



P.O. Box 690, Newman, CA 95360.

Phone: 669-253-0101

Email: admin@logardesign.com

Structural Calculations

For:

INTERIOR REMODEL

Into a 1-Story Structure

At:

Residence: 4456 Gina St, Fremont, CA 94538

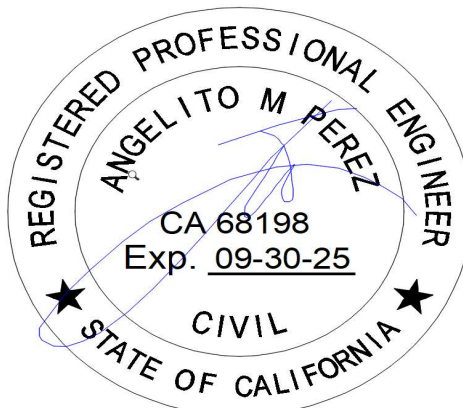
Prepared for

Jose

May 2, 2024

Job Number: LGRAS24014

Rev. 1



Angelito M Perez P.E.

Professional Engineer, CA 68198



5/23/2024, 4:36:07 AM

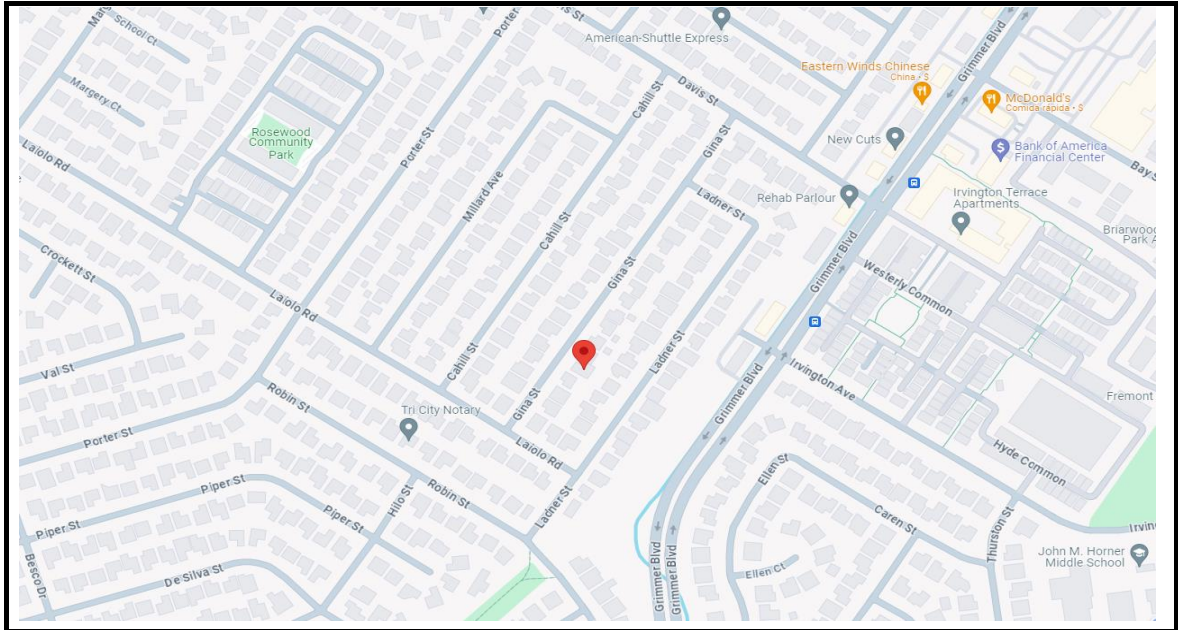
BLD2024-06272

Manoja Dalavai



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For: INTERIOR REMODEL
Residence: 4456 Gina St, Fremont, CA 94538
Date: 15/03/2024
Project No.: LGRAS24014
Source: Google Maps



VECINITY MAPS



ELEVATION VIEW OF SITE



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Date: 15/03/2024

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4456 Gina St, Fremont, CA 94538

VERTICAL LOADING

ROOFING

A. Roof Dead Load:

Typical Roof Slope 2 :12

Roofing - Asphalt	8.00	psf
1/2" Plywood/Sheathing	1.50	psf
Rafters 4x @ 24 oc V.I.F.	2.80	psf
Insulation	1.00	psf
Gypsum Ceiling	2.50	psf
Misc.	1.00	psf
	16.80	psf
Adj. for slope	18.00	psf

B. Roof Live Load: 20.00 psf per IBC

EXTERIOR WALL

Gypsum	2.50	psf
Studs	1.00	psf
Insulation	1.00	psf
Plywood & Misc.	2.50	psf
Stucco	10.00	psf
	17.00	psf

INTERIOR WALL

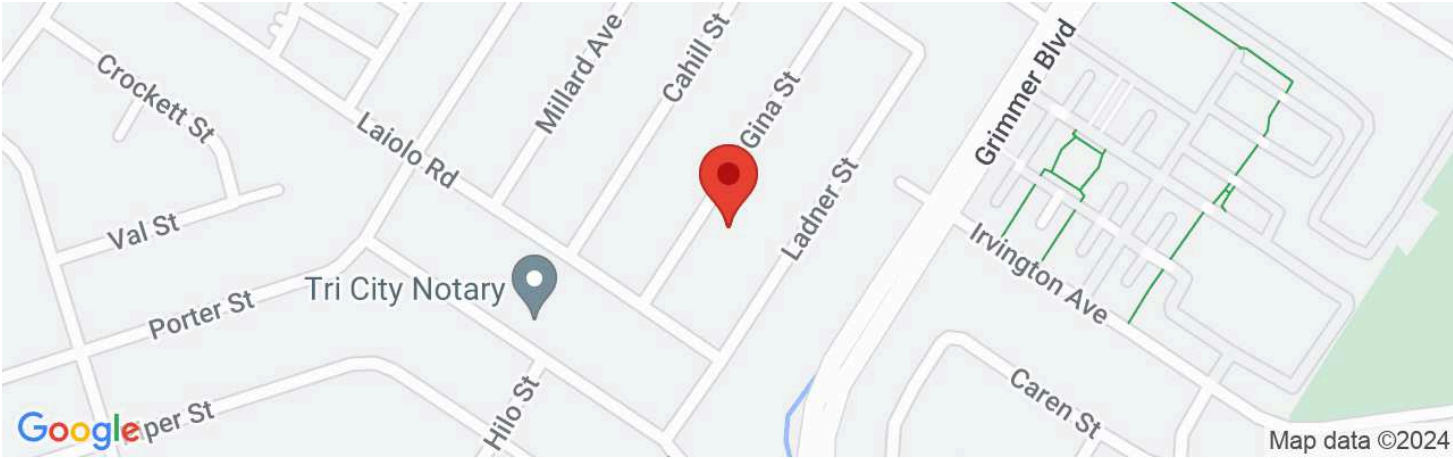
Gypsum	2.50	psf
Studs	1.00	psf
Insulation	1.00	psf
Misc.	1.00	psf
Gypsum	2.50	psf
	8.00	psf

USGS web services were down for some period of time and as a result this tool wasn't operational, resulting in *timeout* error.
USGS web services are now operational so this tool should work as expected.



4456 Gina St, Fremont, CA 94538, EE. UU.

Latitude, Longitude: 37.5319577, -121.9710263



Date	12/3/2024, 09:17:24
Design Code Reference Document	ASCE7-16
Risk Category	II
Site Class	D - Default (See Section 11.4.3)

Type	Value	Description
S _S	2.129	MCE _R ground motion. (for 0.2 second period)
S ₁	0.82	MCE _R ground motion. (for 1.0s period)
S _{MS}	2.555	Site-modified spectral acceleration value
S _{M1}	null -See Section 11.4.8	Site-modified spectral acceleration value
S _{DS}	1.703	Numeric seismic design value at 0.2 second SA
S _{D1}	null -See Section 11.4.8	Numeric seismic design value at 1.0 second SA

Type	Value	Description
SDC	null -See Section 11.4.8	Seismic design category
F _a	1.2	Site amplification factor at 0.2 second
F _v	null -See Section 11.4.8	Site amplification factor at 1.0 second
PGA	0.894	MCE _G peak ground acceleration
F _{PGA}	1.2	Site amplification factor at PGA
PGA _M	1.073	Site modified peak ground acceleration
T _L	8	Long-period transition period in seconds
SsRT	3.052	Probabilistic risk-targeted ground motion. (0.2 second)
SsUH	3.321	Factored uniform-hazard (2% probability of exceedance in 50 years) spectral acceleration
SsD	2.129	Factored deterministic acceleration value. (0.2 second)
S1RT	1.13	Probabilistic risk-targeted ground motion. (1.0 second)
S1UH	1.248	Factored uniform-hazard (2% probability of exceedance in 50 years) spectral acceleration.
S1D	0.82	Factored deterministic acceleration value. (1.0 second)
PGA _d	0.894	Factored deterministic acceleration value. (Peak Ground Acceleration)
PGA _{UH}	1.256	Uniform-hazard (2% probability of exceedance in 50 years) Peak Ground Acceleration
C _{RS}	0.919	Mapped value of the risk coefficient at short periods
C _{R1}	0.905	Mapped value of the risk coefficient at a period of 1 s
C _v	1.5	Vertical coefficient



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INTERIOR REMODEL

Residence:

Projet No.: LGRAS24014

4456 Gina St, Fremont, CA 94538

Bldg Story: 1

Latitude: 37.5319577

Longitude: -121.9710263

Type of Framing System: Bearing Wall

Type of Occupancy: Category II

Site Class: Class D

Height, h: 10.8

Response Modification Coefficient R: 6.5

Importance factor I: 1.0

11.4.1 Mapped Acceleration Parameters

SS= 2.129 g = spectral response acceleration parameter at short periods

S1= 0.820 g = spectral response acceleration parameter at a period of 1 s

11.4.3 Site Coefficients and Adjusted MCE Spectral Resoponse Acceleration Parameters

SMS= $F_a \cdot SS$

F_a = 1.2 = short-period site coefficient (at 0.2 s-period) from Table 11.4-1

SMS= 2.55 g = spectral response acceleration at short periods adjusted for site class effects

SM1= $F_v \cdot S1$

F_v = 1.50 = short-period site coefficient (at 0.1 s-period) from Table 11.4-2

SM1= 1.23 g = spectral response acceleration at short periods adjusted for site class effects

11.4.4 Design Spectral Acceleration Parameters

SDS= $(2/3) \cdot SMS = (2/3) \cdot 2.5548$

SDS= 1.70 g = spectral response acceleration at short periods adjusted for site class effects

SD1= $(2/3) \cdot SM1 = (2/3) \cdot 1.23$

SD1= 0.82 g = spectral response acceleration at short periods adjusted for site class effects

11.4.5 Design Response Spectrum

$T = T_a = (C_t) \cdot (h)^x$

C_t = 0.02 = building period coefficient

x = 0.75 = building period coefficient

T_a = 0.12 s = approximate fundamental period of the building

12.8.1.1 Calculation of Seismic Response Coefficient

$C_s = S_{DS} / (R / I)$ (Equation 12.8-2)

C_s = 0.262 g = seismic response coefficient

Check C_s not exceeding the following values:

1.) $C_{s1} = S_{D1} / T (R / I)$ for $T < T_L$ (equation 12.8-3)

C_{s1} = 1.062 g

Okay

2.) $C_{s2} = 0.01$ = seismic response coefficient (equation 12.8-5)

3.) $C_{s3} = 0.5 S_1 / (R / I)$ (Equation 12.8-6)

C_{s3} = 0.063 g

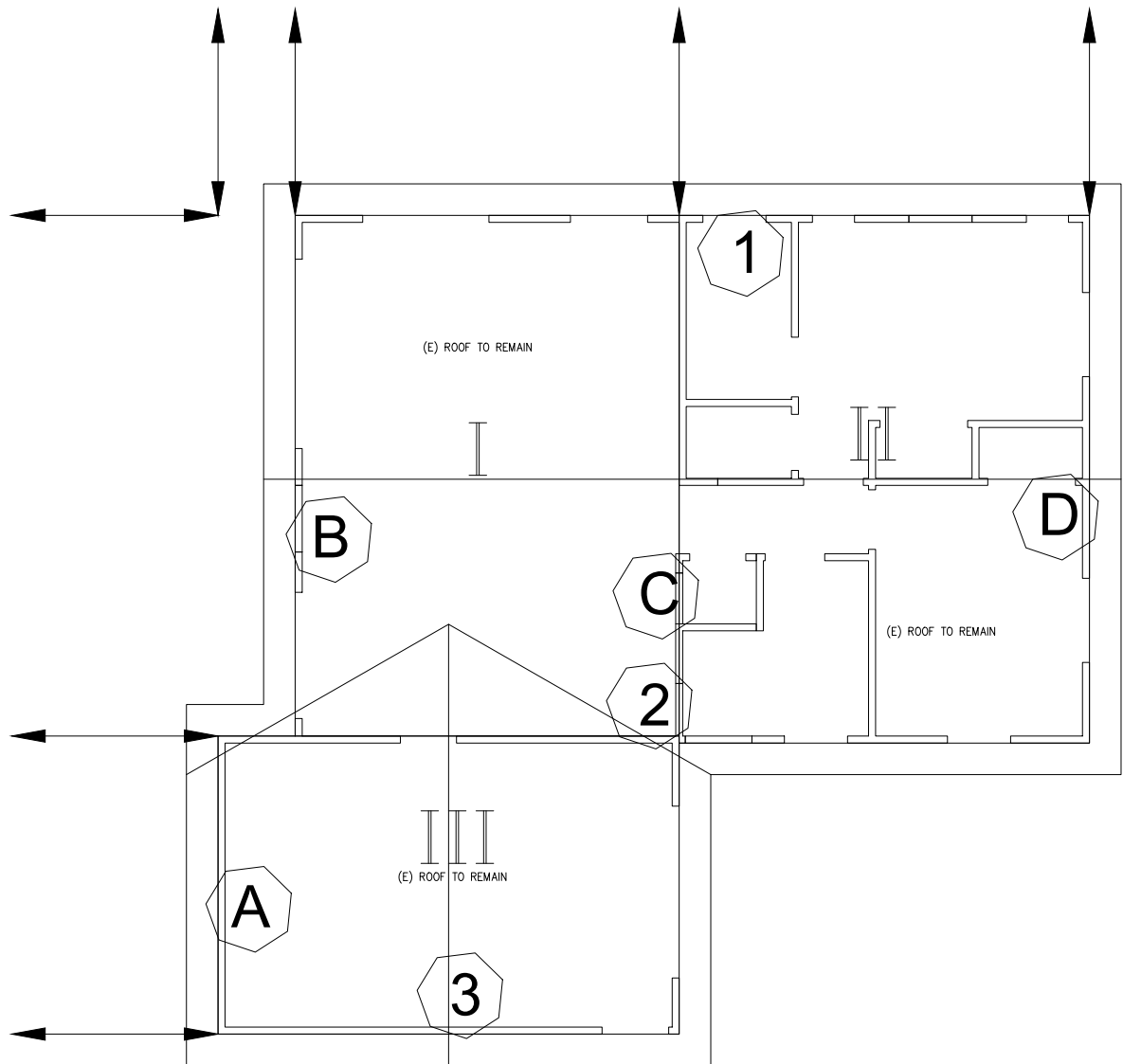
Okay

Seismic Coefficient, C_s = 0.262 g = seismic response coefficient

W = the total dead load of the building (on following page)

$V = C_s W$

LATERAL ANALYSIS





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For: INTERIOR REMODEL
Residence: 4456 Gina St, Fremont, CA 94538
Date: 02/05/2024
Projet No.: LGRAS24014

Transverse & Longitudinal Lateral Loadings

Tributary Building Weights:

Weight of Roof:	18 psf	1500 sf			27000 lbs
Weight of Exterior Walls:	17 psf	160.0 ft	8 ft	0.5	10880 lbs
Weight of Interior Walls:	8 psf	94.0 ft	8 ft	0.5	3008 lbs
Total Weight					40888 lbs

Cs (Per ASCE 7, Sec. 12.8-1.1)

Cs =	0.262
------	-------

Seismic Base Shear: $V = C_s \cdot W \cdot p$ (Per ASCE 7, Eq. 12.8-1)

V =	0.7	0.262	40888 lbs	1.3
V =	9750 lbs			

AREAS FOR GRID LINES

AREA I 452 sf

AREA II 489 sf

AREA III 310 sf

$\Sigma =$ 1251 sf

Transverse Loading

$V_{\text{East-West}} = 9750 \text{ lbs} / 1251 \text{ sf}$

$V_{\text{East-West}} = 7.8 \text{ psf}$

				SW Length	Nailing Sched	Factor
Line 1:	7.8 psf	471 sf	3667 lbs	7.75 ft	3 in 3	473 plf
Line 2:	7.8 psf	626 sf	4875 lbs			
Line 3:	7.8 psf	155 sf	1208 lbs			
$\Sigma =$	1251 sf		9750 lbs			

Longitudinal Loading

$V_{\text{North-South}} = 9750 \text{ lbs} / 1251 \text{ sf}$

$V_{\text{North-South}} = 7.8 \text{ psf}$

Line A:	7.8 psf	155 sf	1208 lbs
Line B:	7.8 psf	226 sf	1761 lbs
Line C:	7.8 psf	626 sf	4875 lbs
Line D:	7.8 psf	245 sf	1906 lbs
$\Sigma =$	1251 sf		9750 lbs

Shearwall Stability:

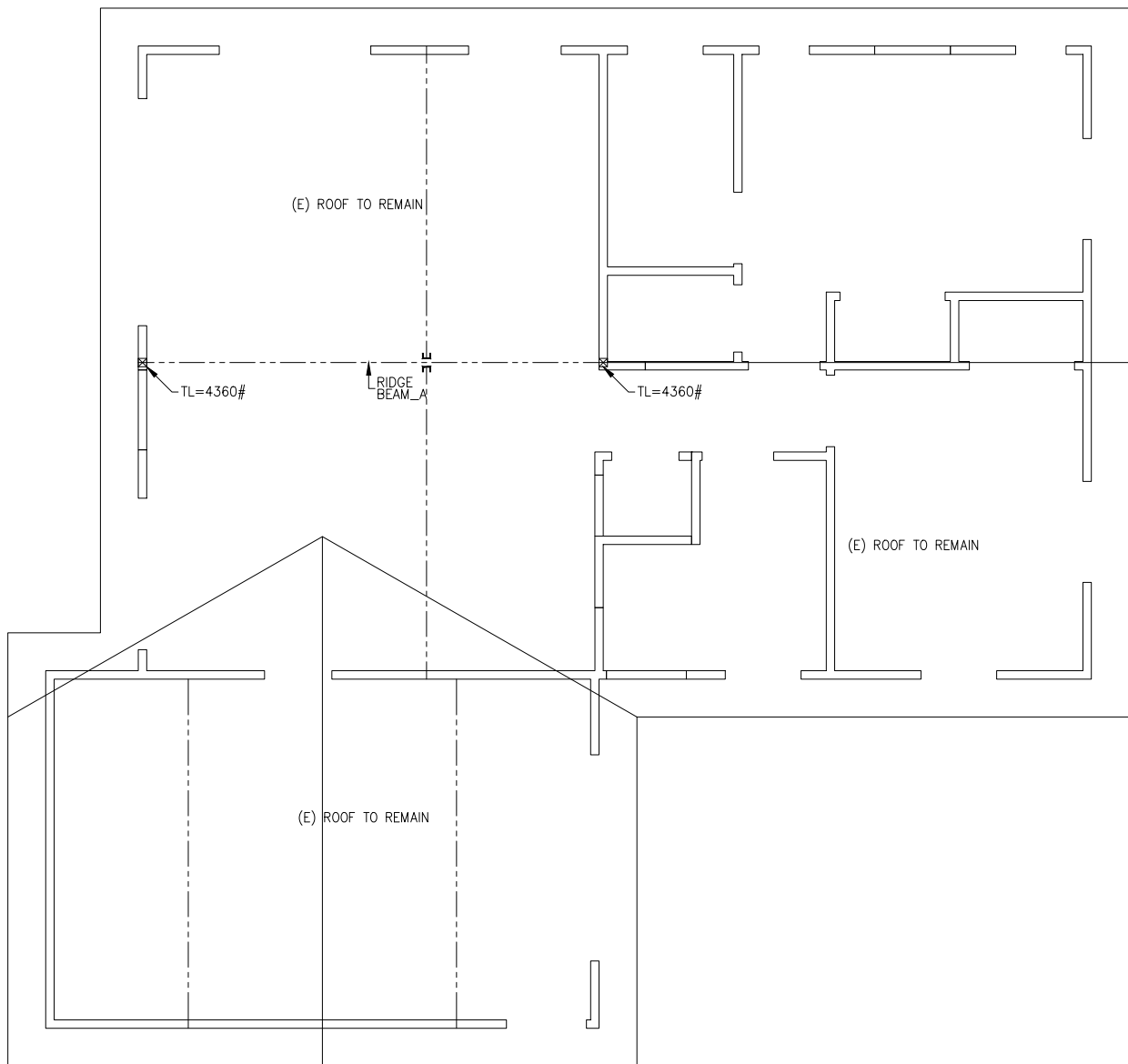
	SW Ht.	SW Ht*FORCE	(/0.7)	($\Omega=2.5$)	
Line 1:	473 plf	8.0 ft	3784 lbs	5406 lbs	13514 lbs Use Simpson HDU4 w/4x4" Post; Cap. = 4565 lbs.



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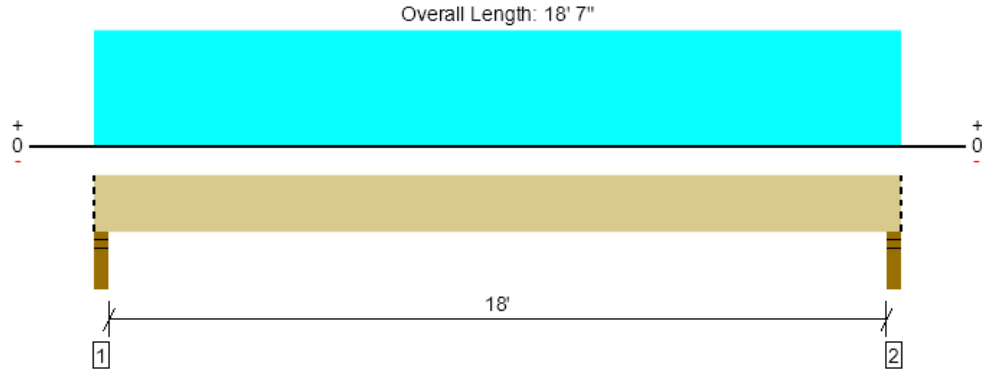
SHEAR WALL SCHEDULE							NOTE #12
SHEAR WALL CONNECTION			SHEAR TRANSFER NOTE #11	SILL PLATE CONNECTIONS (SEE NOTE #9 @ EXISTING CONCRETE)		ANCHOR BOLTS (A.B.'S) REMARKS: SHEAR BOLTS	SHEAR WALL CAPACITY (#/')
MARK	MATERIAL	PLYWOOD NAILING		NAILING OR CLIPS (T.N.)	NAILING (S.N.) FOR 2x SOLE PLATE ONLY		
	3/8" CDX PLYWOOD P.I.: 24/0 *	8d AT 6" O.C. E.N. 8d AT 12" O.C. F.N.	16d AT 5" O.C. OR A35 @ 16" O.C. OR LTP4 AT 24" O.C.		16d AT 5" O.C.	5/8"Ø A.B. AT 4'-0" O.C.	260
	3/8" CDX PLYWOOD P.I.: 24/0 *	8d AT 4" O.C. E.N. 8d AT 12" O.C. F.N.	16d AT 3" O.C. OR A35 @ 12" O.C. OR LTP4 AT 20" O.C.			5/8"Ø A.B. AT 3'-3" O.C.	380
	3/8" CDX PLYWOOD P.I.: 24/0 **	8d AT 3" O.C. E.N. 8d AT 12" O.C. F.N.	A35 @ 10" O.C. OR LTP4 AT 16" O.C.			5/8"Ø A.B. AT 2'-4" O.C.	490
	3/8" CDX PLYWOOD P.I.: 24/0 **	8d AT 2" O.C. E.N. 8d AT 12" O.C. F.N.	A35 @ 10" O.C. OR LTP4 AT 12" O.C.			5/8"Ø A.B. AT 1'-8" O.C.	636
	1/2" CDX PLYWOOD P.I.: 24/0 **	10d AT 2" O.C. E.N. 10d AT 12" O.C. F.N.	2-A35 @ 12" O.C. OR LTP4 AT 10" O.C.			5/8"Ø A.B. AT 1'-6" O.C.	770
	1/2" STR. PLYWOOD P.I.: 24/0 **	10d AT 2" O.C. E.N. 10d AT 12" O.C. F.N.	2-A35 @ 12" O.C. OR LTP4 AT 8" O.C.			5/8"Ø A.B. AT 1'-4" O.C.	870
	3/8" CDX PLYWOOD ** EACH SIDE P.I.: 24/0	8d AT 3" O.C. E.N. 8d AT 12" O.C. F.N.	2-A35 @ 12" O.C. OR LTP4 AT 8" O.C.			5/8"Ø A.B. AT 1'-2" O.C.	980
	3/8" CDX PLYWOOD ** EACH SIDE P.I.: 24/0	8d AT 2" O.C. E.N. 8d AT 12" O.C. F.N.	NOTE #10 LTP4 AT 12" O.C. EACH SIDE, STAGGER			5/8"Ø A.B. AT 11" O.C.	1272
	1/2" STRUCT I PLYWOOD** EACH SIDE P.I.: 24/0	10d AT 2" O.C. E.N. 10d AT 12" O.C. F.N.	NOTE #10 LTP4 AT 8" O.C. EACH SIDE, STAGGER			5/8"Ø A.B. AT 8" O.C.	1740



***STRUCTURAL MEMBERS (CHECK LIST)**

***LOADS TO SUPPORTS (CHECK LIST)**

Roof Members, Ridge Beam_A
1 piece(s) 3 1/2" x 11 7/8" 2.2E Parallam® PSL



Drawing is Conceptual. All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	4358 @ 2"	7656 (3.50")	Passed (57%)	--	1.0 D + 1.0 Lr (All Spans)
Shear (lbs)	3757 @ 1' 3 3/8"	10044	Passed (37%)	1.25	1.0 D + 1.0 Lr (All Spans)
Moment (Ft-lbs)	19525 @ 9' 3 1/2"	24878	Passed (78%)	1.25	1.0 D + 1.0 Lr (All Spans)
Live Load Defl. (in)	0.583 @ 9' 3 1/2"	0.913	Passed (L/376)	--	1.0 D + 1.0 Lr (All Spans)
Total Load Defl. (in)	1.139 @ 9' 3 1/2"	1.217	Passed (L/192)	--	1.0 D + 1.0 Lr (All Spans)

- Deflection criteria: LL (L/240) and TL (L/180).
- Allowed moment does not reflect the adjustment for the beam stability factor.

Member Length : 18' 7"
System : Roof
Member Type : Drop Beam
Building Use : Residential
Building Code : IBC 2021
Design Methodology : ASD
Member Pitch : 0/12

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Roof Live	Factored	
1 - Stud wall - DF	3.50"	3.50"	1.99"	2128	2230	4358	Blocking
2 - Stud wall - DF	3.50"	3.50"	1.99"	2128	2230	4358	Blocking

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	18' 7" o/c	
Bottom Edge (Lu)	18' 7" o/c	

- Maximum allowable bracing intervals based on applied load.

Vertical Loads	Location (Side)	Tributary Width	Dead (0.90)	Roof Live (1.25)	Comments
0 - Self Weight (PLF)	0 to 18' 7"	N/A	13.0	--	
1 - Uniform (PSF)	0 to 18' 7" (Front)	12'	18.0	20.0	Roof Load

Weyerhaeuser Notes

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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

ForteWEB Software Operator	Job Notes
Ismael Arcos Structural Engineering (408) 659-5580 i.arcos@gd-se.com Rev. 0	



3/14/2024 6:19:04 PM UTC
ForteWEB v3.7, Engine: V8.4.0.40, Data: V8.1.5.0
File Name: 4456 Gina St, Fremont, CA 94538



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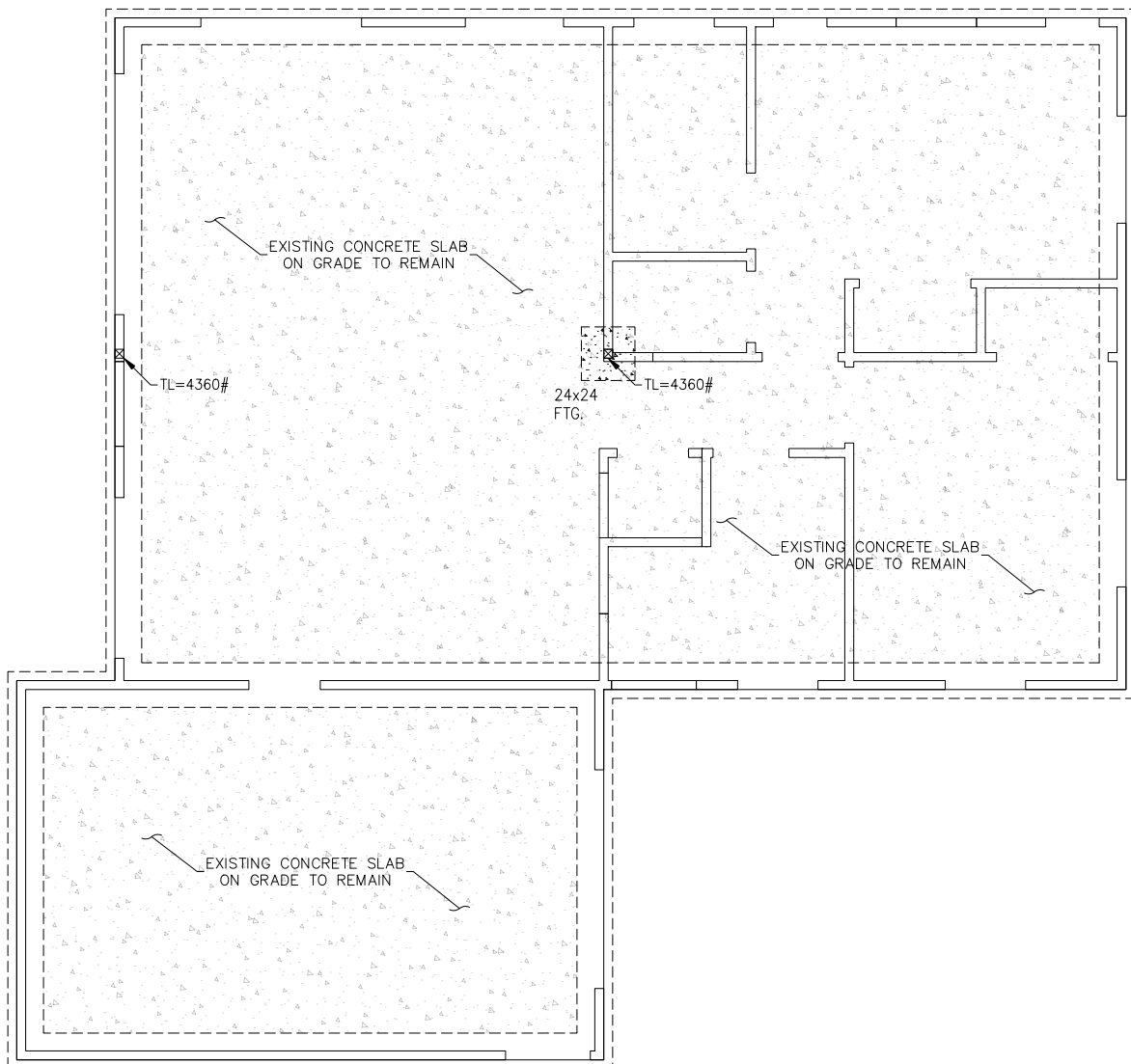
Allowable Point Loads on Doug Fir Wood Posts / Columns

Post Size	Height	L_e / d	F_{CE}	C_P	$F_C p^{erp}$	$F_C p^{rll}$	Area of post	P_{ALLOW}
(inches)	(feet)	(in / in)	(psi)		(psi)	(psi)	(in ²)	(lbs)

4 x 4	8	27.4	634	0.41	625	1350	12.25	6810
	9	30.9	501	0.34	625	1350	12.25	5568
	10	34.3	406	0.28	625	1350	12.25	4612
	11	37.7	335	0.23	625	1350	12.25	3870
	12	41.1	282	0.20	625	1350	12.25	3287
	13	44.6	240	0.17	625	1350	12.25	2824
	14	48.0	207	0.15	625	1350	12.25	2450

4 x 6	8	27.4	634	0.41	625	1350	19.25	10701
	9	30.9	501	0.34	625	1350	19.25	8750
	10	34.3	406	0.28	625	1350	19.25	7247
	11	37.7	335	0.23	625	1350	19.25	6081
	12	41.1	282	0.20	625	1350	19.25	5165
	13	44.6	240	0.17	625	1350	19.25	4437
	14	48.0	207	0.15	625	1350	19.25	3849

4 x 8	8	27.4	634	0.41	625	1350	25.38	14106
	9	30.9	501	0.34	625	1350	25.38	11535
	10	34.3	406	0.28	625	1350	25.38	9553
	11	37.7	335	0.23	625	1350	25.38	8016
	12	41.1	282	0.20	625	1350	25.38	6809
	13	44.6	240	0.17	625	1350	25.38	5849
	14	48.0	207	0.15	625	1350	25.38	5074



***STRUCTURAL MEMBERS (CHECK LIST)**
***LOADS TO SUPPORTS (CHECK LIST)**



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ALLOWABLE LOAD ON SQUARE PAD FOOTING

SOIL BEARING CAPACITY = **1,500 PSF**

P1 = ABP x FOOTING SIZE

P2 = WEIGHT OF FOOTING

DENSITY CONCRETE= **150**

P ALLOW = ALLOWABLE CONCENTRATED LOAD ON FOOTING(NOT INCLUDING FOOTING WEIGHT)

MARK	FOOTING SIZE (DIAMETER FEET)	FOOTING THICK (INCH)	P1 (LBS)	P2 (LBS)	P ALLOW WITH FOOTING WEIGHT	P ALLOW WITHOUT FOOTING WEIGHT
1	1.5	18	3375	506	2869	3375
2	2	18	6000	900	5100	6000
3	2.5	18	9375	1406	7969	9375
4	3	18	13500	2025	11475	13500
5	3.5	18	18375	2756	15619	18375
6	4	18	24000	3600	20400	24000
7	4.5	18	30375	4556	25819	30375

EXISTING FOUNDATION CHECK CAPACITY

Property soil:

SOIL BEARING CAPACITY = 1500 psf

Angle, $\Phi = 60^\circ$

Actuating load :

$P_u = 4360$ lbs

Property Post:

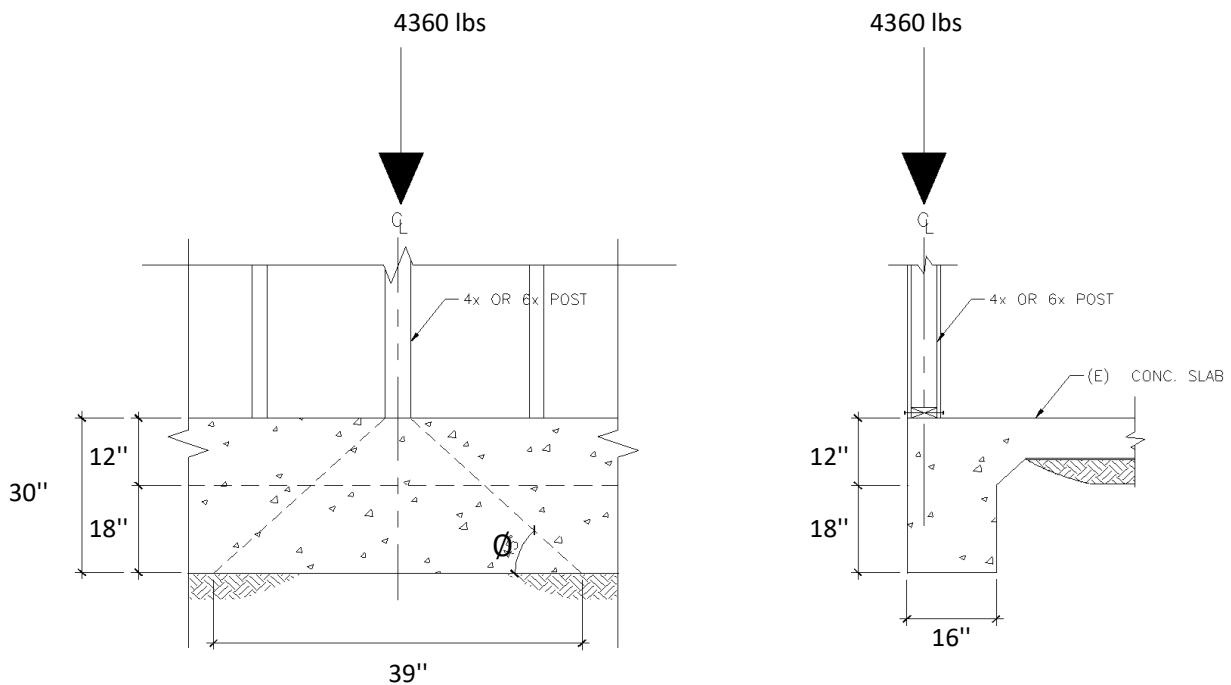
size post : 4" x 4"

Dimensions Footing:

height 1: 12" V.I.F.

height 2: 18" V.I.F.

Width: 16" V.I.F.



$$\text{Area} = 39/12 \times 16/12 = 4.3 \text{ ft}^2$$

$$f = \frac{P}{A} = \frac{4360 \text{ lbs}}{4.3 \text{ ft}^2} = 1006 \text{ psf}$$

1006 psf < 1500 psf OK