sI_n - A)^{-1}B.$$

Analogously, =
$$C(sl_n - A)^{-1} (l_n - \underbrace{(sl_n - A)V(sl_r - \hat{A})^{-1}W^T}_{=:Q(s)})B$$
.

If
$$s_* \in \mathbb{C} \setminus (\Lambda(A) \cup \Lambda(\hat{A}))$$
, then $Q(s)^H$ is a projector onto $\mathcal{W} \Longrightarrow if (s_* I_n - A)^{-*} C^T \in \mathcal{W}$, then $C(s_* I_n - A)^{-1} (I_n - Q(s_*)) = 0$,

hanas

$$C(s_*I_n-A)^{-1}(I_n-Q(s_*))=0,$$

hence

$$G(s_*) - \hat{G}(s_*) = 0 \Rightarrow G(s_*) = \hat{G}(s_*)$$
, i.e., \hat{G} interpolates G in s_* !

Model Reduction by Projection

Projection --> Rational Interpolation

A Petrov-Galerkin projected ROM interpolates the transfer function:

Theorem 3.3

[Grimme '97, Villemagne/Skelton '87]

Given the ROM

$$\hat{A} = W^T A V$$
, $\hat{B} = W^T B$, $\hat{C} = C V$, $(\hat{D} = D)$,

and $s_* \in \mathbb{C} \setminus (\Lambda(A) \cup \Lambda(\hat{A}))$, if either

•
$$(s_*I_n - A)^{-1}B \in \text{range}(V)$$
, or

•
$$(s_*I_n - A)^{-*}C^T \in \text{range}(W)$$
,

then the interpolation condition

$$G(s_*)=\hat{G}(s_*).$$

in s* holds.

Note: extension to Hermite interpolation conditions later!

Basic method:

Assume A is diagonalizable, $T^{-1}AT = D_A$, project state-space onto A-invariant subspace $V = \operatorname{span}(t_1, \ldots, t_r)$, $t_k = \operatorname{eigenvectors}$ corresp. to "dominant" modes / eigenvalues of A. Then with

$$V = T(:,1:r) = [t_1,...,t_r], \quad \tilde{W}^H = T^{-1}(1:r,:), \quad W = \tilde{W}(V^H\tilde{W})^{-1},$$

reduced-order model is

$$\hat{A} := W^H A V = \operatorname{diag} \{\lambda_1, \dots, \lambda_r\}, \quad \hat{B} := W^H B, \quad \hat{C} = C V$$

Also computable by truncation:

$$T^{-1}AT = \begin{bmatrix} \hat{A} \\ A_2 \end{bmatrix}, \quad T^{-1}B = \begin{bmatrix} \hat{B} \\ B_2 \end{bmatrix}, \quad CT = [\hat{C}, C_2], \quad \hat{D} = D.$$

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Properties:

Simple computation for large-scale systems, using, e.g., Krylov subspace methods (Lanczos, Arnoldi), Jacobi-Davidson method.

Basic method:

$$T^{-1}AT = \begin{bmatrix} \hat{A} \\ A_2 \end{bmatrix}, \quad T^{-1}B = \begin{bmatrix} \hat{B} \\ B_2 \end{bmatrix}, \quad CT = [\hat{C}, C_2], \quad \hat{D} = D.$$

Properties:

Error bound:

$$\left|\left|G-\hat{G}\right|\right|_{\infty} \leq ||C_2|| \, ||B_2|| \, \frac{1}{\min_{\lambda \in \Lambda(A_2)} |\mathrm{Re}(\lambda)|}.$$

Proof:

$$G(s) = C(sI - A)^{-1}B + D = CTT^{-1}(sI - A)^{-1}TT^{-1}B + D$$

$$= CT(sI - T^{-1}AT)^{-1}T^{-1}B + D$$

$$= [\hat{C}, C_2] \begin{bmatrix} (sI_r - \hat{A})^{-1} \\ (sI_{n-r} - A_2)^{-1} \end{bmatrix} \begin{bmatrix} \hat{B} \\ B_2 \end{bmatrix} + D$$

$$= \hat{G}(s) + C_2(sI_{n-r} - A_2)^{-1}B_2,$$

Basic method:

$$T^{-1}AT = \begin{bmatrix} \hat{A} \\ A_2 \end{bmatrix}, \quad T^{-1}B = \begin{bmatrix} \hat{B} \\ B_2 \end{bmatrix}, \quad CT = [\hat{C}, C_2], \quad \hat{D} = D.$$

Properties:

Error bound:

$$\left|\left|G-\hat{G}\right|\right|_{\infty} \leq ||C_2|| \, ||B_2|| \, \frac{1}{\min_{\lambda \in \Lambda(A_2)} |\operatorname{Re}(\lambda)|}.$$

Proof:

$$G(s) = \hat{G}(s) + C_2(sI_{n-r} - A_2)^{-1}B_2$$

observing that
$$\left|\left|G-\hat{G}\right|\right|=\sup_{\omega\in\mathbb{R}}\sigma_{\mathsf{max}}(C_2(\jmath\omega I_{n-r}-A_2)^{-1}B_2)$$
, and

$$C_2(\jmath\omega I_{n-r}-A_2)^{-1}B_2=C_2\operatorname{diag}\left(\frac{1}{\jmath\omega-\lambda_{r+1}},\ldots,\frac{1}{\jmath\omega-\lambda_n}\right)B_2.$$

Basic method:

Assume A is diagonalizable, $T^{-1}AT = D_A$, project state-space onto A-invariant subspace $V = \operatorname{span}(t_1, \ldots, t_r)$, $t_k = \operatorname{eigenvectors}$ corresp. to "dominant" modes / eigenvalues of A. Then reduced-order model is

$$\hat{A} := W^H A V = \operatorname{diag} \{\lambda_1, \dots, \lambda_r\}, \quad \hat{B} := W^H B, \quad \hat{C} = CV$$

Also computable by truncation:

$$T^{-1}AT = \begin{bmatrix} \hat{A} \\ A_2 \end{bmatrix}, \quad T^{-1}B = \begin{bmatrix} \hat{B} \\ B_2 \end{bmatrix}, \quad CT = [\hat{C}, C_2], \quad \hat{D} = D.$$

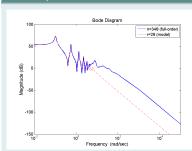
Difficulties:

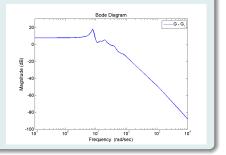
- Eigenvalues contain only limited system information.
- Dominance measures are difficult to compute. ([Litz '79] use Jordan canoncial form; otherwise merely heuristic criteria, e.g., [VARGA '95]. Recent improvement: dominant pole algorithm.)
- Error bound not computable for really large-scale problems.

Example

BEAM, SISO system from SLICOT Benchmark Collection for Model Reduction, n = 348, m = q = 1, reduced using 13 dominant complex conjugate eigenpairs, error bound yields $\left| \left| G - \hat{G} \right| \right|_{\infty} \le 1.21 \cdot 10^3$

Bode plots of transfer functions and error function





Extensions

Base enrichment

Static modes are defined by setting $\dot{x} = 0$ and assuming unit loads, i.e., $u(t) \equiv e_i, i = 1, \ldots, m$:

$$0 = Ax(t) + Be_j \implies x(t) \equiv -A^{-1}b_j.$$

Projection subspace V is then augmented by $A^{-1}[b_1, \ldots, b_m] = A^{-1}B$.

Interpolation-projection framework $\implies G(0) = \hat{G}(0)!$

If two sided projection is used, complimentary subspace can be augmented by $A^{-T}C^T \Longrightarrow G'(0) = \hat{G}'(0)!$ (If $m \neq q$, add random vectors or delete some of the columns in $A^{-T}C^{T}$).

Extensions

Guyan reduction (static condensation)

Partition states in masters $x_1 \in \mathbb{R}^r$ and slaves $x_2 \in \mathbb{R}^{n-r}$ (FEM terminology) Assume stationarity, i.e., $\dot{x} = 0$ and solve for x_2 in

$$0 = \begin{bmatrix} A_{11} & A_{12} \\ A_{21} & A_{22} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} B_1 \\ B_2 \end{bmatrix} u$$

$$\Rightarrow x_2 = -A_{22}^{-1} A_{21} x_1 - A_{22}^{-1} B_2 u.$$

Inserting this into the first part of the dynamic system

$$\dot{x}_1 = A_{11}x_1 + A_{12}x_2 + B_1u, \quad y = C_1x_1 + C_2x_2$$

then yields the reduced-order model

$$\dot{x}_1 = (A_{11} - A_{12}A_{22}^{-1}A_{21})x_1 + (B_1 - A_{12}A_{22}^{-1}B_2)u
y = (C_1 - C_2A_{22}^{-1}A_{21})x_1 - C_2A_{22}^{-1}B_2u.$$

Dominant Poles

Pole-Residue Form of Transfer Function

Consider partial fraction expansion of transfer function with D=0:

$$G(s) = \sum_{k=1}^{n} \frac{R_k}{s - \lambda_k}$$

with the residues $R_k := (Cx_k)(y_k^H B) \in \mathbb{C}^{q \times m}$.

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Note: this follows using the spectral decomposition $A = XDX^{-1}$, with

 $X = [x_1, \dots, x_n]$ the right and $X^{-1} =: Y = [y_1, \dots, y_n]^H$ the left eigenvector matrices:

$$G(s) = C(sI - XDX^{-1})^{-1}B = CX(sI - \operatorname{diag}\{\lambda_1, \dots, \lambda_n\})^{-1}YB$$

$$= [Cx_1, \dots, Cx_n] \begin{bmatrix} \frac{1}{s - \lambda_1} & & \\ & \ddots & \\ & & \frac{1}{s - \lambda_n} \end{bmatrix} \begin{bmatrix} y_1^H B \\ \vdots \\ y_n^H B \end{bmatrix}$$

$$= \sum_{k=1}^n \frac{(Cx_k)(y_k^H B)}{s - \lambda_k}.$$

Dominant Poles

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with the residues $R_k := (Cx_k)(y_k^H B) \in \mathbb{C}^{q \times m}$.

Note: $R_k = (Cx_k)(y_k^H B)$ are the residues of G in the sense of the residue theorem of complex analysis:

$$\operatorname{res} (G, \lambda_{\ell}) = \lim_{s \to \lambda_{\ell}} (s - \lambda_{\ell}) G(s) = \sum_{k=1}^{n} \underbrace{\lim_{s \to \lambda_{\ell}} \frac{s - \lambda_{\ell}}{s - \lambda_{k}}}_{= \begin{cases} 0 \text{ for } k \neq \ell \\ 1 \text{ for } k = \ell \end{cases}}_{= \frac{s - \lambda_{\ell}}{s - \lambda_{k}}} R_{k} = R_{\ell}.$$

Pole-Residue Form of Transfer Function

Consider partial fraction expansion of transfer function with D=0:

$$G(s) = \sum_{k=1}^{n} \frac{R_k}{s - \lambda_k}$$

with the residues $R_k := (Cx_k)(y_k^H B) \in \mathbb{C}^{q \times m}$.

As projection basis use spaces spanned by right/left eigenvectors corresponding to dominant poles, i.e., (λ_i, x_i, y_i) with largest

$$||R_k||/|\operatorname{re}(\lambda_k)|.$$

Pole-Residue Form of Transfer Function

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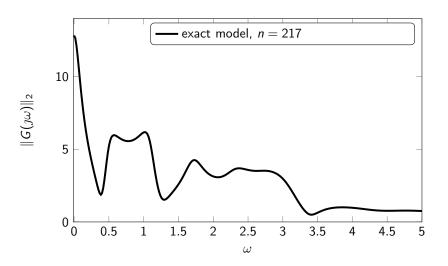
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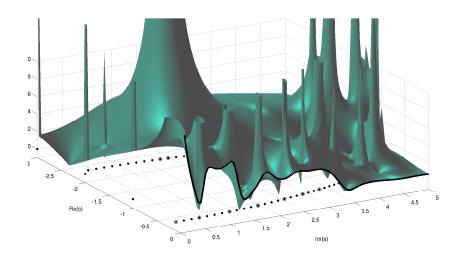
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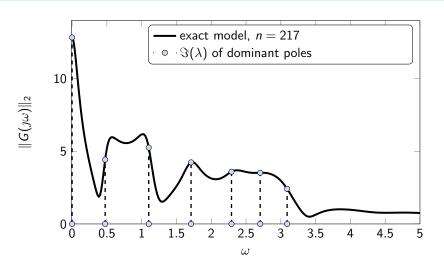
$$||R_k||/|\operatorname{re}(\lambda_k)|$$
.

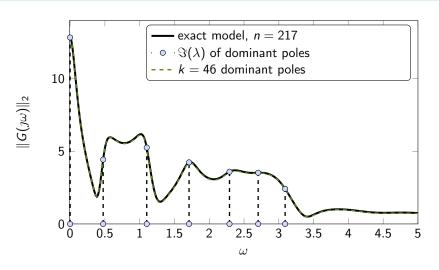
Remark

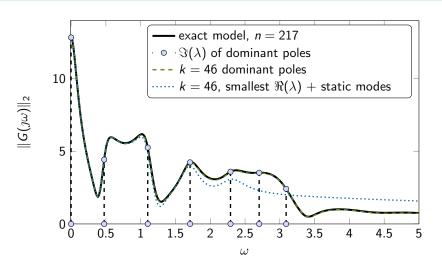
The dominant modes have most important influence on the input-output behavior of the system and are responsible for the "peaks" in the frequency response.











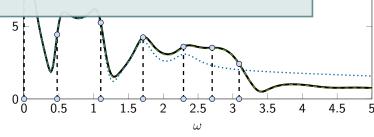
nodes

Dominant Poles

Random SISO Example ($B, C^T \in \mathbb{R}^n$)

Algorithms for computing dominant poles and eigenvectors:

- Subspace Accelerated Dominante Pole Algorithm (SADPA),
- Rayleigh-Quotient-Iteration (RQI),
- Jacobi-Davidson-Method.



- Model Reduction by Projection
 - Projection and Interpolation
 - Modal Truncation
 - Rational Interpolation
 - H₂-Optimal Model Reduction

Rational Interpolation

Computation of reduced-order model by projection

Given an LTI system $\dot{x} = Ax + Bu$, y = Cx with transfer function $G(s) = C(sI_n - A)^{-1}B$, a reduced-order model is obtained using projection approach with $V, W \in \mathbb{R}^{n \times r}$ and $W^T V = I_r$ by computing

$$\hat{A} = W^T A V, \quad \hat{B} = W^T B, \quad \hat{C} = C V.$$

Petrov-Galerkin-type (two-sided) projection: $W \neq V$,

Galerkin-type (one-sided) projection: W = V.

Model Reduction by Projection

Rational Interpolation

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Petrov-Galerkin-type (two-sided) projection: $W \neq V$,

Galerkin-type (one-sided) projection: W = V.

Rational Interpolation/Moment-Matching

Choose V, W such that

$$G(s_i) = \hat{G}(s_i), \quad j = 1, \ldots, k,$$

and

$$\frac{d^i}{ds^i}G(s_j) = \frac{d^i}{ds^i}\hat{G}(s_j), \quad i = 1, \dots, K_j, \quad j = 1, \dots, k.$$

Rational Interpolation

Theorem (simplified) [GRIMME '97, VILLEMAGNE/SKELTON '87]

lf

$$\operatorname{span} \left\{ (s_1 I_n - A)^{-1} B, \dots, (s_k I_n - A)^{-1} B \right\} \subset \operatorname{Ran}(V),$$

$$\operatorname{span} \left\{ (s_1 I_n - A)^{-T} C^T, \dots, (s_k I_n - A)^{-T} C^T \right\} \subset \operatorname{Ran}(W),$$

then

$$G(s_j) = \hat{G}(s_j), \quad \frac{d}{ds}G(s_j) = \frac{d}{ds}\hat{G}(s_j), \quad \text{for } j = 1, \dots, k.$$

Rational Interpolation

Theorem (simplified) [GRIMME '97, VILLEMAGNE/SKELTON '87]

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then

$$G(s_j) = \hat{G}(s_j), \quad \frac{d}{ds}G(s_j) = \frac{d}{ds}\hat{G}(s_j), \quad \text{for } j = 1, \dots, k.$$

Remarks:

using Galerkin/one-sided projection yields $G(s_i) = \hat{G}(s_i)$, but in general

$$\frac{d}{ds}G(s_j)\neq \frac{d}{ds}\hat{G}(s_j).$$

Model Reduction by Projection

Rational Interpolation

Theorem (simplified) [GRIMME '97, VILLEMAGNE/SKELTON '87]

lf

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then

$$G(s_j) = \hat{G}(s_j), \quad \frac{d}{ds}G(s_j) = \frac{d}{ds}\hat{G}(s_j), \quad \text{for } j = 1, \dots, k.$$

Remarks:

k=1, standard Krylov subspace(s) of dimension $K \rightsquigarrow$ moment-matching methods/Padé approximation,

$$\frac{d^i}{ds^i}G(s_1)=\frac{d^i}{ds^i}\hat{G}(s_1), \quad i=0,\ldots,K-1(+K).$$

Rational Interpolation

Theorem (simplified) [GRIMME '97, VILLEMAGNE/SKELTON '87]

lf

$$\operatorname{span}\left\{(s_1I_n-A)^{-1}B,\ldots,(s_kI_n-A)^{-1}B\right\}\subset\operatorname{Ran}(V),$$

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Remarks:

computation of V, W from rational Krylov subspaces, e.g.,

- dual rational Arnoldi/Lanczos [Grimme '97],
- Iterative Rational Krylov-Algo. [Antoulas/Beattie/Gugercin '07].

\mathcal{H}_2 -Optimal Model Reduction

Best \mathcal{H}_2 -norm approximation problem

Find
$$\arg \min_{\hat{G} \in \mathcal{H}_2 \text{ of order } \leq r} \left| \left| G - \hat{G} \right| \right|_2$$
.

\mathcal{H}_2 -Optimal Model Reduction

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.

 \rightsquigarrow First-order necessary \mathcal{H}_2 -optimality conditions:

For SISO systems

$$G(-\mu_i) = \hat{G}(-\mu_i),$$

$$G'(-\mu_i) = \hat{G}'(-\mu_i).$$

where μ_i are the poles of the reduced transfer function \hat{G} .

\mathcal{H}_2 -Optimal Model Reduction

Best \mathcal{H}_2 -norm approximation problem

Find
$$\arg \min_{\hat{G} \in \mathcal{H}_2 \text{ of order } \leq r} \left\| G - \hat{G} \right\|_2$$
.

 \rightsquigarrow First-order necessary \mathcal{H}_2 -optimality conditions:

For MIMO systems

$$G(-\mu_i)\tilde{B}_i = \hat{G}(-\mu_i)\tilde{B}_i, \qquad \text{for } i = 1, \dots, r,$$

$$\tilde{C}_i^T G(-\mu_i) = \tilde{C}_i^T \hat{G}(-\mu_i), \qquad \text{for } i = 1, \dots, r,$$

$$\tilde{C}_i^T G'(-\mu_i)\tilde{B}_i = \tilde{C}_i^T \hat{G}'(-\mu_i)\tilde{B}_i, \qquad \text{for } i = 1, \dots, r,$$

where $T^{-1}\hat{A}T = \text{diag}\{\mu_1, \dots, \mu_r\} = \text{spectral decomposition and}$

$$\tilde{B} = \hat{B}^T T^{-T}, \quad \tilde{C} = \hat{C} T.$$

→ tangential interpolation conditions.

Construct reduced transfer function by Petrov-Galerkin projection $\mathcal{P} = VW^T$, i.e.

$$\hat{G}(s) = CV (sI - W^T AV)^{-1} W^T B,$$

where V and W are given as the rational Krylov subspaces

$$V = [(-\mu_1 I - A)^{-1} B, \dots, (-\mu_r I - A)^{-1} B],$$

$$W = [(-\mu_1 I - A^T)^{-1} C^T, \dots, (-\mu_r I - A^T)^{-1} C^T].$$

Then

$$G(-\mu_i) = \hat{G}(-\mu_i)$$
 and $G'(-\mu_i) = \hat{G}'(-\mu_i)$,

for i = 1, ..., r as desired.

 \rightsquigarrow iterative algorithms (IRKA/MIRIAm) that yield \mathcal{H}_2 -optimal models.

[Gugercin et al. '06], [Bunse-Gerstner et al. '07], [Van Dooren et al. '08]

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for $i = 1, \ldots, r$ as desired.

 \rightsquigarrow iterative algorithms (IRKA/MIRIAm) that yield \mathcal{H}_2 -optimal models.

[Gugercin et al. '06], [Bunse-Gerstner et al. '07], [Van Dooren et al. '08]

Construct reduced transfer function by Petrov-Galerkin projection $\mathcal{P} = VW^T$, i.e.

$$\hat{G}(s) = CV (sI - W^T AV)^{-1} W^T B,$$

where V and W are given as the rational Krylov subspaces

$$V = [(-\mu_1 I - A)^{-1} B, \dots, (-\mu_r I - A)^{-1} B],$$

$$W = [(-\mu_1 I - A^T)^{-1} C^T, \dots, (-\mu_r I - A^T)^{-1} C^T].$$

Then

$$G(-\mu_i) = \hat{G}(-\mu_i)$$
 and $G'(-\mu_i) = \hat{G}'(-\mu_i)$,

for i = 1, ..., r as desired.

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The Basic IRKA Algorithm

Algorithm 1 IRKA (MIMO version/MIRIAm)

Input: A stable, B, C, \hat{A} stable, \hat{B} . \hat{C} . $\delta > 0$.

Output: A^{opt}, B^{opt}, C^{opt}

1: while
$$(\max_{j=1,...,r}\left\{rac{|\mu_j-\mu_j^{
m old}|}{|\mu_j|}
ight\}>\delta)$$
 do

diag $\{\mu_1, \dots, \mu_r\} := T^{-1}\hat{A}T$ = spectral decomposition, $\tilde{B} = \hat{B}^H T^{-T}$. $\tilde{C} = \hat{C} T$

3:
$$V = \left[(-\mu_1 I - A)^{-1} B \tilde{B}_1, \dots, (-\mu_r I - A)^{-1} B \tilde{B}_r \right]$$

4:
$$W = \left[(-\mu_1 I - A^T)^{-1} C^T \tilde{C}_1, \dots, (-\mu_r I - A^T)^{-1} C^T \tilde{C}_r \right]$$

5:
$$V = \text{orth}(V), W = \text{orth}(W), W = W(V^H W)^{-1}$$

6:
$$\hat{A} = W^H \hat{A} V$$
, $\hat{B} = W^H \hat{B}$, $\hat{C} = CV$

7: end while

8:
$$A^{opt} = \hat{A}$$
, $B^{opt} = \hat{B}$, $C^{opt} = \hat{C}$

Outline

- Linear Time Invariant Systems
- 2 Norms of Signals and Systems
- Introduction to Model Reduction
- 4 Model Reduction by Projection
- Balanced Truncation
 - The Basic Method
 - Theoretical Background
 - Singular Perturbation Approximation
 - Balancing-Related Methods

Basic principle:

• Recall: a stable system Σ , realized by (A, B, C, D), is called balanced, if the Gramians, i.e., solutions P, Q of the Lyapunov equations

$$AP + PA^{T} + BB^{T} = 0, A^{T}Q + QA + C^{T}C = 0,$$

satisfy:
$$P = Q = \operatorname{diag}(\sigma_1, \dots, \sigma_n)$$
 with $\sigma_1 \ge \sigma_2 \ge \dots \ge \sigma_n > 0$.

• $\Lambda(PQ)^{\frac{1}{2}} = \{\sigma_1, \dots, \sigma_n\}$ are the Hankel singular values (HSVs) of Σ .

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- Compute balanced realization of the system via state-space transformation

$$\mathcal{T}: (A, B, C, D) \mapsto (TAT^{-1}, TB, CT^{-1}, D)$$

$$= \left(\begin{bmatrix} A_{11} & A_{12} \\ A_{21} & A_{22} \end{bmatrix}, \begin{bmatrix} B_1 \\ B_2 \end{bmatrix}, \begin{bmatrix} C_1 & C_2 \end{bmatrix}, D \right)$$

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Motivation:

The HSVs $\Lambda(PQ)^{\frac{1}{2}}=\{\sigma_1,\ldots,\sigma_n\}$ are system invariants: they are preserved under

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in transformed coordinates, the Gramians satisfy

$$(TAT^{-1})(TPT^{T}) + (TPT^{T})(TAT^{-1})^{T} + (TB)(TB)^{T} = 0,$$

$$(TAT^{-1})^{T}(T^{-T}QT^{-1}) + (T^{-T}QT^{-1})(TAT^{-1}) + (CT^{-1})^{T}(CT^{-1}) = 0$$

$$\Rightarrow (TPT^{T})(T^{-T}QT^{-1}) = TPQT^{-1},$$

hence
$$\Lambda(PQ) = \Lambda((TPT^T)(T^{-T}QT^{-1})).$$

Implementation: SR Method

- Compute (Cholesky) factors of the Gramians, $P = S^T S$, $Q = R^T R$.
- ② Compute SVD $SR^T = \begin{bmatrix} U_1, U_2 \end{bmatrix} \begin{bmatrix} \Sigma_1 \\ \Sigma_2 \end{bmatrix} \begin{bmatrix} V_1^T \\ V_2^T \end{bmatrix}$.
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 $\implies VW^T$ is a projector, hence BT is a projection method.

Properties:

- Reduced-order model is stable with HSVs $\sigma_1, \ldots, \sigma_r$.
- Adaptive choice of *r* via computable error bound:

$$||y - \hat{y}||_2 \le \left(2\sum_{k=r+1}^n \sigma_k\right) ||u||_2.$$

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Theoretical Background

Linear, Time-Invariant (LTI) Systems

$$\dot{x} = Ax + Bu,$$
 $A \in \mathbb{R}^{n \times n},$ $B \in \mathbb{R}^{n \times m},$
 $y = Cx,$ $C \in \mathbb{R}^{q \times n},$ $x(-\infty) = 0.$

Alternative to State-Space Operator: Hankel Operator

Instead of

$$\mathcal{S} \colon u \mapsto y, \quad y(t) = \int_{-\infty}^t Ce^{A(t-\tau)} Bu(\tau) \, d\tau \quad \text{for all } t \in \mathbb{R}.$$

use the Hankel operator: (the future response of the past inputs)

$$\mathcal{H} \colon u_- \mapsto y_+, \quad y_+(t) = \int_{-\infty}^0 C e^{A(t-\tau)} B u(\tau) \ \mathrm{d} \tau \quad \text{for } t > 0,$$

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$$= Ce^{At} x(0; u_{-}) \quad \text{for } t > 0.$$

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- The operator \mathcal{H} is compact $\Rightarrow \mathcal{H}$ has discrete SVD
 - \rightarrow The Hankel singular values: $\{\sigma_i\}_{i=1}^{\infty}: \sigma_1 \geq \sigma_2 \geq \ldots \geq 0$
 - \rightarrow An SVD-type approximation of the linear map \mathcal{H} is possible!

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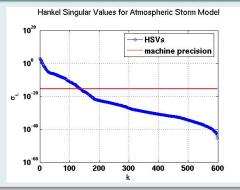
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But: computationally unfeasible for large-scale systems.

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Theorem

Let P, Q be the controllability and observability Gramians of an LTI system Σ . Then the Hankel singular values $\Lambda(PQ)^{\frac{1}{2}} = \{\sigma_1, \dots, \sigma_n\}$ are the singular values of the Hankel operator associated to Σ .

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Balanced Truncation

The Hankel Singular Values are Singular Values!

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$$= \frac{1}{\sigma^2} PQz$$

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.

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Theorem

Let the reduced-order system $\hat{\Sigma}$: $(\hat{A}, \hat{B}, \hat{C}, \hat{D})$ with $r \leq \hat{n}$ be computed by balanced truncation. Then the reduced-order model $\hat{\Sigma}$ is balanced, stable, minimal, and its HSVs are $\sigma_1, \ldots, \sigma_r$.

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Let the reduced-order system $\hat{\Sigma}$: $(\hat{A}, \hat{B}, \hat{C}, \hat{D})$ with $r \leq \hat{n}$ be computed by balanced truncation. Then the reduced-order model $\hat{\Sigma}$ is balanced, stable, minimal, and its HSVs are $\sigma_1, \ldots, \sigma_r$.

Proof: Note that in balanced coordinates, the Gramians are diagonal and equal to

$$\operatorname{diag}(\Sigma_1, \Sigma_2) = \operatorname{diag}(\sigma_1, \dots, \sigma_r, \sigma_{r+1}, \dots, \sigma_n).$$

Hence, the Gramian satisfies

$$\begin{bmatrix} A_{11} & A_{12} \\ A_{21} & A_{22} \end{bmatrix} \begin{bmatrix} \Sigma_1 \\ \Sigma_2 \end{bmatrix} + \begin{bmatrix} \Sigma_1 \\ \Sigma_2 \end{bmatrix} \begin{bmatrix} A_{11} & A_{12} \\ A_{21} & A_{22} \end{bmatrix}^T + \begin{bmatrix} B_1 \\ B_2 \end{bmatrix} \begin{bmatrix} B_1 \\ B_2 \end{bmatrix}^T = 0,$$

whence we obtain the "controllability Lyapunov equation" of the reduced-order system,

$$A_{11}\Sigma_1 + \Sigma_1 A_{11}^T + B_1 B_1^T = 0.$$

The result follows from $\hat{A}=A_{11}, \hat{B}=B_1, \Sigma_1>0$, the solution theory of Lyapunov equations and the analogous considerations for the observability Gramian. (Minimality is a simple consequence of $\hat{P}=\Sigma_1=\hat{Q}>0$.)

Assume the system

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} A_{11} & A_{12} \\ A_{21} & A_{22} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} B_1 \\ B_2 \end{bmatrix} u, \quad y = \begin{bmatrix} C_1, C_2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + Du$$

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Particularly, if $G(0) = \hat{G}(0)$ ("zero steady-state error") is required, one can apply the same condensation technique as in Guyan reduction: instead of $x_2 = 0$, set $\dot{x}_2 = 0$. This yields the reduced-order model

$$\dot{x}_1 = (A_{11} - A_{12}A_{22}^{-1}A_{21})x_1 + (B_1 - A_{12}A_{22}^{-1}B_2)u,
y = (C_1 - C_2A_{22}^{-1}A_{21})x_1 + (D - C_2A_{22}^{-1}B_2)u,$$

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- the same properties as the reduced-order model w.r.t. stability, minimality, error bound, but $\hat{D} \neq D$;
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Note:

- A_{22} invertible as in balanced coordinates, $A_{22}\Sigma_2 + \Sigma_2 A_{22}^T + B_2 B_2^T = 0$ and (A_{22}, B_2) controllable, $\Sigma_2 > 0 \Rightarrow A_{22}$ stable.
- If the original system is not balanced, first compute a minimal realization by applying balanced truncation with $r = \hat{n}$.

Basic Principle

Given positive semidefinite matrices $P = S^T S$, $Q = R^T R$, compute balancing state-space transformation so that

$$P = Q = \operatorname{diag}(\sigma_1, \ldots, \sigma_n) = \Sigma, \quad \sigma_1 \ge \ldots \ge \sigma_n > 0,$$

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Classical Balanced Truncation (BT)

[Mullis/Roberts '76, Moore '81]

- P = controllability Gramian of system given by (A, B, C, D).
- Q = observability Gramian of system given by (A, B, C, D).
- P, Q solve dual Lyapunov equations

$$AP + PA^{T} + BB^{T} = 0, \qquad A^{T}Q + QA + C^{T}C = 0.$$

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LQG Balanced Truncation (LQGBT) [Jonckheere/Silverman '83]

- P/Q = controllability/observability Gramian of closed-loop systembased on LQG compensator.
- P, Q solve dual algebraic Riccati equations (AREs)

$$0 = AP + PA^T - PC^TCP + B^TB,$$

$$0 = A^T Q + QA - QBB^T Q + C^T C.$$

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Given positive semidefinite matrices $P = S^T S$, $Q = R^T R$, compute balancing state-space transformation so that

$$P = Q = \operatorname{diag}(\sigma_1, \ldots, \sigma_n) = \Sigma, \quad \sigma_1 \ge \ldots \ge \sigma_n > 0,$$

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Balanced Stochastic Truncation (BST) [Desai/Pal '84, Green '88]

- P = controllability Gramian of system given by (A, B, C, D), i.e., solution of Lyapunov equation $AP + PA^T + BB^T = 0$.
- Q = observability Gramian of right spectral factor of power spectrum of system given by (A, B, C, D), i.e., solution of ARE

$$\hat{A}^T Q + Q \hat{A} + Q B_W (DD^T)^{-1} B_W^T Q + C^T (DD^T)^{-1} C = 0,$$

where $\hat{A} := A - B_W (DD^T)^{-1} C$, $B_W := BD^T + PC^T$.

Basic Principle

Given positive semidefinite matrices $P = S^T S$, $Q = R^T R$, compute balancing state-space transformation so that

$$P = Q = \operatorname{diag}(\sigma_1, \dots, \sigma_n) = \Sigma, \quad \sigma_1 \ge \dots \ge \sigma_n > 0,$$

and truncate corresponding realization at size r with $\sigma_r > \sigma_{r+1}$.

Positive-Real Balanced Truncation (PRBT)

Jreen '88]

- Based on positive-real equations, related to positive real (Kalman-Yakubovich-Popov-Anderson) lemma.
- P, Q solve dual AREs

$$0 = \bar{A}P + P\bar{A}^{T} + PC^{T}\bar{R}^{-1}CP + B\bar{R}^{-1}B^{T}, 0 = \bar{A}^{T}Q + Q\bar{A} + QB\bar{R}^{-1}B^{T}Q + C^{T}\bar{R}^{-1}C,$$

where
$$\bar{R} = D + D^T$$
. $\bar{A} = A - B\bar{R}^{-1}C$.

Basic Principle

Given positive semidefinite matrices $P = S^T S$, $Q = R^T R$, compute balancing state-space transformation so that

$$P = Q = \operatorname{diag}(\sigma_1, \ldots, \sigma_n) = \Sigma, \quad \sigma_1 \ge \ldots \ge \sigma_n > 0,$$

and truncate corresponding realization at size r with $\sigma_r > \sigma_{r+1}$.

Other Balancing-Based Methods

- Bounded-real balanced truncation (BRBT) based on bounded real lemma [OPDENACKER/JONCKHEERE '88];
- H_{∞} balanced truncation (HinfBT) closed-loop balancing based on H_{∞} compensator [Mustafa/Glover '91].

Both approaches require solution of dual AREs.

Frequency-weighted versions of the above approaches.

Properties

- Guaranteed preservation of physical properties like
 - stability (all).
 - passivity (PRBT),
 - minimum phase (BST).
- Computable error bounds, e.g.,

$$\begin{split} \mathsf{BT:} \quad & \left| \left| \left| G - G_r \right| \right|_{\infty} \quad \leq 2 \sum_{j=r+1}^n \sigma_j^{BT}, \\ \mathsf{LQGBT:} \quad & \left| \left| \left| G - G_r \right| \right|_{\infty} \quad \leq \ 2 \sum_{j=r+1}^n \frac{\sigma_j^{\mathsf{LQG}}}{\sqrt{1 + (\sigma_j^{\mathsf{LQG}})^2}} \\ \\ \mathsf{BST:} \quad & \left| \left| \left| G - G_r \right| \right|_{\infty} \quad \leq \left(\prod_{j=r+1}^n \frac{1 + \sigma_j^{\mathsf{BST}}}{1 - \sigma_j^{\mathsf{BST}}} - 1 \right) \left| \left| \left| G \right| \right|_{\infty}, \end{split}$$

- Can be combined with singular perturbation approximation for steady-state performance.
- Computations can be modularized.

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