# An efficient kinetic modeling in plasmas by using the AWBS transport equation

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Text of abstract.

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### I. INTRODUCTION

The first attempts of modern kinetic modeling of 46 plasma can be tracked back to the fifties, when Co-47 hen, Spitzer, and Routly (CSR) [1] in detail demonstrated the fact, that in the ionized gas the effect of Coulomb collisions between electrons and ions predominantly results from frequently occurring events of cumulative small deflections rather than occasional close en-48 counters. This effect was originally described in [2] and 49 Chandrasekhar [3] proposed to use the diffusion equation 50 model of the Fokker-Planck type (FP) [4].

As a result, a classical paper by Spitzer and Harm (SH) <sup>52</sup> [5] provides the computed electron distribution function <sup>53</sup> spanning from low to high Z plasmas, and more importantly, the current and heat flux formulas, which are widely used in almost every plasma hydrodynamic code nowadays. The distribution function is of the form  $f^0 + \mu f^1$ , where  $f^0$  and  $f^1$  are isotropic and  $\mu$ , is the direction cosine between the particle trajectory and some <sup>55</sup> preferred direction in space. It should be emphasized <sup>56</sup> that the SH solution expresses a small perturbation of <sup>57</sup> equilibrium, i.e. that  $f^0$  is the Maxwell-Boltzmann dis- <sup>58</sup> tribution and  $\mu f^1$  represents a very small deviation.

The actual cornerstone of the modern FP simulations  $_{60}$  was set in place by Rosenbluth [6], when he derived a simplified form of the FP equation for a finite expansion of the distribution function, where all the terms are computed according to plasma conditions, including  $f^0$ , which of course needs to tend to the Maxwell-Boltzmann  $_{61}$  distribution.

In is the purpose of this paper to present an efficient 63 alternative to FP model based on the Albritton-Williams-Bernstein-Swartz collision operator (AWBS) [7]. In Section II we propose a modified form of the AWBS collision operator, where its important properties are further presented in Section III with the emphasis on its comparison to the full FP solution in local diffusive regime. Section IV focuses on the performance of the AWBS transport equation model compared to modern kinetic codes including FP codes Aladin and Impact, and PIC code Calder, where the cases related to real laser generated plasma conditions are studied. Finally, the most important outcomes of our research are concluded in Section V.

#### II. THE AWBS KINETIC MODEL

The electrons in plasma can be modeled by the deterministic model of charged particles

$$\frac{\partial f}{\partial t} + \boldsymbol{v} \cdot \nabla_{\boldsymbol{x}} f + \tilde{\boldsymbol{E}} \cdot \nabla_{\boldsymbol{v}} f = C_{ee}(f) + C_{ei}(f), \quad (1)$$

where  $f(t, \boldsymbol{x}, \boldsymbol{v})$  represents the density function of electrons at time t, spatial point  $\boldsymbol{x}$ , and velocity  $\boldsymbol{v}$ , and  $\tilde{\boldsymbol{E}} = \frac{q_e}{m_e} \boldsymbol{E}$  is the existing electric field in plasma.

The generally accepted form of the electron-electron collision operator  $C_{ee}$  is the Fokker-Planck form published by Landau [8]

$$C_{FP}(f) = \Gamma \int \nabla_{\boldsymbol{v}} \nabla_{\boldsymbol{v}} (\boldsymbol{v} - \tilde{\boldsymbol{v}}) \cdot (f \nabla_{\tilde{\boldsymbol{v}}} f - f \nabla_{\boldsymbol{v}} f) \, d\tilde{\boldsymbol{v}}, \tag{2}$$

where  $\Gamma = \frac{q_e^4 \ln \Lambda}{q_e^4 e^2 m_e^2}$  and  $\ln \Lambda$  is the Coulomb logarithm. In principal, the electron-ion collision operator  $C_{ei}$  could be expressed in the form similar to (2), but since ions are considered to be motionless compared to electrons, the scattering operator, i.e. no change in the velocity magnitude, expressed in spherical coordinates is widely accepted

$$C_{ei}(f) = \frac{\nu_{ei}}{2} \left( \frac{\partial}{\partial \mu} \left( (1 - \mu^2) \frac{\partial f}{\partial \mu} \right) + \frac{1}{\sin^2(\phi)} \frac{\partial^2 f}{\partial \theta^2} \right), (3)$$

where  $\mu = \cos(\phi)$ ,  $\phi$  and  $\theta$  are the polar and azimuthal angles, and  $\nu_{ei} = \frac{Zn_e\Gamma}{v^3}$  is the electron-ion collision frequency.

Fish introduced an alternative form of  $C_{ee}$  in [9] referred to as high-velocity limit electron collision operator

$$C_H(f) = v\nu_e \frac{\partial}{\partial v} \left( f + \frac{v_{th}^2}{v} \frac{\partial f}{\partial v} \right) + \frac{\nu_e}{2} \left( 1 - \frac{v_{th}^2}{2v^2} \right) \left( \frac{\partial}{\partial \mu} \left( (1 - \mu^2) \frac{\partial f}{\partial \mu} \right) + \frac{1}{\sin^2(\phi)} \frac{\partial^2 f}{\partial \theta^2} \right), \tag{4}$$

where  $\nu_e = \frac{n_e \Gamma}{v^3}$  is the electron-electron collision frequency and  $v_{th} = \sqrt{\frac{k_B T_e}{m_e}}$  is the electron thermal velocity. The linear form of  $C_H$  arises from an assumption that the fast electrons predominantly interact with the thermal (slow) electrons, which simplifies importantly the nonlinear form (2).

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The aim of this work is to use a yet simpler form of the electron-electron collision operator, i.e. the AWBS formulation [7], where we propose the following form

$$C_{AWBS}(f) = v \frac{\nu_e}{2} \frac{\partial}{\partial v} (f - f_M) + \frac{\nu_{ei} + \frac{\nu_e}{2}}{2} \left( \frac{\partial}{\partial \mu} \left( (1 - \mu^2) \frac{\partial f}{\partial \mu} \right) + \frac{1}{\sin^2(\phi)} \frac{\partial^2 f}{\partial \theta^2} \right), \quad (5)$$

where  $f_M$  is the Maxwell-Boltzmann equilibrium distribution.  $C_{AWBS}$  represents the complete  $C_{ee} + C_{ei}$  collision operator in (1).

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The complete form of collision operator (5) was previously introduced in [10, 11], nevertheless, we intentionally use a half of the electron-electron collisional frequency modification  $\frac{\nu_e}{2}$ , because this formulation provides very promising results compared to the full FP operator as emphasized in Section III.

The Maxwell-Boltzmann averaged e-e scattering in (4) can be approximated as  $\nu_e \int \left(1 - \frac{v_{th}^2}{2v^2}\right) f_M 4\pi v^2 dv = \frac{\nu_e}{2}$ . 112

### III. BGK, AWBS, AND FOKKER-PLANCK MODELS IN LOCAL DIFFUSIVE REGIME

In a broad analysis of the electron transport, any qual-119 itative information about its properties are highly wel-120 come. Even better, if one can extract some qualitative 121 information, which provides comparative and reliable re-122 sults in a clear way, the confidence of using a transport 123 model, e.g. (5), can lead to efficient yet relatively cheap computation cost predictions of real physics.

In this paper, we can try to find an approximate solution to the so-called local diffusive regime of electro transport, where the diffusive regime, in general, refers to a low anisotropy in angle given by  $\mu$ , and local means that the mean free path of electrons  $\lambda_{ei}$  is rather restricted compared to the plasma spatial scale. In the words of mathematics this corresponds to the first order expansion in  $\lambda_{ei}$  and  $\mu$  of the distribution function as

$$\tilde{f}(z, v, \mu) = f^{0}(z, v) + f^{1}(z, v)\lambda_{ei}\mu,$$
 (6)

where z is the spatial coordinate along the axis z, v the magnitude of transport velocity, and  $\lambda_{ei} = \frac{v}{\nu_{ei}} = \frac{v^4}{Zn_e\Gamma}$ . In other words, one can say that by evaluating numerically  $\tilde{f}$  in (6), we accept some error of the order<sub>125</sub>  $O(\lambda_{ei}^2) + O(\mu^2)$ . The expansion in a small parameter  $\lambda_{ei}$  is also coherent with a time-steady approximation due to the relation between the mean free path and collision frequency, where the higher the collision frequency the more steady the solution.

In order to start, we express the time-steady left hand<sub>127</sub> side of (1) in 1D and insert the approximation (6), which<sub>128</sub>

leads to

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$$\mu \left( \frac{\partial \tilde{f}}{\partial z} + \frac{\tilde{E}_z}{v} \frac{\partial \tilde{f}}{\partial v} \right) + \frac{\tilde{E}_z (1 - \mu^2)}{v^2} \frac{\partial \tilde{f}}{\partial \mu} = \mu \left( \frac{\partial f^0}{\partial z} + \frac{\tilde{E}_z}{v} \frac{\partial f^0}{\partial v} \right) + \frac{\tilde{E}_z \lambda_{ei}}{v^2} f^1 + O(\mu^2), \quad (7)$$

and is truncated for low anisotropy, i.e. with error  $O(\mu^2)$ .

## A. The BGK local diffusive electron transport

Even though the BGK plasma collisional operator [12]

$$\frac{1}{v}C_{BGK}(\tilde{f}) = \frac{\tilde{f} - f_M}{\lambda_e} + \frac{1}{2\lambda_{ei}} \frac{\partial}{\partial \mu} (1 - \mu^2) \frac{\partial \tilde{f}}{\partial \mu}, \quad (8)$$

where  $\lambda_e = Z\lambda_{ei}$ , is not actually used in our nonlocal transport simulations, we consider it useful to include this simplest form of the Boltzmann transport collision operator, because of two reasons: a) it can be treated analytically in the local diffusive regime; and b) it represents the so-called phenomenological collision operator by explicitly using the Maxwell-Boltzmann equilibrium distribution  $f_M$ , which proves to be very useful in coupling of the nonlocal electron transport to hydrodynamics.

If one applies the action of the right hand side, i.e. of (8), on the approximation (6) and sets the result to be equal to the left hand side (7), the corresponding terms in  $\mu$  are governed by the following equations

$$f^{0} = f_{M} + \frac{\tilde{E}_{z}}{v^{2}} f^{1} Z \lambda_{ei}^{2}, \tag{9}$$

$$f^{1} = -\frac{Z}{Z+1} \left( \frac{\partial f^{0}}{\partial z} + \frac{\tilde{E}_{z}}{v} \frac{\partial f^{0}}{\partial v} \right), \tag{10}$$

i.e.  $f^0 = f_M + O(\lambda_{ei}^2)$  and  $f^1 = -\frac{Z}{Z+1} \left( \frac{\partial f_M}{\partial z} + \frac{\tilde{E}_z}{v} \frac{\partial f_M}{\partial v} \right)$ . Now the electric current expressing the contribution of every electron naturally tends to zero, i.e. the *quasineutrality* constraint, which lead to an analytic formula of the self-consistent electric field

$$\mathbf{j} \equiv q_e \int \mathbf{v} f^1 \, d\mathbf{v} = \mathbf{0} \to \tilde{\mathbf{E}} = v_{th}^2 \left( \frac{\nabla \rho}{\rho} + \frac{5}{2} \frac{\nabla T}{T} \right).$$
(11)

Consequently, based on (9), (10), and (11), the analytic formula (6) of the electron distribution function reads

$$\tilde{f} = f_M - \frac{Z}{Z+1} \left( \frac{v^2}{2v_{th}^2} - 4 \right) \frac{1}{T} \frac{\partial T}{\partial z} f_M \lambda_{ei} \mu, \qquad (12)$$

which is nothing else than the famous Lorentz electronion collision gas model [13] scaled by a constant depending on Z, naturally arising from the BGK model (8).

### B. The AWBS local diffusive electron transport

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The main object of this work presented in Sec II simplifies in 1D to a relatively simple form of the Boltzmann transport collision operator (compared to (2))

$$\frac{1}{v}C_{AWBS}(f) = \frac{v}{2\lambda_e} \frac{\partial}{\partial v} (f - f_M) 
+ \frac{1}{2} \left( \frac{1}{\lambda_{ei}} + \frac{1}{2\lambda_e} \right) \frac{\partial}{\partial \mu} (1 - \mu^2) \frac{\partial f}{\partial \mu}.$$
(13)

Similarly to the BGK model, AWBS 13 is also referred to as a phenomenological model, since it explicitly uses the Maxwell-Boltzmann equilibrium distribution  $f_M$ , and also, makes it a very attractive model of the non-local electron transport to be coupled to hydrodynamics via the plasma electron temperature and density.

A qualitative information about the AWBS model is obtained while repeating the action on (6) by the left hand side (7) and by the right hand side (13) and setting the equality. The corresponding terms in  $\mu$  are then governed by the following equations

$$\frac{\partial}{\partial v} \left( f^0 - f_M \right) = \frac{\tilde{E}_z}{v^3} f^1 2 Z \lambda_{ei}^2, \qquad (14)$$

$$\frac{v}{2 Z \lambda_{ei}} \frac{\partial \left( f^1 \lambda_{ei} \right)}{\partial v} - \frac{2Z + 1}{2Z} f^1 = \frac{\partial f^0}{\partial z} + \frac{\tilde{E}_z}{v} \frac{\partial f^0}{\partial v}, \qquad (15)$$

i.e.  $f^0 = f_M + O(\lambda_{ei}^2)$ , however, the  $f^1$  does not have a straightforward analytic formula. In reality,  $f^1$  arises from the ordinary differential equation (by inserting  $f_M$  into (15))

$$\frac{\partial f^{1}}{\partial v} + \frac{1}{v}(3 - 2Z)f^{1} =$$

$$\frac{2Z}{v} \left( \frac{1}{\rho} \frac{\partial \rho}{\partial z} + \left( \frac{v^{2}}{2v_{th}^{2}} - \frac{3}{2} \right) \frac{1}{T} \frac{\partial T}{\partial z} - \frac{\tilde{E}_{z}}{v_{th}^{2}} \right) f_{M}. \quad (16)$$

We will stick with a numerical solution of (16), where the details about the resulting distribution function can be found in Section III D.

# C. The Fokker-Planck local diffusive electron transport

The Fokker-Plank (2) collision operator can be also written as [14]

$$\frac{1}{v}C_{FP}(f) = \frac{\Gamma}{v} \left( 4\pi f^2 + \frac{\nabla_{\boldsymbol{v}}\nabla_{\boldsymbol{v}}f : \nabla_{\boldsymbol{v}}\nabla_{\boldsymbol{v}}g}{2} \right), \quad (17)$$

where  $g(\boldsymbol{v}) = \int |\boldsymbol{v} - \tilde{\boldsymbol{v}}| f(\tilde{\boldsymbol{v}}) \, \mathrm{d}\tilde{\boldsymbol{v}}$  is the Rosenbluth potential [6]. Since we are interested in the approximate solution in the local diffusive regime, it is convenient to use a low anisotropy approximation  $\tilde{g} = g^0(f^0) + g^1(f^1)\lambda_{ei}\mu$ , which arises based on Eq. 45 of [6].

For a better clarity we present the action of (17) in 1D

$$C_{FP}(\tilde{f}) = \Gamma \left( 4\pi f^{02} + \frac{1}{2} \frac{\partial^2 f^0}{\partial v^2} \frac{\partial^2 g^0}{\partial v^2} + \frac{1}{v^2} \frac{\partial f^0}{\partial v} \frac{\partial g^0}{\partial v} \right)$$

$$+ \frac{\mu}{Zn_e} \left[ 8\pi f^0 f^1 v^4 - v \left( \frac{\partial f^0}{\partial v} g^1 + \frac{\partial g^0}{\partial v} f^1 \right) \right]$$

$$+ \frac{1}{v^2} \left( \frac{\partial f^0}{\partial v} \frac{\partial (g^1 v^4)}{\partial v} + \frac{\partial g^0}{\partial v} \frac{\partial (f^1 v^4)}{\partial v} \right)$$

$$+ \frac{1}{2} \left( \frac{\partial^2 f^0}{\partial v^2} \frac{\partial^2 (g^1 v^4)}{\partial v^2} + \frac{\partial^2 g^0}{\partial v^2} \frac{\partial^2 (f^1 v^4)}{\partial v^2} \right) \right] + O(\lambda_{ei}^2, \mu^2), \tag{18}$$

truncated by the quadratic terms in the angular anisotropy and the transport localization.

If once more repeated the action on (6) by the left hand side (7) and by the right hand side (17) and setting the equality, the equation governing  $f^0$  corresponding to  $\mu^0$  takes the form

$$4\pi f^{0^2} + \frac{1}{2} \frac{\partial^2 f^0}{\partial v^2} \frac{\partial^2 g^0}{\partial v^2} + \frac{1}{v^2} \frac{\partial f^0}{\partial v} \frac{\partial g^0}{\partial v} = \frac{\tilde{E}_z}{v^5} f^1 Z n_e \lambda_{ei}^2 - \frac{2}{v^2} \left( \frac{\partial f^1 \lambda_{ei}}{\partial v} - \frac{f^1 \lambda_{ei}}{v} \right) \left( \frac{\partial g^1 \lambda_{ei}}{\partial v} - \frac{g^1 \lambda_{ei}}{v} \right), \quad (19)$$

where the fundamental property of the Fokker-Planck collision operator tending to the Maxwell-Boltzmann distribution  $f_M$  [15], leads to  $f^0 = f_M + O(\lambda_{ei}^2)$ , where we write an explicit form of the quadratic term  $O(\lambda_{ei}^2)$  obtained from the truncation (18). The equality corresponding to  $\mu$  takes the form

$$\frac{1}{Zn_e} \left[ \frac{1}{2} \left( \frac{\partial^2 f_M}{\partial v^2} \frac{\partial^2 (g^1 v^4)}{\partial v^2} + \frac{\partial^2 g_M}{\partial v^2} \frac{\partial^2 (f^1 v^4)}{\partial v^2} \right) \right. \\
+ \frac{1}{v^2} \left( \frac{\partial f_M}{\partial v} \frac{\partial (g^1 v^4)}{\partial v} + \frac{\partial g_M}{\partial v} \frac{\partial (f^1 v^4)}{\partial v} \right) \\
- v \left( \frac{\partial f_M}{\partial v} g^1 + \frac{\partial g_M}{\partial v} f^1 \right) + 8\pi f_M f^1 v^4 \right] - v f^1 \\
= v \frac{\partial f_M}{\partial z} + \tilde{E}_z \frac{\partial f_M}{\partial v}, \quad (20)$$

which is the equation governing the unknown  $f^1$ .

In principle, the solution to the equation (20) is very ambitious, as demonstrated in [1, 3, 6], fortunately, one can use the explicit evaluation of the electron distribution function published in [5], which takes the following form

$$f^{1}(z,v) = \frac{1}{\lambda_{ei}} \frac{m_e^2}{4\pi q_e^4 \ln \Lambda} \frac{v_{2th}^4}{Z}$$

$$\left(2d_T(v/v_{2th}) + \frac{3}{2} \frac{\gamma_T}{\gamma_E} d_E(v/v_{2th})\right) \frac{f_M}{n_e} \frac{1}{T} \frac{\partial T_e}{\partial z}, \quad (21)$$

where  $d_T(x) = ZD_T(x)/B$ ,  $d_E(x) = ZD_E(x)/A$ ,  $\gamma_T$ , and  $\gamma_E$  are represented by numerical values in TABLE I, TABLE II, and TABLE III in [5], and  $v_{2th} = \sqrt{\frac{k_B T_e}{2m_e}}$ .

	Z=1	Z=2	Z=4	Z = 16	Z = 116
$ar{\Delta}oldsymbol{q}_{AWBS}$	0.057	0.004	0.038	0.049	0.004

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TABLE I. Relative error  $\bar{\Delta}q_{AWBS} = |q_{AWBS} - q_{SH}|/q_{SH}|^{176}$  of the AWBS kinetic model equation (5) showing the discrep-<sup>177</sup> ancy (maximum around 5%) with respect to the original so-<sup>178</sup> lution of the heat flux given by numerical solution in Spitzer<sup>179</sup> and Harm [5].

# D. Summary of the BGK, AWBS, and Fokker-Planck local diffusive transport

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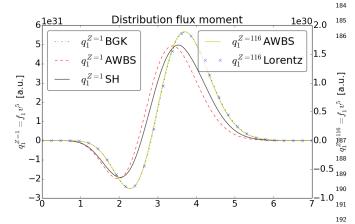


FIG. 1. The flux velocity moment of the anisotropic part<sup>193</sup> of the electron distribution function in low Z=1 and high Z=116 plasmas in diffusive regime.

- Rescale BGK according to Lorentz to match SH<sup>19</sup><sub>19</sub>; heat flux.
- Emphasize the outstanding match between our modified  $\frac{\nu_e}{2}$  AWBS model and the SH profiles of  $q_1$  (define) in TABLE I.
- Stress the visual results of AWBS compared to FP presented in FIG. 1.
- Raise a discussion about the structure of  $f^1$  equa-204 tions (10), (16), and (20).
- Point out the behavior of the maximum velocity of  $q_1$ .

### IV. BENCHMARKING THE AWBS NONLOCAL TRANSPORT MODEL

### A. AP1 implementation

AP1 represents the abbreviation AWBS-P1, i.e. the use of collision operator (5) and the P1 angular discretization, i.e. the lowest order anisotropy approximation. AP1 in general belongs to the so-called angular moments method and the electron distribution function takes the form

$$\tilde{f} = \frac{f_0}{4\pi} + \frac{3}{4\pi} \boldsymbol{n} \cdot \boldsymbol{f_1},$$

which consists of the isotropic part  $f_0 = \int_{4\pi} \tilde{f} d\mathbf{n}$  and the directional part  $\mathbf{f_1} = \int_{4\pi} \mathbf{n} \tilde{f} d\mathbf{n}$ , where  $\mathbf{n}$  is the transport direction (the solid angle).

The first two angular moments applied to the steady form of (1) with collision operator (5) lead to the AP1 model equations

$$v\frac{\nu_e}{2}\frac{\partial}{\partial v}(f_0 - 4\pi f_M) = v\nabla \cdot \mathbf{f_1} + \tilde{\mathbf{E}} \cdot \frac{\partial \mathbf{f_1}}{\partial v} + \frac{2}{v}\tilde{\mathbf{E}} \cdot \mathbf{f_1}(22)$$
$$v\frac{\nu_e}{2}\frac{\partial \mathbf{f_1}}{\partial v} - \nu_{scat}\mathbf{f_1} = \frac{v}{3}\nabla f_0 + \frac{\tilde{\mathbf{E}}}{3}\frac{\partial f_0}{\partial v}, \tag{23}$$

where  $\nu_{scat} = \nu_{ei} + \frac{\nu_e}{2}$ . The strategy of solving (22) and (23) resides in integrating  $\frac{\partial f_0}{\partial v}$  and  $\frac{\partial f_1}{\partial v}$  in velocity magnitude while starting the integration from infinite velocity to zero velocity, which corresponds to decelerating electrons. It should be noted, that in practice we start the integration from  $v = 7v_{th}$ , which represents a sufficiently high velocity.

### 1. Nonlocal electric field treatment

Similarly to (11), one can obtain the model equation of the electric field  $\tilde{E}$  by evaluating the zero current condition (a velocity integration of (23))

$$\int_{v} \left( \frac{\frac{\nu_{e}}{2} v^{2}}{\nu_{scat}} \frac{\partial \mathbf{f_{1}}}{\partial v} - \frac{v^{2}}{3\nu_{scat}} \nabla f_{0} - \frac{v}{3\nu_{scat}} \frac{\partial f_{0}}{\partial v} \tilde{\mathbf{E}} \right) v^{2} dv = 0,$$
(24)

from which it is easy to express  $\tilde{E}$  once  $f_0$  and  $f_1$  are known, or in other words, the integral-differential model equations need to be solved simultaneously, which is achieved by k-iteration of  $f_0^k(\tilde{E}^k)$ ,  $f_1^k(\tilde{E}^k)$ , i.e. (22), (23), and  $\tilde{E}^{k+1}(f_0^k, f_1^k)$ , i.e. (24), until the current evaluation (24) converges to zero. In particular, the first iteration starts with  $\tilde{E} = 0$  in (22) and (23).

Interestingly, we have encountered a very specific property of the AP1 model with respect to the electric field magnitude. The easiest way how to demonstrate this is to write the model equations (22) and (23) in 1D and eliminate one of the partial derivatives with respect to v.

$\mathrm{Kn}^e$	$10^{-4}$	$10^{-3}$	$10^{-2}$	10 <sup>-1</sup>	1
$v_{lim}/v_{th}$	70.8	22.4	7.3	3.1	1.8

TABLE II.  $\sqrt{3}v^{\frac{\nu_e}{2}} > |\tilde{\boldsymbol{E}}|$ .

In the case of elimination of  $\frac{\partial f_0}{\partial v}$  one obtains the following<sub>233</sub> equation <sup>234</sup>

$$\left(v\frac{\nu_{e}}{2} - \frac{2\tilde{E}_{z}^{2}}{3v\nu_{e}}\right)\frac{\partial f_{1_{z}}}{\partial v} = \frac{2\tilde{E}_{z}}{3\nu_{e}}\frac{\partial f_{1_{z}}}{\partial z} + \frac{4\pi\tilde{E}_{z}}{3}\frac{\partial f_{M}}{\partial v}$$

$$+ \frac{v}{3}\frac{\partial f_{0}}{\partial z} + \left(\frac{4\tilde{E}_{z}^{2}}{3v^{2}\nu_{e}} + \left(\nu_{ei} + \frac{\nu_{e}}{2}\right)\right)f_{1_{z}}.$$

$$(25)_{240}^{236}$$

It is convenient to write the left hand side of (25) as  $\frac{2}{3v\nu_e}\left(\left(\sqrt{3}v\frac{\nu_e}{2}\right)^2 - \tilde{E}_z^2\right)$  from where it is clear that the bracket is negative if  $\sqrt{3}v\frac{\nu_e}{2} = \sqrt{3}\frac{n_e\Gamma}{2v^2} < |\tilde{\boldsymbol{E}}|$ , i.e. there is a velocity limit for a given magnitude  $|\tilde{\boldsymbol{E}}|$ , when the collisions are no more fully dominant and the electric<sub>242</sub> field introduces a comparable effect to friction in the elec-<sub>243</sub> tron transport.

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Since the last term on the right hand side<sub>245</sub> of (25) is dominant, the solution behaves as  $f_1 \sim \exp\left(-\left(\frac{4\bar{E}_z^2}{3v^2\nu_e} + \left(\nu_{ei} + \frac{\nu_e}{2}\right)\right) / \left(v\frac{\nu_e}{2} - \frac{2\bar{E}_z^2}{3v\nu_e}\right)v\right)$ , which becomes ill-posed for velocities above the limit.

In order to provide a stable model, we introduce a re- $_{247}$  duced electric field

$$|\tilde{\boldsymbol{E}}_{red}| = \sqrt{3}v\frac{\nu_e}{2},\tag{26}$$

ensuring that the bracket on the left hand side of (25) remains positive. Further more we define two quantities  $^{249}$ 

$$\omega_{red} = rac{| ilde{m{E}}_{red}|}{| ilde{m{E}}|}, \quad 
u_{scat}^E = rac{| ilde{m{E}}| - | ilde{m{E}}_{red}|}{v}.$$

introducing the reduction factor of the electric field to be applied  $\omega_{red}$  and the compensation of the electric field effect in terms of scattering  $\nu_{scat}^E$ . Consequently, the AP1<sup>251</sup> model (22), (23), and (24) can be formulated as well posed with the help of  $\omega_{red}$  and  $\nu_{scat}^E$ . However, before<sub>252</sub> doing so, we introduce a slightly different approximation<sub>253</sub> to the electron distribution function as

$$\tilde{f} = \frac{4\pi f_M + \delta f_0}{4\pi} + \frac{3}{4\pi} \boldsymbol{n} \cdot \boldsymbol{f_1}. \tag{27}$$

where  $\delta f_0$  represents the departure of isotropic part<sup>257</sup> from the Maxwell-Boltzmann equilibrium distribution  $f_M$ , which we keep intentionally in the distribution func-<sup>258</sup> tion approximation.

Then, the stable AP1 model reads

$$v\frac{\nu_{e}}{2}\frac{\partial\delta f_{0}}{\partial v} = v\nabla\cdot\boldsymbol{f_{1}} + \tilde{\boldsymbol{E}}\cdot\left(\omega_{red}\frac{\partial\boldsymbol{f_{1}}}{\partial v} + \frac{2}{v}\boldsymbol{f_{1}}\right), \quad (28)$$

$$v\frac{\nu_{e}}{2}\frac{\partial\boldsymbol{f_{1}}}{\partial v} = \tilde{\nu}_{scat}\boldsymbol{f_{1}} + \frac{v}{3}\nabla\left(4\pi f_{M} + \delta f_{0}\right)$$

$$+\frac{\tilde{\boldsymbol{E}}}{3}\left(4\pi\frac{\partial f_{M}}{\partial v} + \omega_{red}\frac{\partial \delta f_{0}}{\partial v}\right), \quad (29)$$

where  $\tilde{\nu}_{scat} = \nu_{ei} + \nu^E_{scat} + \frac{\nu_e}{2}$ . The reason for keeping  $f_M$  in the distribution function approximation (27) can be seen in the last term on the right hand side of (29), which provides the effect of electric field on directional quantities as current or heat flux. In principle, the explicit use of  $f_M$  ensures the proper effect of  $\tilde{E}$  if  $\delta f_0 \ll f_M$ , i.e. no matter what the reduction  $\omega_{red}$  is. Apart from its stability, it also exhibits much better convergence of the electric field, which is now given by the zero current condition of (29) as

$$\tilde{\mathbf{E}} = \frac{\int_{v} \left( \frac{\nu_{e}}{2\tilde{\nu}_{scat}} v^{2} \frac{\partial \mathbf{f}_{1}}{\partial v} - \frac{v^{2}}{3\tilde{\nu}_{scat}} \nabla \left( 4\pi f_{M} + \delta f_{0} \right) \right) v^{2} \, \mathrm{d}v}{\int_{v} \frac{v}{3\tilde{\nu}_{scat}} \left( 4\pi \frac{\partial f_{M}}{\partial v} + \omega_{red} \frac{\partial \delta f_{0}}{\partial v} \right) v^{2} \, \mathrm{d}v}.$$
(36)

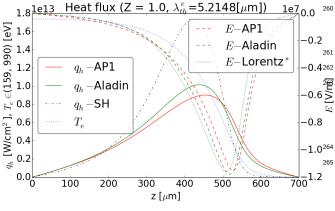
For practical reasons we present in TABLE II some explicit values of velocity limit corresponding to varying transport conditions expressed in terms of Knudsen number  $\mathrm{Kn}^e = \frac{\lambda_e |\nabla T_e|}{T_e}$ , where  $\frac{T_e}{|\nabla T_e|}$  stands for the length scale of plasma.

# B. Aladin, Impact, and Calder kinetic codes

- Brief description of the Aladin code FIG. 2, FIG. 3.
- Brief description of the Impact code FIG. 4.
- Brief description of the Calder code FIG. 5.

## C. Simulation results

- Multiple runs analyzing the performance of AP1 with respect to Aladin/Impact/Calder along wide range of Kn<sup>e</sup> shown in FIG. 6.
- Realistic hydro simulation setting provided by HY-DRA, a comparison between AP1, Impact, and SNB shown in FIG. 7.
- Comment on and summarize the velocity limits for all figs.



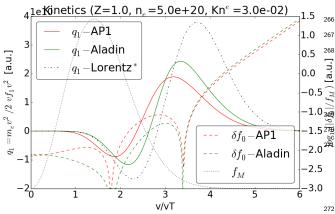


FIG. 2. Snapshot 20 ps. Left: correct steady solution of  $_{274}$  heat flux. Right: Aladins results are correct. Velocity limit  $4.4\ v_{th}$ ..

### V. CONCLUSIONS

- The most important point is that we introduce a collision operator, which is coherent with the full FP, i.e. no extra dependence on Z.
- Touch pros/contras of linearized FP in Aladin and Impact vs AWBS
- Raise discussion about what is the weakest point of AP1 for high Kns: the velocity limit or phenomenological Maxwellization?
- Summarize useful outcomes related to plasma physics as the tendency of the velocity maximum in  $q_1$  with respect to Z and  $\operatorname{Kn}^e$ .
- Emphasize the good results of Aladin (compared to Impact) and also outstanding results of Calder while being PIC.

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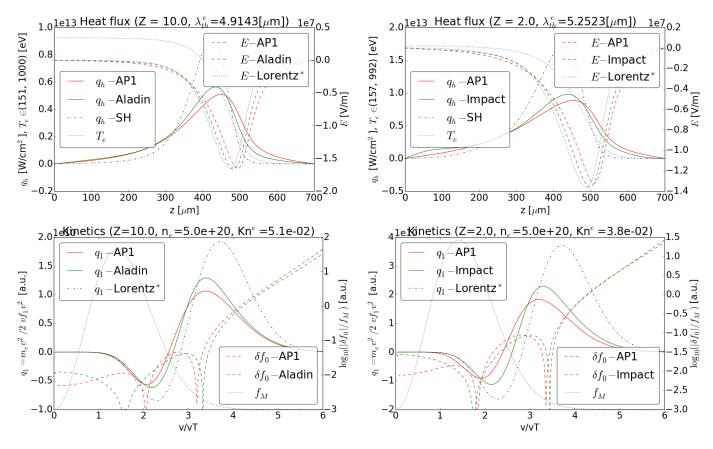


FIG. 3. Snapshot 12 ps. Left: correct steady solution of heat flux. Right: correct comparison to kinetic profiles at point 442  $\mu$ m by Aladin. Velocity limit 3.4  $v_{th}$ .

FIG. 4. Snapshot 12 ps. Left: correct steady solution of heat flux. Right: correct comparison to kinetic profiles at point 437  $\mu m$  by Impact. Velocity limit 4.0  $v_{th}$ .

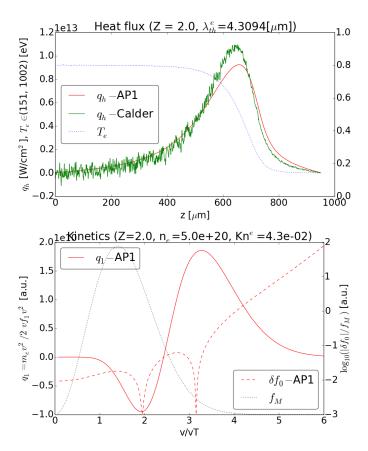


FIG. 5. Snapshot 11 ps. Left: correct steady solution of heat flux. Right: Kinetic profiles at point of maximum flux by AP1. Kinetics profiles by CALDER should be added. Velocity limit 3.8  $v_{th}$ .

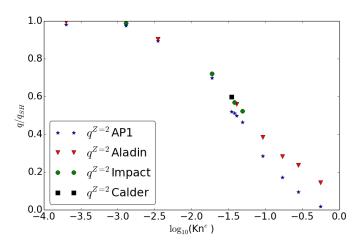


FIG. 6. Simulation results for the case Z=2 computed by AP1/Aladin/Impact/Calder. Every point corresponds to the maximum heat flux in a "tanh" temperature simulation, which can be characterized by Kn. The range of  $\log_{10}(\mathrm{Kn}) \in (0,-4)$  can be expressed as equivalent to the electron density approximate range  $n_e \in (1e19,3.5e22)$  of the 50  $\mu$ m slope tanh case. In the case of Kn = 0.56,  $q_{Aladin}/q_{AP1} \approx 7.9$ .

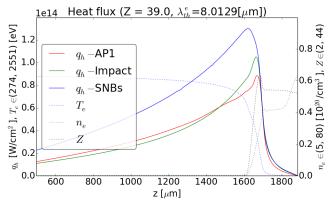


FIG. 7.