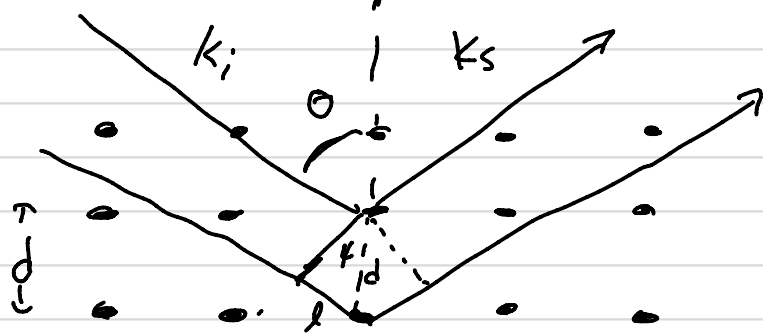


Lecture 8 -

RDFs continued

Last time: characterized liquid/gas structure by  $g(r)$ , the radial distribution function:  $g(r) = \frac{N-1}{4\pi r^2} \langle \delta(r-r') \rangle$

But how do we measure the structure of these systems - do by scattering expt, like for a solid. Recall:



$$l = d \sin \psi$$

$$\text{path dist} = 2l = 2d \sin \psi$$

Constructive interference when  $2d \sin \psi = n\lambda$   
(Bragg Scattering)

For a plane wave,  $\psi(\vec{r}) = e^{-i\vec{k} \cdot \vec{r}}$ , [ $\vec{k} \cdot \vec{r}$  is phase at a point]

In this scattering experiment, energy photon comes in with momentum  $|\vec{k}_i| = 2\pi/\lambda$  and leaves with momentum  $\vec{k}_s$

Phase at  $\vec{r}_1$  is  $-\vec{k}_i \cdot \vec{r}_1$  and  $\vec{r}_2$  is  $-\vec{k}_i \cdot \vec{r}_2$

Phase diff is  $-\vec{k}_i \cdot (\vec{r}_1 - \vec{r}_2) = \delta\phi_i$

$$\delta\phi_i \approx |\vec{k}| |\vec{r}_1 - \vec{r}_2| \cos\theta \quad \text{where } \theta \text{ is angle}$$

between incoming wave &  $\vec{r}_2 - \vec{r}_1$

$$= 2\pi/\lambda d \cos\theta$$

$$\delta\phi_s = \vec{k}_s \cdot (\vec{r}_1 - \vec{r}_2)$$

$$\delta\phi = \delta\phi_s + \delta\phi_i = (\vec{k}_s - \vec{k}_i) \cdot (\vec{r}_1 - \vec{r}_2)$$

$$= \underbrace{\vec{q}}_{\text{momentum transfer}} \cdot (\vec{r}_1 - \vec{r}_2)$$

for elastic,  $\theta_{in} = \theta_{out}$

$$\delta\theta = 4\pi/\lambda d \cos\theta$$

constructive  $\delta\theta = 2\pi n$

Bragg again

$$\Rightarrow 4\pi/\lambda d \cos\theta = 2\pi n \Rightarrow 2d \cos\theta = n\lambda$$

Turns out, outgoing wave is sum over all scattering events

$$\psi(\vec{q}) = \sum_{j=1}^N f_j e^{-i\vec{q} \cdot \vec{R}_j}$$

pos of particles  $\vec{R}_j$

change in wave vec  $\vec{k}_s - \vec{k}_i$

$f_j$  is form factor that depends on how atom interacts w/ light

$$\text{Intensity} = |\psi^* \psi| = \sum_{i=1}^N \sum_{j=1}^N f_i f_j e^{-i\vec{q} \cdot (\vec{R}_j - \vec{R}_i)}$$

The "structure factor" is defined by  
normalizing by  $\sum_{i=1}^N f_i^2$

$$S(q) = \frac{1}{\sum_{i=1}^N f_i^2} \sum_i \sum_j e^{-iq \cdot (R_j - R_i)} \cdot f_i \cdot f_j$$

if all the same type,  $f_i = f$

$$\Rightarrow S(q) = \frac{1}{N f^2} \cdot f^2 \sum_{i,j} e^{-iq \cdot (R_j - R_i)} = \boxed{\frac{1}{N} \sum_{i,j} e^{-iq \cdot (R_j - R_i)}}$$

To actually compute, avg over mc motions

$$S(q) = \left\langle \frac{1}{N} \sum_{i,j} e^{-iq \cdot \Delta R} \right\rangle = \frac{1}{N} \left\langle \left| \sum_i e^{iq \cdot R_i} \right|^2 \right\rangle$$

↑  
rewrite

± doesn't matter

Separate into self,  $i=j$ ,  $R_i - R_j = 0$  & distinct

$$S(q) = 1 + \frac{1}{N} \left\langle \sum_{i \neq j} e^{-iq \cdot (\vec{R}_j - \vec{R}_i)} \right\rangle$$

↑  
N · (N-1) terms  $e^{iq \cdot \vec{R}_j - \vec{R}_i}$   
 $\langle e^{iq \cdot \vec{R}_j - \vec{R}_i} \rangle = \langle e^{iq \cdot \vec{R}_2 - \vec{R}_1} \rangle$  avg, value  
doesn't depend on particle pair

$$\Rightarrow S(q) = 1 + (N-1) \langle e^{-iq \cdot (\vec{R}_2 - \vec{R}_1)} \rangle$$

$$= 1 + (N-1) \cdot \frac{\int dR_1 dR_2 \dots dR_N e^{-iq \cdot (\vec{R}_2 - \vec{R}_1)} e^{-\beta U(\vec{x})}}{\mathcal{Z}}$$

$$= 1 + (N-1) \cdot \int dR_1 \int dR_2 e^{-iq \cdot (R_2 - R_1)} \underbrace{\frac{\int dR^{N-1} e^{-\beta U(\vec{x})}}{\mathcal{Z}}}_{\frac{\rho^2 g^2(R_1, R_2)}{N \cdot N-1}}$$

switched to k

↓

$$S(k) = 1 + \frac{1}{N} \cdot \int d\vec{r}_1 \int d\vec{r}_2 \rho^2 g(\vec{r}_1, \vec{r}_2) e^{-i\vec{k}(\vec{r}_2 - \vec{r}_1)}$$

$$= 1 + \frac{1}{N} \int d\vec{R} d\vec{r} \rho^2 g(\vec{r}, \vec{R}) e^{i\vec{k} \cdot \vec{r}} \quad \vec{R} = \vec{r}_2 - \vec{r}_1$$

defined  $\int d\vec{R} g(\vec{r}, \vec{R}) = V g(\vec{r})$

$$= 1 + \frac{1}{\rho} \int d\vec{r} \rho^2 g(\vec{r}) e^{-i\vec{k} \cdot \vec{r}}$$

$$= 1 + \rho \int d\vec{r} g(\vec{r}) e^{-i\vec{k} \cdot \vec{r}}$$

Reminder:  $\tilde{f}(k) = FT[f(x)] = \int_{-\infty}^{\infty} dx e^{-ikx} f(x)$

$$= 1 + \rho \int_0^{\pi} d\theta \int_0^{2\pi} d\phi \int_0^{\infty} dr r^2 \sin\theta g(r) e^{-ikr \cos\theta}$$

$$u = \cos\theta$$

$$du = -\sin\theta d\theta$$

$$= 1 + 2\pi\rho \int_{-1}^1 du \int_0^{\infty} dr r^2 g(r) e^{+ikru}$$

$$= 1 + 2\pi\rho \int_0^{\infty} dr r^2 g(r) \cdot \frac{1}{ikr} \cdot \left[ e^{+ikru} \right]_{u=-1}^1 \quad \left| \quad \frac{e^{+iax} - e^{-iax}}{2i} = +\sin(ax) \right.$$

$$= 1 + 4\pi\rho \int_0^{\infty} dr \cdot r^2 g(r) \frac{\sin(kr)}{kr} \quad \leftarrow \text{can predict } S(k) \text{ from liquid struct}$$

## Thermodynamic Quantities from $g(r)$

Very interesting result:  $g(r) = e^{-\beta w(r)}$

Reversible work theorem,  $w(r)$  is work to move two particles from infinite separation to separation  $r$  - reversibly, const  $N, V, T$

Work =  $\Delta A$  in process

$$\text{work done by the force} = \int_{+\infty}^r F(r) dr, \quad \text{work you have to do} = \int_r^{\infty} F(r) dr$$

But what is  $F$ ? ,  $-\nabla U(r)$  averaged over positions of other particles, if reversibly slow

$$\begin{aligned} \left\langle -\frac{\partial U(r_{12})}{\partial r_{12}} \right\rangle &= \frac{\int dr_3 dr_4 \dots dr_N -\frac{dU}{dr_{12}} e^{-\beta U(r)} }{\int dr_3 dr_4 \dots dr_N e^{-\beta U(r)}} \\ &= \int dr^{N-2} \cdot \frac{1}{\beta} \frac{d}{dr_{12}} e^{-\beta U(r)} / \int dr^{N-2} e^{-\beta U(r)} \\ &= k_B T \frac{d}{dr_{12}} \log \left[ \int dr^{N-2} e^{-\beta U(r)} \right] \\ \left[ g^{(2)}(r_1, r_2) = \frac{1}{N(N-1)} \int dr^{N-2} e^{-\beta U(r)} \right] \\ &= k_B T \frac{d}{dr_{12}} \log(g^{(2)}(r_1, r_2)) = k_B T \frac{d}{dr} \log(g(r)) \end{aligned}$$

$$\Rightarrow w(R) = \int_R^\infty k_B T \left[ \frac{d}{dr} \log g(r) \right] dr$$

$$= k_B T \log g(r) \Big|_R^\infty = 0 - \underline{k_B T \log g(R)}$$

$$\Rightarrow g(R) = e^{-\beta w(R)}$$

$w(R)$  is called the "potential of Mean force"  $\rightarrow \langle -\frac{\partial U}{\partial r} \rangle = -\frac{d}{dr} w(r)$

and it is what we

often want to calculate in free energy methods & what we fit for coarse grained forces

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Lets look at how the RDF is connected to the avg energy

first  $E = -\frac{\partial \log Q}{\partial \beta}$ ,  $Q = \frac{Z}{N! \lambda^{3N}}$ ,  $\lambda = \sqrt{\frac{2\pi m}{\beta \hbar^2}}$

$$E = -\frac{\partial}{\partial \beta} \left[ \log Z - \frac{3}{2} N \log \beta + \text{const} \right]$$

$$= \underbrace{\frac{3}{2} N k_B T}_{\langle \text{kinetic } E \rangle} - \underbrace{\frac{\partial \log Z}{\partial \beta}}_{\langle U \rangle}$$

So to get potential energy, only need  
(configurational) partition function

Now let's consider potentials  $U(\vec{r}) = \sum_i \sum_{j>i} u(r_{ij})$   
(pairwise)

then  $\langle u_{\text{pair}} \rangle = \frac{1}{Z} \sum_i \sum_{j>i} \int d\vec{r}^N u(r_i - r_j) e^{-\beta u_{\text{pair}}(\vec{r})}$   
but by relabeling can just write  
 $\int d\vec{r}^N u(r_1 - r_2) e^{-\beta u(\vec{r})}$

$$= \frac{N \cdot (N-1)}{2} \cdot \frac{1}{Z} \int d\vec{r}^N u(r_{12}) e^{-\beta u_{\text{pair}}(\vec{r})}$$

$$= \frac{1}{2} \int d\vec{r}_1 d\vec{r}_2 u(r_{12}) \frac{N \cdot (N-1)}{2} \int d\vec{r}^{N-2} e^{-\beta u_{\text{pair}}(\vec{r})}$$

$$= \rho^2 / 2 \int d\vec{r}_1 d\vec{r}_2 u(\vec{r}_{12}) g^{(2)}(\vec{r}_1, \vec{r}_2)$$

like before  $= \rho^2 / 2 \int d\vec{r} u(\vec{r}) g(\vec{r})$

if isotropic  $= \frac{N^2}{2V} \cdot 4\pi \int dr r^2 u(r) g(r) = \left( 2\pi N \rho \int_0^\infty dr r^2 u(r) g(r) \right)$

note - kind of what you expect,

$N$  particles dist away is  $4\pi \rho \int dr g(r) r^2$

so this is energy at that dist  $\times$  # pairs at that dist  $\cdot N/2$



What about pressure?

$$P = kT \frac{\partial}{\partial V} \ln Q(N, V, T) = kT \frac{\partial}{\partial V} \log Z(N, V, T)$$

$$Z(N, V, T) = \int_V d\mathbf{r}^N e^{-\beta U(\mathbf{r})} \quad , \text{ somewhere is volume dependence}$$

Imagine changing volume as moving everything closer together or further apart

$$\text{Say } \vec{s}_i = V^{-1/3} \vec{r}_i$$

$$\Rightarrow Z(N, V, T) = V^N \int d\mathbf{s}_N e^{-\beta U(V^{1/3} \vec{s}_1, V^{1/3} \vec{s}_2, \dots, V^{1/3} \vec{s}_N)}$$

$$\frac{dZ}{dV} = NV^{N-1} \int d\mathbf{s}_N \dots + V^N \int d\mathbf{s}_N \cdot -\beta \frac{dU}{dV}(V^{1/3} \dots) e^{-\beta U(\dots)}$$

$$\frac{dZ}{dV} = \frac{N}{V} \cdot Z$$

$$\begin{aligned} \text{chain rule } \frac{dU}{dV} &= \sum_{i=1}^N \frac{\partial U}{\partial (V^{1/3} s_i)} \frac{\partial V^{1/3} s_i}{\partial V} = \sum_{i=1}^N \left( \frac{1}{3} V^{-2/3} s_i \right) \frac{\partial U}{\partial r_i} \\ &= \sum_{i=1}^N \frac{1}{3V} \cdot r_i \frac{\partial U}{\partial r_i} = -\frac{1}{3V} \sum_{i=1}^N r_i \cdot F_i \end{aligned}$$

$$\frac{dZ}{dV} = \frac{N}{V} Z + \int d\mathbf{r}^N \cdot \frac{\beta}{3V} \sum_{i=1}^N r_i \cdot F_i e^{-\beta U(\mathbf{r})}$$

$$P = k_B T \frac{\partial \log Z}{\partial V} = k_B T \cdot \frac{1}{Z} \frac{dZ}{dV} = \frac{N k_B T}{V} + \frac{1}{3V} \left\langle \sum_{i=1}^N r_i \cdot F_i \right\rangle \quad \swarrow \text{virial}$$

$$\langle r_i^2 / 2m \rangle = \frac{3}{2} N k_B T \Rightarrow$$

$$P = \frac{1}{3V} \left\langle \sum_{i=1}^N \frac{p_i^2}{m} + r_i \cdot F_i \right\rangle \quad \swarrow \text{pressure estimator in MD}$$

Lastly, consider  $U_{\text{pair}} = \frac{1}{2} \sum_i \sum_j u(r_{ij})$

$$F_i = \sum_{j=1}^N -\frac{\partial u(r_{ij})}{\partial r_i} = \sum_{j=1}^N f_{ij}, \quad \text{note } f_{ij} = -f_{ji}$$

$$\frac{1}{3V} \left\langle \sum_{i=1}^N r_i F_i \right\rangle = \frac{1}{3V} \cdot \frac{1}{Z} \int d\mathbf{r}^N \sum_{i=1}^N \sum_{j=1}^N r_i f_{ij} e^{-\beta U_{\text{pair}}}$$

$$= \frac{1}{3V} \cdot \frac{1}{Z} \int d\mathbf{r}^N \sum_{i>j} r_{ij} f_{ij} e^{-\beta U_{\text{pair}}}$$

each integral identical by swapping particles

$$= \frac{N(N-1)}{2} \cdot \frac{1}{3V} \cdot \frac{1}{Z} \int d\mathbf{r}_1 d\mathbf{r}_2 r_{12} f_{12} \int d\mathbf{r}^{N-2} e^{-\beta u(r)}$$

$$= -\frac{\rho^2}{2} \cdot \frac{1}{3V} \cdot \int d\mathbf{r}_1 d\mathbf{r}_2 r_{12} \frac{du}{dr_{12}} g(r_{12})$$

$$= -\frac{\rho^2}{6V} \int d\mathbf{r} d\mathbf{R} r \frac{du}{dr} g(r, R)$$

$$= -\rho^2/6 \int d\vec{r} \vec{r} \frac{du}{dr} g(r)$$

isotropic

$$= -\rho^2/6 \cdot 4\pi \int dr r^3 \frac{du}{dr} g(r)$$

$$P/kT = \rho - \frac{2\pi\rho^2}{3k_B T} \int_0^\infty dr r^3 \left( \frac{du}{dr} \right) g(r) \quad \star$$

$g(r)$  depends on  $\rho$  &  $T$

Imagine  $g(r)$  can be written as

$$g(r, \rho) = \sum_{j=0}^{\infty} \rho^j g_j(r) \quad g_j \text{ somehow related to } d^j g / d\rho^j$$

then  $P/k_B T = \rho + \sum_{j=2}^{\infty} B_{j+2} \rho^{j+2}$

$$B_{j+2}(T) = - \frac{2\pi}{3k_B T} \int_0^{\infty} r^3 u'(r) g_j(r, T) dr$$

at small  $\rho$ ,  $\beta P \approx \rho + \rho^2 B_2$

$$B_2 \approx - \frac{2\pi}{3k_B T} \int_0^{\infty} dr r^3 u'(r) g(r)$$

one can show for low  $\rho$ ,  $g(r) \approx e^{-\beta u(r)}$

$$u(r) = -k_B T \log g(r)$$

HW? prob  
4.5

$$\begin{aligned} B_2 &\approx - \frac{2\pi}{3} \int_0^{\infty} dr r^3 \left[ \frac{d}{dr} (g(r)-1) \right] \\ &= \frac{2\pi}{3} \left[ r^3 (g(r)-1) \Big|_0^{\infty} - \int_0^{\infty} 3r^2 (g(r)-1) dr \right] \\ &= -2\pi \int_0^{\infty} r^2 (g(r)-1) dr \end{aligned}$$

$\left\{ \begin{aligned} \frac{dg(r)}{dr} &= -\beta \frac{du(r)}{dr} g(r) \\ \frac{d(g(r)-1)}{dr} &= \frac{dg(r)}{dr} \end{aligned} \right.$

Low  $\rho$ ,  $g(r) = e^{-\beta u(r)}$

