

RBE502 - Homework Set 8

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Introduction

In this assignment, we will be looking at a 2 link robotic arm as depicted in the figure below. We will be designing a feedback, feedforward controller to stabilize the robotic arm on a desired orientation/position.

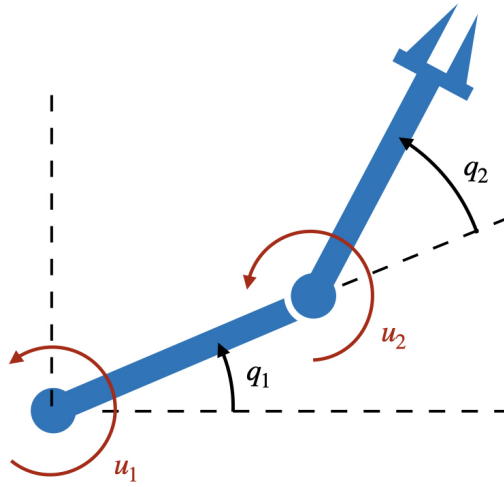


Figure 1: 2 link robotic arm

This arm can be expressed mathematically as a double pendulum system as depicted in the following figure. Within this system, we can define $M(q)$, $T(q)$, and $\phi(q, \dot{q})$ as:

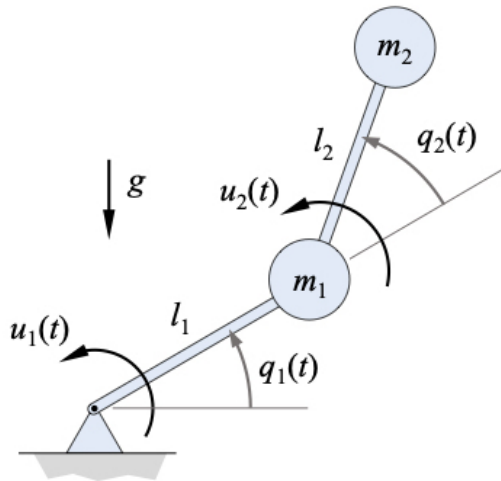


Figure 2: Double pendulum system

$$M(q) = \begin{bmatrix} (m_1 + m_2)l_1^2 + m_2 * l_2^2 + 2l_1 l_2 m_2 \cos q_2 & m_2 l_2 (l_1 \cos q_2 + l_2) \\ m_2 l_2 (l_1 \cos q_2 + l_2) & m_2 l_2^2 \end{bmatrix} \quad (1)$$

$$T(q) = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \quad (2)$$

$$\phi(q) = \begin{bmatrix} (m_1 + m_2)gl_1 \cos q_1 + m_2 l_2 (g \cos(q_1 + q_2) - l_1 \dot{q}_2 (2\dot{q}_1 + \dot{q}_2) \sin q_2) \\ m_2 l_2 (l_1 \dot{q}_1^2 + g \cos q_1 + q_2) \end{bmatrix} \quad (3)$$

We further define $x = [q_1 \quad q_2 \quad \dot{q}_1 \quad \dot{q}_2]^T$. From this we can compile these equations into a system:

$$\dot{x} = \begin{bmatrix} q \\ \dot{q} \end{bmatrix} = f(x) + g(x)u = \begin{bmatrix} -M^{-1}\dot{q} \\ -M^{-1}\phi(q, \dot{q}) \end{bmatrix} + \begin{bmatrix} \mathbf{0} \\ M^{-1}T(q) \end{bmatrix} u \quad (4)$$

From this we can select a desired state, x_d , and define the error dynamics as:

$$\dot{e} = \dot{x}_d - \dot{x} = 0 - f(x) - g(x)u = -f(x_d - e) - g(x_d - e)u \quad (5)$$

We further simplify this by defining $f_e(u) = -f(x_d - e)$ and $g_e(u) = -g(x_d - e)$, thus making our final equation $\dot{e} = f_e(e) + g_e(e)u$.

Part A

In this section, we will write $\phi(q, \dot{q}) = [\phi_1(q_1, \dot{q}_1) \quad \phi_2(q_2, \dot{q}_2)]^T$ as $\phi(q, \dot{q}) = C(q, \dot{q})q + G(q)$. To do this, we will find the vectors $C(q, \dot{q})$ and $G(q)$.

For $C(q, \dot{q})$, we factor both ϕ_1 and ϕ_2 for our components q_1 and q_2 . This results in the following vectors factored for each, where ϕ_{if} is the factored vector of ϕ_i :

$$C(q, \dot{q}) = \phi_{1f} + \phi_{2f} = \begin{bmatrix} -2l_1 \sin(q_2) \\ -l_1 \dot{q}_2 \sin(q_2) \end{bmatrix} + \begin{bmatrix} l_1 l_2 m_2 \dot{q}_1 \sin(q_2) \\ 0 \end{bmatrix} = \begin{bmatrix} l_1 l_2 m_2 \dot{q}_1 \sin(q_2) - 2l_1 \sin(q_2) \\ -l_1 \dot{q}_2 \sin(q_2) \end{bmatrix} \quad (6)$$

To solve for G , we will first need to find the potential energy of the system, U , which consists of the potential energy of each link, U_1 and U_2 .

$$U_1 = g l_1 \sin(q_1) (m_1 + m_2) \quad (7)$$

$$U_2 = g m_2 (l_2 \sin(q_1 + q_2) + l_1 \sin(q_1)) \quad (8)$$

$$U = U_1 + U_2 = g l_1 \sin(q_1) (m_1 + m_2) + g m_2 (l_2 \sin(q_1 + q_2) + l_1 \sin(q_1)) \quad (9)$$

$G(q)$ is the partial gradient of the potential energy by q where $q = [q_1 \quad q_2]^T$.

$$G(q) = \frac{\partial U}{\partial q} = \begin{bmatrix} g m_2 (l_2 \cos(q_1 + q_2) + l_1 \cos(q_1)) + g l_1 \cos(q_1) (m_1 + m_2) \\ g l_2 m_2 \cos(q_1 + q_2) \end{bmatrix} \quad (10)$$

Thus our equation with a solved $C(q, \dot{q})$ and $G(q)$ is:

$$\phi(q, \dot{q}) = C(q, \dot{q})\dot{q} + G(q) \quad (11)$$

$$\phi(q, \dot{q}) = \begin{bmatrix} l_1 l_2 m_2 \dot{q}_1 \sin(q_2) - 2l_1 \sin(q_2) \\ -l_1 \dot{q}_2 \sin(q_2) \end{bmatrix} + \begin{bmatrix} g m_2 (l_2 \cos(q_1 + q_2) + l_1 \cos(q_1)) + g l_1 \cos(q_1) (m_1 + m_2) \\ g l_2 m_2 \cos(q_1 + q_2) \end{bmatrix} \quad (12)$$

Part B

Here, we define values for m_1 , m_2 , l_1 , l_2 , and g respectively to $10kg$, $4kg$, $1m$, $2m$, and $9.8\frac{m}{s^2}$. We are aiming to define a PD controller with gravity compensation as $u = [K_p \quad K_d] (x_d - x) + G(q)$. We further define $[K_p \quad K_d]$ as:

$$[K_p \quad K_d] = \begin{bmatrix} 2 & 0 & 3 & 0 \\ 0 & 12 & 0 & 7 \end{bmatrix} \quad (13)$$

We aim to simulate this system from an initial position $x_0 = [0 \quad 0 \quad 0 \quad 0]^T$ to various positions.

$$x_d = [0 \quad \frac{\pi}{2} \quad 0 \quad 0]^T$$

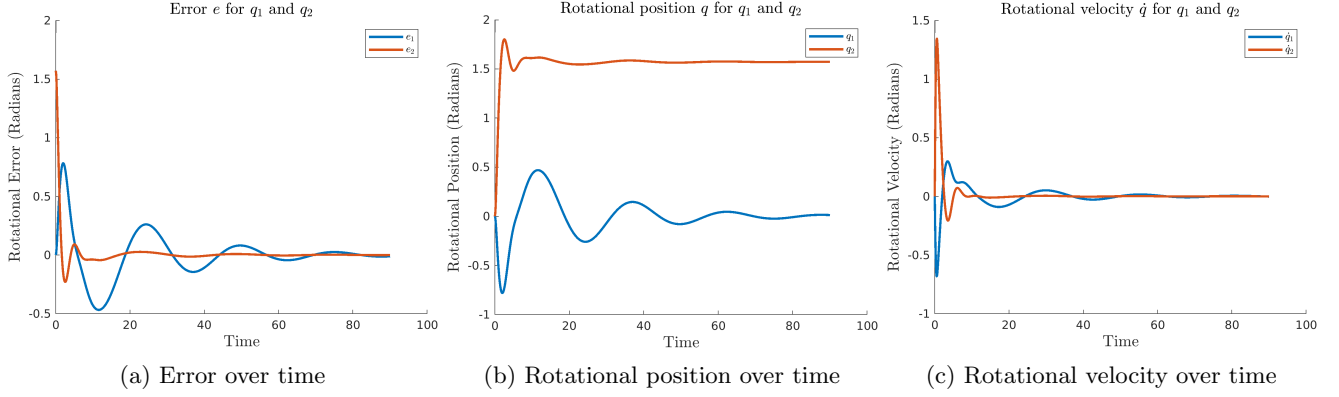


Figure 3: System response with $x_d = [0 \quad \frac{\pi}{2} \quad 0 \quad 0]^T$

$$x_d = [\frac{\pi}{2} \quad 0 \quad 0 \quad 0]^T$$

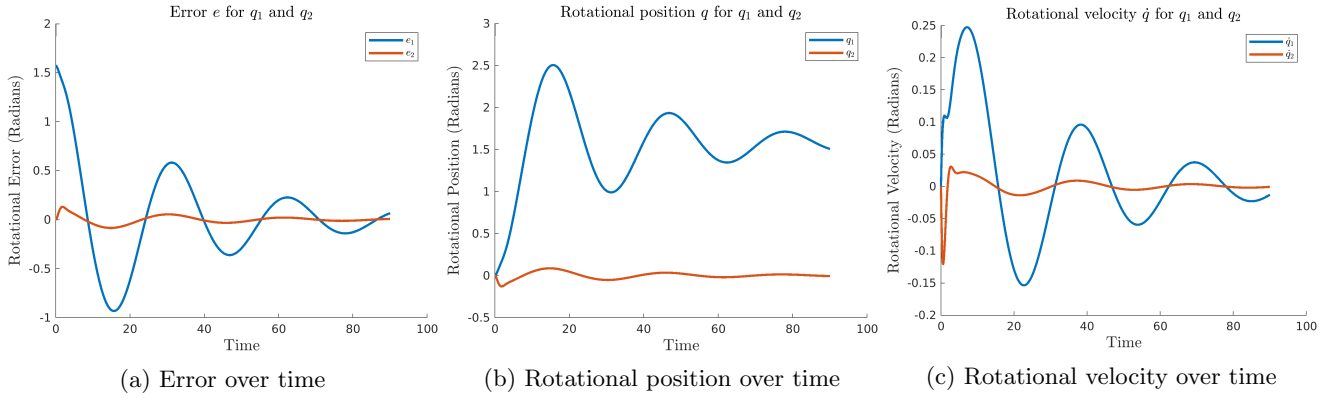


Figure 4: System response with $x_d = [\frac{\pi}{2} \quad 0 \quad 0 \quad 0]^T$

$$x_d = \begin{bmatrix} \frac{\pi}{4} & \frac{\pi}{4} & 0 & 0 \end{bmatrix}^T$$

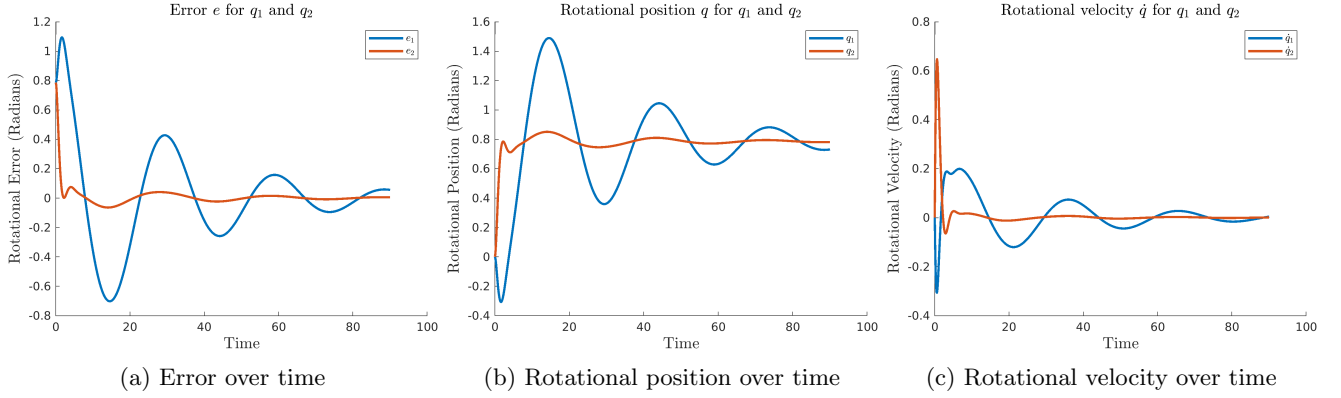


Figure 5: System response with $x_d = \begin{bmatrix} \frac{\pi}{4} & \frac{\pi}{4} & 0 & 0 \end{bmatrix}^T$

Part B Conclusions

We see that these systems do converge onto a given location, but at a far slower rate than we saw with feedback linearization. We also see that we also have significant movement of joints that were otherwise in the correct position prior.

To experiment, we modified some values in both the K_p and the K_d control matrices. Modifying the K_p values resulted in control over the magnitude of the initial swings of error, but resulted in larger and longer oscillations. We did see faster overall convergence when tweaking the K_d values to higher values, but still struggled to find a convergence time below 20 seconds.

Likewise, looking at the rotational velocities and large changes in rotations in both joints to achieve the desired positions, this control system seems almost inefficient in its approach to establishing the desired orientation of q_d .

This gravity compensation is, from this experiment, better at holding a position against gravity or outside perturbances than being utilized as a methodology for moving an arm into a widely different desired orientation.