

# EECS 16B Midterm 2 Review Session

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Presented by <NAMES GO HERE >(HKN)

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# HKN Drop-In Tutoring

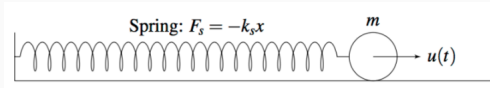
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# State-Space Representations

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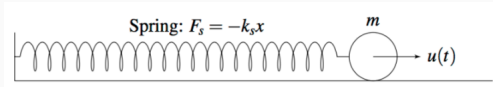
# State Space Modeling: Example

Assume we have the following spring system:



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We can model the system as a linear continuous time state space model:

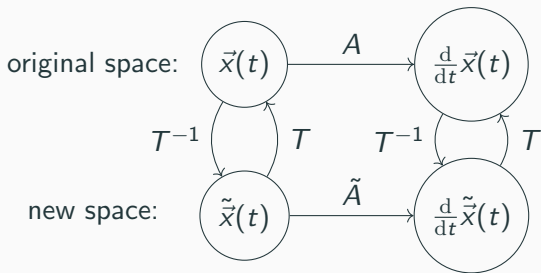
$$\frac{d}{dt}\vec{x}(t) = A\vec{x}(t) + \vec{b}u(t)$$

$$\vec{y}(t) = C\vec{x}(t)$$

in which:

$$\vec{x}(t) = \begin{bmatrix} x(t) \\ v(t) \end{bmatrix}, A = \begin{bmatrix} 0 & 1 \\ -\frac{k_s}{m} & 0 \end{bmatrix}, \vec{b} = \begin{bmatrix} 0 \\ 1 \end{bmatrix}, \text{ and } C = \begin{bmatrix} 0 & 1 \end{bmatrix}$$

# State Space Modeling:



Always apply operations to right side first

$$\tilde{A} = T^{-1}AT$$

$$\tilde{\vec{x}}(t) = T^{-1}\vec{x}(t)$$

## State Space Modeling Procedure:

1. Set up differential equation of the form:

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5. Solve  $\frac{d}{dt}\tilde{\vec{x}}(t) = \tilde{A}\tilde{\vec{x}}(t) + T\vec{b}u(t)$

6. Convert solution back to  $\vec{x}(t)$

# State Space Modeling:

Continuous time solution:

$$\tilde{x}(t) = e^{\lambda t} \tilde{x}(0) + \frac{e^{\lambda t} - 1}{\lambda} u(t) + w(t)$$

Discrete time solution:

$$x_d(i+1) = e^{\lambda \Delta} x_d(i) + \frac{e^{\lambda \Delta} - 1}{\lambda} u(i) + w(i)$$

# **Stability, Observability, and Controllability**

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## Stability, Observability, Controllability:

given:

$$\vec{x}(i+1) = A\vec{x}(i) + Bu(i)$$

$$\vec{y}(i) = C\vec{x}(i)$$

in which:

$\vec{x}$  is our state,

$\vec{u}$  is our input,

$\vec{y}$  is what we can observe:



## Stability (Discrete time):

Discrete time model:

if  $|\lambda_i| < 1$  for all  $\lambda_i$  of  $A$ , system is stable

intuition: if any  $|\lambda_i| \geq 1$ , state vector is increasing each time step  
will be infinitely magnified over time

## Stability (Continuous time):

Continuous time model:

if the  $\text{Re}\{\lambda_i\} < 0$  for all  $\lambda_i$  of  $A$  are strictly negative, system is stable

intuition: if real part of eigenvalue is positive, state vector is increasing over time and will be infinitely magnified over time

## Feedback:

if system is controllable, we can set:  $u(t) = K\vec{x}(t)$

plugging in, we get:  $\vec{x}(t+1) = (A + BK)\vec{x}(t)$

we can find the eigenvalues of  $(A + BK)$  to check for stability

## Stability Example:

given the following system:

$$\vec{x}[t+1] = \begin{bmatrix} -5 & 0 \\ 7 & 6 \end{bmatrix} \vec{x}[t] + \begin{bmatrix} 2 \\ -1 \end{bmatrix} u[t]$$

$$\vec{y}[t] = \begin{bmatrix} 1 & 1 \end{bmatrix} \vec{x}[t]$$

## Stability Check:

$$\lambda = 6, -5$$

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System is unstable

# Eigenvalue Placement

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# Eigenvalue Placement





# Why?

- Recall that we are always interested in determining if a given system is BIBO (bounded input bounded output) stable.
- More precisely, if we have a system described by  $\vec{x}(t+1) = A\vec{x}(t) + Bu(t) + \vec{w}(t)$  we would like the eigenvalues of  $A \in \mathbb{R}^{n \times n}$ , to satisfy the following property :  $|\lambda_i| < 1$ .
- So what if we have a  $\lambda$  that does not satisfy this property?
- This is where eigenvalue placement comes into play!
- Assuming the system is controllable, we will use closed loop controls to change the eigenvalues such that they satisfy this property.

## How?

- Assume e.g. a DT system. Input:  $u[t]$  If the system is controllable then we can use feedback, which means that we can let the input depend on the output,  $\vec{x}[t]$ .
- We would like to change the matrix multiplying  $\vec{x}[t]$  such that  $|\lambda_i| < 1$ , so let's see what happens when we let  $u[t] = K\vec{x}[t]$ , where  $K \in \mathbb{R}^{1 \times n}$ .
- Using this input we have:

$$\begin{aligned}\vec{x}[t+1] &= A\vec{x}[t] + Bu[t] + \vec{w}[t] \\ &= A\vec{x}[t] + BK\vec{x}[t] + \vec{w}[t] \\ &= (A + BK)\vec{x}[t] + \vec{w}[t]\end{aligned}$$

- Strategically choosing  $K$  allows us to have specific  $\lambda$ 's for  $A + BK$  (Good!).
- This process is called coefficient matching.

## Example

- Suppose we are given a controllable system defined by:

$$\vec{x}[t+1] = \begin{bmatrix} 2 & -1 \\ 0 & 1 \end{bmatrix} \vec{x}[t] + \begin{bmatrix} 2 \\ -1 \end{bmatrix} u[t]$$

- Is the system stable?

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- Is the system stable? No!  $\lambda = 2, 1$
- What if we let

$$u[t] = \begin{bmatrix} f_1 & f_2 \end{bmatrix} \vec{x}[t]$$

Then we have:

$$\vec{x}(t+1) = \begin{bmatrix} -2 & -1 \\ 0 & 1 \end{bmatrix} \vec{x}[t] + \begin{bmatrix} 2 \\ -1 \end{bmatrix} \begin{bmatrix} f_1 & f_2 \end{bmatrix} \vec{x}[t]$$

- Solve for the values of  $f_1$  and  $f_2$  such that  $\lambda_1 = -0.25$  and  $\lambda_2 = 0$

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- The answer is  $f_1 = -1.50$  and  $f_2 = 0.25$
- Although the process is very messy hopefully you see why eigenvalue placement is very important to stabilize systems.

# Controllable Canonical Form

- Controllable Canonical Form (CCF) for any controllable system is a special form that allows us to simplify the process of eigenvalue placement. It takes on the following form:

$$A^* = \begin{bmatrix} 0 & 1 & 0 & \dots & 0 \\ 0 & 0 & 1 & \dots & 0 \\ \vdots & \dots & \dots & \dots & 0 \\ 0 & \dots & \dots & \dots & 1 \\ \alpha_0 & \alpha_1 & \dots & \dots & \alpha_{n-1} \end{bmatrix}$$

$$B^* = \begin{bmatrix} 0 \\ 0 \\ \vdots \\ 0 \\ 1 \end{bmatrix}$$

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- The characteristic polynomial of  $A^*$  is  $\lambda^n - \sum_{i=0}^{n-1} \alpha_i \lambda^i = 0$ .
- So how does it help with eigenvalue placement?



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- So how does it help with eigenvalue placement? The last row of this matrix determines the eigenvalues of  $A^*$  so modifying the last row will allow us to (easily) modify the eigenvalues.

## How to convert to CCF

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- Recall the matrix we used to check controllability?

$$C = \begin{bmatrix} B & AB & \dots & A^{n-1}B \end{bmatrix}$$

$$C^* = \begin{bmatrix} B^* & A^*B^* & \dots & A^{*n-1}B^* \end{bmatrix}$$

- We then have  $T := C^*C^{-1}$ , such that  $A^* = TAT^{-1}$  and  $B^* = TB$ .
- Remember, all controllable matrices with single input can be transformed into CCF!

## Example

Consider the following discrete time system:

$$\vec{x}[t+1] = \begin{bmatrix} -2 & 2 & 0 \\ 2 & -4 & 2 \\ 0 & 1 & -1 \end{bmatrix} \vec{x}[t] + \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix} u[t]$$

- (a) Is the system stable? Is it controllable?
- (b) Using an appropriate transformation ( $\vec{z}[t] = T\vec{x}[t]$ ), bring the system to controllable canonical form.
- (c) Using the state feedback  $u[t] =$

$$\begin{bmatrix} f_1 & f_2 & f_3 \end{bmatrix}$$

$\vec{z}[t]$  bring the eigenvalues of the system to  $0, 0.75, -0.25$ .

## Solutions to Example

(a) The characteristic polynomial is:

$\lambda^3 + 7\lambda^2 + 8\lambda = \lambda(\lambda^2 + 7\lambda + 8) = 0$ , therefore the eigenvalues of  $A$  are  $\{0, -5.56, -1.44\}$ . As we can see there are  $|\lambda_i| > 1$  therefore the system is not stable.

The controllability matrix  $C =$

$$\begin{bmatrix} 1 & -2 & 8 \\ 0 & 2 & -12 \\ 0 & 0 & 2 \end{bmatrix}$$

$C$  has full rank so the system is controllable

(b) As we previously mentioned the coefficients of the characteristic polynomial are closely related to the last row of the  $A^*$  matrix. Therefore, the CCF of the system is:

$$\vec{z}[t+1] = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ 0 & -8 & -7 \end{bmatrix} \vec{x}[t] + \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} u[t]$$

## Example Solutions Continued

(c) Our system then becomes:

$$\vec{z}[t+1] = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ f_1 & f_2 - 8 & f_3 - 7 \end{bmatrix} \vec{x}[t]$$

Which means its characteristic polynomial is :

$$\lambda^3 - (f_3 - 7)\lambda^2 - (f_2 - 8)\lambda - f_1 = 0.$$

Now, we know the characteristic polynomial should be

$\lambda(\lambda - \frac{3}{4})(\lambda + \frac{1}{4})$ , so we can equate the two and solve for the feedback vector  $\vec{f}^T = \begin{bmatrix} 0 & \frac{1}{2} & \frac{3}{16} \end{bmatrix}$ .

# Linearization

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- Recall that if we have  $\frac{dx}{dt} = \lambda x(t) + bu(t)$  we know a solution to this is:

$$x(t) = x(0)e^{\lambda t} + \int_0^t e^{\lambda(t-\tau)} u(\tau) d\tau$$

- What if we had  $\frac{dx}{dt} = f(x(t)) + bu(t)$ , where  $f$  is nonlinear (e.g *sin*)?

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- Big Picture: linearize  $f$  around an operating point and then treat it as a linear function in a small neighborhood of that point.
- Why linearization?

It allows you to treat the system as a linear one, which is very helpful as linear ODE are (usually) much easier to solve!

## Linearizing a Single-Variable Function

- Suppose we have  $f(x)$  that is a non linear function. We can use a first order Taylor polynomial to linearize the function, this is equivalent to finding the slope of the tangent line of  $f(x)$  at a particular point.
- From calculus:  $f(x) \approx f(x^*) + f'(x^*)(x - x^*)$ .
- As long as we are within some (very small)  $\delta$  neighborhood of  $x^*$  the linearization is valid.
- Example: Linearize  $f(x) = 3e^{x^2+2}$  around  $x^*$

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- Example: Linearize  $f(x) = 3e^{x^2+2}$  around  $x^*$
- Solution:

$$f(x^*) = 3e^{(x^*)^2+2}$$

$$f'(x) = 3e^{x^2+2}(2x) = 6xe^{x^2+2}$$

$$f'(x^*) = 6x^*e^{(x^*)^2+2}$$

$$\text{Therefore : } f(x) \approx 3e^{(x^*)^2+2} + 6x^*e^{(x^*)^2+2}(x - x^*)$$

## Linearizing Steps for $\frac{dx}{dt} = f(x(t)) + b(u(t))$

- (i) Choose, or you may be given, a DC input point. That is, a point  $u^* \equiv u(t)$  that is constant with time.

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- (ii) Find a DC operating point,  $x^* \equiv x(t)$ . That is, solve  $\frac{dx^*}{dt} = f(x^*) + bu^*$ . Notice that this boils down to finding an  $x^*$  such that  $f(x^*) + bu^* = 0$ .

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- (iii) Define  $x_I(t) = x(t) - x^*$  and  $u_I(t) = u(t) - u^*$ , and re-write the ODE in terms of  $x_I(t)$  and  $u_I(t)$ . By plugging in you get:  
$$\frac{dx_I(t)}{dt} = f(x_I(t) + x^*) + b(u_I(t) + u^*)$$



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- (iv) It is ok to assume at this point that  $u_I(t)$  is small, that means that the  $u(t)$  in step 1 does not deviate too much from  $u^*$ .

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- (iv) It is ok to assume at this point that  $u_I(t)$  is small, that means that the  $u(t)$  in step 1 does not deviate too much from  $u^*$ .
- (v) Linearize the ODE:  $f(x_I(t) + x^*) \approx f(x^*) + f'(x^*)x_I(t)$ . Here we assume that  $x_I(t)$  is also small. This is something that we will need to verify in the next step!

## Linearizing Steps for $\frac{dx}{dt} = f(x(t)) + b(u(t))$ (Continued)

(vi) Plug (vi) back into (iii) and we obtain :

$$\frac{dx_I}{dt} \approx f'(x^*)x_I(t) + \cancel{f(x^*)} + b'(u^*)u_I(t) + \cancel{b(u^*)} = f'(x^*)x_I(t) + b'(u^*)u_I(t)$$

(vii) Verify the linearization!

How do we know if the linearization is valid?

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(vii) Verify the linearization!

How do we know if the linearization is valid? Well, if we have  $\frac{dx_I(t)}{dt} = \lambda x_I(t) + bu(t)$  we know the solution doesn't blow up if  $\lambda < 0$  as we will have a term  $e^{\lambda t}$ .

This means that we want  $m = f'(x^*) < 0$ .

## Linearizing Steps for $\frac{dx}{dt} = f(x(t)) + b(u(t))$ (Continued)

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$$\frac{dx_I}{dt} \approx f'(x^*)x_I(t) + \cancel{f(x^*)} + b'(u^*)u_I(t) + \cancel{b(u^*)} = f'(x^*)x_I(t) + b'(u^*)u_I(t)$$

(vii) Verify the linearization!

How do we know if the linearization is valid? Well, if we have

$\frac{dx_I(t)}{dt} = \lambda x_I(t) + bu(t)$  we know the solution doesn't blow up if  $\lambda < 0$  as we will have a term  $e^{\lambda t}$ .

This means that we want  $m = f'(x^*) < 0$ .

So what do we do if  $m > 0$ ?

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So what do we do if  $m > 0$ ?

Two options:

- We can go back and change our DC operating point  $(x^*, u^*)$
- Or, if the linearized system is **controllable**, we can solve an **eigenvalue placement** problem for a state stabilizing state feedback rule  $u = Kx$ .

## Practice Problem

Linearize  $\frac{dx}{dt} = \cos(x(t)) + bu(t)$  about  $u^* = 0$ .

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Linearize  $\frac{dx}{dt} = \cos(x(t)) + bu(t)$  about  $u^* = 0$ .

*Hint:*  $\cos(x^*) = 0$  has multiple solutions, which means that we can find numerous DC operating points, can you guess which one would result in a stable system ?



## Practice Problem Solution

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What if we had chosen a different DC Operating point, say  $-\frac{\pi}{2}$ ?

When we linearize the system we see that the solution will "explode" around that particular DC operating point.



## Linearization of Vector Functions

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For example:  $f_1(\vec{x}) \approx f_1(\vec{x}^*) + \frac{\partial f_1}{\partial x_1}(x_1 - x_1^*) + \dots + \frac{\partial f_1}{\partial x_n}(x_n - x_n^*)$

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Repeating this for all  $n$  functions in  $\vec{f}$  we see we get a system of scalar, linearized, multivariate functions which makes you think, wouldn't it be nice to express it in a shorthand matrix notation?

# Jacobian Matrix

We can use the Jacobian to express everything nicely and neatly. The Jacobian is the name given to the matrix of partial derivatives of  $\vec{f}$ , and it is denoted by  $J_{\vec{x}}$ ,  $\nabla_{\vec{x}}\vec{f}$ , or, more rarely,  $D\vec{f}(\vec{x})$ .

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Continuing from the previous slide we have:

$$\begin{bmatrix} f_1(\vec{x}) \\ \vdots \\ f_n(\vec{x}) \end{bmatrix} \approx \begin{bmatrix} f_1(\vec{x}^*) \\ \vdots \\ f_n(\vec{x}^*) \end{bmatrix} + \begin{bmatrix} \frac{\partial f_1}{\partial x_1} & \cdots & \frac{\partial f_1}{\partial x_n} \\ \vdots & \ddots & \vdots \\ \frac{\partial f_n}{\partial x_1} & \cdots & \frac{\partial f_n}{\partial x_n} \end{bmatrix} (\vec{x} - \vec{x}^*)$$

## Linearization with Jacobians Example

$$\text{Linearize } \vec{f}(\vec{x}(t)) = \begin{bmatrix} \sin(x_1(t) \times x_2(t)) + 2x_1(t)x_3^2(t) \\ x_3(t) \cos(x_2(t)) + \frac{x_1(t)}{x_3(t)} \\ x_1(t) + 2x_3(t)x_2^3(t) \end{bmatrix} \text{ about } \vec{x}^* = \begin{bmatrix} 0 \\ 2\pi \\ \frac{2\pi}{3} \end{bmatrix}$$



# Solutions

Find the Jacobian:

$$\begin{bmatrix} x_2(t) \cos(x_1(t) \times x_2(t)) + 2x_3^2(t) & x_1(t) \cos(x_1(t) \times x_2(t)) & 4x_1(t)x_3(t) \\ \frac{1}{x_3(t)} & -x_3(t) \sin(x_2(t)) & \cos(x_2(t)) - \frac{x_1(t)}{x_3^2(t)} \\ 1 & 6x_3(t)x_2^2(t) & 2x_2^3(t) \end{bmatrix}$$

Evaluate the Jacobian about  $\vec{x}^*$ :

$$\begin{bmatrix} 5\pi & 0 & 0 \\ \frac{2\pi}{3} & 0 & 1 \\ 1 & 36\pi^3 & 16\pi^3 \end{bmatrix}$$

Linearize:

$$\vec{f}(\vec{x}(t)) \approx \begin{bmatrix} 0 \\ \frac{3\pi}{4} \\ 24\pi^4 \end{bmatrix} + \begin{bmatrix} 5\pi & 0 & 0 \\ \frac{2\pi}{3} & 0 & 1 \\ 1 & 36\pi^3 & 16\pi^3 \end{bmatrix} \begin{bmatrix} x_1(t) - 0 \\ x_2(t) - \frac{3\pi}{4} \\ x_3(t) - 24\pi^4 \end{bmatrix}$$

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To linearize  $\frac{d\vec{x}}{dt} = \vec{f}(\vec{x}(t), \vec{u}(t))$  we use a similar procedure as we did for the scalar case.

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- (iv) Plug (iv) back into the ODE:  
$$\frac{d\vec{x}}{dt} \approx \cancel{\vec{f}(\vec{x}^*, \vec{u}^*)} + J_{\vec{x}}\vec{x}_l(t) + J_{\vec{u}}\vec{u}_l(t)$$

# Singular Value Decomposition

---

# SVD Theorem

Any matrix  $A \in \mathbb{R}^{m \times n}$  can be decomposed into the product of three matrices

$$A = U \Sigma V^T$$

$$U : m \times m$$

$$\Sigma : m \times n$$

$$V^T : n \times n$$

Such that  $U, V$  are unitary matrices and  $\Sigma$  only has nonnegative values along its main diagonal.



## SVD: Compact Form

We can also express the SVD as

$$A = \mathcal{U}S\mathcal{V}^T$$

$$\mathcal{U} : m \times r$$

$$S : r \times r$$

$$\mathcal{V}^T : r \times n$$

where  $r$  is the rank of  $A$ . The compact form matrices maintain properties of the original matrices, but have entries removed whenever they correspond to zero singular values.

## SVD: Outer Product Form

Lastly, we can express

$$A = \sum_{i=1}^r \sigma_i \vec{u}_i \vec{v}_i^T$$

where  $\vec{u}_i, \vec{v}_i$  are the columns of  $U, V$ , respectively, and  $\sigma_i$  are corresponding diagonal entry of the matrix  $\Sigma$

## Computing SVD with $A^T A$

$$\begin{aligned} A^T A &= U \Sigma V^T V \Sigma^T U^T \\ &= U \Sigma^2 U^T \end{aligned}$$

This is an eigen decomposition since  $\Sigma^2$  is diagonal and  $U^{-1} = U^T$ . Thus solving for the eigenvalues and eigenvectors of  $A^T A$  give  $\lambda_i = \sigma_i^2$  with eigenvectors which correspond to the right singular vectors. We need to sort by decreasing  $\sigma_i$ .

**Side note:**  $\Sigma^T \Sigma$  is not actually equal to  $\Sigma^2$ , but the former product yields a matrix with singular values squared on the diagonal entries, hence we call it  $\Sigma^2$

## Computing SVD with $A^T A$

Given a right singular vector  $\vec{v}_i$  which we found from the previous part, we can apply it

$$\begin{aligned} A\vec{v}_i &= \left( \sum_{k=1}^r \sigma_k \vec{u}_k \vec{v}_k^T \right) \vec{v}_i \\ &= \sum_{k=1}^r \sigma_k \vec{u}_k \vec{v}_k^T \vec{v}_i \\ &= \sigma_i \vec{u}_i \\ \vec{u}_i &= \frac{1}{\sigma_i} A\vec{v}_i \end{aligned}$$

## Computing SVD with $AA^T$

Similar calculations yield  $\sigma_i = \sqrt{\lambda_i}$  of  $AA^T$  with eigenvectors as left singular vectors, and  $\vec{v}_i = \frac{1}{\sigma_i} A^T \vec{u}_i$

# Intepretation of SVD

- Unitary matrices act as rotation in a given space. A diagonal matrix stretches in a given coordinate space.
- [SVD visualization \(open in browser\)](#)

For a product  $A\vec{x}$ , we can decompose every vector  $\vec{x}$  into a linear combination of right singular vectors

$$\vec{x} = \sum_{i=1}^n \alpha_i \vec{v}_i$$

Thus, we can see exactly which parts of  $\vec{x}$  affect the output.

# Compression of Low-Rank Matrices

- Suppose I had a matrix  $A \in \mathbb{R}^{m \times n}$  with  $m, n \gg \text{rank}(A)$ . How could I more efficiently store  $A$  and compute products like  $A\vec{x}$ ?



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- With the SVD, we only have to save  $r$  set of two vectors and a scalar, which saves us a lot of space if the rank is small with respect to the matrix. Also, less computation is carried out if we represent the matrix as the outer product form.

# Principle Component Analysis

---

PCA is a linear dimensionality reduction tool. Given data  $\vec{x}_i \in \mathbb{R}^d$ , we can create a mapping  $T : \mathbb{R}^d \rightarrow \mathbb{R}^{d'}$ ,  $d' < d$  such that the variance in the dataset is still captured

1. Store data row-major in  $A \in \mathbb{R}^{n \times d}$

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5. To project data into the representative subspace:  
$$T(\vec{x}) := V_{d'}^T \vec{x}$$



The mapping  $T$  can then be expressed as

$$T(\vec{x}) = V_k^T \vec{x}$$

If we apply this transformation onto the entire dataset (which has *row vectors*), we can say

$$T(A) = B = V_k^T A$$

where  $B \in \mathbb{R}^{n \times k}$ .

If we were to show the projected vectors in the original space, we can multiply back with the projection vectors

$$A' = V_k B$$

# Discretization

---

## Discretization: Q1

Suppose we have a scalar system

$$\frac{d}{dt}x(t) = \alpha x(t) + \vec{\beta}^T \vec{u}(t)$$

and we apply a constant input  $\vec{u}_n$  for times  $t \in [nT, (n+1)T)$  for some  $T > 0$ . Given  $x(nT)$  solve the differential equation.

## Discretization: Q1 Sol

From  $t = nT$  to  $t = (n+1)T$ ,  $\vec{\beta}^T \vec{u}$  is a constant scalar. Thus, we can solve this like a normal differential equation. Let  $x = x' - \frac{\vec{\beta}^T \vec{u}}{\alpha}$ .

$$\frac{d}{dt}x'(t) = \alpha(x'(t) - \frac{\vec{\beta}^T \vec{u}}{\alpha}) + \vec{\beta}^T \vec{u}$$

$$= \alpha x'$$

$$x'(t) = Ae^{\alpha(t-nT)}$$

$$x(t) + \frac{\vec{\beta}^T \vec{u}}{\alpha} = Ae^{\alpha(t-nT)}$$

$$x(t) = Ae^{\alpha(t-nT)} - \frac{\vec{\beta}^T \vec{u}}{\alpha}$$

## Discretization: Q1 Sol Continued

At this point we can use our initial condition to get

$$x(nT) = A - \frac{\vec{\beta}^T \vec{u}}{\alpha}$$

$$A = x(nT) + \frac{\vec{\beta}^T \vec{u}}{\alpha}$$

$$x = \left( x(nT) + \frac{\vec{\beta}^T \vec{u}}{\alpha} \right) e^{\alpha(t-nT)} - \frac{\vec{\beta}^T \vec{u}}{\alpha}$$

## Discretization: Q2

Using the differential equation derived from question 1, create a discrete-time system to model the continuous time. In other words, if  $x[n] = x(nT)$ ,  $\vec{u}[n] = \vec{u}(nT)$ , find a relation such that

$$x[n+1] = A_d x[n] + B_d \vec{u}[n]$$

## Discretization: Q2 Sol

We can solve the previous solution for  $x((n+1)T)$

$$x((n+1)T) = \left( x(nT) + \frac{\vec{\beta}^T \vec{u}(nT)}{\alpha} \right) e^{\alpha((n+1)T - nT)} - \frac{\vec{\beta}^T \vec{u}(nT)}{\alpha}$$

$$x[n+1] = e^{\alpha T} x[n] + \frac{e^{\alpha T} - 1}{\alpha} \vec{\beta}^T \vec{u}[n]$$

We see that  $A_d = e^{\alpha T}$ ,  $B_d = ((e^{\alpha T} - 1)/\alpha) \vec{\beta}^T$



## Discretization: Q3

Instead of a scalar, we instead have a diagonal matrix  $A$  such that

$$\frac{d}{dt}\vec{x} = A\vec{x} + B\vec{u}$$

Discretize this system in the same way as Q2.

Expanding the original system out line-by-line gives

$$\frac{d}{dt}x_i = a_i x_i + b_i \vec{u}_i$$

where  $x_i$  is the  $i$ th variable of  $\vec{x}$ ,  $a_i$  is the diagonal entry of  $A$ , and  $b_i$  is the row of  $B$ .

## Discretization: Generic Matrix

Math not shown, but we can perform a change of basis from our original space to our diagonal space, and then apply the results of the previous part.