Multibody Dynamics B - Assignment 9

July 4, 2019

Short problem statement

In this assignment we are concerned with the rotary motion of a torque-free satellite in deep space, which results in no gravity force and no drag. We will determine the rotation matrix for a z-x-z rotation and use that to determine coordinates and angular velocities in both the inertial and body frame and Euler angles and their rate of change. Furthermore, we will determine the motion of the satellite for 60 seconds, through numerical integration using the Runge-Kutta 4th order, and look at how the Euler angles and angular velocities will change, both in the inertial and body frame.

0.1 a) Rotation matrix R

Now we want to determine the rotation matrix at t=0 which transforms the body fixed frame coordinates Bx into the space fixed frame coordinates Nx as in ${}^Nx = {}^NR_B{}^Bx$. The body fixed coordinate base vectors as expressed in the state space frame are given as ${}^Ne_x = e_x' = (0.768, 0.024, 0.640)$, ${}^Ne_y = e_y' = (-0.424, 0.768, 0.480)$ and ${}^Ne_z = e_z' = (-0.480, -0.640, 0.600)$. Now we also know that the space fixed coordinate base vectors for the global system in x-y-z are

$$e_x = \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} \quad e_y = \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix} \quad e_x = \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}$$

Now we can write the position vector in terms of both the state space frame and the body-fixed frame as in

$$\mathbf{p} = p_1 e_1 + p_2 e_2 + p_3 e_3$$

$$\mathbf{p} = p_1' e_1' + p_2' e_2' + p_3' e_3'$$

Now it is important to note that for a rigid body these coordinates are constant. Now if we want to keep track of the position of point P in the inertial frame from the body-fixed frame positions we take the expression of the inertial-frame coordinates and substitute for vector \mathbf{p} the expression in terms of the body-fixed components, this means

$$p_i = (p_1'e_1' + p_2'e_2' + p_3'e_3')\mathbf{e}_i$$
 $i = 1..3$

which we can write as

$$p_i = (\mathbf{e}_i \mathbf{e}'_j) p'_j$$
 $i, j = 1...3$

where $\mathbf{e}_i \mathbf{e}_j$ is the linear transformation which maps the coordinates of point P in terms of the body-fixed frame into the coordinates expressed in the initially fixed frame. This transformation matrix, $\mathbf{e}_i \mathbf{e}_j$, is the rotation matrix $^N \mathbf{R}_B$, so we have

$$p = Rp'$$

where

$$R = e_i e'_j$$

$$= \begin{bmatrix} e_x & e_y & e_x \end{bmatrix}^T \begin{bmatrix} e'_x & e'_y & e'_x \end{bmatrix}$$

$$= \begin{bmatrix} 0.7680 & -0.4240 & -0.4800 \\ 0.0240 & 0.7680 & -0.6400 \\ 0.6400 & 0.4800 & 0.6000 \end{bmatrix}$$

0.2 b) Euler angles

Now we determine the associated Euler angles (z-x-z) ϕ , θ and ψ at t=0 from the rotation matrix found in section **a**). Now for a z-x-z rotation we have the following rotation matrices, which follow 1.) Rotation about z-axis by an angle ϕ 2.) Rotation about x-axis by an angle θ 3.) Rotation about z-axis by an angle ψ

$$R_{\phi} = \begin{bmatrix} \cos(\phi) & -\sin(\phi) & 0 \\ \sin(\phi) & \cos(\phi) & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$R_{\theta} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos(\theta) & -\sin(\theta) \\ 0 & \sin(\theta) & \cos(\theta) \end{bmatrix}$$

$$R_{\psi} = \begin{bmatrix} \cos(\psi) & -\sin(\psi) & 0 \\ \sin(\psi) & \cos(\psi) & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

Now the rotation matrix for the Euler angles is the product of the three elementary rotation matrices in the following order

$$\begin{split} R &= R_{\phi} R_{\theta} R_{\psi} \\ &= \begin{bmatrix} \cos(\phi) \cos(\psi) - \cos(\theta) \sin(\phi) \sin(\psi) & -\cos(\phi) \sin(\psi) - \cos(\psi) \cos(\theta) \sin(\phi) & \sin(\phi) \sin(\theta) \\ \cos(\psi) \sin(\phi) + \cos(\phi) \cos(\theta) \sin(\psi) & \cos(\phi) \cos(\psi) \cos(\theta) - \sin(\phi) \sin(\psi) & -\cos(\phi) \sin(\theta) \\ \sin(\psi) \sin(\theta) & \cos(\psi) \sin(\theta) & \cos(\psi) \sin(\theta) \end{bmatrix} \end{split}$$

Now we compare this rotation matrix to that which we found in section 0.1 and find the appropriate Euler angles. This gives us:

$$\begin{split} \theta &= cos^{-1}(R_{3,3}) = acos(0.6) = 0.9273 rad \\ \phi &= sin^{-1}(\frac{R_{1,3}}{sin(\theta)}) = sin^{-1}(\frac{0.48}{sin(0.9273)}) = -0.6435 rad \\ \psi &= sin^{-1}(\frac{R_{3,1}}{sin(\theta)}) = sin^{-1}(\frac{0.64}{sin(0.9273)}) = 0.9273 rad \end{split}$$

0.3 c) Angular velocities

Now we determine the angular velocities at t=0 in the body fixed frame. We are given the angular velocities in the state space frame at t=0, they are ${}^{N}\omega=(7.67952,0.23936,6.40060)$ rad/s. We use equation 19.60 in the book which tells us that we can use the rotation matrix ${}^{B}\mathbf{R}_{N}$, where ${}^{B}\mathbf{R}_{N}=({}^{N}\mathbf{R}_{B})^{-1}$, to transform the angular velocities in the state space frame to the body-fixed frame, so we have

$${}^{B}\omega = {}^{B}\mathbf{R}_{N}{}^{N}\omega$$
$$= \begin{bmatrix} 10\\0\\0.001 \end{bmatrix}$$

0.4 d) Rate of change of the Euler angles

Now we determine the rate of change of the Euler angles $(\dot{\phi}, \dot{\theta}, \dot{\psi})$ at t = 0. Now this can be determined using equation 19.61 in the book which tells us that

$$\begin{split} {}^{B}\boldsymbol{\omega} &= {}^{N}\boldsymbol{\omega}_{\psi} + {}^{B}\mathbf{R}_{\psi}{}^{B}\boldsymbol{\omega}_{\theta} + {}^{B}\mathbf{R}_{\psi}{}^{B}\boldsymbol{\kappa}_{\theta}{}^{B}\boldsymbol{\omega}_{\phi} \\ &= \begin{bmatrix} 0 \\ 0 \\ \dot{\psi} \end{bmatrix} + {}^{B}\mathbf{R}_{\psi}{}^{\begin{bmatrix} \dot{\theta} \\ 0 \\ 0 \end{bmatrix}} + {}^{B}\mathbf{R}_{\psi}{}^{B}\mathbf{R}_{\theta}{}^{\begin{bmatrix} 0 \\ 0 \\ \dot{\phi} \end{bmatrix}} \\ \begin{bmatrix} \boldsymbol{\omega}_{x}' \\ \boldsymbol{\omega}_{y}' \\ \boldsymbol{\omega}_{z}' \end{bmatrix} &= \begin{bmatrix} sin(\psi)sin(\theta) & cos(\psi) & 0 \\ cos(\psi)sin(\theta) - sin(\psi) & 0 \\ cos(\theta) & 0 & 1 \end{bmatrix} \begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix} \end{split}$$

So rearranging this equation, i.e. we multiply the inverse of the matrix through the equation, we get

$$\begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix} = \frac{1}{\sin(\theta)} \begin{bmatrix} \sin(\psi) & \cos(\psi) & 0 \\ \cos(\psi)\sin(\theta) & -\sin(\psi)\sin(\theta) & 0 \\ -\sin(\psi)\cos(\theta) & -\cos(\psi)\cos(\theta) & \sin(\theta) \end{bmatrix} \begin{bmatrix} \omega_x' \\ \omega_y' \\ \omega_z' \end{bmatrix} = \begin{bmatrix} 10.0000 \\ 6.0000 \\ -5.9990 \end{bmatrix}$$

0.5 e) Mass moment of inertia

We determine the mass moment of inertia matrix ${}^{B}\mathbf{I}_{C}$ at the CoM in the body fixed frame, where the satelite is modeled as a rectangular box with mass m=60 kg, and dimensions $l_{x}=0.4$, $l_{y}=1.2$ and $l_{z}=0.3$ in the body fixed frame. We align the the principal axes of the body such that we get a diagonal mass moment of inertia, i.e. such that the object is symmetric around its principal axes. Furthermore we know that moment of inertia around the CoM of a object is

 $1/12mL^2$. Now we use the form of equation 18.28 in the book and get:

$$I_{xx} = \frac{1}{12}m(l_y^2 + l_z^2) = 7.6500kgm^2$$

$$I_{yy} = \frac{1}{12}m(l_x^2 + l_z^2) = 1.2500kgm^2$$

$$I_{zz} = \frac{1}{12}m(l_x^2 + l_y^2) = 8.000kgm^2$$

$$^B\mathbf{I}_C = \begin{bmatrix} I_{xx} & 0 & 0\\ 0 & I_{yy} & 0\\ 0 & 0 & I_{zz} \end{bmatrix}$$

0.6 f) Euler equations of motion and state equations

Now we write down the Euler equations of motion for the rigid body and the state equations $= \mathbf{f}(\mathbf{y})$ where the state variables \mathbf{y} are the Euler angles and the angular velocities expressed in the body fixed frame. So we have

$$\mathbf{y} = \begin{bmatrix} \phi \\ \theta \\ \psi \\ \omega_x' \\ \omega_y' \\ \omega_z' \end{bmatrix}$$

Now the Euler equations of motion are, equation 19.66 in the book,

$$\sum_{B} {}^{B}M_{C} = {}^{B}\mathbf{I}_{C} {}^{B}\dot{\omega} + {}^{B}\omega \times ({}^{B}\mathbf{I}_{C} {}^{B}\omega)$$

By rearranging the equation we can solve for angular accelerations,

$${}^{B}\dot{\omega} = ({}^{B}\mathbf{I}_{C})^{-1} \left(\sum {}^{B}M_{C} - {}^{B}\omega \times ({}^{B}\mathbf{I}_{C}{}^{B}\omega) \right) \tag{1}$$

Now since the satellite is in deep space and no gravity nor drag is exerted on the body the external moment applied on the body is zero, i.e. $M_C = 0$ so we have

$${}^{B}\dot{\omega} = ({}^{B}\mathbf{I}_{C})^{-1}{}^{B}\omega \times ({}^{B}\mathbf{I}_{C}{}^{B}\omega)$$

Furthermore we can find the Euler angles as depicted in section 0.4. Thus the state equations are

$$\begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix} = \frac{1}{\sin(\theta)} \begin{bmatrix} \sin(\psi) & \cos(\psi) & 0 \\ \cos(\psi)\sin(\theta) & -\sin(\psi)\sin(\theta) & 0 \\ -\sin(\psi)\cos(\theta) & -\cos(\psi)\cos(\theta) & \sin(\theta) \end{bmatrix} \begin{bmatrix} \omega_x' \\ \omega_y' \\ \omega_z' \end{bmatrix}$$

$$\begin{bmatrix} \dot{\omega}_x' \\ \dot{\omega}_y' \\ \dot{\omega}_z' \end{bmatrix} = \begin{bmatrix} \frac{I_{yy}\omega_y'\omega_z' - I_{zz}\omega_x'\omega_z'}{I_{xx}} \\ -\frac{I_{xx}\omega_x'\omega_z' - I_{zz}\omega_x'\omega_z'}{I_{yy}} \\ \frac{I_{yy}}{I_{zz}} \end{bmatrix}$$

0.7 g) Motion of the satellite

Now we determine the motion of the satellite as a function of time by numerical integration of the state equations for 60 seconds. We plot the Euler angles as a function of time and the angular velocities expressed in the body fixed frame as a function of time.

The numerical integration method that we use is the Runge-Kutta 4th order method which follows the scheme

$$k_1 = f(t_n, y_n)$$

$$k_2 = f(t_n + h/2, y_n + h/2 * k_1)$$

$$k_3 = f f(t_n + h/2, y_n + h/2 * k_2)$$

$$k_4 = f f(t_n + h, y_n + h * k_3)$$

$$y_{n+1} = y_n + \frac{h}{6}(k_1 + 2k_2 + 2k_3 + k_4)$$

This method is used over 60 seconds with a time step of $h = 9.1553 * 10^{-4}$, the Matlab code for the numerical integration can be found in appendix A. Now the plots for the Euler angles and angular velocities can be seen in figures 1a and 1b.

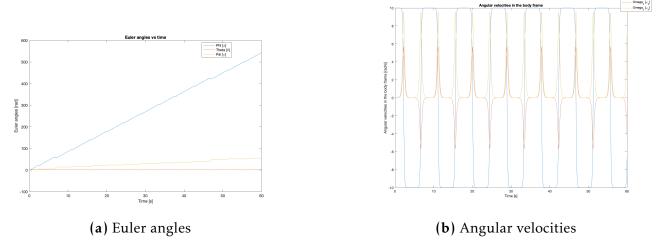


Figure 1: Euler angles and angular velocities expressed in the body fixed frame as a function of time.

We have a closer look at each of the angles and angular velocities in separate graphs in figure 2 below.

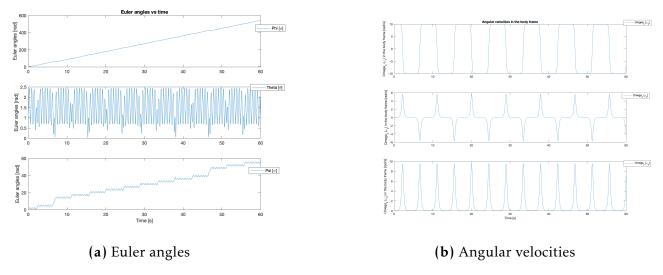


Figure 2: Euler angles and angular velocities expressed in the body fixed frame as a function of time.

What we observe is that ϕ is constant and increases with time, meaning a constant increase in spinning around the z axis expressed in the body fixed frame. Furthermore we observe that θ wiggles around the 1.5 rad constantly however we observe that there are some disturbances periodically, about every 5 seconds. This wiggle in θ seems to affect the ψ angle as it also wiggles, we also observe the same disturbances, which results in a jump in the angle ψ . Now looking at the angular velocities, nothing special happens, we notice that they are periodic which is what we expect since there is no external force so nothing should disturb the angular velocities of the body, i.e. no acceleration of the total system is happening, they only shift with the rotation of the body, since the system has a constant velocity. Moreover, we see that when the ω_x decreases ω_y and ω_z increase and the same can be observed when ω_x increases then ω_y and ω_z decrease where ω_y and ω_z are in phase, this is expected since the body has a constant velocity. We should note that it is strange that there are disturbances about every 5 seconds.

0.8 h) Trajectory of a point p

We plot the Euler angles θ and ψ separately from ϕ to look better at what is happening at the disturbances. Furthermore, we plot the 3D trajectory of a point $p = (l_x/2, 0, 0)$ on the satellite through the span of 60 seconds.

Now we plot only the θ and ψ as a function of time, this can be seen in figure 3 below.

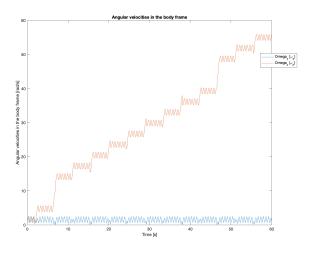


Figure 3: Euler angles θ and ψ as functions of time.

We notice that the wiggle in θ definitely seems to affect ψ , furthermore we notice that the disturbances are synced up. Looking further into this we notice that this happens when the angle is close to $\theta = 0 + k\pi$. Now if we look at the state equations we notice that what happens is that when $\theta = 0 + k\pi$, $sin(\theta) = 0$ the matrix

$$B = \frac{1}{\sin(\theta)} \begin{bmatrix} \sin(\psi) & \cos(\psi) & 0\\ \cos(\psi)\sin(\theta) & -\sin(\psi)\sin(\theta) & 0\\ -\sin(\psi)\cos(\theta) & -\cos(\psi)\cos(\theta) & \sin(\theta) \end{bmatrix}$$

is singular so we are unable to determine the time derivatives of the Euler angles from the angular speeds. This singular configuration is usually called 'gimbal lock. What happens is actually that we can not determine what $\dot{\phi}$ and $\dot{\psi}$ are as they are both rotating around the z-axis. We could avoid this by redefining the rotational matrix such that it rotates around each axis, like z-x-y rotations.

Now we also look at the trajectory of the point p on the satellite during the time-span of 60 seconds, this can be seen in figure 4 below.

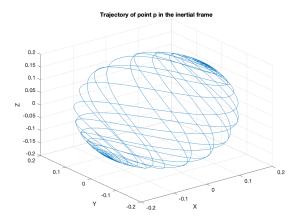


Figure 4: 3D trajectory of a point p on the satellite over a time-span of 60 seconds.

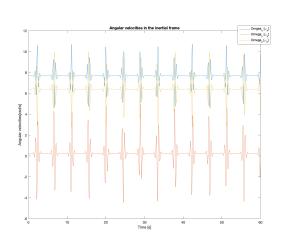
What we notice is that the trajectory resembles that of a sort of ellipsoid around the origin. What we also notice is that the satellite starts with small circles, than moves into a sort of bigger circles, which result in a sort of half-helix, which again moves into smaller circles. The satellite also moves according to how big the circles at the 'ends' are, when they are small, like in the beginning, the satellite moves farther in the y and z direction but when the end circles are bigger they move closer to the origin, less deviation in the y and z direction.

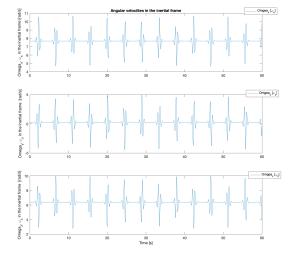
0.9 i) Angular velocities in the space fixes frame and angular momentum

We plot the three components of the angular velocities expressed in the space fixed frame as a function of time and the angular momentum in the space fixed frame as a function of time. Now the angular velocities in the inertial frame can be calculated from the rotation matrix and the angular velocities in the body fixed frame from the equation

$${}^{N}\omega = {}^{N}\mathbf{R}_{B}{}^{B}\omega$$

Now we have the rotation matrix, which can be seen in section 0.2 and the angular velocities in the body frame and the Euler angles at each time-step, like can be seen in section 0.7. This allows us to calculate the angular velocities in the state space frame for each time-step, using the equation above. These angular velocities can be seen in figure 5.





(a) Angular velocities together

(b) Angular velocities separately

Figure 5: Angular velocities in the state space frame as a function of time.

Looking at the angular velocities in the state space frame we see that they make sense. We notice that the angular velocities are completely out of phase as in ω_x is completely out of phase from ω_y and ω_z , which makes sense since there is no external force acting on the system and so the angular velocities should stay the same. It is also what you would expect that ω_z follows the phase of ω_y since it is affected by it' rotation, and this is in line with what we saw in section 0.7, where the angular velocities in the body frame for ω_y and ω_z were working in phase and reacting to how the ω_x behaved, similarly to what can be seen here.

Now angular momentum expressed in the state space frame can be found by finding the angular momentum in the body frame and pre-multiplying that with the rotation matrix found in section 0.2. This can be described in equation form as

$${}^{N}\mathbf{H}_{C} = {}^{N}\mathbf{R}_{B}{}^{B}\mathbf{I}_{C}{}^{B}\omega$$

where the rotation matrix and the angular velocities in the body frame are taking for each timestep. The angular momentum vector **H** expressed in the space fixed frame as a function of time can be seen in figure 6 below.

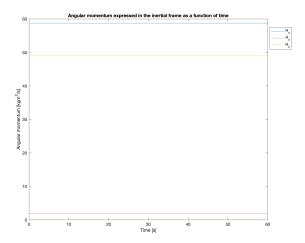


Figure 6: Angular momentum as a function of time.

This is what we expected since there is no external force, as there is no gravity and no drag, and thus no external momentum is applied and thus the momentum should be in the same direction and have the same value through the whole time-span of 60 seconds, actually the momentum should be same for any time-span as long as there is no external force applied.

0.10 i) Invariants

Now we determine three invariants which we can use to check our result.

The three invariants that I found were angular momentum, distance between 2 points on the object and the kinetic energy of the system, since there is no external force and thus the velocity is constant. First the angular momentum can be seen in figure 6 above, and obviously it can be seen that the angular momentum does not change with time.

Now we can look at the distance between two points on the satellite, this can be seen in figure 7 below.

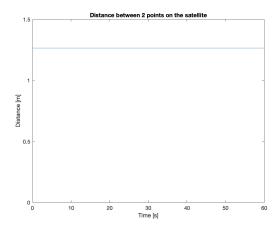


Figure 7: Distance between two points on the satellite as a function of time.

Like we can see the distance between two points on the satellite does not change, which is what we expected, this should of course always be true, since if this was not the case the object would be ripping apart or some other non-expected situations.

Now the kinetic energy of the system can be calculated as

$$T = \frac{1}{2} {}^{B} \omega^{T B} \mathbf{I}_{C} {}^{B} \omega$$

where we take ${}^{B}\omega$ for each time-step. Now we look at the kinetic energy of the system as a function of time in figure 8 below.

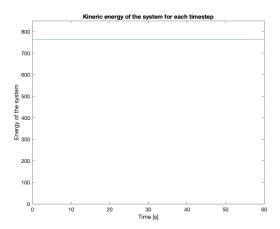


Figure 8: Kinetic energy of the system as a function of time.

We can see that the kinetic energy of the system is invariant of time. This is expected since there are no external forces acting on the system and thus the velocity never changes, since there is no acceleration, and thus the kinetic energy is the same at all times. We should note that if we look carefully at the kinetic energy it is not completely invariant, the same can be said about the angular momentum, due to the singularity problem we described in 0.8, i.e. there are small disturbances in the calculations due to θ being close to $0 + k\pi$. However these disturbances affect the momentum and energy so little that it can't be seen unless you look at decimal places at 10^{-6} for our step size in the numerical integration.

Appendix A

Matlab code

```
1 %% a) Find Rotation Matrix from the body to the inertial frame nRb
2 % Body frame
a = bx = [0.768; 0.024; 0.640];
4 \text{ e\_by} = [-0.424; 0.768; 0.480];
5 e_bz = [-0.480; -0.640; 0.600];
e_b = [e_bx, e_by, e_bz];
8 % Inertial frame
9 e x = [1;0;0];
10 e_y = [0;1;0];
11 e_z = [0;0;1];
12 e = [e_x, e_y, e_z];
13
14 % Rotation matrix from body to inertial frame
15 R = e*e_b;
17 %% b) Determine the Euler angles (z-x-z)
18 syms phi theta psi
19 ang = [phi; theta; psi];
21 % Find first the rotation marixes about z-x-z axes, i.e. phi, theta and psi,
22 % individually
23
24 R_phi = [\cos(phi) - \sin(phi)] % Same rotation matrix as in 19.26 ...
    in the book
         sin(phi) cos(phi) 0;
          0 0 1];
26
27
28 R_{theta} = [1 0 0;
                                           % Same rotation matrix as in 19.28 ...
    in the book
            0 cos(theta) -sin(theta);
29
             0 sin(theta) cos(theta)];
30
R_psi = [cos(psi) - sin(psi) 0;
                                    % Same rotation matrix as in 19.30 ...
     in the book
          sin(psi) cos(psi) 0;
33
34
          0 0 1];
35
37 % The final rotation matrix
39  R_Eul = R_phi*R_theta*R_psi;
40
41 matlabFunction(R_Eul, 'File', 'Rhw9');
42
43 % Now we find the value of the angles
45 theta = acos(R(3,3));
46 phi = asin(R(1,3)/sin(theta));
  psi = asin(R(3,1)/sin(theta));
48
```

```
49 Eul = [phi;theta;psi];
   %% c) Finding the angular velocities in the body frame
51
52
  % Angular velocities in the inertia frame at t=0
  w0_i = [7.67952; 0.23936; 6.40060];
55
  % Calculate angular velocities in body frame, using equation 19.60
   w0 b = inv(R) * w0 i;
57
59
   %% d) Find the rate of change of Euler angles
   % we use equation 19.70 to determine the rate of change
   B = [\sin(psi) * \sin(theta) \cos(psi) 0;
62
       cos(psi)*sin(theta) -sin(psi) 0;
63
64
       cos(theta) 0 1];
  dEul = inv(B) *w0_b;
66
67
   %% e) Find the inertia matrix bIc in the body fixed frame.
68
70 \text{ m} = 60;
             % [kg]
71
1_x = 0.4;
              % [m]
               % [m]
1_y = 1.2;
1 z = 0.3;
               % [m]
75
  % Moment of inertia around the center of mass is 1/12*ml^2, and we use the
  % inertia matrix form in equation 18.28, i.e. we align the principal axes of
  % the body such that we get a diagonal mass moment of inertia, i.e. such
  % that the object is symmetric around its pricipal axes.
  bIx = 1/12*m*(1_y^2+1_z^2);
82 bly = 1/12*m*(1_x^2+1_z^2);
  bIz = 1/12*m*(1_x^2+1_y^2);
   bIc = diag([bIx bIy bIz]);
85
86
87
  %% f) Equation of motion
   syms bwx bwy bwz Ixx Iyy Izz
89
90
  wb = [bwx; bwy; bwz];
   I = diag([Ixx Iyy Izz]);
93
   dwb = inv(I) * (-cross(wb, (I*wb)));
   %% g) Numerical Integration with the Runge-Kutta 4th order method
97
  % setup
99 time=60;
100 nn=16;
101 N=2.^n;
102 h=time./N;
103
104 t= 0;
```

```
v_{105} y0 = [phi; theta; psi; w0_b];
   ang = [phi; theta; psi; w0_b];
   for j=1:N
107
       k1 = qa(y0);
108
       k2=qa(y0 + h/2*k1);
109
       k3=qa(y0 + h/2*k2);
110
111
       k4 = qa(y0 + h*k3);
       qn= y0+1/6*h*(k1+2*k2+2*k3+k4);
112
113
114
       y0 = qn;
       q_n(j,:) = qn;
115
116
       t = t+h;
        T(j)=t;
117
   end
118
119
120
   %% Plots
   q_plot = [ang'; q_n];
121
122
   T_plot = [0; T'];
123
   figure(1)
124
125 plot(T_plot,q_plot(:,1),T_plot,q_plot(:,2),T_plot,q_plot(:,3));
126 xlabel('Time [s]')
127 ylabel('Euler angles [rad]')
128 legend('Phi [\phi]', 'Theta [\theta]', 'Psi [\psi]')
   title('Euler angles vs time')
129
130
131
   figure(2)
132 plot(T_plot,q_plot(:,4),T_plot,q_plot(:,5),T_plot,q_plot(:,6));
133 xlabel('Time [s]')
134 ylabel('Angular velocities in the body frame [rad/s]')
135 legend('Omgea_x [\omega_x]', 'Omega_y [\omega_y]', 'Omega_z [\omega_z]')
   title ('Angular velocities in the body frame')
136
137
  figure(3)
138
139 subplot (311)
140 plot(T_plot, q_plot(:,1))
141 title('Euler angles vs time')
142 ylabel('Euler angles [rad]')
143
  legend('Phi [\phi]')
144
145 subplot (312)
146 plot(T_plot, q_plot(:, 2))
  vlabel('Euler angles [rad]')
   legend('Theta [\theta]')
149
   subplot (313)
150
   plot(T_plot,q_plot(:,3))
151
   ylabel('Euler angles [rad]')
  legend('Psi [\psi]')
   xlabel('Time [s]')
154
155
156 figure (4)
157 subplot (311)
158 plot (T_plot, q_plot (:, 4))
159 title('Angular velocities in the body frame')
160 ylabel('Omega_x (\omega_x) in the body frame [rad/s]')
```

```
legend('Omgea_x [\omega_x]')
161
162
   subplot (312)
163
   plot(T_plot, q_plot(:,5))
  ylabel('Omega_y (\omega_y) in the body frame [rad/s]')
   legend( 'Omega_y [\omega_y]')
167
   subplot (313)
  plot(T_plot, q_plot(:, 6))
169
   ylabel('Omega_z (\omega_z) in the body frame [rad/s]')
   legend('Omega_z [\omega_z]')
171
   xlabel('Time [s]')
173
  figure (9)
174
plot (T_plot, q_plot (:, 2), T_plot, q_plot (:, 3))
176 xlabel('Time [s]')
177 ylabel('Angular velocities in the body frame [rad/s]')
178 legend('Omega_y [\omega_y]', 'Omega_z [\omega_z]')
179 title('Angular velocities in the body frame')
  %% h) 3D trajectory of point p
180
   p = [(1_x)/2;0;0];
181
182
   p_I = R_Euler(p,q_plot(:,1:3));
183
184
   figure(5)
185
186 plot3(p_I(:,1),p_I(:,2),p_I(:,3))
  grid on
188 xlabel('X')
   ylabel('Y')
   zlabel('Z')
190
   title('Trajectory of point p in the inertial frame')
191
192
   %% i) plot the angular velocities in the inertial frame
193
194
   w_i = R_Euler_vel(q_plot);
195
196
  figure(6)
197
  plot(T_plot, w_i(:,1), T_plot, w_i(:,2), T_plot, w_i(:,3))
  title('Angular velocities in the inertial frame')
199
   ylabel('Angular velocities[rad/s]')
200
   xlabel('Time [s]')
201
   legend('Omgea_x [\omega_x]', 'Omega_y [\omega_y]', 'Omega_z [\omega_z]')
203
204
205
  figure(7)
   subplot (311)
206
  plot (T_plot, w_i(:,1))
207
   title('Angular velocities in the inertial frame')
   ylabel('Omega_x, \omega_x in the inertial frame [rad/s]')
   legend('Omgea_x [\omega_x]')
210
211
212 subplot (312)
213 plot(T_plot, w_i(:,2))
214 ylabel('Omega_y, \omega_y in the inertial frame [rad/s]')
   legend('Omgea_y [\omega_y]')
215
216
```

```
217 subplot (313)
218 plot(T_plot, w_i(:, 3))
219 ylabel('Omega_z, \omega_z in the inertial frame [rad/s]')
220 legend('Omgea_z [\omega_z]')
221 xlabel('Time [s]')
222
   %% i) Angular momentum vector in the inertial frame
223
224
   momentum_i = R_Euler_mom(q_plot);
225
226
   figure(8)
227
  plot(T_plot, momentum_i(:,1), T_plot, momentum_i(:,2), T_plot, momentum_i(:,3))
229 ylabel('Angular momentum [kgm^2/s]')
230 xlabel('Time [s]')
231 title('Angular momentum expressed in the inertial frame as a function of time')
232
  legend('H_x', 'H_y', 'H_z')
233
   %% j) Invariants
234
235
   % distance between two points on the satellite.
236
p1 = [0; 1_y; 0];
  p2 = [1_x; 0; 0];
238
239
240 P_1 = R_Euler(p1, q_plot(:, 1:3));
   P_2 = R_Euler(p2, q_plot(:, 1:3));
241
242
   for i = 1:length(T_plot)
244
       dist(i,:) = norm(P_1(i,:)-P_2(i,:));
   end
245
246
  figure(10)
247
248 plot(T_plot,dist)
249 ylabel('Distance [m]')
250 xlabel('Time [s]')
251 title('Distance between 2 points on the satellite')
   yaxis([0 1.5])
252
253
   %% Kinetic energy of the system
254
255
   T = R_Euler_KE(q_plot);
256
257
  figure(11)
258
259 plot(T_plot,T)
260 xlabel('Time [s]')
261 ylabel('Energy of the system')
  title('Kineric energy of the system for each timestep')
   %yaxis([0 850])
263
   %% Functions
265
266
267 function state_d = qa(y)
_{268} phi = y(1);
_{269} theta = y(2);
psi = y(3);
271
272 \text{ wb} = y(4:6);
```

```
273
   % Find the rate of change in angular velocities
274
275 \text{ m} = 60; % [kg]
276
   1_x = 0.4;
277
                 % [m]
   l_y = 1.2;
                 % [m]
278
   1_z = 0.3;
                % [m]
279
280
281
   bIx = 1/12*m*(l_y^2+l_z^2);
282
   bly = 1/12*m*(1_x^2+1_z^2);
283
   bIz = 1/12*m*(l_x^2+l_y^2);
284
285
   bIc = diag([bIx bIy bIz]);
286
287
288
   dwb = inv(bIc) * (-cross(wb, (bIc*wb)));
289
290
   % Find the rate of change for Euler angles
   B = [\sin(psi) * \sin(theta) \cos(psi) 0;
291
        cos(psi) *sin(theta) -sin(psi) 0;
292
        cos(theta) 0 1];
293
294
   dEul = inv(B) *wb;
295
296
   state_d = [dEul;dwb];
297
   end
298
299
300
301
   function position = R_Euler(p, angles)
302
303
   for i = 1:length(angles)
304
305
        phi = angles(i,1);
        theta = angles(i,2);
306
        psi = angles(i,3);
307
308
        R_Eul = Rhw9(phi, psi, theta);
309
310
311
        position(i,:) = R_Eul*p;
   end
312
313
314
   end
315
316
   function angvel = R_Euler_vel(angles)
317
   for i = 1:length(angles)
318
        phi = angles(i,1);
319
        theta = angles(i,2);
320
        psi = angles(i,3);
321
322
        wx = angles(i, 4);
323
        wy = angles(i, 5);
324
        wz = angles(i, 6);
325
326
        wb = [wx; wy; wz];
327
328
```

```
329
        R_Eul = Rhw9(phi, psi, theta);
330
        angvel(i,:) = R_Eul*wb;
331
332
   end
333
   end
334
335
    function momentum = R_Euler_mom(angles)
336
337
   m = 60;
                % [kg]
338
339
340
   1_x = 0.4;
                 % [m]
   1_y = 1.2;
                 % [m]
341
   1_z = 0.3;
                 % [m]
342
343
344
   bIx = 1/12*m*(l_y^2+l_z^2);
345
346
   bly = 1/12*m*(l_x^2+l_z^2);
   blz = 1/12*m*(1_x^2+1_y^2);
347
348
   bIc = diag([bIx bIy bIz]);
349
350
351
352
   for i = 1:length(angles)
        phi = angles(i,1);
353
        theta = angles(i, 2);
354
        psi = angles(i,3);
355
356
357
        wx = angles(i, 4);
        wy = angles(i, 5);
358
        wz = angles(i, 6);
359
360
361
        wb = [wx; wy; wz];
362
        R_Eul = Rhw9(phi, psi, theta);
363
364
        momentum(i,:) = R_Eul*blc*wb;
365
366
    end
367
   end
368
369
    function kenergy = R_Euler_KE(angles)
370
371
372
   m = 60;
                % [kg]
373
   1_x = 0.4;
374
                 % [m]
   l_y = 1.2;
                 % [m]
375
   1_z = 0.3;
                 % [m]
376
377
378
   bIx = 1/12*m*(l_y^2+l_z^2);
379
   bly = 1/12*m*(1_x^2+1_z^2);
380
   blz = 1/12*m*(1_x^2+1_y^2);
381
382
   bIc = diag([bIx bIy bIz]);
383
384
```

```
|385 for i = 1:length(angles)
386
        wx = angles(i, 4);
387
        wy = angles(i,5);
388
        wz = angles(i, 6);
389
390
        wb = [wx; wy; wz];
391
392
393
        kenergy(i,:) = wb'*bIc*wb;
394
   end
395
396
   end
```