Engineering Fluid Mechanics

工程流体力学

第8章 不可压缩粘性流体的外部流动

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第8章 不可压缩粘性流体的外部流动



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引言

什么是不可压缩流体的外部流动?

"南昌号"驱逐舰







海水围绕军舰流动、海水围绕海上钻井平台流动...

引言

在上世纪初之前,流体力学的研究分为两个分支:一是研究流体运动 时不考虑黏性,运用数学工具分析流体的运动规律。另一个是不用数学理 论而完全建立在实验基础上对流体运动进行研究,解决了技术发展中许多 重要问题,但其结果常受实验条件限制。这两个分支的研究方法完全不同, 这种理论和实验分离的现象持续了150多年,直到上世纪初普朗特提出了 边界层理论为止。由于边界层理论具有广泛的理论和实用意义,因此得到 了迅速发展,成为黏性流体动力学的一个重要领域。

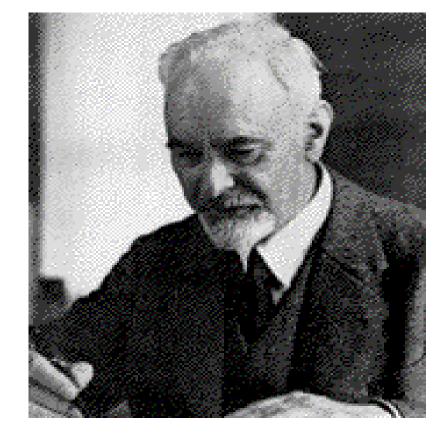
本章主要介绍边界层的基本概念及研究方法。

8.1 边界层的概念

第三届国际数学大会 德国海登堡

德国著名的力学家 - 普朗特

(论黏性很小的流体运动)



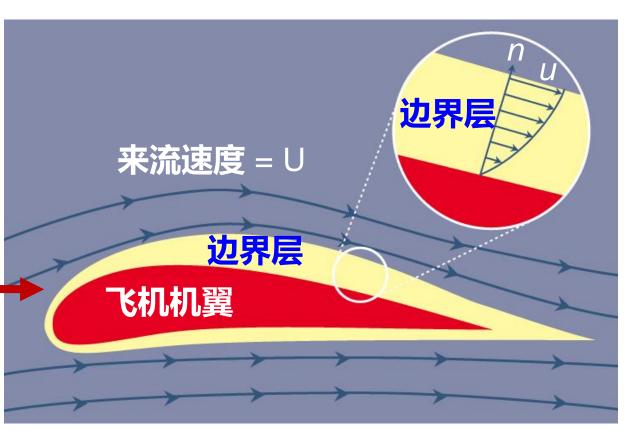
Ludwig Prandtl (1875-1953)

水和空气等<u>黏度很小的流体,在大雷诺数下</u>绕物体流动时, 黏性对流动的影响仅限于紧贴物体壁面的薄层中,而在这一薄层 外黏性影响很小,完全可以忽略不计,这一薄层称为边界层。

8.1 边界层的概念 - 什么是边界层?

气流绕过机翼形成的边界层

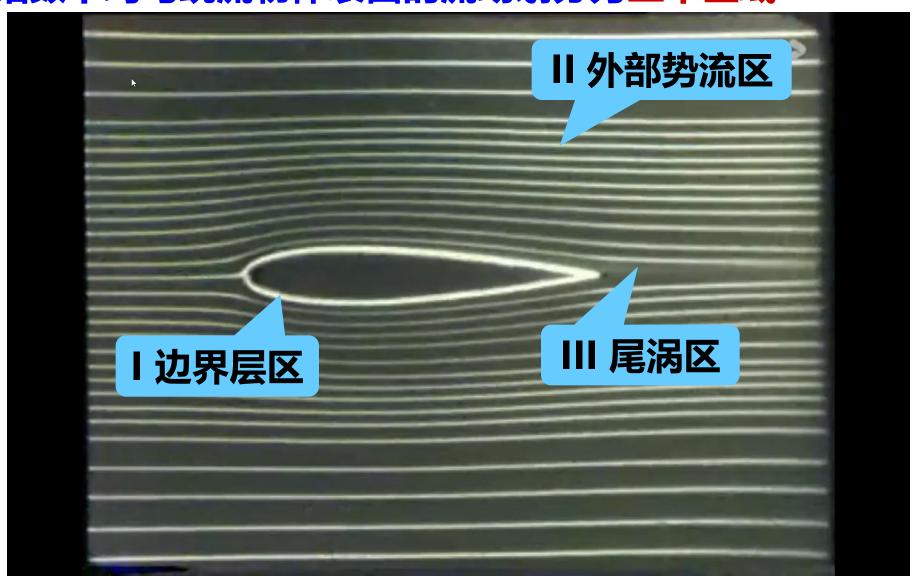




边界层内、外区域并没有明显的分界面,一般将壁面流速为零与流速达到来流速度的99%处之间的距离定义为边界层厚度。

8.1 边界层的概念 - 实验现象

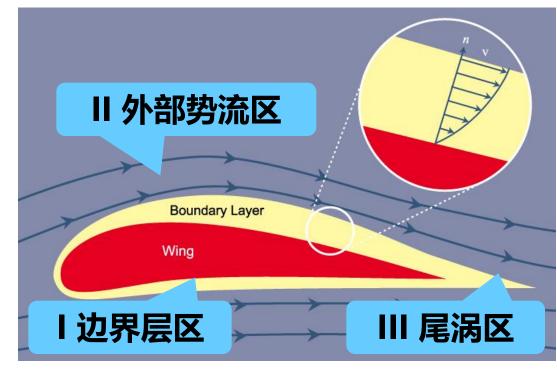
大雷诺数下均匀绕流物体表面的流场划分为三个区域:



8.1 边界层的概念 – 粘性流体外部流动的流场划分

流场的求解可分为两个区进行

■ 在边界层和尾涡区内,黏性力作用显著,黏性力和惯性力有相同的数量级,属于黏性流体的有旋流动区;



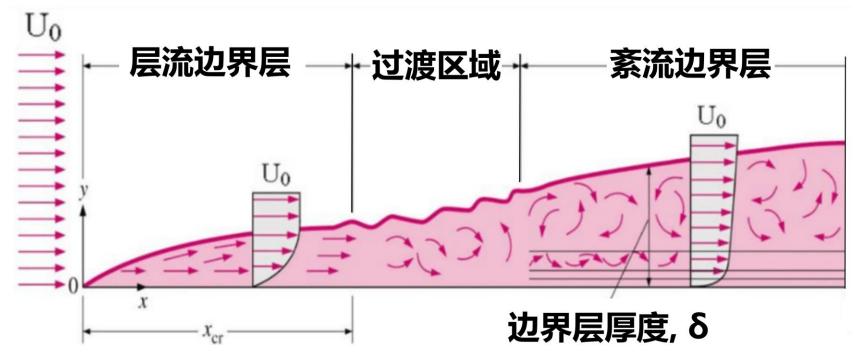
■ 在边界层和尾涡区外,流体的运动速度几乎相同,速度梯度很小,边界层外部的流动不受固体壁面的影响,即使黏度较大的流体,黏性力也很小,主要是惯性力。所以可将这个区域看作是理想流体势流区,可以利用前面介绍的理想流体伯努里方程来研究流场的速度分布。

普朗特边界层理论开辟了用理想流体理论和黏性流体理论联合研究的一条新途径。

image: http://howthingsfly.si.edu/;

8.1 边界层的概念 – 层流边界层与紊流边界层

按流动状态,流体可分为层流和紊流。



判别边界层层流、紊流的准则数:

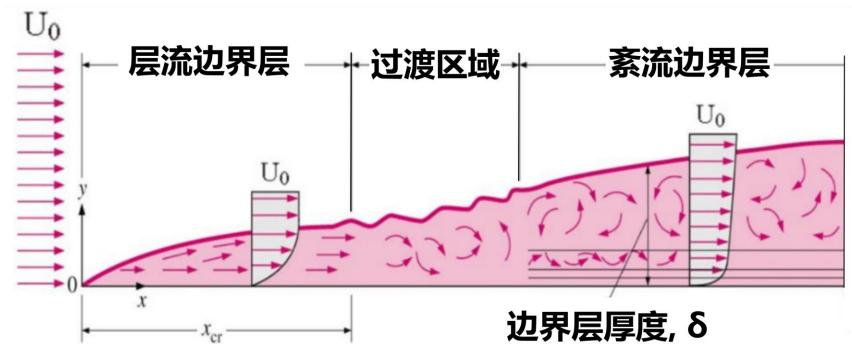
$$Re_x = \frac{V_{\infty}x}{v}$$
 x - 离物体前缘点的距离

平板上的临界雷诺数

$$Re = 3 \times 10^5 \sim 10^6$$

8.1 边界层的概念 – 层流边界层与紊流边界层

按流动状态,流体可分为层流和紊流。

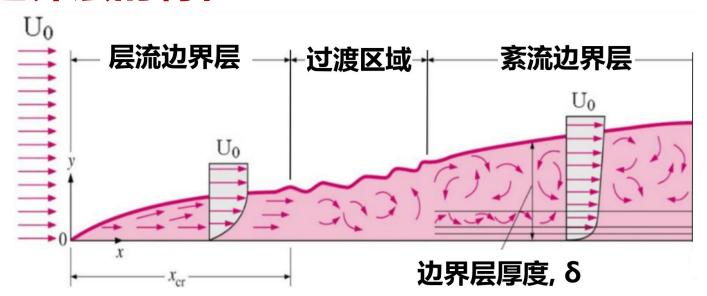


边界层的分类:

- 1. 层流边界层, 当Re较小时, 边界层内全为层流, 称为层流边界层;
- 2. <mark>混合边界层</mark>,除前部起始部分有一小片层流区,其余大部分为紊流区,称为混合边界层;
- 3. <u>紊流边界层,当Re较大时,边界层内全为紊流,称为紊流边界层</u>;

image: https://www.nuclear-power.net/;

8.1 边界层的概念 – 边界层的特征

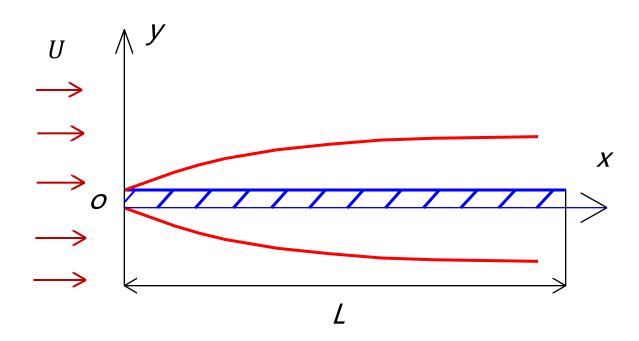


边界层的特征:

- (1) 与物体的长度相比, 边界层的厚度很小;
- (2) 边界层内沿边界层厚度的速度变化非常急剧,即速度梯度很大;
- (3) 边界层沿着流体流动的方向逐渐增厚;
- (4) 边界层中各截面上的压强等于同一截面上边界层外边界上的压强;
- (5) 在边界层内粘滞力和惯性力是同一数量级的;
- (6) 边界层内流体的流动存在层流和紊流两种流动状态。

- 根据六条特征,通过数量级比较,对N-S方程进行简化

例:为简单起见,设流体沿平壁作二维不可压定常流动,假定边界层内为层流,并不考虑质量力:



流体沿平壁作二维不可压定常流动模型

不可压缩粘性流动的NS方程 (假设:层流、定常、忽略质量力、二维流动)

$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} = \int_{x} -\frac{1}{\rho} \frac{\partial p}{\partial x} + v \left(\frac{\partial^{2} u}{\partial x^{2}} + \frac{\partial^{2} u}{\partial y^{2}} + \frac{\partial^{2} u}{\partial z^{2}} \right)$$

$$\frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z} = f_y - \frac{1}{\rho} \frac{\partial p}{\partial y} + v \left(\frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} + \frac{\partial^2 v}{\partial z^2} \right)$$

$$\frac{\partial w}{\partial t} + u \frac{\partial w}{\partial x} + v \frac{\partial w}{\partial y} + w \frac{\partial w}{\partial z} = f_y - \frac{1}{\rho} \frac{\partial p}{\partial z} + v \left(\frac{\partial^2 w}{\partial x^2} + \frac{\partial^2 w}{\partial y^2} + \frac{\partial^2 w}{\partial z^2} \right)$$

忽略质量力

不可压缩粘性流动的NS方程(假设:层流、定常、忽略质量力、二维流动):

$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} = \int_{x} -\frac{1}{\rho} \frac{\partial p}{\partial x} + v \left(\frac{\partial^{2} u}{\partial x^{2}} + \frac{\partial^{2} u}{\partial y^{2}} + \frac{\partial^{2} u}{\partial z^{2}} \right)$$

$$\frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z} = f_y - \frac{1}{\rho} \frac{\partial p}{\partial y} + v \left(\frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} + \frac{\partial^2 v}{\partial z^2} \right)$$

$$\left. \frac{\partial w}{\partial t} + u \frac{\partial w}{\partial x} + v \frac{\partial w}{\partial y} + w \frac{\partial w}{\partial z} = f_y - \frac{1}{\rho} \frac{\partial p}{\partial z} + v \left(\frac{\partial^2 w}{\partial x^2} + \frac{\partial^2 w}{\partial y^2} + \frac{\partial^2 w}{\partial z^2} \right) \right\}$$

问题: 上述N-S 方程仍然无法直接求解, 怎么办?

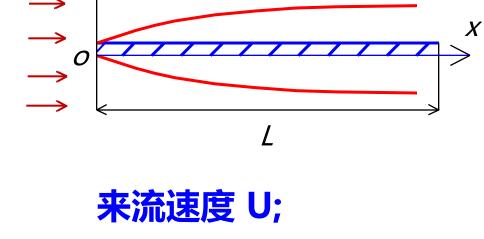
思路: 量纲分析

(1) N-S方程化简为如下形式:

$$u\frac{\partial u}{\partial x} + v\frac{\partial u}{\partial y} = -\frac{1}{\rho}\frac{\partial p}{\partial x} + v\left(\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2}\right)$$

$$u\frac{\partial v}{\partial x} + v\frac{\partial v}{\partial y} = -\frac{1}{\rho}\frac{\partial p}{\partial y} + v\left(\frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2}\right)$$

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0$$



平板前缘至某点距离 L

边界层厚度 δ;

边界条件:

$$y = 0,$$
 $u = v = 0$
 $y = \delta,$ $u = U$

(2) 量纲分析

特征量选择: 特征速度 U; 特征长度 L;

$$\left(\begin{array}{ccc}
u\frac{\partial u}{\partial x} + | & v\frac{\partial u}{\partial y} = - & \left|\frac{1}{\rho}\frac{\partial p}{\partial x} + & \right|v\left(\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2}\right) \\
\left(\begin{array}{ccc}
u\frac{\partial v}{\partial x} + | & v\frac{\partial v}{\partial y} = - & \left|\frac{1}{\rho}\frac{\partial p}{\partial y} + & \left|v\left(\frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2}\right)\right| \\
\frac{\partial u}{\partial x} + & \left|\frac{\partial v}{\partial y} = 0
\right.
\right)$$
(8-2)

(2) 量纲分析

特征量选择:特征速度 U;特征长度 L;

$$\left(\frac{u}{\mathbf{U}}\right)\frac{\partial(u/\mathbf{U})}{\partial(x/\mathbf{L})} + \left(\frac{v}{\mathbf{U}}\right)\frac{\partial(u/\mathbf{U})}{\partial(y/\mathbf{L})} = -\frac{\partial\left(\frac{p}{\rho\mathbf{U}^{2}}\right)}{\partial(x/\mathbf{L})} + \left(\frac{v}{\mathbf{U}\mathbf{L}}\right)\left(\frac{\partial^{2}(u/\mathbf{U})}{\partial(x/\mathbf{L})^{2}} + \frac{\partial^{2}(u/\mathbf{U})}{\partial(y/\mathbf{L})^{2}}\right) \\
\left(\frac{u}{\mathbf{U}}\right)\frac{\partial(v/\mathbf{U})}{\partial(x/\mathbf{L})} + \left(\frac{v}{\mathbf{U}}\right)\frac{\partial(v/\mathbf{U})}{\partial(y/\mathbf{L})} = -\frac{\partial\left(\frac{p}{\rho\mathbf{U}^{2}}\right)}{\partial(y/\mathbf{L})} + \left(\frac{v}{\mathbf{U}\mathbf{L}}\right)\left(\frac{\partial^{2}(u/\mathbf{U})}{\partial(x/\mathbf{L})^{2}} + \frac{\partial^{2}(u/\mathbf{U})}{\partial(y/\mathbf{L})^{2}}\right) \\
\frac{\partial(u/\mathbf{U})}{\partial(x/\mathbf{L})} + \frac{\partial(v/\mathbf{U})}{\partial(y/\mathbf{L})} = 0$$
(8-3)

带入公式 (7-3) 得到:

(2) 量纲分析

$$u^* \frac{\partial u^*}{\partial x^*} + v^* \frac{\partial u^*}{\partial y^*} = -\frac{\partial p^*}{\partial x^*} + \frac{1}{Re_L} \left(\frac{\partial^2 u^*}{\partial x^{*2}} + \frac{\partial^2 u^*}{\partial y^{*2}} \right)$$

$$u^* \frac{\partial v^*}{\partial x^*} + v^* \frac{\partial v^*}{\partial y^*} = -\frac{\partial p^*}{\partial y^*} + \frac{1}{Re_L} \left(\frac{\partial^2 v^*}{\partial x^{*2}} + \frac{\partial^2 v^*}{\partial y^{*2}} \right)$$

$$\frac{\partial u^*}{\partial x^*} + \frac{\partial v^*}{\partial y^*} = 0$$

$$(8-4)$$

$$0 \le y \ll \delta \implies y \sim \delta \implies \frac{y}{L} \sim \frac{\delta}{L} \implies y^* \sim \delta^*$$

$$0 \le x \ll L \implies x \sim L \implies \frac{x}{L} \sim 1 \implies x^* \sim 1$$

$$0 \le u \ll U \implies u \sim U \implies \frac{u}{U} \sim 1 \implies u^* \sim 1$$

$$0 \le u \ll U \implies u \sim U \implies \frac{u}{U} \sim 1 \implies u^* \sim 1$$

(2) 量纲分析

$$u^* \frac{\partial u^*}{\partial x^*} + v^* \frac{\partial u^*}{\partial y^*} = -\frac{\partial p^*}{\partial x^*} + \frac{1}{Re_L} \left(\frac{\partial^2 u^*}{\partial x^{*2}} + \frac{\partial^2 u^*}{\partial y^{*2}} \right)$$

$$u^* \frac{\partial v^*}{\partial x^*} + v^* \frac{\partial v^*}{\partial y^*} = -\frac{\partial p^*}{\partial y^*} + \frac{1}{Re_L} \left(\frac{\partial^2 v^*}{\partial x^{*2}} + \frac{\partial^2 v^*}{\partial y^{*2}} \right)$$

$$\frac{\partial u^*}{\partial x^*} + \frac{\partial v^*}{\partial y^*} = 0$$

$$(8-4)$$

由连续性方程得:
$$\frac{\partial u^*}{\partial x^*} = -\frac{\partial v^*}{\partial y^*} \sim 1$$
 且 $y^* \sim \delta^*$ \longrightarrow $v^* \sim \delta^*$

将上述量级分析,带入公式(7-4):

(2) 量纲分析

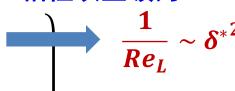
$$u^* \frac{\partial u^*}{\partial x^*} + v^* \frac{\partial u^*}{\partial y^*} = -\frac{\partial p^*}{\partial x^*} + \frac{1}{Re_L} \left(\frac{\partial^2 u^*}{\partial x^{*2}} + \frac{\partial^2 u^*}{\partial^2 y^{*2}} \right) \xrightarrow{\text{All 2-30 as } 30.5} \frac{1}{Re_L} \sim \delta^{*2}$$

$$1 \cdot 1 \quad \delta^* \cdot \frac{1}{\delta^*}$$

$$u^* \frac{\partial v^*}{\partial x^*} + v^* \frac{\partial v^*}{\partial y^*} = -\frac{\partial p^*}{\partial y^*} + \frac{1}{Re_L} \left(\frac{\partial^2 y^*}{\partial x^{*2}} + \frac{\partial^2 v^*}{\partial y^{*2}} \right)$$
(8-5) 略去高阶小项

$$\mathbf{1} \cdot \boldsymbol{\delta}^* \quad \boldsymbol{\delta}^* \cdot \mathbf{1}$$

$$oldsymbol{\delta}^* \qquad rac{\mathbf{1}}{oldsymbol{\delta}^*}$$



$$\frac{\partial u^*}{\partial x^*} + \frac{\partial v^*}{\partial y^*} = 0$$

(3) 得到普朗克边界层方程

$$u\frac{\partial u}{\partial x} + v\frac{\partial u}{\partial y} = -\frac{1}{\rho}\frac{\partial p}{\partial x} + v\frac{\partial^{2} u}{\partial y^{2}}$$

$$\frac{\partial p}{\partial y} = 0$$

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0$$

$$(8-7)$$

边界条件为:

$$y = 0,$$
 $u = v = 0$
 $y = \delta,$ $u = U$

(4) 补充说明

$$u\frac{\partial u}{\partial x} + v\frac{\partial u}{\partial y} = -\frac{1}{\rho}\frac{\partial p}{\partial x} + v\frac{\partial^{2} u}{\partial y^{2}}$$

$$\frac{\partial p}{\partial y} = 0$$

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0$$

$$(8-7)$$

$$\frac{\partial p}{\partial v} = 0$$
 说明: 1. p 只是 x 的函数,即 $\frac{\partial p}{\partial x} = \frac{dp}{dx}$

2. 延抛物面法线方向,边界层内压强不变,等于边界层界处势流压强。

根据理想流体势流伯努利方程:
$$\frac{p}{\rho} + \frac{1}{2}U^2 = C$$

两边对x求导数:
$$-\frac{1}{\rho}\frac{dp}{dx} = U\frac{dU}{dx}$$
 (8-8a)

根据牛顿切应力公式:
$$v \frac{\partial^2 u}{\partial y^2} = \frac{1}{\rho} \frac{d\tau}{dy}$$
 (8-8b)

将公式(8-8a),(8-8b)带入公式 (8-7) 得:

$$u\frac{\partial u}{\partial x} + v\frac{\partial u}{\partial y} = U\frac{dU}{dx} + \frac{1}{\rho}\frac{d\tau}{dy}$$

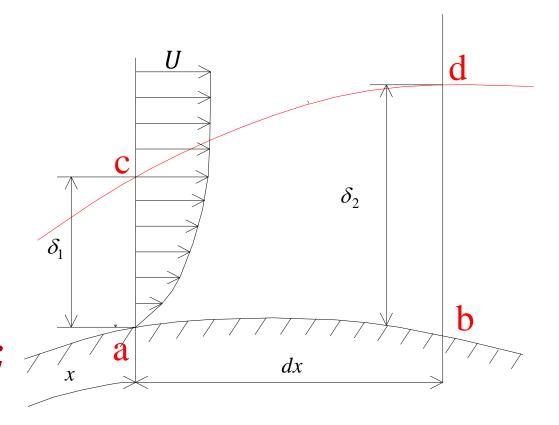
$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0$$
(8-8c)

(8-8c)是普朗克边界层方程的另一表达形式。

下面我们讨论卡门边界动量积分关系式,求解扰流阻力计算问题

- (1) 沿边界层取微小控制体,建立质量、动量传递关系;
 - (2) 建立微小控制体的受力方程;

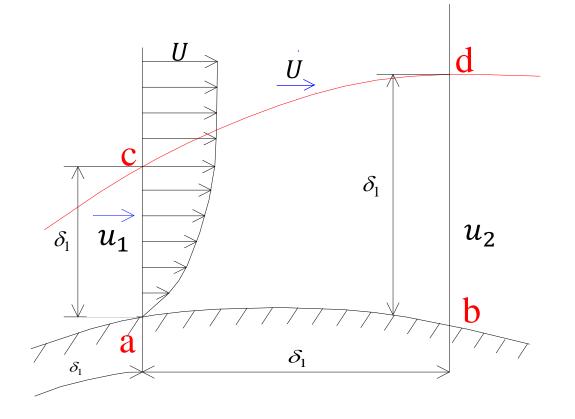
(3) 建立动量变化与应力间关系;



(1) 控制体内的质量、动量传递

ac面流入的动量流率: $\dot{K}_{ac} = \int_{0}^{\delta_1} \rho u_1^2 dy$ 质量流率: $\dot{m}_{ac} = \int_{0}^{\delta_1} \rho u_1 dy$

bc面流出的动量流率: $\dot{K}_{bd} = \int_{0}^{\delta_2} \rho u_2^2 dy$ 质量流率: $\dot{m}_{bd} = \int_{0}^{\delta_2} \rho u_2 dy$



根据质量守恒*cd*面流入的质量流率:

$$\dot{m}_{cd} = \dot{m}_{bd} - \dot{m}_{ac} = \int_{0}^{\delta_{2}} \rho u_{2} dy - \int_{0}^{\delta_{1}} \rho u_{1} dy$$

cd面流入的动量流率:

$$\dot{K}_{cd} = U\left(\int_0^{\delta_2} \rho u_2 dy - \int_0^{\delta_1} \rho u_1 dy\right)$$

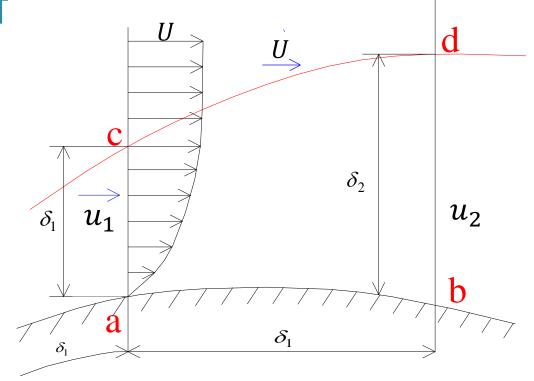
(1) 控制体内的质量、动量传递

单位时间沿x方向经控制面的净动量流率:

$$\Delta \dot{K} = \dot{K}_{bd} - \dot{K}_{ac} - \dot{K}_{cd}$$

$$= \int_0^{\delta_2} \rho u_2^2 dy - \int_0^{\delta_1} \rho u_1^2 dy - U\left(\int_0^{\delta_2} \rho u_2 dy - \int_0^{\delta_1} \rho u_1 dy\right)$$

$$= \rho U^{2} \left\{ \int_{0}^{\delta_{2}} \left[\left(\frac{u_{2}}{U} \right)^{2} - \frac{u_{2}}{U} \right] dy - \int_{0}^{\delta_{1}} \left[\left(\frac{u_{1}}{U} \right)^{2} - \frac{u_{1}}{U} \right] dy \right\}$$
 (8-13)



(2) 控制体受应力

ac面上的总压力: $P_{ac} = p\delta_1$

$$bd$$
面上的总压力: $P_{bd} = \left(p + \frac{dp}{dx}dx\right)\delta_2$

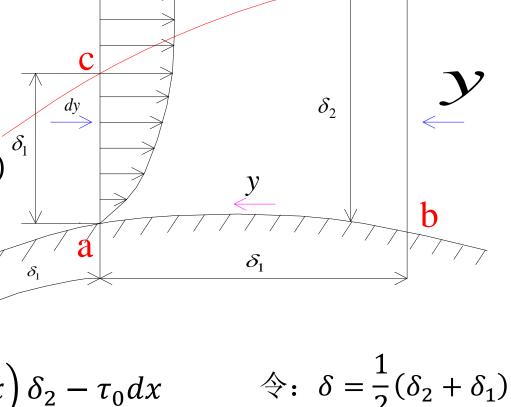
co面上的总压力:
$$P_{cd} = \left(p + \frac{1}{2}\frac{dp}{dx}dx\right)\left(\delta_2 - \delta_1\right)^{\delta_1}$$

ab面上的切应力: $F_{ab} = -\tau_0 dx$

延x方向受到的合力:

$$p\delta_1 + \left(p + \frac{1}{2}\frac{dp}{dx}dx\right)(\delta_2 - \delta_1) - \left(p + \frac{dp}{dx}dx\right)\delta_2 - \tau_0 dx$$

$$= -\frac{1}{2}(\delta_2 + \delta_1)\frac{dp}{dx}dx - \tau_0 dx = -\delta\frac{dp}{dx}dx - \tau_0 dx \quad (7-18)$$



(3) 建立动量变化与应力间关系

根据动量定理得:

$$\delta \frac{dp}{dx} dx + \tau_0 dx = \rho U^2 \left\{ \int_0^{\delta_2} \left[\frac{u_2}{U} - \left(\frac{u_2}{U} \right)^2 \right] dy - \int_0^{\delta_1} \left[\frac{u_1}{U} - \left(\frac{u_1}{U} \right)^2 \right] dy \right\}$$

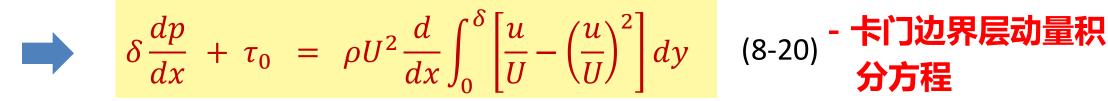
$$\Rightarrow : \quad f_1 = \int_0^{\delta_1} \left[\frac{u_1}{U} - \left(\frac{u_1}{U} \right)^2 \right] dy$$

$$f_2 = \int_0^{\delta_2} \left[\frac{u_2}{U} - \left(\frac{u_2}{U} \right)^2 \right] dy$$

$$dx \rightarrow 0$$



$$df \rightarrow f_2 - f_1$$



注: 因对流动特性和切应力无假设, 层流和湍流都适用

平板层流边界层的近似计算

$$\delta \frac{dy}{dx} + \tau_0 = \rho U^2 \frac{d}{dx} \int_0^{\delta} \left[\frac{u}{U} - \left(\frac{u}{U} \right)^2 \right] dy$$

由于边界层很薄,对势流区影响小, 因此假设:

$$U(x) \approx U_{\infty}$$



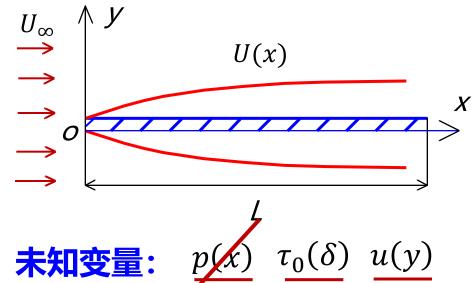
$$\frac{p}{\rho} + \frac{1}{2}U^2 = C$$



边界层外边界压强 p为常数

$$\frac{dp}{dx} = 0$$

$$\tau_0 = \rho U^2 \frac{d}{dx} \int_0^\delta \left[\frac{u}{U} - \left(\frac{u}{U} \right)^2 \right] dy \qquad (8-1)$$



平板层流边界层的近似计算

$$\tau_0 = \rho U^2 \frac{d}{dx} \int_0^{\delta} \left[\frac{u}{U} - \left(\frac{u}{U} \right)^2 \right] dy$$
 未知变量: $\tau_0(\delta)$ $u(y)$

采用幂级数分解u(y), 进而获得边界层内速度分布:

根据边界条件:

$$y = 0, u = 0$$
 $a_0 = 0$



$$a_0 = 0$$

$$y = \delta$$
, $u = U_{\infty}$



$$y = \delta$$
, $u = U_{\infty}$ $U = a_1 \delta + a_2 \delta^2$

$$y = \delta, \frac{du}{dy} = 0 \qquad \qquad 0 = a_1 + 2a_2\delta$$



$$0 = a_1 + 2a_2\delta$$

$$a_2 =$$

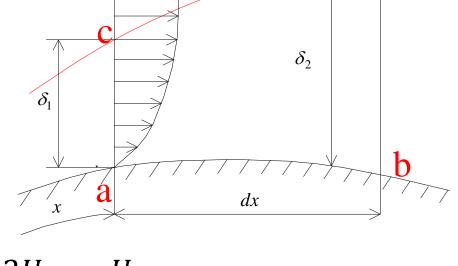
$$a_2 = -\frac{U}{\delta^2}$$

$$a_1 = \frac{20}{\delta}$$



 $u(y) = a_0 + a_1 y + a_2 y^2$

$$a_2 = -\frac{U}{\delta^2} \qquad a_1 = \frac{2U}{\delta} \qquad \qquad u(y) = \frac{2U}{\delta}y - \frac{U}{\delta^2}y^2$$
 (8-22)



平板层流边界层的近似计算

$$\tau_0 = \rho U^2 \frac{d}{dx} \int_0^{\delta} \left[\frac{u}{U} - \left(\frac{u}{U} \right)^2 \right] dy \quad (8-20) \quad 未知变量: \quad \tau_0(\delta) \quad u(y)$$

$$u(y) = \frac{2U}{\delta}y - \frac{U}{\delta^2}y^2 \quad (7-22)$$

根据牛顿内摩擦定律获得

$$au_0(\delta)$$

$$\tau_0 = \mu \left(\frac{du}{dy}\right)_{y=0} = \mu \left[\frac{2U}{\delta} - \frac{2U}{\delta^2}y\right]_{y=0} = \frac{2\mu U}{\delta}$$
(8-23)

将公式(8-22)(8-23)带入(8-20):



$$\delta^2 = \frac{30\nu}{II}x + C$$

考虑边界条件:
$$x = 0, \delta = 0$$
 因此C=0



计算平板扰流的摩擦阻力:

$$\delta = \sqrt{\frac{30\nu}{U}x} = 5.48 \ xRe_x^{-\frac{1}{2}}$$
 (8-24)

首先计算切应力:__

$$\tau_0 = \frac{2\mu U}{\delta} = \sqrt{\frac{2\mu\rho U^3}{15x}} = 0.365\rho U^2 \sqrt{\frac{\nu}{Ux}} = 0.365\rho U^2 Re_x^{-\frac{1}{2}}$$
 (8-25)

延平板积分,获取总摩擦力,平板宽度b,长度L

$$F_{D} = b \int_{0}^{L} \tau_{0} dx = \int_{0}^{L} 0.365 \rho U^{2} \sqrt{\frac{\nu}{Ux}} dx = 0.73 b L \rho U^{2} \sqrt{\frac{\nu}{UL}} = 0.73 b L \rho U^{2} Re_{L}^{-\frac{1}{2}}$$
(8-26)

定义阻力系数 C_D , 其中A为边界层物面的总面积

$$C_D = \frac{F_D}{\frac{1}{2}\rho U^2 A}$$

 $C_D = \frac{F_D}{\frac{1}{2}\rho U^2 A}$ 带入(8-26),平板扰流的 摩擦阻力系数为:

$$C_D = 1.46 Re_L^{-\frac{1}{2}}$$
 (8-28)



近似解与精确解对比:

$$C_D = 1.46 Re_L^{-\frac{1}{2}}$$
 (8-28)

$$C_D = 1.33 Re_L^{-\frac{1}{2}}$$
 (8-28)

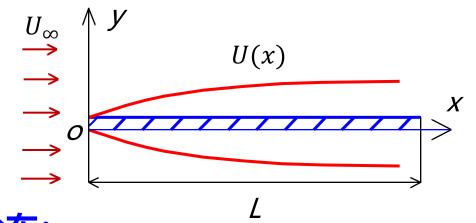
请大家思考误差产生的原因,这一误差是否可以接受? 如何进一步减少这个误差?

边界层内速度分布假设: $u(y) = a_0 + a_1 y + a_2 y^2$

我们还做了哪些假设?

平板紊流边界层的近似计算:

$$\tau_0 = \rho U^2 \frac{d}{dx} \int_0^{\delta} \left[\frac{u}{U} - \left(\frac{u}{U} \right)^2 \right] dy \quad (8-21)$$



采用管内紊流流动规律,描述平板紊流速度分布:

$$\frac{u}{U} = \left(\frac{y}{\delta}\right)^{\frac{1}{7}}$$

$$(8-29)$$

采用施利希廷半经验公式, 描述切应力:

$$\tau_0 = 0.0225 \rho U^2 \left(\frac{\nu}{U\delta}\right)^{\frac{1}{4}} \tag{8-30}$$

将(8-29)(8-30)带入公式(8-21):

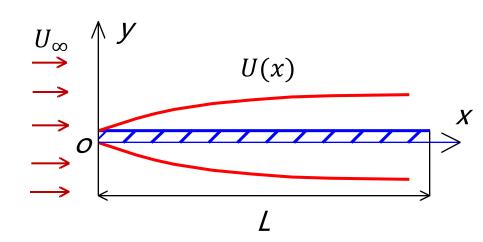
$$0.0225 \left(\frac{v}{U\delta}\right)^{\frac{1}{4}} = \frac{d}{dx} \int_{0}^{\delta} \left(\frac{y}{\delta}\right)^{\frac{1}{7}} \left[1 - \left(\frac{y}{\delta}\right)^{\frac{1}{7}}\right] dy$$





平板紊流边界层的近似计算:

$$0.0225 \left(\frac{\nu}{U\delta}\right)^{\frac{1}{4}} = \frac{7}{72} \frac{d\delta}{dx} \xrightarrow{\longrightarrow} 0$$



积分得到边界层厚度:
$$\delta = 0.37 \left(\frac{\nu}{U}\right)^{\frac{1}{5}} x^{\frac{4}{5}} + C$$

考虑边界条件:

$$x = 0, \delta = 0$$
 $C = 0$



$$C = 0$$

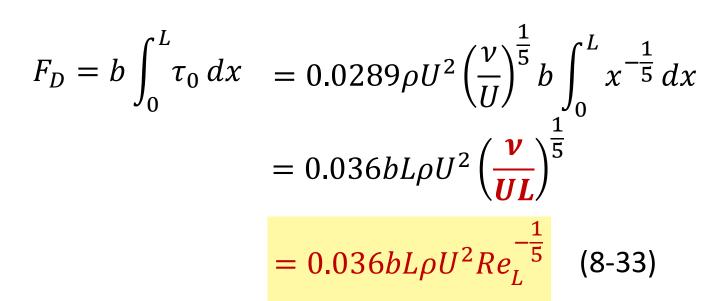
$$\delta = 0.37 \left(\frac{\nu}{U}\right)^{\frac{1}{5}} x^{\frac{4}{5}} = 0.37 x Re_x^{-\frac{1}{5}}$$
 (8-31)

将(8-31)代入(8-30):

$$\tau_0 = 0.0289 \rho U^2 \left(\frac{\nu}{U\delta}\right)^{\frac{1}{5}} = 0.0289 \rho U^2 R e_{\chi}^{-\frac{1}{5}}$$
 (8-32)

平板紊流边界层的近似计算:

总摩擦阻力:



摩擦阻力系数:

$$C_D = \frac{F_D}{\frac{1}{2}\rho U^2 bL} = 0.072 Re_L^{-\frac{1}{5}}$$
 (8-34a)

公式适用范围: $5 \times 10^5 \le \text{Re}_L \le 10^7$

U(x)

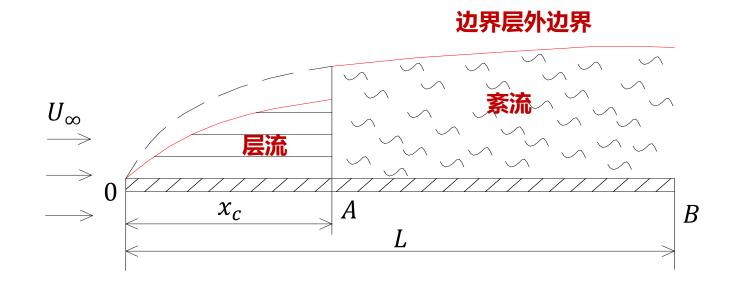
平板的层流、紊流边界层近似计算的比较:

- (1) <mark>速度分布规律</mark>:紊流边界层内沿平板壁面法向截面上的速度比层流边界层的速度增加得快;
- (2) <mark>边界层厚度</mark>:沿平板壁面紊流边界层的厚度比层流边界层得厚度增长得快;
- (3) <mark>切向应力:在其他条件相同的情况下,平板壁面上紊流边界层中的切向应力沿着壁面的减小要比层流边界层中的减小慢些;</mark>
- (4) <mark>摩擦阻力系数</mark>:在同一雷诺数下,紊流边界层的摩擦阻力系数 比层流边界层的大得多。

平板的混合边界层的近似计算

两个假设:

- (1) 在平板的A点层流边界层突然转变为紊流边界层;
- (2) 紊流边界层的厚度变化、层内速度和切向应力的分布都从前缘点O开始计算。

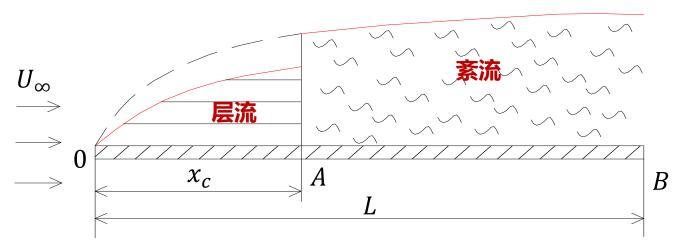


混合边界层的<mark>总摩擦阻力</mark>为层流边界层摩擦阻力与紊流边界层摩擦阻力之和:

$$F_{DM} = F_{DT} \Big|_{0 \le x \le L} - F_{DT} \Big|_{0 \le x \le x_c} + F_{DL} \Big|_{0 \le x \le x_c}$$
 (7-37)

其中: F_{DM} 代表混合边界层的总摩擦力, F_{DL} 表示层流边界层的总摩擦力, F_{DT} 代表紊流边界层的总摩擦阻力。

边界层外边界



如前所述,当不可压缩黏性流体纵向流过平板时,在边界层外部势流沿平板方向的速度是相同的,而且整个流场和边界层内的压强都保持不变。当黏性流体流经曲面物体时,边界层外边界上沿曲面方向的速度是改变的,所以曲面边界层内的压强也将同样发生变化,对边界层内的流动将产生影响。

这一节将着重说明曲面边界层的分离现象

小结

本节课我们讨论如下内容:

- (1) 边界层的概念;
- (2) 通过量纲分析、边界层理论化简N-S方程;
- (3) 绕平板流动的近似计算;

Thanks!

感谢关注 敬请指导