Your PRINTED FULL NAME

SOLUTIONS

Your STUDENT ID NUMBER

Number of additional sheets

- 1. No computers, no tablets, no connected device (phone etc.)
- 2. Pocket calculator allowed
- 3. Closed book, closed notes, closed internet
- 4. Allowed: 1 page (double sided) Chi Chi
- 5. Additional sheets are available and may be submitted (e.g. for graphs).
- 6. Write your name below, and your SID on the top right corner of every page (including this one).
- 7. If you turn in additional sheets:
 - Write your name and/or SID on every sheet, and
 - Write the number of additional sheets you are turning in above where indicated
- 8. Do not write on the back of any page.

Part	1	2	3	4
Score	9	9 + 2	22	10 + 2

1. Laplace Transforms

(a) (4pts) Use Laplace transform tables to derive the Laplace transform for the following time function

$$e^{-at}\sin(wt)\cos(wt)$$

Answer:
$$\frac{w}{(s+a)^2 + 4w^2}$$

Using the trigonometric properties

$$e^{-at}\sin(wt)\cos(wt) = \frac{1}{2}e^{-at}\sin(2wt)$$
 (1pt)

Using the frequency shift property and table of laplace transforms

$$e^{-at}f(s) = f(s+a)$$
 (1pt)

$$\sin(2wt) = \frac{2w}{s^2 + 4w^2} \quad (1\mathbf{pt})$$

Combining the two we get,

$$\frac{1}{2}e^{-at}\sin(2wt) = \frac{1}{2}\frac{2w}{(s+a)^2 + (2w)^2}$$

$$=\frac{w}{(s+a)^2+4w^2} \quad (1\mathbf{pt})$$

(b) (5pt)Use Laplace transforms to solve the following ODE. Assume all forcing functions are zero prior to $t = 0^-$.

$$\frac{d^2x}{dt^2} = 4e^{-t}\cos\left(\frac{t}{2}\right)\sin\left(\frac{t}{2}\right)$$
$$x(0) = 2, \ x'(0) = 3$$

Answer: $4t + 1 + e^{-t}\cos(t)$

Taking the Laplace transform of the ODE then solving for X(s),

$$s^{2}X(s) - sx(0) - x'(0) = \frac{2}{(s+1)^{2} + 1}$$
 (1pt)

$$s^{2}X(s) = 2s + 3 + \frac{2}{(s+1)^{2} + 1}$$

$$= \frac{2s^{3} + 7s^{2} + 10s + 8}{s^{2} + 2s + 2}$$

$$X(s) = \frac{2s^{3} + 7s^{2} + 10s + 8}{s^{2}(s^{2} + 2s + 2)}$$
 (1pt)

Doing partial fraction decomposition we get,

$$X(s) = \frac{A}{s^2} + \frac{B}{s} + \frac{Cs + D}{s^2 + 2s + 2} \quad (\mathbf{1pt})$$
$$= \frac{(B+C)s^3 + (A+2B+D)s^2 + (2A+2B)s + 2A}{s^2(s^2 + 2s + 2)}$$

Solving for coefficients A,B,C,D (1pt)

$$A = \left| \frac{2s^3 + 7s^2 + 10s + 8}{s^2(s^2 + 2s + 2)} \right|_{s=0} = 8/2 = 4$$

$$(2A + 2B) = 10$$

$$B = \frac{10 - 2A}{2} = 1$$

$$B + C = 2$$

$$C = 1$$

$$A + 2B + D = 7$$

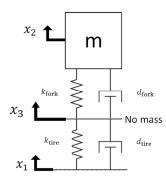
$$D = 1$$

Taking the laplace transform with the coefficients,

$$X(s) = \frac{4}{s^2} + \frac{1}{s} + \frac{s+1}{s^2 + 2s + 2}$$
$$= \frac{4}{s^2} + \frac{1}{s} + \frac{s+1}{(s+1)^2 + 1}$$
$$= 4t + 1 + e^{-t}\cos(t) \quad (1\mathbf{pt})$$

2. Consider a simplified model of a front mountain bike suspension. The input is the position $x_1(t)$ of the rocky terrain and the output is the position $x_2(t)$ of the person with mass m. The spring and damping constants are defined as seen below in the figure. Ignore the effect of gravity.





(a) (4pts)Derive the transfer function $T(s) = \frac{X_2(s)}{X_1(s)}$ in terms of $k_{\text{fork}}, k_{\text{tire}}, d_{\text{fork}}, d_{\text{tire}}$ Note T(s) is the transfer function from position x_1 to position x_2 , derive the transfer function accordingly.

Answer:
$$T(s) = \frac{(d_t s + k_t)(d_f s + k_f)}{ms^2[(d_f + d_t)s + k_f + k_t] + (d_f s + k_f)(d_t s + k_t)}$$

In order to solve this system we created a variable x_3 at the interface between the tire and fork

Writing the system of equations for the mass and at the tire fork interface we get,

for mass

$$m\ddot{x_2} + d_f\dot{x_2} + k_fx_2 = d_f\dot{x_3} + k_fx_3$$
 (1pt)

for the tire fork interface

$$(d_f + d_t)\dot{x_3} + (k_f + k_t)x_3 = k_f x_2 + d_f \dot{x_2} + k_t x_1 + d_t \dot{x_1}$$
 (1pt)

Converting to the Laplace domain

$$(ms^{2} + d_{f}s + k_{f})x_{2} = (d_{f}s + k_{f})x_{3}$$
$$[(d_{f} + d_{t})s + k_{t} + k_{f}]x_{3} = (k_{f} + d_{f}s)x_{2} + (k_{t} + d_{t}s)x_{1}$$
(1pt)

Using substitution,

$$T(s) = \frac{(d_t s + k_t)(d_f s + k_f)}{m s^2 [(d_f + d_t)s + k_f + k_t] + (d_f s + k_f)(d_t s + k_t)}$$
 (1pt)

(b) (2pts) Make the approximation $k_{\text{tire}} = \infty$ and $d_{\text{tire}} = 0$ and derive the new transfer function $T(s) = \frac{X_2(s)}{X_1(s)}$.

Hint: this is equivalent to ignoring the dynamics of the tire.

Answer:

$$T(s) = \frac{(d_f s + k_f)}{m s^2 + d_f s + k_f}$$

This is the same as asking for the transfer function from x_1 to x_3 (the fork tire interface) Using inspection or substituting

$$T(s) = \frac{(d_f s + k_f)}{m s^2 + d_f s + k_f} \quad (2pt)$$

(c) (3pt)Using the second order transfer function obtained from part (b) determine the settling time and percent overshoot for a step response given $k_{\text{fork}} = 200e3 \text{ N/m}$ $d_{\text{fork}} = 10e3 \text{ Ns/m}$ and m = 10 kg

Answer:

$$T_s = .008s$$
 and $\%OS = 98.9\%$

Since $k_f >> d_f$ we are able to make the second order approximations used previously in class

The second order approximation is as follows,

$$s^{2} + 2\xi w_{n}s + w_{n}^{2} = s^{2} + \frac{d_{f}}{m}s + \frac{k_{f}}{m} \quad (\mathbf{1pt})$$

$$w_{n} = \sqrt{20e3}$$

$$\xi = \frac{d_{f}}{2mw_{n}} = 3.535$$

$$T_{s} = \frac{4}{\xi w_{n}} \quad (\mathbf{1pt})$$

$$T_{s} = \frac{8m}{d_{f}} = \frac{8}{1000} = .008s$$

%OS = 0 system is heavily overdamped (1pt)

(d) (2pts) **BONUS:** Write the condition which makes the second order approximation used in part (c) valid.

The form for the second order transfer function used for making second order approximations is:

$$\frac{k}{s^2 + 2\xi w_n + w_n^2}$$

In the case of the simplified bike model the numerator is:

Thus if k is much greater than d, **2pts**

$$k + ds => k$$

3. Consider the following system:

$$\dot{x} = Ax + Bu \quad y = Cx \quad with \quad A = \begin{bmatrix} 0 & 1 \\ 3 & 2 \end{bmatrix} \quad B = \begin{bmatrix} 1 \\ 3 \end{bmatrix} \quad C = \begin{bmatrix} 0 & 1 \end{bmatrix} \quad x_0 = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$
 (1)

(a) (2pts) Compute the eigenvalues of A

Answer: 3,-1

To find the eigenvalues, solve the equation $det(\lambda I - A) = 0$ for all λ (1pt)

$$\begin{vmatrix} \lambda & -1 \\ -3 & \lambda - 2 \end{vmatrix} = 0$$
$$\lambda^2 - 2\lambda - 3 = 0$$
$$\lambda = 3, -1 \quad (\mathbf{1pt})$$

(b) (3pts) Compute the associated eigenvectors of A

Answer:
$$\begin{bmatrix} 1 \\ 3 \end{bmatrix} \begin{bmatrix} 1 \\ -1 \end{bmatrix}$$

Eigenvectors and eigenvalues satisfy the property $(A - \lambda_i I)v_i = 0$ (1pt)

For
$$\lambda_1 = 3$$
:
$$\begin{bmatrix} 3 & -1 \\ -3 & 3 - 2 \end{bmatrix} \begin{bmatrix} v_{11} \\ v_{12} \end{bmatrix} = 0$$

$$\begin{bmatrix} 3 & -1 \\ -3 & 1 \end{bmatrix} \begin{bmatrix} v_{11} \\ v_{12} \end{bmatrix} = 0$$

$$\begin{bmatrix} -1 & -1 \\ -3 & -1 - 2 \end{bmatrix} \begin{bmatrix} v_{21} \\ v_{22} \end{bmatrix} = 0$$

$$\begin{bmatrix} -1 & -1 \\ -3 & -3 \end{bmatrix} \begin{bmatrix} v_{21} \\ v_{22} \end{bmatrix} = 0$$

$$3v_{11} = v_{12}$$

$$v_1 = \begin{bmatrix} 1 \\ 3 \end{bmatrix} \quad (\mathbf{1pt})$$

$$v_2 = \begin{bmatrix} 1 \\ -1 \end{bmatrix} \quad (\mathbf{1pt})$$

(c) (2pts) Find the P and P^{-1} matrices and use them to diagonalize A

Answer:
$$P = \begin{bmatrix} 1 & 1 \\ 3 & -1 \end{bmatrix}$$
, $P^{-1} = \frac{1}{4} \begin{bmatrix} 1 & 1 \\ 3 & -1 \end{bmatrix}$, $D = \begin{bmatrix} 3 & 0 \\ 0 & -1 \end{bmatrix}$

P is constructed by combining the two eigenvectors

$$P = \left[\begin{array}{cc} 1 & 1 \\ 3 & -1 \end{array} \right]$$

Taking the inverse of P gives us

$$P^{-1} = \frac{1}{4} \begin{bmatrix} 1 & 1 \\ 3 & -1 \end{bmatrix} \quad (\mathbf{1pt})$$

The diagonalized $D = P^{-1}AP$

$$D = \frac{1}{4} \begin{bmatrix} 1 & 1 \\ 3 & -1 \end{bmatrix} \begin{bmatrix} 0 & 1 \\ 3 & 2 \end{bmatrix} \begin{bmatrix} 1 & 1 \\ 3 & -1 \end{bmatrix} = \begin{bmatrix} 3 & 0 \\ 0 & -1 \end{bmatrix} \quad (\mathbf{1pt})$$

(d) (3pts) Find e^{At}

Answer:
$$e^{At} = \frac{1}{4} \begin{bmatrix} e^{3t} + 3e^{-t} & e^{3t} - e^{-t} \\ 3e^{3t} - 3e^{-t} & 3e^{3t} + e^{-t} \end{bmatrix}$$

$$e^{At} = Pe^{Dt}P^{-1} \quad (\mathbf{1pt})$$

$$= \frac{1}{4} \begin{bmatrix} 1 & 1 \\ 3 & -1 \end{bmatrix} \begin{bmatrix} e^{3t} & 0 \\ 0 & e^{-t} \end{bmatrix} \begin{bmatrix} 1 & 1 \\ 3 & -1 \end{bmatrix} \quad (\mathbf{1pt})$$

$$= \frac{1}{4} \begin{bmatrix} e^{3t} + 3e^{-t} & e^{3t} - e^{-t} \\ 3e^{3t} - 3e^{-t} & 3e^{3t} + e^{-t} \end{bmatrix} \quad (\mathbf{1pt})$$

(e) (5pts)Compute the output y(t) for a unit step u(t). Use the results from part (d) to determine a soultion for x(t), then find y(t) Answer:

$$y(t) = -1 + e^{3t}$$

The general solution to a state space is,

$$x(t) = e^{At}x_0 + \int_0^t e^{A(t-\tau)}Bu(\tau)d\tau \quad (\mathbf{1pt})$$

Substituting in the initial condition and e^{At}

$$x(t) = \int_{0}^{t} \frac{1}{4} \begin{bmatrix} e^{3(t-\tau)} + 3e^{-(t-\tau)} & e^{3(t-\tau)} - e^{-(t-\tau)} \\ 3e^{3(t-\tau)} - 3e^{-(t-\tau)} & 3e^{3(t-\tau)} + e^{-(t-\tau)} \end{bmatrix} \begin{bmatrix} 1 \\ 3 \end{bmatrix} d\tau \quad (\mathbf{1pt})$$

$$= \int_{0}^{t} \frac{1}{4} \begin{bmatrix} 4e^{3(t-\tau)} \\ 12e^{3(t-\tau)} \end{bmatrix} d\tau$$

$$= \begin{bmatrix} -\frac{1}{3}e^{3(t-\tau)} \\ -e^{3(t-\tau)} \end{bmatrix}_{0}^{t}$$

$$= \begin{bmatrix} -\frac{1}{3} + \frac{1}{3}e^{3t} \\ -1 + e^{3t} \end{bmatrix} \quad (\mathbf{1pt})$$

$$y(t) = Cx(t) = \begin{bmatrix} 0 & 1 \end{bmatrix} \begin{bmatrix} -\frac{1}{3} + \frac{1}{3}e^{3t} \\ -1 + e^{3t} \end{bmatrix} \quad (\mathbf{1pt})$$

$$= -1 + e^{3t} \quad (\mathbf{1pt})$$

(f) (2pts) Given the matrices A,B, and C above determine the transfer function G(s) for the state space system. How do the poles of the transfer function compare to the eigenvalues found in part (a)? **Answer:** =

$$G(s) = \frac{3(s+1)}{s^2 - 2s - 3}$$

$$G(s) = C(sI - A)^{-1}B \quad (1pt)$$

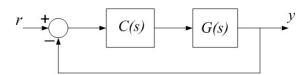
$$= \begin{bmatrix} 0 & 1 \end{bmatrix} \begin{bmatrix} s & -1 \\ -3 & s - 2 \end{bmatrix}^{-1} \begin{bmatrix} 1 \\ 3 \end{bmatrix}$$

$$= \frac{1}{s^2 - 2s - 3} \begin{bmatrix} 0 & 1 \end{bmatrix} \begin{bmatrix} s - 2 & 1 \\ 3 & s \end{bmatrix} \begin{bmatrix} 1 \\ 3 \end{bmatrix}$$

$$= \frac{1}{s^2 - 2s - 3} \begin{bmatrix} 0 & 1 \end{bmatrix} \begin{bmatrix} s + 1 \\ 3s + 3 \end{bmatrix}$$

$$= \frac{3(s+1)}{s^2 - 2s - 3} \quad (1pt)$$

(g) (3pts) Consider the following LTI system:



where
$$C(s) = \frac{K}{s+4}$$
 and $G(s) = \frac{3s+3}{s^2-2s-3}$

Determine for what values of K the system is stable and unstable.

Answer: Stable for K > 4 Unstable for K < 4

The closed loop transfer function was first found

$$T = \frac{CG}{1 + CG} = \frac{K(3s+3)}{s^3 + 2s^2 + (3k-11)s + (3k-12)}$$
 (1pt)

Writing out the Routh Hurwitz table

Since the signs of all the items in the first column need to be the same for the system to be stable,

$$\frac{3K - 10}{2} > 0 \implies K > -\frac{10}{3}$$
$$3K - 12 > 0 \implies K > 4$$

The range of K where both these constraints are satisfied is K > 4

(1pt)

(h) (2pts)What is the steady-state error of the closed-loop system for a unit step input u(t) as a function of K (for values of K that stabilize the system)?

Answer:

$$e_{ss}^{closed} = \frac{4}{4 - K}$$

The general equation for the closed loop steady state error is,

$$e_{ss}^{closed} = \frac{1}{1+K_p}(\mathbf{1pt})$$

where $K_p = \lim_{s \to \infty} G(s)$

$$K_p = -\frac{K}{4}$$

$$e_{ss}^{closed} = \frac{4}{4 - K} (\mathbf{1pt})$$

4. Consider the following LTI system:

$$G(s) = \frac{(s+2)}{(s+1)(s+1)(s+15)}$$
 (2)

Plot the root locus for the system

(a) (3pts) Determine the number of branches and any asymptotes (position and angle) that exist.

Answer:

$$Branches = 3$$
 $Asymptotes = 2$ center: -7.05 angle: $\frac{\pi}{2}, \frac{3\pi}{2}$

The number of branches is equal to the number of open loop poles, 3

The asymptotes can be determined by the following,

#of Asymptotes = #OLPoles - #OLZeros = 3 - 1 = 2 (1pt)
$$center = \frac{(-.1 - 1 - 15) - (-2)}{2} = -7.05$$

$$angle = \frac{(2k+1)\pi}{2} \text{ for } k = 0, 1 \implies angle = \frac{\pi}{2}, \frac{3\pi}{2} \text{ (1pt)}$$

(b) (3pts) How many break in/break away points are there? Be sure to determine the equation that governs the break away points, but note you do not need to explicity find the points.

$$\#breakaway points = 3$$
 $2\sigma^{3} + 22.1\sigma^{2} + 64.4\sigma + 31.7 = 0$

The breaks out can be determined by solving the following equation

$$\frac{dK}{d\sigma} = 0 \quad (1pt)$$

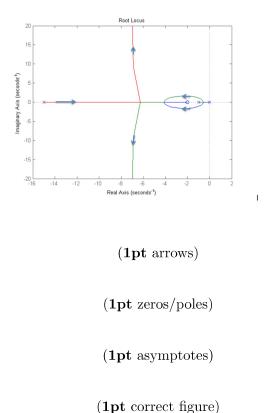
where K is defined as follows,

Answer:

$$K(\sigma) = -\frac{1}{G(\sigma)} = -\frac{(\sigma + .1)(\sigma + 1)(\sigma + 15)}{(\sigma + 2)} = -\frac{\sigma^3 + 16.1\sigma^2 + 16.6\sigma + 1.5}{(\sigma + 2)}$$
(1pt)
$$\frac{dK}{d\sigma} = \frac{2\sigma^3 + 22.1\sigma^2 + 64.4\sigma + 31.7}{(\sigma + 2)^2} = 0$$

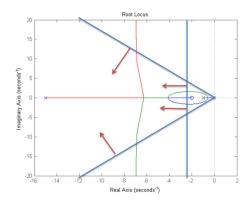
$$2\sigma^3 + 22.1\sigma^2 + 64.4\sigma + 31.7 = 0$$
(1pt)

(c) (4pts) Sketch the root locus. Make sure to label the asymptotes you found in part (a) and the direction of the root locus for increasing K (For ease of plotting assume the breakaways occur at -6,-4,and -.5). **Answer:**



All poles and zeros are located on the real axis. Note how the asymptotes centered at -7.05 affect the root locus. The direction of the root locus is away from the poles and towards the zeros for increasing K.

(d) (2pts) **BONUS:**Plot the feasible region for the poles if the design requirment is to have a minimum damping ratio of 0.5 and a settling time less than 1.6 seconds. (You may use the second order approximation for settling time). Given the region you drew, is it feasible to meet the design requirments (explain)? **Answer:** It is feasible to meet the design requirment!



The red arrows indicate the acceptable region to meet the design specs. Using the second order approximations,

 $\xi = \cos(\theta), \theta$ is the angle from the negative real axis

$$\theta = 60^{\circ}$$

$$T_s = \frac{4}{\xi w_n} = \frac{4}{Re(s)}$$

$$w_n = \frac{4}{\xi 1.6} = 5 \qquad Re(s) = 2.5$$

f(t)	F(s)
$\delta(t)$	1
u(t)	$\frac{1}{a}$
tu(t)	$\frac{s_1}{s^2}$.
$\int t^n u(t)$	$\frac{n!}{s^{n+1}}$
$\sin(\omega t)u(t)$	$\frac{\omega}{s^2+\omega^2}$
$\cos(\omega t)u(t)$	$\frac{s}{s^2 + \omega^2}$

Table 1: Laplace transforms of common functions

$$\begin{vmatrix}
\sin(2\theta) & 2\cos(\theta)\sin(\theta) \\
\cos(2\theta) & \cos(\theta)^2 - \sin(\theta)^2 \\
\tan(2\theta) & \frac{2\tan(\theta)}{1 - \tan(\theta)^2}
\end{vmatrix}$$

Table 2: Trigonometric functions