

An efficient kinetic modeling in hydrodynamics using the AWBS transport equation

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Abstract

The AWBS Boltzmann transport equation for electrons equipped with a simplified e-e collision operator [1] provides an efficient, yet physically relevant, kinetic extension compared the classical Spitzer-Harm heat flux (SH) based on local approximation and flux-limiting. This classical approach is widely used in plasma kinetics models coupled to hydrodynamics. Even though SH reflects the electron-electron collision effect, the essential physical properties of the electron transport cannot be modeled with an explicitly local model. A simple form of the AWBS model opens a way to couple kinetics to hydrodynamic codes while describing the important physics correctly. Since the electron-electron collision effect becomes especially important in the case of low ion potential, we take a special in the case of low Z plasmas.

Keywords: kinetics; hydrodynamics; nonlocal electron transport; laser-heated plasmas.

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7 1. AWBS-P1 modeling of laser heated plasmas

8 1.1. Model equations

The AWBS electron transport equation reads

$$v\mathbf{n}\cdot\nabla f + \tilde{\mathbf{E}}\cdot\mathbf{n}\frac{\partial f}{\partial v} + \frac{\tilde{\mathbf{E}}\cdot\mathbf{e}_\phi - v\tilde{\mathbf{B}}\cdot\mathbf{e}_\theta}{v}\frac{\partial f}{\partial\phi} = v\nu_e\frac{\partial}{\partial v}(f - f_M) + (\nu_{ei} + \nu_e)(f_0 - f),$$

9 where ν_e is the electron-electron collision frequency, ν_{ei} is the electron-ion
10 collision frequency, and $\nu_{ei} = \bar{Z}\nu_e$.

11 In order to eliminate the dimensions of the above transport problem
12 the first-two-moment model based on approximation

$$f = \frac{f_0}{4\pi} + \frac{3}{4\pi}\mathbf{n}\cdot\mathbf{f}_1,$$

13 can be adopted and reads

$$\begin{aligned}\nu_e v \frac{\partial}{\partial v} (f_0 - \tilde{f}_M) &= v\nabla\cdot\mathbf{f}_1 + \tilde{\mathbf{E}}\cdot\frac{\partial\mathbf{f}_1}{\partial v} + \frac{2}{v}\tilde{\mathbf{E}}\cdot\mathbf{f}_1, \\ \nu_e v \frac{\partial}{\partial v} \mathbf{f}_1 - \nu_t \mathbf{f}_1 &= v\nabla\cdot(\mathbf{A}f_0) + \tilde{\mathbf{E}}\cdot\frac{\partial(\mathbf{A}f_0)}{\partial v} + \tilde{\mathbf{B}}\times\mathbf{f}_1,\end{aligned}$$

14 where $\tilde{f}_M = 4\pi f_M$ and the closure matrix takes the form

$$\mathbf{A} = \frac{1}{3}\mathbf{I}.$$

15 Since in the laser heated plasmas the Knudsen number $\text{Kn} = \frac{v_{th}}{\nu_t(v_{th})L} \in$
16 $(0, 1)$, i.e. the collisionality in the kinetics of electrons plays always an im-
17 portant effect for thermal-like particles, the electron distribution function
18 can be treated as out-of-equilibrium approximation

$$f = f_M + \delta f, \tag{1}$$

where the consequent AWBS model reads

$$\begin{aligned}v\mathbf{n}\cdot\nabla(f_M + \delta f) + \tilde{\mathbf{E}}\cdot\mathbf{n}\frac{\partial f_M}{\partial v} + \tilde{\mathbf{E}}\cdot\mathbf{n}\frac{\partial\delta f}{\partial v} + \frac{\tilde{\mathbf{E}}\cdot\mathbf{e}_\phi - v\tilde{\mathbf{B}}\cdot\mathbf{e}_\theta}{v}\frac{\partial\delta f}{\partial\phi} = \\ v\nu_e\frac{\partial\delta f}{\partial v} + (\nu_{ei} + \nu_e)(f_0 - f_M - \delta f),\end{aligned} \tag{2}$$

19 or its P1 approximation equivalent

$$f = \frac{4\pi f_M + \delta f_0}{4\pi} + \frac{3}{4\pi} \mathbf{n} \cdot \mathbf{f}_1. \quad (3)$$

20 where the moment model reads

$$\nu_e v \frac{\partial \delta f_0}{\partial v} = v \nabla \cdot \mathbf{f}_1 + \tilde{\mathbf{E}} \cdot \frac{\partial \mathbf{f}_1}{\partial v} + \frac{2}{v} \tilde{\mathbf{E}} \cdot \mathbf{f}_1, \quad (4)$$

$$\begin{aligned} \nu_e v \frac{\partial \mathbf{f}_1}{\partial v} - \nu_t \mathbf{f}_1 &= \frac{v}{3} \nabla \delta f_0 + \frac{\tilde{\mathbf{E}}}{3} \frac{\partial \delta f_0}{\partial v} + \tilde{\mathbf{B}} \times \mathbf{f}_1 \\ &+ \frac{v}{3} \nabla \tilde{f}_M + \frac{\tilde{\mathbf{E}}}{3} \frac{\partial \tilde{f}_M}{\partial v}. \end{aligned} \quad (5)$$

21 1.2. A consistent treatment of $\tilde{\mathbf{E}}$ field

$$\mathbf{q}_c(\mathbf{x}) = \int_v v \mathbf{f}_1(\mathbf{x}) v^2 dv,$$

22 from (5)

$$\mathbf{q}_c = \int_v \left(\frac{\nu_e v^2}{\nu_t} \frac{\partial \mathbf{f}_1}{\partial v} - \frac{v^2}{3\nu_t} \nabla (\tilde{f}_M + \delta f_0) - \frac{v}{3\nu_t} \frac{\partial (\tilde{f}_M + \delta f_0)}{\partial v} \tilde{\mathbf{E}} \right) v^2 dv, \quad (6)$$

$$a_0(\mathbf{x}) = \int_v \frac{v}{3\nu_t} \frac{\partial (\tilde{f}_M + \delta f_0)}{\partial v}(\mathbf{x}) v^2 dv,$$

$$\mathbf{b}_0(\mathbf{x}) = \int_v \left(\frac{v^2}{3\nu_t} \nabla (\tilde{f}_M(\mathbf{x}) + \delta f_0(\mathbf{x})) - \frac{\nu_e v^2}{\nu_t} \frac{\partial \mathbf{f}_1}{\partial v}(\mathbf{x}) \right) v^2 dv,$$

$$\mathbf{q}_c(\mathbf{x}) = -\mathbf{b}_0(\mathbf{x}) - a_0(\mathbf{x}) \tilde{\mathbf{E}}(\mathbf{x}),$$

$$\tilde{\mathbf{E}}(\mathbf{x}) = -\frac{\mathbf{b}_0(\mathbf{x})}{a_0(\mathbf{x})}. \quad (7)$$

$$\left(v\nu_e - \tilde{\mathbf{E}} \cdot \mathbf{n}\right) \frac{\partial \delta f}{\partial v} = v\mathbf{n} \cdot \nabla(f_M + \delta f) + \tilde{\mathbf{E}} \cdot \mathbf{n} \frac{\partial f_M}{\partial v} + (\nu_{ei} + \nu_e)(f_M + \delta f - f_0), \quad (8)$$

$$\begin{aligned} \frac{\partial \delta f_0}{\partial v} &= \frac{1}{\nu_e v} \left(v \nabla \cdot \mathbf{f}_1 + \tilde{\mathbf{E}} \cdot \frac{\partial \mathbf{f}_1}{\partial v} \right), \\ \nu_e v \frac{\partial \mathbf{f}_1}{\partial v} - \nu_t \mathbf{f}_1 &= \frac{v}{3} \nabla \delta f_0 + \frac{\tilde{\mathbf{E}}}{3} \frac{\partial \delta f_0}{\partial v} + \frac{v}{3} \nabla \tilde{f}_M + \frac{\tilde{\mathbf{E}}}{3} \frac{\partial \tilde{f}_M}{\partial v}, \end{aligned}$$

$$\left(\nu_e v \mathbf{I} - \frac{\tilde{\mathbf{E}} \tilde{\mathbf{E}}}{3\nu_e v} \right) \cdot \frac{\partial \mathbf{f}_1}{\partial v} = \frac{v}{3} \nabla \delta f_0 + \frac{\tilde{\mathbf{E}}}{3\nu_e} \nabla \cdot \mathbf{f}_1 + \frac{v}{3} \nabla \tilde{f}_M + \frac{\tilde{\mathbf{E}}}{3} \frac{\partial \tilde{f}_M}{\partial v} + \nu_t \mathbf{f}_1,$$

$$\left(\nu_e v - \frac{\tilde{E}_z^2}{3\nu_e v} \right) \frac{\partial f_{1z}}{\partial v} = \frac{v}{3} \frac{\partial \delta f_0}{\partial z} + \frac{\tilde{E}_z}{3\nu_e} \frac{\partial f_{1z}}{\partial z} + \frac{v}{3} \frac{\partial \tilde{f}_M}{\partial z} + \frac{\tilde{E}_z}{3} \frac{\partial \tilde{f}_M}{\partial v} + \nu_t f_{1z}. \quad (9)$$

24 2. Simulation results

25 Two cases:

- 26 • constant $n_e = 5 \times 10^{20} [1/\text{cm}^3]$, constant $\bar{Z} = 4$, T_e temperature profile
 27 taken from IMPACT simulation at 12 ps, see Figure 1
- 28 • n_e, T_e, \bar{Z} profiles taken from HYDRA simulation of Gadolinium hohlraum
 29 at 10 ps, see Figure 2 and Figure 3

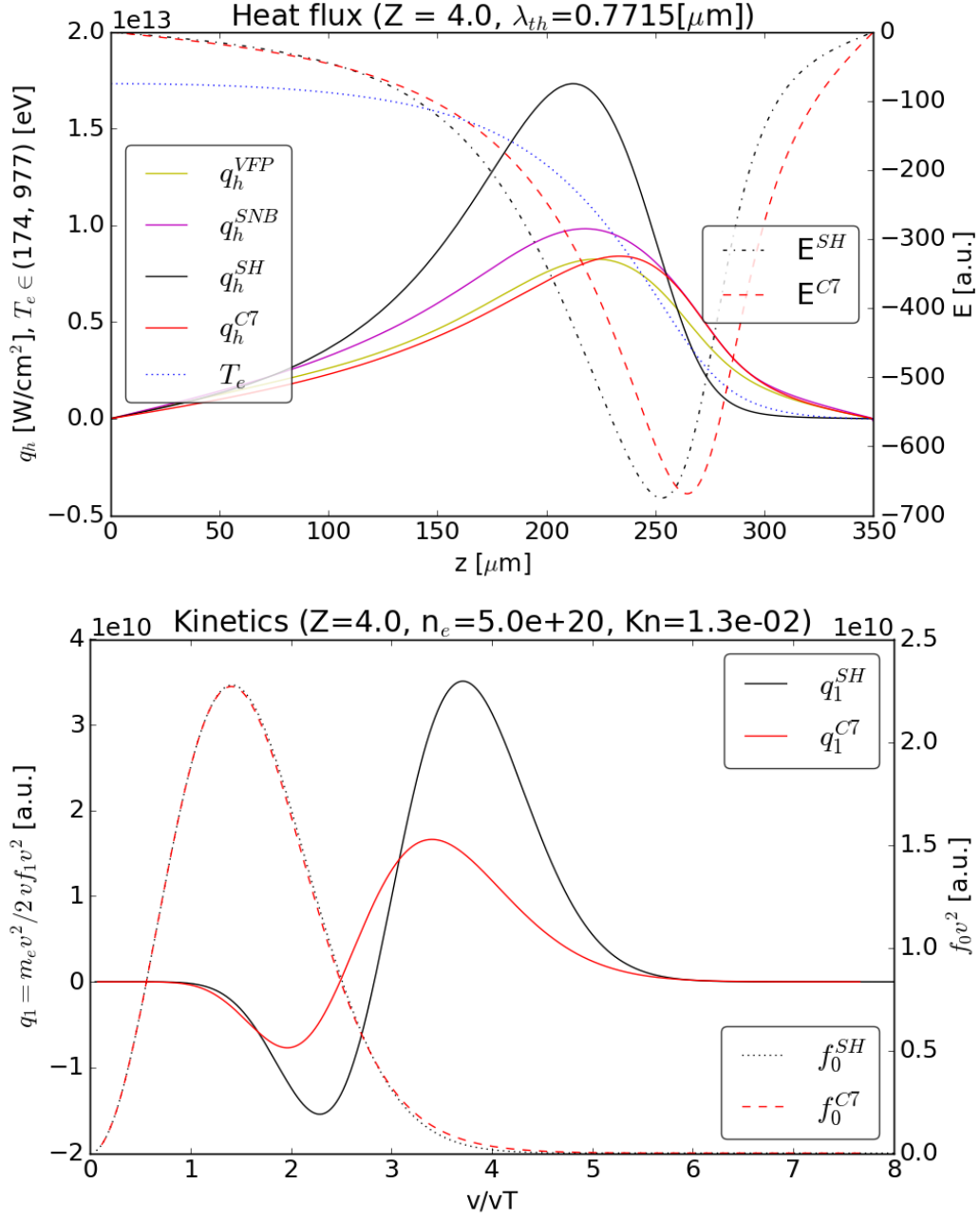


Figure 1: Philippe's preferred test $\bar{Z} = 4$ at 12 ps.

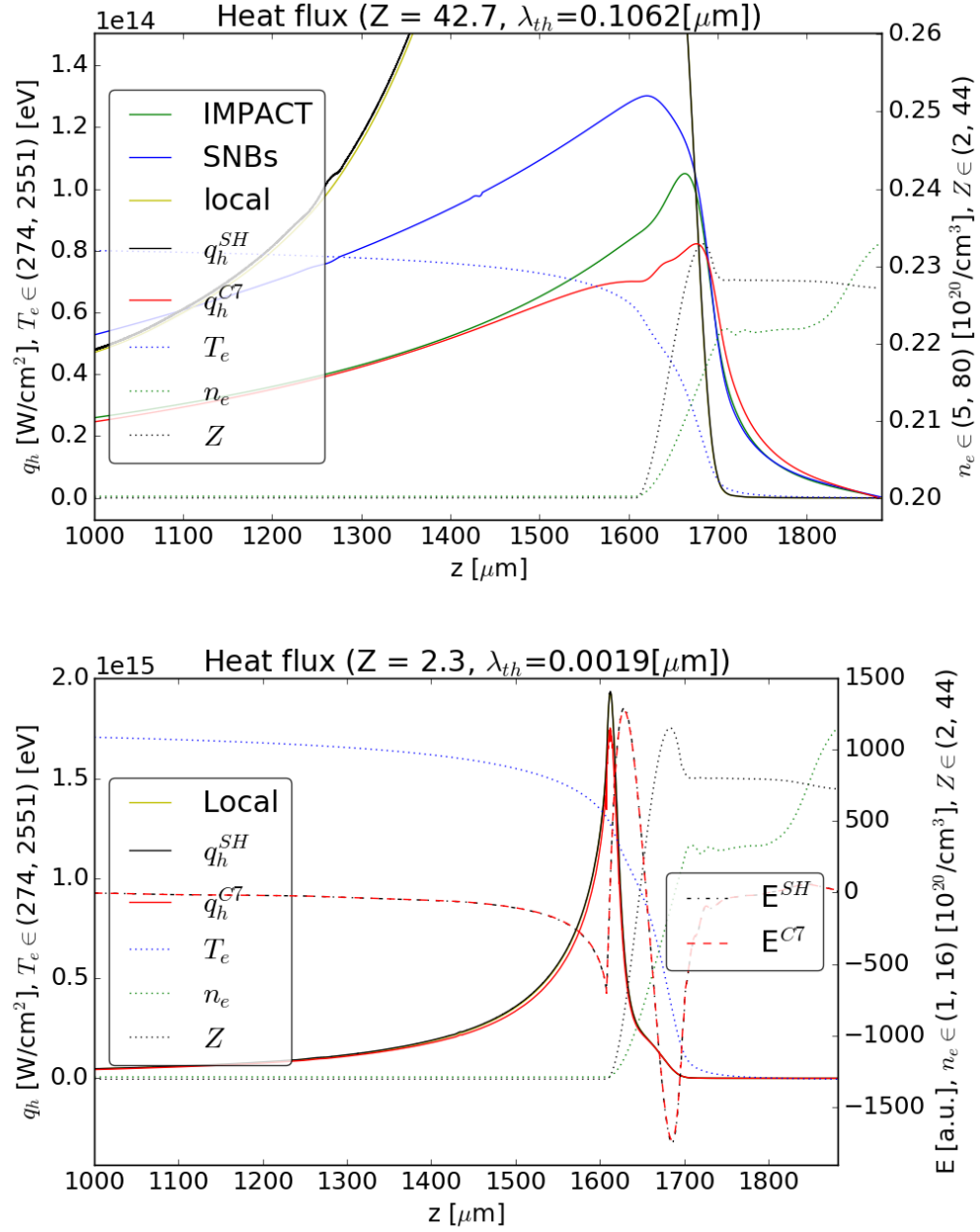


Figure 2:

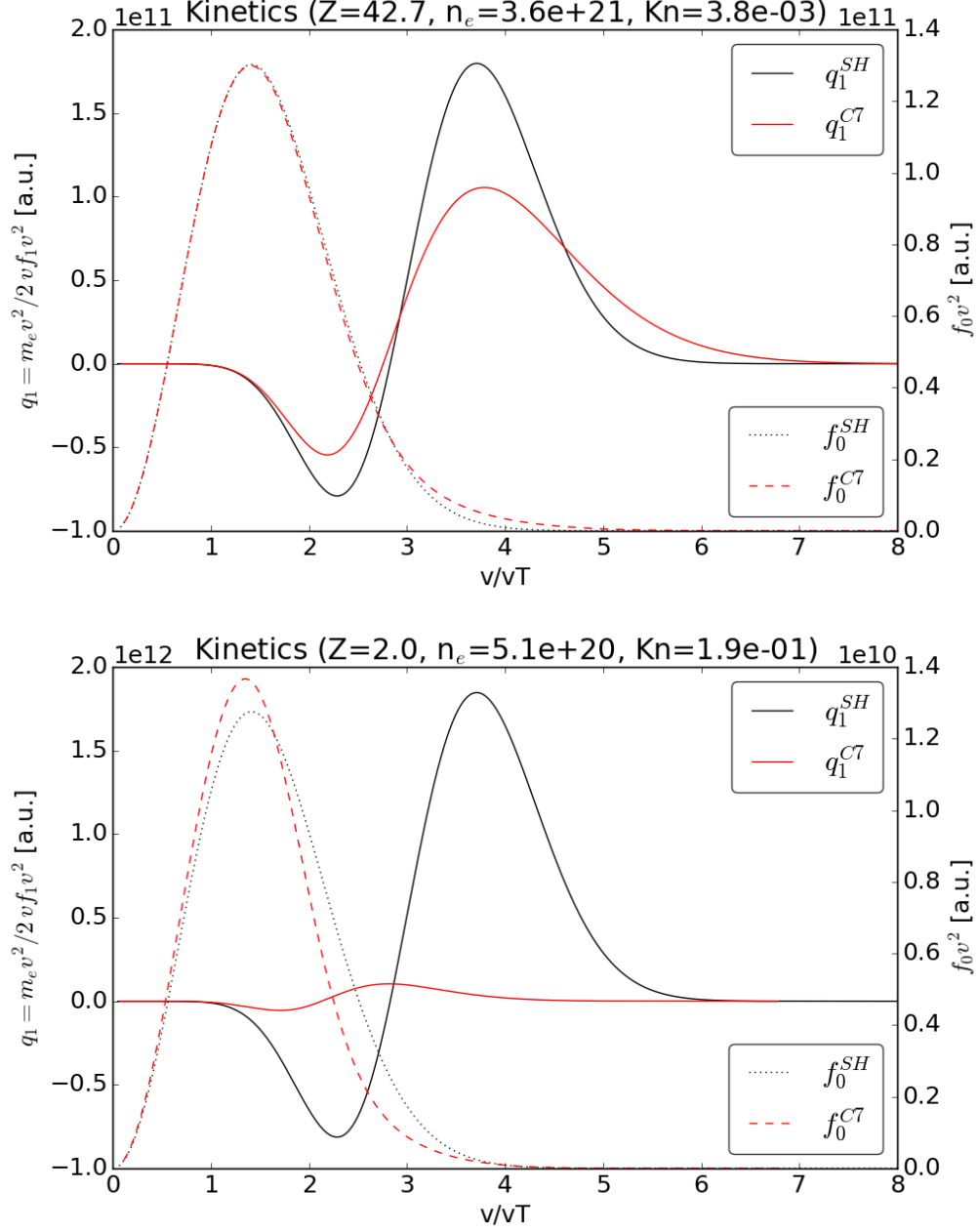


Figure 3: Kinetics profiles for max(flux) point and 1605 microns point for the case of 10ps VFP temperature profile, n_e and Z Hydra profiles.

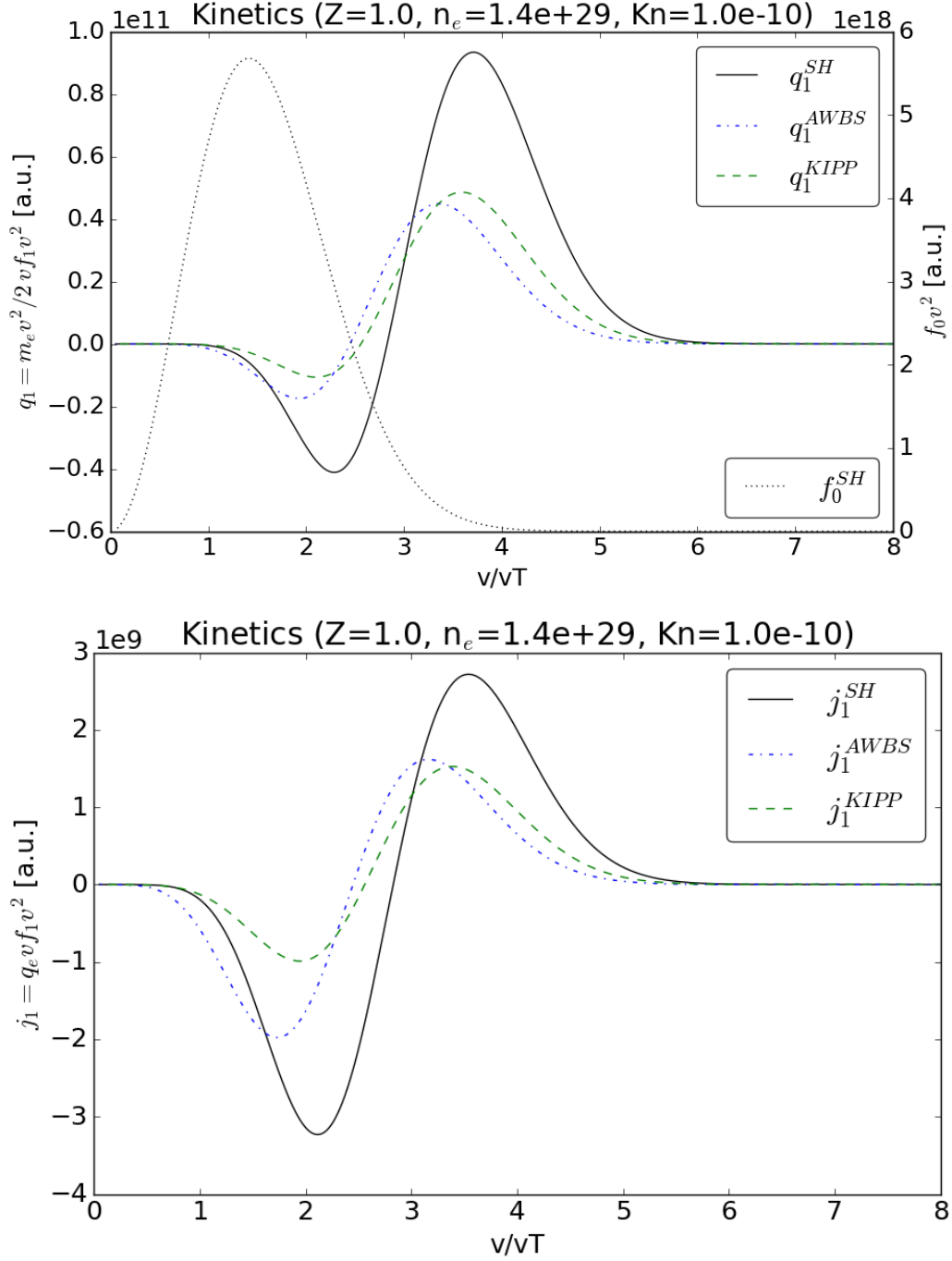


Figure 4: KIPP (by Johnathan) vs AWBS using $\lambda_{ei}^* = \frac{\bar{Z}+0.24}{\bar{Z}+4.2} \lambda_{ei}$, $\bar{Z} = 1$, $v_{th} = \sqrt{\frac{k_B T_e}{m_e}}$
 $f_1^{SH} = -\lambda_{ei}^*(v) \left(\frac{v^2}{2v_{th}^2} - 4 \right) \frac{\mathbf{n} \cdot \nabla T_e}{T_e} f_M$, $f_1^{KIPP} = -\lambda_{ei}^*(v) \left(\frac{3}{16} \frac{v^2}{v_{th}^2} - 1 - \frac{3}{2} \frac{v_{th}^2}{v^2} \right) \frac{\mathbf{n} \cdot \nabla T_e}{T_e} f_M$.

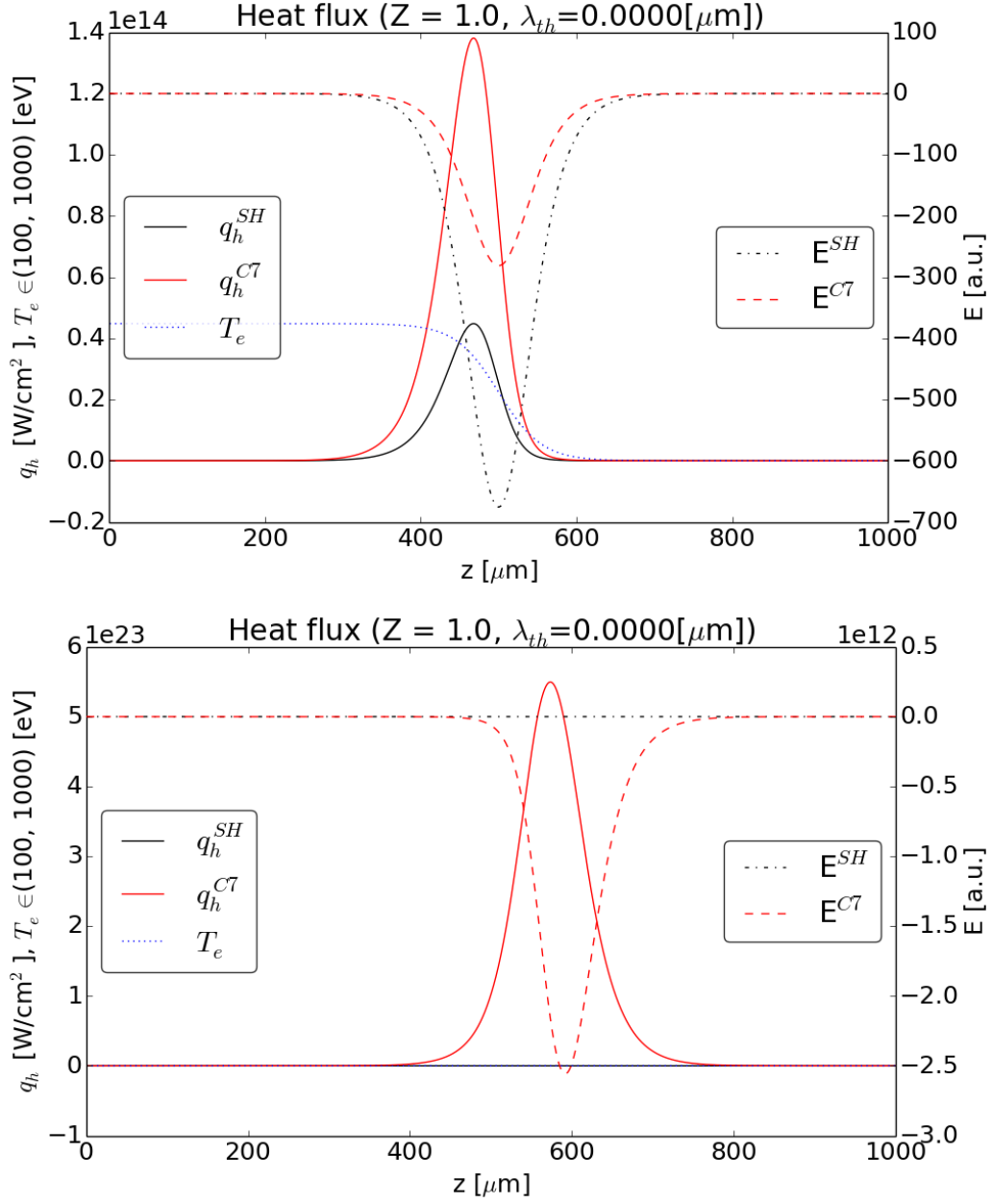


Figure 5: Decelerating (top) vs. accelerating (bottom) computations. Zeroth E field iteration, i.e. no E field effect, of the diffusion regime conditions.

- ³⁰ [1] J. R. Albritton, E. A. Williams, I. B. Bernstein, Nonlocal electron heat
³¹ transport by not quite maxwell-boltzmann distributions, Phys. Rev. Lett.
³² 57 (1986) 1887–1890.