AWBS kinetic modeling of electrons with nonlocal Ohm's law in plasmas relevant to inertial confinement fusion

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A preliminary version... The interaction of lasers with plasmas very often leads to nonlocal transport conditions, where the classical hydrodynamic model fails to describe physical phenomena, such as heat-flow, related to highly mobile particles. In this study the electron distribution in plasma is investigated for the conditions relevant to ICF. In particular, we focus on the transport of nonlocal (supra-thermal) electrons streaming down the temperature gradient in the ablating plasma. Nevertheless, the nature of plasma (ionized gas) requires a correct response of background electrons too. This is achieved by the action of an electric field, which provides a self-consistent Ohms law based on the kinetic modeling. Our approach leans on the Albritton-Williams-Bernstein-Swartz collision operator [1] providing a simple, computationally efficient, transport equation of electrons and is further benchmarked against Vlasov-Fokker-Planck and collisional PIC codes.

I. INTRODUCTION

The first modern attempts at kinetic modeling of plasma can be traced back to the fifties, when Cohen, Spitzer, and Routly (CSR) [2] demonstrated that the effect of Coulomb collisions between electrons and ions in the ionized gas predominantly results from frequently occurring events of cumulative small deflections rather than occasional close encounters. This effect was originally described by Jeans in [3] and Chandrasekhar [4] proposed to use the diffusion equation model of the Vlasov-Fokker-Planck type (VFP) [5].

A classical paper by Spitzer and Harm (SH) [6] provides the computation of the electron distribution func-

tion (EDF) in a plasma (from low to high Z) with a temperature gradient accounting for e-e and e-i collisions. The resulting expressions for current and heat flux are widely used in plasma hydrodynamic models. The distribution function based on the spherical harmonics method in its first approximation (P1) [7] is of the form $f^0 + \mu f^1$, where f^0 and f^1 are isotropic and μ , is the direction cosine between the particle trajectory and some preferred direction in space. It should be emphasized that the SH solution expresses a small perturbation of equilibrium, i.e. that f^0 is the Maxwell-Boltzmann distribution and μf^1 represents a very small anisotropic deviation. This approximation holds for $L_T \gg \lambda_e$, a condition which is often invalid in laser plasmas, where L_T is the temperature length scale and λ_e the mean free path of electrons. It is worth mentioning, that electrons having 3 to 4 times the thermal velocity are dominantly responsible for heat-

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flow and that those faster than 6 times the thermal velocity can be completely neglected in this local theory.

The actual cornerstone of the modern VFP simulations was set in place by Rosenbluth [8], when he derived a simplified form of the VFP equation for a finite expansion of the distribution function, where all the terms are computed according to plasma conditions, including f^0 , which of course needs to tend to the Maxwell-Boltzmann distribution. Consequently, the pioneering work on numerical solution of the VFP equation [9, 10] revealed the importance of the nonlocal electron transport in laser-heated plasmas. In particular, that the heat flow down steep temperature gradients in unmagnetised plasma cannot be described by the classical, local fluid description of transport [6, 11]. This is due to the classical f^1 is not a small deviation (especially for electrons having 3 to 4 times the thermal velocity), i.e. $f^0 \sim f^1$ characterized by $L_T \sim \lambda_e$. It was also shown that a thermal transport inhibition [9] around the peak of the temperature gradient, and a nonlocal preheat ahead of the main heat wave front, naturally appear. These effects are attributed to significant deviations of f^0 from Maxwellian distribution.

Nevertheless, numerical solution of the VFP equation even in the Rosenbluth formalism remains very challenging computationally, because the e-e collision integral is nonlinear. More simple linear forms of e-e collision operator are needed. Although some VFP simulations on experimentally relevant timescales have been performed (for recent examples see [12–18], an extensive review has been conducted by Thomas et al. [19]), their relative computational inefficiency severely limits the range of simulations that can be performed.

It is the purpose of this paper to present an efficient alternative to a full solution of the VFP equation to accurately calculate nonlocal transport, based on the Albritton-Williams-Bernstein-Swartz collision operator (AWBS) [1]. In Section II we propose a modified form of the AWBS collision operator, where its important properties are further presented in Section III with the emphasis on its comparison to the full VFP solution in local diffusive regime. In Section IV we define a full model of electron kinetics and the way of discretizing the electron phase-space and also the coupling of the kinetic model to magneto-hydrodynamics. Section V focuses on the performance of the AWBS transport equation model compared to modern kinetic codes including VFP codes Aladin and Impact [20], and PIC code Calder [21], where the cases related to real laser generated plasma conditions are studied. Finally, the most important outcomes of our research are concluded in Section VI.

II. THE AWBS KINETIC MODEL

The electrons in plasma can be modeled by the deterministic Vlasov model of charged particles

$$\frac{\partial f}{\partial t} + \boldsymbol{v} \cdot \nabla_{\boldsymbol{x}} f + \frac{q_e}{m_e} \left(\boldsymbol{E} + \frac{\boldsymbol{v}}{c} \times \boldsymbol{B} \right) \cdot \nabla_{\boldsymbol{v}} f = C_{ee}(f) + C_{ei}(f),$$
(1)

where $f(t, \boldsymbol{x}, \boldsymbol{v})$ represents the density function of electrons at time t, spatial point \boldsymbol{x} , and velocity \boldsymbol{v} , \boldsymbol{E} and \boldsymbol{B} are the electric and magnetic fields in plasma, q_e and m_e being the charge and mass of electron.

The general form of the e-e collision operator C_{ee} is the Fokker-Planck form published by Landau [22]

$$C_{FP}(f) = \Gamma \int \nabla_{\boldsymbol{v}} \nabla_{\boldsymbol{v}} (\boldsymbol{v} - \tilde{\boldsymbol{v}}) \cdot (f \nabla_{\tilde{\boldsymbol{v}}} f - f \nabla_{\boldsymbol{v}} f) \, d\tilde{\boldsymbol{v}}, \tag{2}$$

where $\Gamma=\frac{4\pi q_e^4 \ln\Lambda}{m_e^2}$ and $\ln\Lambda$ is the Coulomb logarithm. The e-i collision operator C_{ei} could be expressed in a simpler form since massive ions are considered to be motionless compared to electrons during a collision. The scattering operator accounts for the change of electron velocity without change in the velocity magnitude , i.e. angular scattering. It is expressed in spherical coordinates as

$$C_{ei}(f) = \frac{\nu_{ei}}{2} \left(\frac{\partial}{\partial \mu} \left((1 - \mu^2) \frac{\partial f}{\partial \mu} \right) + \frac{1}{1 - \mu^2} \frac{\partial^2 f}{\partial \theta^2} \right), \quad (3)$$

where $\mu=\cos\phi$, ϕ and θ are the polar and azimuthal angles, and $\nu_{ei}=\frac{Zn_e\Gamma}{v^3}$ is the e-i collision frequency.

The e-e collision operator needs to be linearized for efficient computation. Fisch introduced a linear form of C_{ee} in [23] in the high-velocity limit $(v \gg v_{th})$ electron collision operator

$$C_{H}(f) = v\nu_{e} \frac{\partial}{\partial v} \left(f + \frac{v_{th}^{2}}{v} \frac{\partial f}{\partial v} \right) + \frac{\nu_{e}}{2} \left(1 - \frac{v_{th}^{2}}{2v^{2}} \right) \left(\frac{\partial}{\partial \mu} \left((1 - \mu^{2}) \frac{\partial f}{\partial \mu} \right) + \frac{1}{1 - \mu^{2}} \frac{\partial^{2} f}{\partial \theta^{2}} \right),$$
(4)

where $\nu_e = \frac{n_e \Gamma}{v^3}$ is the e-e collision frequency and $v_{th} = \sqrt{\frac{k_B T_e}{m_e}}$ is the electron thermal velocity. The linear form of C_H arises from an assumption that the fast electrons predominantly interact with the thermal (slow) electrons, which is an important simplification to the form (2). However the diffusion term in the e-e collision operator (4) still presents numerical difficulties.

A yet simpler form of the collision operator of electrons was proposed in [24]

$$C_{AWBS}(f) = v\nu_e^* \frac{\partial}{\partial v} (f - f_M) + \frac{\nu_{ei} + \nu_e^*}{2} \left(\frac{\partial}{\partial \mu} \left((1 - \mu^2) \frac{\partial f}{\partial \mu} \right) + \frac{1}{1 - \mu^2} \frac{\partial^2 f}{\partial \theta^2} \right), \quad (5)$$

where $f_M = \frac{n_e}{(2\pi)^{\frac{3}{2}} v_{th}^3} \exp\left(-\frac{v^2}{2v_{th}^2}\right)$ is the Maxwell-Boltzmann equilibrium distribution. Here, the first term representing the AWBS operator [1] accounts for relaxation to equilibrium due to the e-e collisions, and the second term accounts for the e-i and e-e collisions contribution to scattering.

A method of angular momenta for the solution of the electron kinetic equation with the collision operator (5) was introduced in [24, 25].

In (5) we have introduced a modified e-e collision frequency ν_e^* in order to address a proper behavior with respect to Z, which is further analyzed in Section III and promising results compared to the full FP operator are presented.

III. BGK, AWBS, AND FOKKER-PLANCK MODELS IN LOCAL DIFFUSIVE REGIME

An approximate solution to the so-called *local diffusive* regime of electron transport can be found, since the *dif-* fusive regime refers to a low anisotropy given by the projection μ . i.e. modeled by the P1 form of EDF

$$\tilde{f}(z, v, \mu) = f^{0}(z, v) + \mu f^{1}(z, v),$$
 (6)

where z is the spatial coordinate along the axis z, v the magnitude of transport velocity.

The approximate transport solution is then obtained when analyzing the action of the time-steady form of (1) in 1D on the approximation (6) as

$$\mu \left(\frac{\partial \tilde{f}}{\partial z} + \frac{q_e E_z}{m_e v} \frac{\partial \tilde{f}}{\partial v} \right) + \frac{q_e E_z}{m_e} \frac{(1 - \mu^2)}{v^2} \frac{\partial \tilde{f}}{\partial \mu} = \frac{1}{v} C(\tilde{f}), \quad (7)$$

where C is a given collision operator including both e-e and e-i collisions.

The locality of transport is the best expressed in terms of the Knudsen number $Kn=\frac{\lambda}{L},$ where λ is the mean free path of electron and L the characteristic length scale of plasma. Consequently, plasma conditions characterized by $Kn\ll 1$ exhibit a local transport regime. This measure then play a very important role in our analysis, where we use the electron-electron and electronion mean free paths $\lambda_e=Z\lambda_{ei}=\frac{v}{\nu_e},$ and the density and temperature plasma scale lengths $L_{n_e}=n_e/\frac{\partial n_e}{\partial z}$ and $L_{T_e}=T_e/\frac{\partial T_e}{\partial z}.$

In practice, the Knudsen number of thermal electrons is often used as a measure of the locality of transport corresponding to given plasma conditions, where $Kn(v_{th}) < 0.001$ is considered the limit of validity of the local transport theory [26].

A. The BGK local diffusive electron transport

Bhatnagar, Gross, and Krook introduced a very simple form of a collision operator [27]

$$C_{BGK}(\tilde{f}) = \nu_e(f_M - \tilde{f}) + \frac{\nu_{ei} + \nu_e}{2} \frac{\partial}{\partial \mu} (1 - \mu^2) \frac{\partial \tilde{f}}{\partial \mu}.$$
 (8)

In spite of its simple form, BGK collision operator (8) serves as a useful model providing a relevant kinetic response, yet only qualitative with respect to the FP collision operator (2). In particular, the conservation of kinetic energy, momentum, and number of particles is often violated [28].

However, the form of (8) provides a simple analytical treatment of local diffusive transport regime, when used in (7). As a result, one finds a simple form of the BGK isotropic and anisotropic terms of (6) to be

$$f^0 = f_M, (9)$$

$$f^{1} = -\frac{\lambda_{e}}{Z+2} \left(\frac{\partial f_{M}}{\partial z} + \frac{q_{e} E_{z}}{m_{e} v} \frac{\partial f_{M}}{\partial v} \right), \tag{10}$$

where a detailed derivation of (9) and (10) can be found in Appendix A. When the quasi-neutrality constraint imposed by E_L (A8) is used, one finally obtains the analytical BGK form of the anisotropic term

$$f^{1} = -\mu \left(\frac{v^{2}}{2v_{th}^{2}} - 4\right) \frac{1}{Z + 2} \frac{\lambda_{e}}{L_{T_{e}}} f_{M}. \tag{11}$$

The details about the BGK distribution function compared to other collision operators can be found in Section III D.

B. The AWBS local diffusive electron transport

Similarly to the BGK model, the AWBS collision operator 5 explicitly uses equilibration to the Maxwell-Boltzmann distribution f_M . On the other hand, AWBS originates from C_H , which is derived from the full FP operator (2). This makes the AWBS operator to be superior to the BGK operator, which is considered a purely phenomenological model.

If (5) is used in (7), one obtains the following equations governing the AWBS isotropic and anisotropic terms of (6)

$$\frac{\partial f^0}{\partial v} = \frac{\partial f_M}{\partial v},\tag{12}$$

$$\frac{\partial f^1}{\partial v} - \frac{Z + r_A}{v r_A} f^1 = \frac{\lambda_e}{v r_A} \left(\frac{\partial f_M}{\partial z} + \frac{q_e E_z}{m_e v} \frac{\partial f_M}{\partial v} \right), (13)$$

where r_A represents a scaling parameter defining the modified e-e collision frequency as $\nu_e^* = r_A \nu_e$. A detailed derivation of (12) and (13) can be found in Appendix A. Consequently, one finds the AWBS model equation for f^1 in local diffusive regime to be

$$\frac{\partial f_{\text{AWBS}}^1}{\partial v} + \frac{Z + r_A}{v r_A} f_{\text{AWBS}}^1 = \frac{\lambda_e}{v r_A} \left(\frac{1}{L_{n_e}} + \left(\frac{v^2}{2v_{th}^2} - \frac{3}{2} \right) \frac{1}{L_{T_e}} - \frac{q_e E_z}{m_e v_{th}^2} \right) f_M. \quad (14)$$

which can be solved analytically by using quadratures

The details about the AWBS distribution function compared to other collision operators and a proper evaluation of the scaling parameter r_A can be found in Section III D.

C. The Fokker-Planck local diffusive electron transport

The solution to the 1D transport equation (7) using the Fokker-Planck collision operator (2) is very ambitious, as demonstrated in [2, 4, 8], fortunately, one can use the explicit evaluation of the electron distribution function published in [6], which takes the following form

$$f_{\rm SH}^{1} = \frac{v_{2th}^{4}}{\Gamma Z n_{e}} \left(2\tilde{D}_{T} \left(\frac{v}{v_{2th}} \right) + \frac{3}{2} \frac{\gamma_{T}}{\gamma_{E}} \tilde{D}_{E} \left(\frac{v}{v_{2th}} \right) \right) \frac{f_{M}}{T} \frac{\partial T_{e}}{\partial z}, \quad (16)$$

where $\tilde{D}_T(x) = ZD_T(x)/B$, $\tilde{D}_E(x) = ZD_E(x)/A$, γ_T , and γ_E are numerical values in TABLE I, TABLE II, and TABLE III in [6], and $v_{2th} = \sqrt{\frac{k_B T_e}{2m_e}}$.

One should be aware, that the solution of (7) equipped with the full FP collision operator reveals the importance of e-e Coulomb collisions, which is emphasized in the Z dependence of the distribution function, current, heat flux, electric field, etc. In particular, the latter exhibits the following dependence [6]

$$\mathbf{E} = \frac{m_e v_{th}^2}{q_e} \left(\frac{\nabla n_e}{n_e} + \left(1 + \frac{3}{2} \frac{Z + 0.477}{Z + 2.15} \right) \frac{\nabla T_e}{T_e} \right), \quad (17)$$

which for $Z \gg 1$ corresponds to the classical Lorentz electric field (A8).

D. Summary of the BGK, AWBS, and Fokker-Planck local diffusive transport

Ever since the SH paper [6], the effect of microscopic electron transport on the current $\int q_e \boldsymbol{v} \tilde{f} \, d\boldsymbol{v}$ and the heat flux $\int \frac{m_e |\boldsymbol{v}|^2}{2} \boldsymbol{v} \tilde{f} \, d\boldsymbol{v}$ in plasmas under local diffusive conditions has been understood. By overcoming some delicate aspects of the numerical solution to (2) presented

	Z=1	Z=2	Z=4	Z = 16	Z = 116
$ar{\Delta q}_{AWBS}$	0.057	0.004	0.037	0.021	0.004
$\phi(Z)$	-0.037	-0.003	0.04	0.058	0.065

TABLE I. Relative error $\bar{\Delta} q_{AWBS} = |q_{AWBS} - q_{SH}|/q_{SH}$ of the $\nu_e^* = \frac{\nu_e}{2}$ scaling used in the AWBS model (5) showing the discrepancy (maximum 6%) with respect to the original solution of the heat flux given by numerical solution in Spitzer and Harm [6]. The values of $\phi(Z)$ (a weak dependence (23)) are also shown.

in the CSR paper [2], the effect of electron-electron collisions was properly quantified and the correct dependence on Z of the heat flux \boldsymbol{q} was approximated as [6]

$$q = \xi(Z) \ q_L = \frac{Z + 0.24}{Z + 4.2} q_L,$$
 (18)

where ξ is the Z-dependence [29] approximation and q_L is the heat flux given by the Lorentz gas model [30]

$$f_{\text{Lorentz}}^1 = -\mu \left(\frac{v^2}{2v_{th}^2} - 4 \right) \frac{\lambda_{ei}}{L_{T_e}} f_M. \tag{19}$$

In the case of BGK the collision operator (8) needs to be corrected in order to provide a same local behavior as (18), i.e. a correct dependence on Z. Consequently, we define a scaling formula

$$r_B(Z) = \frac{\zeta Z}{\xi(Z + 2\zeta)},\tag{20}$$

based on comparison of the formula (11) to $\xi f_{\rm Lorentz}^1$ and we write a consistent local diffusion version of BGK

$$C_{BGK}(\tilde{f}) = r_B \nu_e(f_M - \tilde{f}) + \frac{r_B}{\zeta} \frac{\nu_{ei} + \zeta \nu_e}{2} \frac{\partial}{\partial \mu} (1 - \mu^2) \frac{\partial \tilde{f}}{\partial \mu}, \tag{21}$$

where the constant ζ can be set arbitrarily, because it does not affect the local EDF of (21)

$$f_{\text{BGK}}^1 = -\mu \left(\frac{v^2}{2v_{th}^2} - 4\right) \frac{\zeta}{r_B(Z)} \frac{1}{Z + 2\zeta} \frac{\lambda_e}{L_{T_e}} f_M,$$
 (22)

which is identical to ξf_{Lorentz}^1 for any value of ζ . One should notice that $r_B(Z\gg 1)=\zeta$, i.e. ζ can be adjusted appropriately for example to better address the transport in nonlocal regime.

We have performed an extensive analysis in the case of the AWBS operator in order to obtain the heat flux behavior while varying Z. As expected, the heat flux magnitude did not match exactly the Z-dependence (18), e.g. for Z=1 the AWBS heat flux was about 60% less

than the SH calculation, while there was a perfect match in the case of $Z \gg 1$. By assuming that the e-e collisions are responsible for this inadequacy, we searched for a scaling of ν_e in (5). Interestingly, we found an almost constant scaling r_A , i.e. with a very weak dependence on Z as

$$\nu_e^* = r_A(Z) \ \nu_e = \left(\frac{1}{2} + \phi(Z)\right) \nu_e \approx \frac{\nu_e}{2},$$
 (23)

where can be approximated as $\phi(Z) = \frac{0.59Z - 1.11}{8.37Z + 5.15} \ll \frac{1}{2}$ for any Z, i.e. we decide to use $r_A = \frac{1}{2}$. Indeed, TABLE I shows $\phi(Z)$ and corresponding relative error (maximum 6%) of the heat flux modeled by (5) vs. SH results represented by (18). It should be noted that the error is calculated with respect to original values presented in TABLE III in [6]. It is worth mentioning, that the zero current condition was imposed in all AWBS calculations, where the consistent electric field yield an equal value to the classical Lorentz value (A8) for any Z.

Nevertheless, the electron-electron collisions scaling [29] represented by (18) provides only an integrated information about the heat flux magnitude. If one takes a closer look at the distribution function itself, the conformity of the modified AWBS collision operator is even more emphasized as can be seen in FIG. 1 showing the flux moment in spherical coordinates of velocity

$$q_1 = \frac{m_e v^2}{2} v f^1 v^2. (24)$$

In the case of the high Z plasma (Z=116), AWBS exactly aligns with the Lorentz gas limit (19). In the opposite case of the low Z Hydrogen plasma (Z=1), the AWBS distribution function approaches closely the numerical SH solution (16). BGK (21) takes the Lorentz gas distribution function for any Z only scaled by ξ . The AWBS collision operator (5) (red dashed line) represented by a derivative with respect to v provides a significant improvement with respect to the SH (Fokker-Planck) solution (16) (solid black line) compared to the simplest BGK model (22) (dashed-dot blue line) in FIG. 1.

IV. THE AWBS NONLOCAL TRANSPORT MODEL OF ELECTRONS

In order to define a nonlocal transport model of electrons, we use the AWBS collision operator and the P1 angular discretization of the electron distribution function

$$\tilde{f}(\boldsymbol{x}, \boldsymbol{n}, v) = f_0(\boldsymbol{x}, v) + \boldsymbol{n} \cdot \boldsymbol{f_1}(\boldsymbol{x}, v),$$
 (25)

consisting of the isotropic part represented by the zeroth angular moment $f_0 = \frac{1}{4\pi} \int_{4\pi} \tilde{f} d\mathbf{n}$ and the directional part represented by the first angular moment $\mathbf{f_1} = \frac{3}{4\pi} \int_{4\pi} \mathbf{n} \tilde{f} d\mathbf{n}$, where \mathbf{n} is the transport direction. Then,

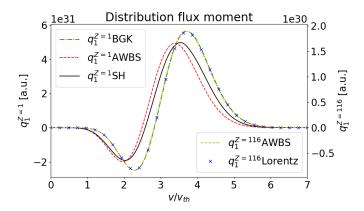


FIG. 1. The flux velocity moment of the anisotropic part of the electron distribution function in low Z=1 and high Z=116 plasmas in diffusive regime. In the case of Z=1 the AWBS model matches very well the reference solution given by the SH calculation [6] in comparison to the BGK model. In the case of Z=116 the AWBS model aligns exactly with the Lorentz gas approximation as expected. The BGK and the SH curves are not shown for Z=116, but also correspond to the Lorentz gas distribution function.

the first two angular moments [28] applied to the stationary form of (1) with collision operator (5) (extended by (23)) lead to the model equations

$$v\frac{\nu_e}{2}\frac{\partial}{\partial v}\left(f_0 - f_M\right) = \frac{v}{3}\nabla \cdot \mathbf{f_1} + \frac{q_e}{m_e}\frac{\mathbf{E}}{3} \cdot \left(\frac{\partial \mathbf{f_1}}{\partial v} + \frac{2}{v}\mathbf{f_1}\right),\tag{26}$$

$$v\frac{\nu_e}{2}\frac{\partial \mathbf{f_1}}{\partial v} - \nu_{scat}\mathbf{f_1} = v\nabla f_0 + \frac{q_e}{m_e}\mathbf{E}\frac{\partial f_0}{\partial v} + \frac{q_e\mathbf{B}}{m_ec} \times \mathbf{f_1},$$
(27)

where $\nu_{scat} = \nu_{ei} + \frac{\nu_e}{2}$. The system of equations (26) and (27) is called the **AP1 model** (AWBS + P1).

The AP1 model gives us information about the electron distribution function providing a bridge between kinetic and fluid description of plasma. For example the *flux* quantities as electric current and heat flux due to the motion of electrons

$$\mathbf{j} = \frac{4\pi}{3}q_e \int v \mathbf{f_1} v^2 dv, \quad \mathbf{q}_h = \frac{4\pi}{3} \frac{m_e}{2} \int v^3 \mathbf{f_1} v^2 dv,$$

where $d\tilde{v} = v^2 dv$ the spherical coordinates metric, are based on corresponding velocity moments (integrals) of the first angular moment of EDF. Consequently, the explicit formula for the first angular moment from (27) proves to be extremely useful

$$f_1 = \frac{\nu_{scat}^2 \mathbf{F}^* + \omega_B \ \omega_B \cdot \mathbf{F}^* - \nu_{scat} \ \omega_B \times \mathbf{F}^*}{\nu_{scat}(\omega_B^2 + \nu_{scat}^2)}, \quad (28)$$

because it provides a valuable information about the dependence of macroscopic flux quantities on electric and magnetic fields in plasma, where $\omega_B = \frac{q_e B}{m_e c}$ is the electron gyro-frequency and $\mathbf{F}^* = v \frac{\nu_e}{2} \frac{\partial \mathbf{f_1}}{\partial v} - v \nabla f_0 - \frac{q_e}{m_e} \mathbf{E} \frac{\partial f_0}{\partial v}$.

A. Nonlocal Ohm's Law

The expression (28) becomes extremely useful when used to describe the electron fluid momentum, i.e. the current velocity moment can be written as

$$\mathbf{j}_{(f,\mathbf{E},\mathbf{B})} = \mathbf{J}_{Ohm} \frac{\partial f_0}{\partial v} \mathbf{E} + \frac{m_e}{q_e} \mathbf{J}_{Ohm} \left(v \nabla f_0 - v \frac{\nu_e}{2} \frac{\partial \mathbf{f_1}}{\partial v} \right),$$
(29)

where we used the following notation $\mathbf{J}_{Ohm} \mathbf{g} = -\frac{4\pi q_e^2}{3m_e} \int v \frac{\nu_{scat}^2 \mathbf{g} + \omega_B}{\nu_{scat}(\omega_B^2 + \nu_{scat})} v^2 \mathrm{d}v$ showing how the operator \mathbf{J}_{Ohm} acts on a general vector field \mathbf{g} . We refer to (29) as to the **nonlocal Ohm's law**. The need for a nonlocal Ohm's law to accurately capture magnetic field advection by the Nernst effect has previously been demonstrated [13, 31, 32], although a full investigation of how well our new Ohm's law captures this is beyond the scope of this article. The proper high Z ($\nu_e \ll \nu_{ei}$) local asymptotic to the standard Ohm's law can be found when $f_0 \to f_M$ and weak magnetization ($\omega_B \ll \nu_{ei}$) is considered. Then (29) simplifies to

$$\mathbf{j} = -\frac{q_e^2}{m_e} \int \frac{v^3}{\nu_{ei}} \left(\mathbf{E} \frac{\partial f_M}{\partial v} + \frac{m_e}{q_e} v \nabla f_M \right) dv =
\frac{16\sqrt{\frac{2}{\pi}} q_e^2 k_B^{\frac{3}{2}} T_e^{\frac{3}{2}}}{m_e^{\frac{5}{2}} \Gamma Z} \left[\mathbf{E} - \frac{\frac{5}{2} n_e k_B \nabla T_e + \nabla n_e k_B T_e}{q_e n_e} \right], \quad (30)$$

which can be directly compared to the local fluid theory

$$\boldsymbol{E} = \sigma(f_0)^{-1} \boldsymbol{j} - \frac{\nabla P(f_0)}{q_e n_e} \xrightarrow{f_0 \to f_M} \boldsymbol{E}_l = \frac{\boldsymbol{j}}{\sigma_l} + \frac{\nabla p_e - \boldsymbol{R}_{T_e}}{q_e n_e}$$
(31)

while addressing properly the local electric field E_l given by the pressure $p_e = n_e k_B T_e$, the thermal force $R_{T_e} = -\frac{3}{2} n_e k_B \nabla T_e$ and the local electrical conductivity $\sigma_l = 16 \sqrt{\frac{2}{\pi}} q_e^2 k_B^{\frac{3}{2}} T_e^{\frac{3}{2}} / m_e^{\frac{5}{2}} \Gamma Z$ [11]. In (31) we defined the non-local electrical tensor conductivity

$$\sigma = \mathbf{J}_{Ohm} \frac{\partial f_0}{\partial v},\tag{32}$$

and the nonlocal microscopic force

$$\nabla P = \sigma^{-1} m_e n_e \mathbf{J}_{Ohm} v \nabla f_0, \tag{33}$$

based on (29).

The local dependence of the AP1 current (30) on electric field and gradients of n_e and T_e clearly demonstrates, that (31) is a local version of (29). This also implies that (29) provides a very important physics related to the magnetic field source in terms of nonlocal Biermann battery, since the curl on the electric field (31) gives

$$\nabla \times \frac{\nabla P}{q_e n_e} \xrightarrow{f_0 \to f_M} \nabla \times \frac{\nabla p_e - \mathbf{R}_{T_e}}{q_e n_e} = \frac{k_B}{q_e n_e} \nabla T_e \times \nabla n_e.$$
(34)

The nonlocal Biermann battery equivalent (34) can lead to a spontaneous magnetic field generation under uniform density plasma profile as has been shown in [33].

A local version of the **nonlocal Ohm's law** (29) compared to the *generalized Ohm's law* (31) when a magnetic field is applied would require a much more delicate analysis and we leave it as a future complementary work.

B. AWBS Nonlocal Magneto-Hydrodynamics

The AWBS nonlocal magneto-hydrodynamic model (Nonlocal-MHD) refers to two temperature single-fluid hydrodynamic model extended by a kinetic model of electrons using the AWBS transport equation, which provides a direct coupling between hydrodynamics and Maxwell equations.

Mass, momentum density, and total energy ρ , $\rho \boldsymbol{u}$, and $E = \frac{1}{2}\rho\boldsymbol{u}\cdot\boldsymbol{u} + \rho\varepsilon_i + \rho\varepsilon_e$, where ρ is the density of plasma, \boldsymbol{u} the plasma fluid velocity, ε_i the specific internal ion energy density, and ε_e the specific internal electron energy density, are modeled by the Euler equations in the Lagrangian frame [34, 35]

$$\frac{\mathrm{d}\rho}{\mathrm{d}t} = -\rho\nabla\cdot\boldsymbol{u},\tag{35}$$

$$\rho \frac{\mathrm{d}\boldsymbol{u}}{\mathrm{d}t} = -\nabla(p_i + p_e) + \boldsymbol{j}_{(f,\boldsymbol{E},\boldsymbol{B})} \times \boldsymbol{B}, \qquad (36)$$

$$\rho C_{V_i} \frac{\mathrm{d}T_i}{\mathrm{d}t} = \left(\rho^2 C_{T_i} - p_i\right) \nabla \cdot \boldsymbol{u} - G(T_i - T_e), \quad (37)$$

$$\rho C_{V_e} \frac{\mathrm{d}T_e}{\mathrm{d}t} = \left(\rho^2 C_{T_e} - p_e\right) \nabla \cdot \boldsymbol{u} + G(T_i - T_e) -\nabla \cdot \boldsymbol{q}_{h(f, \boldsymbol{E}, \boldsymbol{B})} + Q_{\mathrm{IB}},$$
(38)

where T_i is the temperature of ions, T_e the temperature of electrons, p_i the ion pressure, p_e the electron pressure, q_h the heat flux, $Q_{\rm IB}$ the inverse-bremsstrahlung laser absorption (which can also distort the distribution function away from a Maxwellian [36], strongly modifying the transport [37], an effect which will not be considered further here) and $G = \rho C_{V_e} \nu_{ei}$ is the ion-electron energy exchange rate. The thermodynamic closure terms p_e , p_i , $C_{V_i} = \frac{\partial \varepsilon_i}{\partial T_i}$, $C_{T_i} = \frac{\partial \varepsilon_i}{\partial \rho}$, $C_{V_e} = \frac{\partial \varepsilon_e}{\partial T_e}$, $C_{T_e} = \frac{\partial \varepsilon_e}{\partial \rho}$ are obtained from an equation of state (EOS), e.g. the SESAME equation of state tables [38, 39].

The magnetic and electric fields are modeled by Maxwell equations

$$\frac{1}{c}\frac{\partial \mathbf{B}}{\partial t} = -\nabla \times \mathbf{E},\tag{39}$$

$$\frac{1}{c}\frac{\partial \mathbf{E}}{\partial t} = \nabla \times \mathbf{B} - \frac{4\pi}{c}\mathbf{j}_{(f,\mathbf{E},\mathbf{B})},\tag{40}$$

where the initial state of \boldsymbol{B} and \boldsymbol{E} obeys the Gauss's law. We have explicitly written the current and heat flux as dependent on electron kinetics, represented by the electron distribution function f, and electric and magnetic fields. In principal, $\boldsymbol{j}_{(f,\boldsymbol{E},\boldsymbol{B})}$ and $q_{h(f,\boldsymbol{E},\boldsymbol{B})}$ can be referred to as the *kinetic closure* and is provided by the **AP1** model (26) and (27).

C. Numerical Implementation of the AWBS Electron Kinetics

It is well known, that as the electron transport exhibits a quasi-steady behavior, the same holds for the electric field in (40) on the time scale of the fluid. Consequently, Ampere's law (40) takes a quasi-steady form $\frac{4\pi}{c} j_{(f,E,B)} = \nabla \times \mathbf{B}$ when used in hydrodynamics. Proceeding further, one can make use of the **nonlocal Ohm's law** (29) to write a fully kinetic form of Ampere's law governing the electric field \mathbf{E}

$$\mathbf{J}_{Ohm} \frac{\partial f_0}{\partial v} \mathbf{E} + \frac{m_e}{q_e} \mathbf{J}_{Ohm} v \nabla f_0 = \frac{c}{4\pi} \nabla \times \mathbf{B}. \tag{41}$$

In order to solve the kinetics of electrons, we adopt a high-order finite element discretization [40, 41] of the model equations (26), (27), (41)

$$\mathbf{M}_{(\frac{v\nu_{e}}{2})}^{L_{2}} \cdot \frac{\mathrm{d}\boldsymbol{f_{0}}}{\mathrm{d}v} - \mathbf{V}_{(\frac{q_{e}\boldsymbol{E}}{3m_{e}})}^{L_{2}} \cdot \frac{\mathrm{d}\boldsymbol{f_{1}}}{\mathrm{d}v} = \mathbf{D}_{(\frac{v}{3})}^{L_{2}} \cdot \boldsymbol{f_{1}} + \mathbf{M}_{(\frac{2q_{e}\boldsymbol{E}}{3m_{e}v})}^{L_{2}} \cdot \boldsymbol{f_{1}} + \mathbf{b}_{(\frac{2q_{e}\boldsymbol{E}}{3m_{e}v})}^{L_{2}}, \qquad (42)$$

$$\mathbf{M}_{(\frac{v\nu_{e}}{2})}^{H_{1}} \cdot \frac{\mathrm{d}\boldsymbol{f_{1}}}{\mathrm{d}v} - \mathbf{V}_{(\frac{q_{e}\boldsymbol{E}}{m_{e}})}^{H_{1}} \cdot \frac{\mathrm{d}\boldsymbol{f_{0}}}{\mathrm{d}v} = \mathbf{G}_{(v)}^{H_{1}} \cdot \boldsymbol{f_{0}} + \mathbf{M}_{(\nu_{scat})}^{H_{1}} \cdot \boldsymbol{f_{1}} + \mathbf{C}_{(\frac{q_{e}\boldsymbol{B}}{m_{e}v}\boldsymbol{X})}^{H_{1}} \cdot \boldsymbol{f_{1}}, \qquad (43)$$

$$\mathbf{J}_{(\frac{\partial f_{0}}{\partial v})}^{ND} \cdot \boldsymbol{E} = \mathbf{J}\mathbf{G}_{(\frac{m_{e}v}{q_{e}})}^{ND} \cdot \boldsymbol{f_{0}} + \boldsymbol{b}_{(\frac{c}{4\pi}\nabla\boldsymbol{X}\boldsymbol{B})}^{ND}, \qquad (44)$$

where the continuous differential operators are represented by standard discrete analogs (matrices of bilinear forms) $\mathbf{M}, \mathbf{G}, \mathbf{D}, \mathbf{V}, \mathbf{C}$, i.e. mass, gradient, divergence, vector field dot product, and vector field curl, and by $\mathbf{J}, \mathbf{J}\mathbf{G}$ matrices specific to **nonlocal Ohm's law** (29). The linear form \mathbf{b} represents sources, i.e. temperature T_e via $\frac{\partial f_M}{\partial v}$ and the curl of the magnetic field \mathbf{B} . These finite element discrete analogs are defined on piece-wise continuous L_2 finite element space (domain of f_0), continuous H_1 finite element space (domain of f_1) [40], and Nedelec finite element space (domain of f_1). We do not show their definitions since it is out of the scope of this article.

The strategy of solving (42) and (43) resides in integrating $\frac{\mathrm{d}f_0}{\mathrm{d}v}$ and $\frac{\mathrm{d}f_1}{\mathrm{d}v}$ along the velocity magnitude. This is done by starting the integration from the maximum velocity ($v=7v_{th}^{max}$ is a sufficiently high limit) to zero velocity using the Implicit Runge-Kutta method. The value v_{th}^{max} equals the electron thermal velocity corresponding to the maximum electron temperature in the current profile of plasma. It should be noted, that the backward integration concept is crucial for the model, since it corresponds to the deceleration of electrons due to collisions [42]. Consequently, we refer to decelerating AP1 model, which however, leads to the limitation of the electric field described in Appendix B.

V. BENCHMARKING THE AWBS NONLOCAL TRANSPORT MODEL

Having shown several encouraging properties of the AWBS transport equation defined by (5) under local diffusive conditions in Section III, this section focuses on analyzing its behavior under nonlocal plasma conditions, extensively investigated in numerous publications [9, 24, 26, 43–46]. A variety of tests suitable for benchmarking the nonlocal electron transport models have been published [24, 25, 29, 47–49], we focus on conditions relevant to inertial confinement fusion plasmas generated by lasers.

We show results of our implementation of the AP1 nonlocal transport model presented in Section IV benchmarked against simulation results provided by a rather complete set of kinetic models with varying complexity. The most reliable models represents a collisional Particle-In-Cell code Calder [21, 50] resolving the plasma frequency time scale, and a standard VFP codes Aladin and Impact [20]. In addition, we compare the SNB nonlocal transport model [51] used in hydrodynamic codes. That is a first time when a collisional PIC code is used for benchmarking of nonlocal electron transport models.

Calder PIC code

The particle evolution in the phase-space, including small angle binary collisions, is described with the Maxwell equations (39), (40) coupled with the ion and electron Vlasov equations with the Landau-Beliaev-Budker collisions integral (LBB) [22, 52]

$$\frac{\partial f_{\alpha}}{\partial t} + \mathbf{v} \cdot \nabla_{\mathbf{x}} f_{\alpha} + q_{\alpha} \left(\mathbf{E} + \mathbf{v} \times \mathbf{B} \right) \nabla_{\mathbf{p}} f_{\alpha} = C_{LBB}(f_{\alpha}, f_{\alpha}) + \sum_{\beta} C_{LBB}(f_{\alpha}, f_{\beta}). \quad (45)$$

The LBB collision integral takes the form

$$C_{LBB}(f_{\alpha}, f_{\beta}) = -\frac{\partial}{\partial \mathbf{p}} \cdot \frac{\Gamma_{\alpha\beta}}{2} \left[\int \mathbf{U}(\mathbf{p}, \mathbf{p}') \cdot (f_{\alpha} \nabla_{\mathbf{p}'} f_{\beta}' - f_{\beta}' \nabla_{\mathbf{p}} f_{\alpha}) \right] d^{3} \mathbf{p}',$$
(46)

where its relativistic kernel reads $\mathbf{U}(\mathbf{p}, \mathbf{p}') = \frac{r^2/\gamma\gamma'}{(r^2-1)^{3/2}}$ $\left[(r^2-1)\mathbf{I} - \mathbf{p} \otimes \mathbf{p} - \mathbf{p}' \otimes \mathbf{p}' + r(\mathbf{p} \otimes \mathbf{p}' + \mathbf{p}' \otimes \mathbf{p})\right]$ with $\gamma = \sqrt{1+\mathbf{p}^2}$, $\gamma' = \sqrt{1+\mathbf{p}'^2}$ and $r = \gamma\gamma' - \mathbf{p} \cdot \mathbf{p}'$. The momentum \mathbf{p}_{α} (\mathbf{p}_{β}) is normalized to $m_{\alpha}c$ (resp. $m_{\beta}c$). The collision operator (46) tends to (2) in the non-relativistic limit. The aforementioned model is solved in 3D by the PIC code CALDER. [21, 50].

Impact and Aladin VFP codes

PIC simulations are extremely expensive as the collisions require description of the velocity space in 3 dimensions. Yet, a reduction of dimensions can be done by developing the distribution function in a Cartesian tensor series, equivalent to expansion in the spherical harmonics [53]. The first order form corresponds to

the P1 approximation (25) and coupled with the Landau-Fokker-Planck collisional operator (2) leads to the P_1 -VFP model [20, 53]:

$$\frac{\partial f_0}{\partial t} + \frac{v}{3} \nabla \cdot \mathbf{f_1} + \frac{q_e}{3m_e v^2} \frac{\partial}{\partial v} (v^2 \mathbf{E} \cdot \mathbf{f_1}) = C_{ee}^0(f_0), (47)$$

$$\frac{\partial \mathbf{f_1}}{\partial t} + v \nabla f_0 + \frac{q_e \mathbf{E}}{m_e} \frac{\partial f_0}{\partial v} + \frac{q_e \mathbf{B}}{m_e} \times \mathbf{f_1} = -\nu_{ei} \mathbf{f_1}. (48)$$

where only the isotropic part of the distribution function in in the e-e collision integral (2) is used as the following

$$C_{ee}^{0}(f_{0}) = \frac{\Gamma}{v^{2}} \frac{\partial}{\partial v} \left[C(f_{0})f_{0} + D(f_{0}) \frac{\partial f_{0}}{\partial v} \right], \quad (49)$$

$$C(f_{0}(v)) = 4\pi \int_{0}^{v} f_{0}(u)u^{2} du,$$

$$D(f_{0}v)) = \frac{4\pi}{v} \int_{0}^{v} u^{2} \int_{u}^{\infty} w f_{0}(w) dw du.$$

The codes Impact and Aladin solve the system (47) and (48) with the Maxwell equations (39) and (40) in two spatial dimensions, assuming immobile ions.

The model AP1 uses similar equations as Aladin and Impact with the difference, that AP1 describes the steady-state electron distribution function with respect to the ions, and is using a simplified (linear) collision operator inherently coupled to ions via the hydrodynamic equations.

SNB approach

Now considered as a standard nonlocal electron transport models in hydrodynamic codes, SNB [51] represents an efficient P1 method based on the velocity dependent form of the collision BGK operator. It uses EDF approximation representing deviation from the local BGK theory

$$\tilde{f} = f_M + \delta f_0 + \boldsymbol{n} \cdot (\boldsymbol{f_1}_M + \delta \boldsymbol{f_1}). \tag{50}$$

Equations for the zero and first angular moments follow from the electron transport equation with scaled collision operator (21) according to the SNB approximation (50) (similar to (26) and (27))

$$r_{B}\delta f_{0} = -\frac{v}{3}\nabla \cdot \delta \mathbf{f_{1}} - \frac{v}{3}\nabla \cdot \mathbf{f_{1}}_{M}$$

$$-\frac{q_{e}}{m_{e}} \frac{\mathbf{E}}{3} \cdot \left(\frac{\partial \mathbf{f_{1}}_{M}}{\partial v} + \frac{\partial \delta \mathbf{f_{1}}}{\partial v} + \frac{v}{v} \cdot (\mathbf{f_{1}}_{M} + \delta \mathbf{f_{1}})\right),$$

$$\frac{v_{ei}}{\xi} \delta \mathbf{f_{1}} = -v\nabla \delta f_{0} - \frac{q_{e}}{m_{e}} \mathbf{E} \frac{\partial \delta f_{0}}{\partial v}$$

$$-\frac{v_{ei}}{\xi} \mathbf{f_{1}}_{M} - v\nabla f_{M} - \frac{q_{e}}{m_{e}} \mathbf{E} \frac{\partial f_{M}}{\partial v},$$

$$= 0 \text{ defines } \mathbf{f_{1}}_{M}$$

$$(52)$$

where the magnetic field was neglected, the under-braced part of (52) when δf_0 and δf_1 are zero defines the local

anisotropic term

$$\mathbf{f_{1}}_{M} = -\xi \lambda_{ei} f_{M} \left(\frac{\nabla n_{e}}{n_{e}} + \left(\frac{v^{2}}{2v_{th}^{2}} - \frac{3}{2} \right) \frac{\nabla T_{e}}{T_{e}} - \frac{q_{e} \mathbf{E}}{m_{e} v_{th}^{2}} \right), \tag{53}$$

and the efficiency of SNB resides in omitting the electric field effect (crossed out terms in (51) and (52)), which leads to a simple diffusion equation for the correction to the isotropic part of the distribution function

$$\frac{1}{\lambda_e^{SNB}} \delta f_0 - \nabla \cdot \frac{\lambda_{ei}^{SNB}}{3} \nabla \delta f_0 = \nabla \cdot \frac{\xi \lambda_{ei}}{3} f_M \frac{\nabla T_e}{T_e}, \quad (54)$$

where $\frac{1}{\lambda_{ei}^{SNB}} = \frac{\nu_{ei}}{\xi v} + \frac{|q_e E|}{\frac{1}{2} m_e v^2}$ and $\lambda_e^{SNB} = \frac{v}{r_B \nu_e}$, and the source term based on f_{1M} simplifies by avoiding the electric field effect, density gradient and the v-dependent bracket in (53). The missing effect of E in (54) is accounted for by an isotropic scattering in definition of λ_{ei}^{SNB} [51]. Consequently, the effect of the electric field in SNB is accounted for only via f_{1M} , where the electric field is fixed to E_L .

As shown previously, the BGK collision operator (21) provides one free parameter ζ . We propose to use $\zeta=2$ giving $r_B(Z\gg 1)=2$ which agrees with r=2 in SNB formulation proposed in [49] for the case of ICF relevant plasma. We also have $r_B(Z=1)=1.677$, which means that our pure kinetic derivation of SNB varies just slightly from a constant value $r_B=2$ [49], yet it provides slightly better results. The explicit form of the anisotropic part of EDF then reads $f_1=f_{1M}-\lambda_{ei}^{SNB}\nabla\delta f_0$.

A. Heat-bath problem

AP1 is compared to Calder, Aladin, Impact, and SNB by calculating the heat flow in the case of a homogeneous plasma with a large temperature variation

$$T_e(z) = 0.575 - 0.425 \tanh((z - 450)s),$$
 (55)

which exhibits a steep gradient at the point 450 μ m connecting a hot bath ($T_e = 1 \text{ keV}$) and cold bath ($T_e = 0.17 \text{ keV}$) and s is the parameter of steepness. This test is referred to as a simple non-linear heat-bath problem and originally was introduced in [47] and further investigated in [24, 25, 48, 49].

The total computational box size is 700 μ m. We performed Aladin, Impact, and Calder simulations showing an evolution of temperature starting from the initial profile (55). Due to the initial distribution function being approximated by a Maxwellian, the first phase of the simulation exhibits a transient behavior of the heat flux. After several ps the distribution adjusts properly to its asymptotic form and the heat flux profiles can be usefully compared. We then take the temperature profiles from Aladin/Impact/Calder and compare with AP1 and SNB models which calculate a stationary heat flow for a given

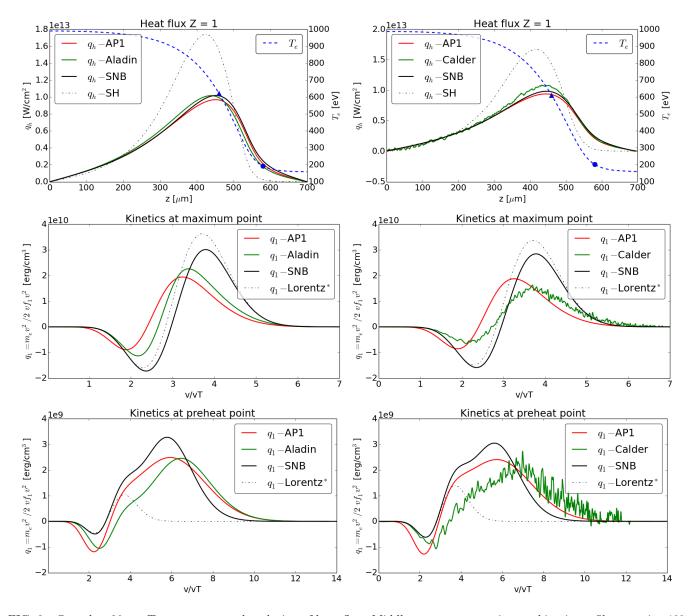


FIG. 2. Snapshot 20 ps. Top: correct steady solution of heat flux. Middle: correct comparison to kinetic profiles at point 460 μ m by Aladin and Calder. Velocity limit 4.2/4.3 v_{th} at temperature 622.4/611.3 eV. Bottom: correct comparison to kinetic profiles at point 580 μ m by Aladin. Velocity limit 9.1/8.5 v_{th} at temperature 192.3/202.4 eV.

temperature profile. For all heat-bath simulations the electron density, Coulomb logarithm and ionisation were kept constant and uniform. The Coulomb logarithm was held fixed throughout, $\ln\Lambda=7.09$.

We show AP1 results for two ionization states, namely Z=1,10 in FIG. 2 and FIG. 3, respectively, corresponding to a moderate nonlocality (Kn^e $\sim 10^{-2}$) leading to a roughly 40 % inhibition compared to the local SH heat flux maximum. The original temperature profile steepness $s=1/50\mu {\rm m}$. It is preferable to use Kn^e = $\frac{\lambda_e}{\sqrt{Z+1}L_{T_e}}$ instead of Kn = $\frac{\lambda_{ei}}{L_{T_e}}$, because $\sqrt{Z+1}$ provides a better scaling of nonlocality with respect to ionization [26], i.e. the flux inhibition and Kn^e are kept approximately

the same when varying Z in FIG. 2 and FIG. 3. In addition to the heat flux profiles, we also show the distribution function details related to the approximate point of the heat flux maximum (460 μ m) and to the point of the nonlocal preheat effect (580 μ m) in the form of the flux moment of EDFs anisotropic part (24). The nonlocal preheat effect shows a very good agreement with previous results published in [48].

The top left plot of FIG. 2 shows heat flux profiles computed by Aladin, AP1, and SNB corresponding to the temperature T_e profile computed by Aladin and the top right plot of FIG. 2 shows heat flux profiles computed by Calder, AP1, and SNB corresponding to the temperature T_e profile computed by Calder. Both

kinetic simulations by Aladin and Calder evolved up to 20 ps for Z=1. The anisotropic part of EDF, in particular the heat flux velocity moment q_1 , at the heat flux maximum (triangle point) and at the nonlocal preheat region (circle point) computed by AP1 and SNB, and by Aladin and Calder are shown in the middle. The AP1 EDF profiles provide a reasonable match to the reference green line EDF by Aladin on the left. It should be noted, that the difference in q_1 resembles to the low Ztrend shown in FIG. 1 where AP1 corresponds to AWBS and Aladin to BGK curve. This may suggest that AP1 tends to compute better kinetics in this low Z case then the isotropic collision operator (49) used by Aladin and Impact. In general, Calder exhibits a lack of return current (negative part of q_1), i.e. the electron number is not exactly conserved. This probably arises from the nature of the Monte Carlo method used to solve (46) and its sensitivity to Gauss law of charge conservation.

In the top plot of FIG. 3 we show heat flux profiles computed by Aladin, AP1, and SNB corresponding to the temperature T_e profile computed by Aladin up to 12 ps for Z = 10. Corresponding profiles of a selfconsistently calculated electric fields by Aladin and AP1 (using the nonlocal Ohm's law) are shown in the higher middle plot. Also the local theory based electric field E_L used by SNB is shown. The EDFs q_1 at the point of the approximate heat flux maximum (triangle) of the temperature profile is shown in the lower middle plot, where a very precise match between AP1 and Aladin can be observed, and q_1 at the preheat point (circle) of the temperature profile is shown in the bottom plot. In the latter case AP1 shows a very similar properties as Aladin with a difference in magnitude corresponding to a higher heat flux computed by AP1 at this point.

SNB shows very good results of the heat flux profile in all three cases, i.e. compared to Aladin and Calder in FIG. 2 and to Aladin in FIG. 3. However, one can observe that the EDF kinetic solution of SNB provides only a qualitative image with respect to the reference green line solution. This is illustrated for example in FIG. 3, where the kinetics at preheat point plot reveals an insufficient electric field treatment (no return current). The kinetics at maximum point plot shows that the solution SNB solution approaches closely the local Lorentz* solution and that significantly recedes from the reference fully kinetic solution (green line). These discrepancies can be attributed to the use of an inconsistent electric field in the case of SNB which uses E_L . An electric field comparison is shown in FIG. 3, where it is shown that the local electric field treatment E_L used in SNB fails in the preheat region and consequently leads to a significant violation of the plasma quasi-neutrality, i.e. a non-zero current, where one can observe an uncontrolled stream of electrons in the preheat and also an overestimation of negative return current around the heat flux maximum.

The AP1 model equations (26), (27), and (41) in general show a very good performance in all three cases when compared to the fully kinetic results (green line) by Al-

Kn^e	10^{-4}	10^{-3}	10^{-2}	10 ⁻¹	1
v_{lim}/v_{th}	70.8	22.4	7.3	3.1	1.8

TABLE II. Scan over varying nonlocality (Kn^e) showing the limit of the collision friction dominance over the deceleration of electrons due to the electric field force. The electric field effect is dominant for electrons with higher velocity than v_{lim} defined in (56). Kn^e and v_{th} are evaluated from the same plasma profiles.

adin and Calder, which can be assigned to the consistent treatment of \boldsymbol{E} via nonlocal Ohm's law (29) in (41) (no \boldsymbol{B} field in 1D).

In addition, the Knudsen number Kn^e has been varied among the simulation runs in order to address a broad range of nonlocality of the electron transport corresponding to the laser-heated plasma conditions, i.e. $\mathrm{Kn}^e \in (0.0001,1)$. The variation of Kn^e arises from the variation of the uniform electron density $n_e \in (10^{19},10^{23})$ cm⁻³ or the length scale given by the slope of the temperature profile $s \in (1/2500,1/25)\mu\mathrm{m}$. Results showing the heat flux maximum of an extensive set of simulations of varying Kn^e is shown in FIG. 4.

When analyzing the simulation results shown in FIG. 4, we observed that the maximum of q_1 at the maximum point tends to decrease with increasing Kn^e and that the interval of electron velocities important for the heat transport always belongs to $3v_{th} < v < 4v_{th}$ for an example refer to the kinetics at maximum point in FIG. 2 and FIG. 3. We have also found an important observation related to the electron-electron collisions. The force acting on electrons is dominated by electric field above the velocity limit

$$v_{lim} = \sqrt{\frac{\sqrt{3}\Gamma m_e}{2q_e} \frac{n_e}{|E|}},\tag{56}$$

and this limit drops down significantly with increasing Knudsen number as can be seen in TABLE II. As a consequence, the electrons responsible for the heat flux $(3v_{th} < v < 4v_{th})$ are preferably affected by the electric field rather than by collisions when $\mathrm{Kn}^e > 10^{-1}$. According to TABLE II collsions dominate stopping for $v < 3.1v_{th}$ when $\mathrm{Kn}^e = 10^{-1}$ and even a much lower value $v < 1.8v_{th}$ when $\mathrm{Kn}^e = 1.0$. This explains the unsatisfactory results of the decelerating AP1 model for high Kn^e shown in FIG. 4. Notably, the AP1 limited electric field effect (described in Appendix B) leads to a steep increase of error with respect to VFP code Aladin for $\mathrm{Kn}^e > 10^{-1}$. For example $v_{lim} \sim 4.3v_{th}$ for the maximum point EDF in FIG. 2.

B. Hohlraum problem

Additionally to the steep temperature gradients, the laser-heated plasma experiments also involve steep density gradients and variation in ionization, which is a dominant effect in multi-material hohlraums at the interface between the helium gas-fill and the ablated high Z plasma.

In [49], a kinetic simulation of laser pulse interaction with a gas filled hohlraum was presented. Plasma profiles provided by a HYDRA simulation in 1D geometry of a laser-heated gadolinium hohlraum containing a helium gas at time of 20 ns were used as input for the IMPACT [20] VFP code. For simplicity, the Coulomb logarithm was treated as a constant $\ln \Lambda_{ei} = \ln \Lambda_{ee} = 2.1484$. In reality, in the low-density corona $\ln \Lambda$ reaches 8, which, however, does not affect the heat flux profile significantly. FIG. 5 shows the electron temperature T_e evolved during 10 ps by Impact and the electron density n_e profile Along with plasma profiles the heat flux profiles of AP1, Impact, and SNB are also shown.

One can observe a very good match between AP1 and Impact computations in the preheat region. It is worth mentioning that in the surroundings of the heat flux maximum ($\sim 1662 \mu m$) the profiles of all plasma variables exhibit steep gradients with a change from $T_e = 2.5 \text{ keV}$, n_e $=5\times10^{20}~\mathrm{cm}^3,\,Z=2$ to $T_e=0.3~\mathrm{keV},\,n_e=6\times10^{21}~\mathrm{cm}^3$, Z=44 across approximately 100 μm (between 1600 μm and 1700 μ m), starting at the helium-gadolinium interface. In this region, we can see a qualitative match between AP1 and Impact providing a same sign of the heat flux divergence contributing to hydro, however, we observe that the electric field limitation explained in Appendix B leads to a stronger drop of the decelerating AP1 heat flux on the material interface, which then closely aligns to the Impact heat flux in the corona. On the other hand, SNB overestimates significantly the heat flux in the lower density part of the plasma up to the point of the heat flux maximum given by Impact (green line in FIG. 5), and more importantly, the opposite sign of the heat flux divergence compared to Impact (and AP1) in the steep gradients region close to the material interface. In the preheat region SNB performs very well same as AP1. Nevertheless, it is important to stress that SNB required only 25 velocity groups compared to 250 velocity groups used by Impact and AP1 for this ICF relevant plasma conditions, thus making it a very efficient modeling approach even though its description of kinetics is rather qualitative.

VI. CONCLUSIONS

In conclusion, we have performed a thorough analysis of the AWBS transport equation for electrons originally introduced in [24] and extended it by adding the nonlocal version of Ohm's law. After properly redefining the e-e collission term, we have shown that the AWBS simpli-

fied linear form of the Fokker-Planck collision operator keeps some important kinetic properties analyzed in local diffusive regime, e.g. provides a correct dependence on Z (BGK requires an additional fix) and inherently includes the anisotropic part of the distribution function f_1 , which compares very well to the full Fokker-Planck operator. Under nonlocal transport plasma conditions, we benchmarked AP1 against the reference VFP codes Aladin and Impact, collisional PIC code Calder. and we also included the standard nonlocal approach SNB. AP1 performed very well over all simulation cases while capturing the important kinetic features compared to the reference kinetic codes. Furthermore, our extensive analysis of the anisotropic part of the EDF provided by AP1 showed a very good match to all Aladin, Impact, and Calder. This suggests a promising AP1's capability in predicting general transport coefficients and the seeding of parametric laser plasma instabilities sensitive to the Landau damping of longitudinal plasma waves [24, 54], which is of great importance in ICF related plasmas [55]. Other kinetic effects as perpendicular transport, e.g heat flow or magnetic field advection, occurring in magnetised plasma [56] are introduced in AP1 via the nonlocal Ohm's law. We have also shown a slightly new formulation of SNB based on the scaled BGK collision operator (21), which performed really well in the heat-bath problem in the sence of heat flux profile, however, its EDF output is rather qualitative which also lead to non-precise results of the hohlraum problem. On the other hand we also observed an inaccurate kinetic results of the decelerating AP1 computation for highly nonlocal plasma conditions, which was explained by the velocity limit applied to the action of the electric field. A general (not only the decelerating) numerical solution of the AP1 model will be the main focus of our future work.

ACKNOWLEDGMENTS

Appendix A: Analysis of local diffusive regime

In order to analyze the local diffusive regime of BGK collision operator (8), we adopt the P2 form of EDF

$$\tilde{f}(z,v,\mu) = f^0(z,v) + \mu f^1(z,v) + \frac{3\mu^2 - 1}{2} f^2(z,v),$$
 (A1)

where f^2 helps us to quantify the validity of the local transport regime. The left hand side of (7) acts on (A1) as

$$\begin{split} \mu \left(\frac{\partial \tilde{f}}{\partial z} + \frac{q_e E_z}{m_e v} \frac{\partial \tilde{f}}{\partial v} \right) + \frac{q_e E_z}{m_e} \frac{1 - \mu^2}{v^2} \frac{\partial \tilde{f}}{\partial \mu} &= \frac{q_e E_z}{m_e v^2} f^1 \\ + \mu \left[\frac{\partial}{\partial z} \left(f^0 - \frac{f^2}{2} \right) + \frac{q_e E_z}{m_e v} \frac{\partial}{\partial v} \left(f^0 - \frac{f^2}{2} \right) + \frac{3q_e E_z}{m_e v^2} f^2 \right] \\ + \mu^2 \left[\frac{\partial f^1}{\partial z} + \frac{q_e E_z}{m_e v} \frac{\partial f^1}{\partial v} - \frac{q_e E_z}{m_e v^2} f^1 \right] + O(\mu^3). \quad (A2) \end{split}$$

The action on (A1) of the BGK operator (8) reads

$$\frac{1}{v}C_{BGK}(\tilde{f}) = \frac{f_M - \tilde{f}}{\lambda_e} + \frac{1}{2}\left(\frac{Z}{\lambda_e} + \frac{1}{\lambda_e}\right)\frac{\partial}{\partial\mu}(1 - \mu^2)\frac{\partial\tilde{f}}{\partial\mu},$$

$$= \frac{f_M - f^0}{\lambda_e} + \frac{(3Z + 4)f^2}{2\lambda_e}$$

$$-\mu\frac{Z + 2}{\lambda_e}f^1 - \mu^2\frac{9(Z + 1)}{2\lambda_e}f^2. \tag{A3}$$

Consequently, if the isotropic and anisotropic parts of (A2) and (A3) are compared, one finds the following equations

$$f^{0} = f_{M} + \frac{\lambda_{e}q_{e}E_{z}}{m_{e}v^{2}}f^{1} + \frac{3Z+4}{2}f^{2}, \tag{A4}$$

$$f^{1} = -\frac{\lambda_{e}}{Z+2} \left[\frac{\partial f^{0}}{\partial z} + \frac{q_{e}E_{z}}{m_{e}v} \frac{\partial f^{0}}{\partial v} + \frac{3q_{e}E_{z}}{m_{e}v^{2}} f^{2} - \frac{1}{2} \frac{\partial f^{2}}{\partial z} - \frac{q_{e}E_{z}}{2m_{e}v} \frac{\partial f^{2}}{\partial v} \right], \tag{A5}$$

$$f^{2} = -\frac{2\lambda_{e}}{2m_{e}v} \left[\lambda_{e}q_{e}E_{z} f^{1} - \frac{\partial f^{1}}{\partial z} - \frac{q_{e}E_{z}}{2m_{e}v} \frac{\partial f^{1}}{\partial v} \right] \tag{A6}$$

 $f^{2} = \frac{2\lambda_{e}}{9(Z+1)} \left[\frac{\lambda_{e}q_{e}E_{z}}{m_{e}v^{2}} f^{1} - \frac{\partial f^{1}}{\partial z} - \frac{q_{e}E_{z}}{m_{e}v} \frac{\partial f^{1}}{\partial v} \right]$ (A6)

It is valid to assume that $f^0 \approx f_M$, i.e. that $f_M \gg \frac{\lambda_e q_e E_z}{m_e v^2} f^1 + \frac{3Z+1}{2} f^2$ in (A4) and $f^0 \gg f^2$ in (A5), for local transport conditions $Kn \ll 1$ and the quasi-neutrality constraint, corresponding to a zero current

$$j \equiv \frac{4\pi q_e}{3} \int v f^1 v^2 dv = 0, \tag{A7}$$

leads to the electric field (same as the classical Lorentz electric field \boldsymbol{E}_L [30])

$$E_z = \frac{m_e v_{th}^2}{q_e} \left(\frac{1}{L_{n_e}} + \frac{5}{2} \frac{1}{L_{T_e}} \right),$$
 (A8)

and the anisotropic part of EDF takes the form (11).

It should be noticed that f^0 equilibrates to f_M as $O\left(Kn^2 \ v/v_{th}\right)$, since one can show that $\frac{\lambda_e q_e E_z}{m_e v^2} f^1 \sim Kn^2$ and $f^2 \sim Kn^2 \ v/v_{th}$, when $f^0 = f_M$ and $E_z = E_L$ in (A5) and (A6).

In the case of the AWBS operator (5) used in (7), its action on (6) reads

$$\frac{1}{v}C_{AWBS}(\tilde{f}) = \frac{vr_A}{\lambda_e} \frac{\partial}{\partial v} \left(\tilde{f} - f_M \right)
+ \frac{1}{2} \left(\frac{Z}{\lambda_e} + \frac{r_A}{\lambda_e} \right) \frac{\partial}{\partial \mu} (1 - \mu^2) \frac{\partial \tilde{f}}{\partial \mu}
= \frac{vr_A}{\lambda_e} \frac{\partial}{\partial v} \left(f^0 - f_M \right)
+ \mu \left(\frac{vr_A}{\lambda_e} \frac{\partial f^1}{\partial v} - \frac{Z + r_A}{\lambda_e} f^1 \right), \quad (A9)$$

where $\nu_e^* = r_A \nu_e = \frac{v r_A}{\lambda_e}$ with r_A being a scaling parameter of the standard e-e collision frequency. Its purpose is to match AWBS heat flux to results obtained by Spitzer and Harm [6] obtained for any Z. Section III C shows that this match can be found with a constant $r_A = 0.5$.

One finds the following equations if the isotropic and anisotropic parts of (A2) and (A9) are compared

$$\frac{\partial}{\partial v} \left(f^0 - f_M \right) = \frac{\lambda_e q_e E_z}{r_A m_e v^2} \frac{f^1}{v}, \tag{A10}$$

$$\frac{vr_A}{\lambda_e} \frac{\partial f^1}{\partial v} - \frac{Z + r_A}{\lambda_e} f^1 = \frac{\partial f^0}{\partial z} + \frac{q_e E_z}{m_e v} \frac{\partial f^0}{\partial v}.$$
 (A11)

If we assume that $\frac{\partial f^0}{\partial v} = \frac{\partial f_M}{\partial v}$, i.e. $f^0 = f_M$, the anisotropic part of the AWBS operator is governed by the equation (13).

Appendix B: AP1 electric field limit

Interestingly, we have encountered a very specific property of the AP1 model with respect to the electric field magnitude. The easiest way how to demonstrate this is to write the model equations (26) and (27) in 1D (z-axis). Then, due to its linear nature, it is easy to eliminate one of the partial derivatives with respect to v, i.e. $\frac{\partial f_0}{\partial v}$ or $\frac{\partial f_{1z}}{\partial v}$. In the case of elimination of $\frac{\partial f_0}{\partial v}$ one obtains the following equation

$$\left(v\frac{\nu_e}{2} - \frac{2q_e^2 E_z^2}{3m_e^2 v \nu_e}\right) \frac{\partial f_{1_z}}{\partial v} = \frac{2q_e E_z}{3m_e \nu_e} \frac{\partial f_{1_z}}{\partial z} + \frac{4\pi q_e E_z}{3m_e} \frac{\partial f_M}{\partial v} + \frac{v}{3} \frac{\partial f_0}{\partial z} + \left(\frac{4q_e^2 E_z^2}{3m_e^2 v^2 \nu_e} + \left(\nu_{ei} + \frac{\nu_e}{2}\right)\right) f_{1_z}.$$
(B1)

It is convenient to write the bracket on the left hand side of (B1) as $\frac{2}{3v\nu_e}\left(\left(\sqrt{3}v\frac{\nu_e}{2}\right)^2 - \frac{q_e^2}{m_e^2}E_z^2\right)$ from where it is clear that the bracket is negative if $\sqrt{3}v\frac{\nu_e}{2} < \frac{q_e}{m_e}|\pmb{E}|$, i.e. there is a velocity limit for a given magnitude $|\pmb{E}|$, when the collisions are no more fully dominant and the electric field introduces a comparable effect to the collision friction in the electron transport.

It can be shown, that the last term on the right hand side of (B1) is dominant and the solution behaves as

$$\Delta \mathbf{f_1} \sim \exp\left(\frac{\frac{4q_e^2 E_z^2}{3m_e^2 v^2 \nu_e} + \left(\nu_{ei} + \frac{\nu_e}{2}\right)}{v \frac{\nu_e}{2} - \frac{2q_e^2 E_z^2}{3m_e^2 v \nu_e}} \Delta v\right), \tag{B2}$$

where $\Delta v < 0$ represents a velocity step of the implicit Euler numerical integration of decelerating electrons. However, (B2) exhibits an exponential growth for velocities above the friction limit (bracket on the left hand side of (B1))

$$v_{lim} = \sqrt{\frac{\sqrt{3}\Gamma m_e}{2q_e}} \frac{n_e}{|\mathbf{E}|},\tag{B3}$$

which makes the problem to be ill-posed.

In order to provide a stable model, we introduce a reduced electric field to be acting as the accelerating force of electrons

$$|\mathbf{E}_{red}| = \sqrt{3}v \frac{m_e}{q_e} \frac{\nu_e}{2},\tag{B4}$$

ensuring that the bracket on the left hand side of (B1) remains positive. We define a quantity $\eta_{red} = \frac{|E_{red}|}{|E|}$. Then, the AP1 model (26), (27) can be formulated as

well posed

$$v\frac{\nu_{e}}{2}\frac{\partial}{\partial v}\left(f_{0}-f_{M}\right) = \frac{v}{3}\nabla\cdot\boldsymbol{f_{1}} + \frac{q_{e}}{m_{e}}\frac{\boldsymbol{E}}{3}\cdot\left(\eta_{red}\frac{\partial\boldsymbol{f_{1}}}{\partial v} + \frac{2(2-\eta_{red})}{v}\boldsymbol{f_{1}}\right),$$

$$(B5)$$

$$v\frac{\nu_{e}}{2}\frac{\partial\boldsymbol{f_{1}}}{\partial v} - \nu_{scat}\boldsymbol{f_{1}} = v\nabla f_{0} + \frac{q_{e}\eta_{red}}{m_{e}}\boldsymbol{E}\frac{\partial f_{0}}{\partial v} + \frac{q_{e}\boldsymbol{B}}{m_{e}c}\times\boldsymbol{f_{1}},$$

$$(B6)$$

while introducing the reduction factor of the accelerating electric field and the compensation of the electric field effect via its angular term.

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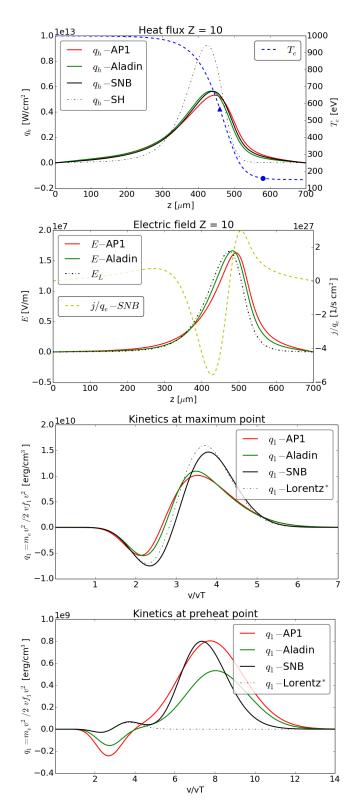


FIG. 3. Snapshot 12 ps. Top: correct steady solution of heat flux. Middle: correct comparison to kinetic profiles at point 460 μ m by Aladin. Velocity limit 3.3 v_{th} at temperature 569.2 eV. Bottom: correct comparison to kinetic profiles at point 580 μ m by Aladin. Velocity limit 13.1 v_{th} at temperature 159.4 eV. TODO Fig reordered so change description, E field and current now in Z=10.

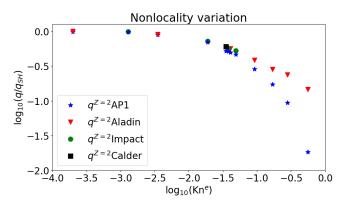


FIG. 4. Simulation results for the case Z=2 computed by AP1/Aladin/Impact/Calder. Every point corresponds to the maximum heat flux in a "tanh" temperature simulation, which can be characterized by Kn. The range of $\log_{10}(\mathrm{Kn}) \in (0,-4)$ can be expressed as equivalent to the electron density approximate range $n_e \in (1e19,3.5e22)$ of the 50 μ m slope tanh case. In the case of Kn = 0.56, $q_{Aladin}/q_{AP1} \approx 7.9$.

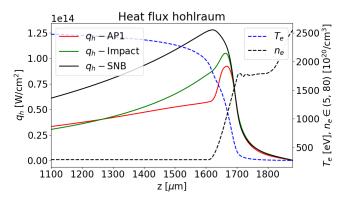


FIG. 5. Heat flux profiles by AP1, Impact and SNB along the electron temperature T_e , electron density n_e , and ionization Z profiles in a laser-heated gadolinium hohlraum containing a helium gas-fill.