

Introduction to Robotics

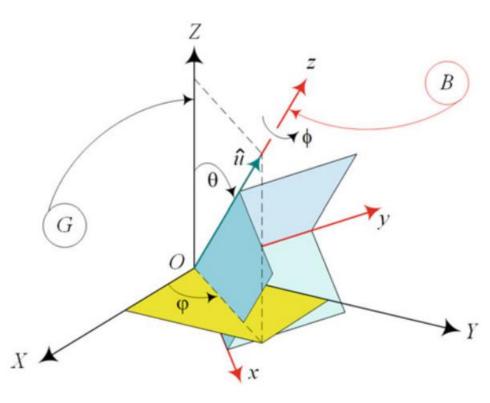


Chapter 3. Orientation Kinematics

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- Any rotation ϕ of a rigid body with **a fixed point O** about a fixed axis \hat{u} can be **decomposed** into three rotations about three given non-coplanar axes including the global or body principal exes.
- Determination of the angle and axis is called the orientation kinematics of rigid bodies.



Axis of rotation \hat{u} when it is coincident with the local z-axis

• Assume **a body frame B** (Oxyz) rotates ϕ about a line indicated by a unit vector \hat{u} with direction cosines u_1 , u_2 , u_3 .

$$\hat{\mathbf{u}} = u_1 \hat{I} + u_2 \hat{J} + u_3 \hat{K} = \begin{bmatrix} u_1 & u_2 & u_3 \end{bmatrix}^T$$

$$\sqrt{u_1^2 + u_2^2 + u_3^2} = 1$$

- ⇒ This is called **axis**—angle representation of a rotation.
- Two parameters are necessary to define the unit vector \hat{u} through \mathbf{O} , and one is necessary to define the amount of **rotation** ϕ of the rigid body about \hat{u} .

• The axis—angle transformation matrix ${}^{G}\mathbf{R_{B}}$ that maps the coordinates in the **local frame B** (Oxyz) to the corresponding coordinates in the **global frame G** (OXYZ)

$$^{G}\mathbf{r} = ^{G}\mathbf{R}_{\mathbf{R}}^{B}\mathbf{r}$$

where,

$${}^{G}R_{B} = \begin{bmatrix} u_{1}^{2} \operatorname{vers} \phi + c\phi & u_{1}u_{2} \operatorname{vers} \phi - u_{3}s\phi & u_{1}u_{3} \operatorname{vers} \phi + u_{2}s\phi \\ u_{1}u_{2} \operatorname{vers} \phi + u_{3}s\phi & u_{2}^{2} \operatorname{vers} \phi + c\phi & u_{2}u_{3} \operatorname{vers} \phi - u_{1}s\phi \\ u_{1}u_{3} \operatorname{vers} \phi - u_{2}s\phi & u_{2}u_{3} \operatorname{vers} \phi + u_{1}s\phi & u_{3}^{2} \operatorname{vers} \phi + c\phi \end{bmatrix}$$

$${}^{G}R_{B} = R_{\hat{u},\phi} = \mathbf{I}\cos\phi + \hat{u}\hat{u}^{T}\operatorname{vers}\phi + \tilde{u}\sin\phi$$

 $\operatorname{vers}\phi = \operatorname{versine}\phi = 1 - \cos\phi = 2\sin^{2}\frac{\phi}{2}$

• \tilde{u} is the skew symmetric matrix corresponding to the vector \hat{u} .

$$\hat{u} = \begin{bmatrix} u_1 \\ u_2 \\ u_3 \end{bmatrix} \qquad \tilde{u} = \begin{bmatrix} 0 & -u_3 & u_2 \\ u_3 & 0 & -u_1 \\ -u_2 & u_1 & 0 \end{bmatrix}$$

- A matrix $\tilde{\boldsymbol{u}}$ is skew symmetric if: $\tilde{\boldsymbol{u}}^T = -\tilde{\boldsymbol{u}}$
- Given a transformation matrix ${}^{G}R_{R}$ we can obtain the axis $\hat{\mathbf{u}}$ and angle ϕ of the rotation by

where,
$$\tilde{u} = \frac{1}{2\sin\phi} \left({}^GR_B - {}^GR_B^T \right)$$

$$\cos\phi = \frac{1}{2} \left(\operatorname{tr} \left({}^GR_B \right) - 1 \right)$$

Example 1

Axis—angle rotation when $\hat{\mathbf{u}} = \hat{\mathbf{K}}$. Simplifying the axis—angle rotation matrix for a special known case axis of rotation.

- The local frame B (Oxyz) rotates about the **Z-axis**, $\hat{u} = \hat{K} = \begin{bmatrix} 0 & 0 & 1 \end{bmatrix}^T$
- The transformation matrix reduces to

$${}^{G}R_{B} = \begin{bmatrix} 0 \operatorname{vers} \phi + \cos \phi & 0 \operatorname{vers} \phi - 1 \sin \phi & 0 \operatorname{vers} \phi + 0 \sin \phi \\ 0 \operatorname{vers} \phi + 1 \sin \phi & 0 \operatorname{vers} \phi + \cos \phi & 0 \operatorname{vers} \phi - 0 \sin \phi \\ 0 \operatorname{vers} \phi - 0 \sin \phi & 0 \operatorname{vers} \phi + 0 \sin \phi & 1 \operatorname{vers} \phi + \cos \phi \end{bmatrix}$$
$$= \begin{bmatrix} \cos \phi - \sin \phi & 0 \\ \sin \phi & \cos \phi & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

 \Rightarrow which is equivalent to the rotation matrix about the Z-axis of global frame.

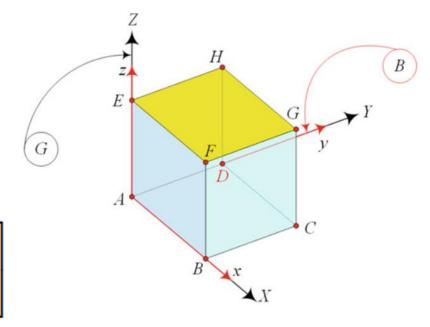
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Example 2: Axis and angle of rotation

Consider a cubic rigid body with a fixed point at A and a unit length of edges as is shown in Figure. If we turn the cube 45 [deg] about $\mathbf{u} = [\mathbf{1} \ \mathbf{1} \ \mathbf{1}]^T$, then we can find the global coordinates of its corners using Rodriguez transformation matrix.

$$\phi = \frac{\pi}{4} \qquad \hat{u} = \frac{\mathbf{u}}{\sqrt{3}} = \begin{bmatrix} 0.57735 \\ 0.57735 \\ 0.57735 \end{bmatrix}$$

$$= \begin{bmatrix} 0.80474 & -0.31062 & 0.50588 \\ 0.50588 & 0.80474 & -0.31062 \\ -0.31062 & 0.50588 & 0.80474 \end{bmatrix}$$



Example 2: Axis and angle of rotation

The local coordinates of the corners are

	$ ^{B}\mathbf{r}_{B}$	$ ^{B}\mathbf{r}_{C} $	$ {}^B\mathbf{r}_D $	$ ^{B}\mathbf{r}_{E} $	$ ^{B}\mathbf{r}_{F} $	$ ^{B}\mathbf{r}_{G} $	$ {}^B\mathbf{r}_H $
x	1	1	0	0	1	1	0
y	0	1	1	0	0	1	1
z	0	0	0	1	1	1	1

The global coordinates of the corners after the rotation will be

$${}^{G}\mathbf{r}=R_{\hat{u},\phi}{}^{B}\mathbf{r}$$

			$^{G}\mathbf{r}_{D}$				
X	0.804	0.495	-0.31	0.505	1.310	1	0.196
Y	0.505	1.31	0.804	-0.31	0.196	1	0.495
\overline{Z}	-0.31	0.196	0.505	0.804	0.495	1	1.31

Example 2: Axis and angle of rotation

Point G is on the axis of rotation, so its coordinates will not change. Points B, D, F, and H are in a symmetric plane indicated by \hat{u} . Therefore, they will move on a circle.

Let us call the midpoint of the cube by P

$${}^{B}\mathbf{r}_{P} = \frac{1}{2} \left({}^{B}\mathbf{r}_{B} + {}^{B}\mathbf{r}_{H} \right) = \frac{1}{2} \left({}^{B}\mathbf{r}_{F} + {}^{B}\mathbf{r}_{D} \right) = \begin{bmatrix} 0.5 \\ 0.5 \\ 0.5 \end{bmatrix}$$

$${}^{G}\mathbf{r}_{P} = \frac{1}{2} \left({}^{G}\mathbf{r}_{B} + {}^{G}\mathbf{r}_{H} \right) = \frac{1}{2} \left({}^{G}\mathbf{r}_{F} + {}^{G}\mathbf{r}_{D} \right) = \begin{bmatrix} 0.5\\0.5\\0.5 \end{bmatrix}$$

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3.1. Axis—Angle Rotation

Example 3: Axis and angle of a rotation matrix

A body coordinate frame B undergoes three Euler rotations (φ , θ , ψ) = (30, 45, 60) deg with respect to a global frame G.

• The rotation matrix to transform coordinates of **B** to **G** is

$${}^{G}R_{B} = {}^{B}R_{G}^{T} = \begin{bmatrix} R_{z,\psi} & R_{x,\theta} & R_{z,\varphi} \end{bmatrix}^{T} = R_{z,\varphi}^{T} & R_{x,\theta}^{T} & R_{z,\psi}^{T} \\ = \begin{bmatrix} 0.12683 & -0.92678 & 0.35355 \\ 0.78033 & -0.12683 & -0.61237 \\ 0.61237 & 0.35355 & 0.70711 \end{bmatrix}$$

The unique angle-axis of rotation for this rotation matrix can then be

found
$$\phi = \arccos\left(\frac{1}{2}\left(\operatorname{tr}\left({}^{G}R_{B}\right) - 1\right)\right)$$

 $= \arccos(-0.14645) = 1.7178 \,\text{rad} = 98 \,\text{deg}$

Example 3: Axis and angle of a rotation matrix

$$\tilde{u} = \frac{1}{2\sin\phi} \begin{pmatrix} {}^{G}R_{B} - {}^{G}R_{B}^{T} \end{pmatrix}$$

$$= \begin{bmatrix} 0.0 & -0.86285 - 0.13082 \\ 0.86285 & 0.0 & -0.48822 \\ 0.13082 & 0.48822 & 0.0 \end{bmatrix}$$

$$\hat{u} = \begin{bmatrix} 0.48822 \\ -0.13082 \\ 0.86285 \end{bmatrix}$$

• We may verify the angle-axis rotation formula and derive the same rotation matrix

$${}^{G}R_{B} = R_{\hat{u},\phi} = \mathbf{I}\cos\phi + \hat{u}\,\hat{u}^{T}\,\mathrm{vers}\,\phi + \tilde{u}\sin\phi$$

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3.2. Euler Parameters

- Assume ϕ to be the angle of rotation of a body coordinate frame B(Oxyz) about $\hat{u} = u_1\hat{I} + u_2\hat{J} + u_3\hat{K}$ relative to a global frame G(OXYZ).
- Euler Rigid Body Rotation Theorem. The most general displacement of a rigid body with one fixed point is a rotation about an axis.
- To find the axis and angle of rotation we introduce the Euler parameters e_0 , e_1 , e_2 , e_3 such that e_0 is a scalar and e_1 , e_2 , e_3 are components of a vector e,

$$e_0 = \cos \frac{\phi}{2}$$

 $\mathbf{e} = e_1 \hat{I} + e_2 \hat{J} + e_3 \hat{K} = \hat{u} \sin \frac{\phi}{2}$
 $e_1^2 + e_2^2 + e_3^2 + e_0^2 = e_0^2 + \mathbf{e}^T \mathbf{e} = 1$

• The transformation matrix ${}^{G}R_{B}$ to satisfy the equation ${}^{G}r = {}^{G}R_{B}{}^{B}r$ can be derived based on Euler parameters.

$${}^{G}R_{B} = R_{\hat{u},\phi} = (e_{0}^{2} - \mathbf{e}^{2})\mathbf{I} + 2\mathbf{e}\,\mathbf{e}^{T} + 2e_{0}\tilde{e}$$

$$= \begin{bmatrix} e_{0}^{2} + e_{1}^{2} - e_{2}^{2} - e_{3}^{2} & 2\left(e_{1}e_{2} - e_{0}e_{3}\right) & 2\left(e_{0}e_{2} + e_{1}e_{3}\right) \\ 2\left(e_{0}e_{3} + e_{1}e_{2}\right) & e_{0}^{2} - e_{1}^{2} + e_{2}^{2} - e_{3}^{2} & 2\left(e_{2}e_{3} - e_{0}e_{1}\right) \\ 2\left(e_{1}e_{3} - e_{0}e_{2}\right) & 2\left(e_{0}e_{1} + e_{2}e_{3}\right) & e_{0}^{2} - e_{1}^{2} - e_{2}^{2} + e_{3}^{2} \end{bmatrix}$$

where, **e** is the skew symmetric matrix corresponding to vector **e**.

$$\tilde{e} = \begin{bmatrix} 0 & -e_3 & e_2 \\ e_3 & 0 & -e_1 \\ -e_2 & e_1 & 0 \end{bmatrix}$$

• Given a transformation matrix ${}^{G}R_{B}$ we may obtain Euler parameters

$$e_0^2 = \frac{1}{4} \left(\operatorname{tr} \left({}^G R_B \right) + 1 \right)$$
$$\tilde{e} = \frac{1}{4e_0} \left({}^G R_B - {}^G R_B^T \right)$$

• Determine the angle ϕ and axis of rotation $\hat{\boldsymbol{u}}$.

$$\cos \phi = \frac{1}{2} \left(\operatorname{tr} \left({}^{G}R_{B} \right) - 1 \right)$$

$$\tilde{u} = \frac{1}{2 \sin \phi} \left({}^{G}R_{B} - {}^{G}R_{B}^{T} \right)$$

• Euler parameters provide a well-suited, redundant, and non-singular rotation description for arbitrary and large rotations.

Example 4: Axis—angle rotation ${}^G\!R_B$ for a ϕ and $\hat{\mathbf{u}}$

Euler parameters for rotation $\phi = 30$ deg about $\hat{u} = (\hat{I} + \hat{J} + \hat{K})/\sqrt{3}$

$$e_0 = \cos\frac{\pi}{12} = 0.966$$

$$\mathbf{e} = \hat{u}\sin\frac{\phi}{2} = e_1\hat{I} + e_2\hat{J} + e_3\hat{K} = 0.149\left(\hat{I} + \hat{J} + \hat{K}\right)$$

• The corresponding transformation matrix ${}^{G}R_{R}$ is

$${}^{G}R_{B} = (e_{0}^{2} - \mathbf{e}^{2})\mathbf{I} + 2\mathbf{e}\,\mathbf{e}^{T} + 2e_{0}\tilde{e}$$

$$= \begin{bmatrix} 0.91 & -0.244 & 0.333 \\ 0.333 & 0.91 & -0.244 \\ -0.244 & 0.333 & 0.91 \end{bmatrix}$$

Euler parameters and Euler angles relationship

• The following relationships between Euler angles and Euler parameters

Or

$$e_0 = \cos\frac{\theta}{2}\cos\frac{\psi + \varphi}{2}$$
$$e_1 = \sin\frac{\theta}{2}\cos\frac{\psi - \varphi}{2}$$

$$e_1 = \sin\frac{\theta}{2}\cos\frac{\psi - \varphi}{2}$$

$$e_2 = \sin\frac{\theta}{2}\sin\frac{\psi - \varphi}{2}$$

$$e_3 = \cos\frac{\theta}{2}\sin\frac{\psi + \varphi}{2}$$

$$\varphi = \cos^{-1} \frac{2 (e_2 e_3 + e_0 e_1)}{\sin \theta}$$

$$\theta = \cos^{-1} \left[2 \left(e_0^2 + e_3^2 \right) - 1 \right]$$

$$\psi = \cos^{-1} \frac{-2(e_2e_3 - e_0e_1)}{\sin \theta}$$

Calculate the Euler parameters

$$e_0 = \pm \frac{1}{2} \sqrt{1 + r_{11} + r_{22} + r_{33}}$$

Case 1
$$e_0 = \pm \frac{1}{2} \sqrt{1 + r_0}$$
$$e_1 = \frac{1}{2} \frac{r_{32} - r_{23}}{r_{32} - r_{23}}$$

$$\frac{1}{r_{23}} - r_{23} = \frac{1}{r_{13}} - \frac{1}{r_{13$$

$$e_1 = \frac{1}{4} \frac{r_{32} - r_{23}}{e_0}$$
 $e_2 = \frac{1}{4} \frac{r_{13} - r_{31}}{e_0}$ $e_3 = \frac{1}{4} \frac{r_{21} - r_{12}}{e_0}$

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Case 2

$$e_{1} = \pm \frac{1}{2} \sqrt{1 + r_{11} - r_{22} - r_{33}}$$

$$e_{2} = \frac{1}{4} \frac{r_{21} + r_{12}}{e_{1}} \quad e_{3} = \frac{1}{4} \frac{r_{31} - r_{32}}{e_{13}}$$

$$\mathbf{Case 3}$$

$$e_{1} = \pm \frac{1}{2} \sqrt{1 + r_{11}} - r_{22} - r_{33}$$

$$e_{2} = \frac{1}{4} \frac{r_{21} + r_{12}}{e_{1}} \quad e_{3} = \frac{1}{4} \frac{r_{31} + r_{13}}{e_{1}} \quad e_{0} = \frac{1}{4} \frac{r_{32} + r_{23}}{e_{1}}$$

$$e_2 = \pm \frac{1}{2} \sqrt{1 - r_{11} + r_{22} - r_{33}}$$

$$r_{13} - r_{33}$$

$$e_3 = \frac{1}{4} \frac{r_{32} + r_{23}}{e_2}$$
 $e_0 = \frac{1}{4} \frac{r_{13} - r_{31}}{e_2}$ $e_1 = \frac{1}{4} \frac{r_{21} + r_{12}}{e_2}$

Case 4

$$e_3 = \pm \frac{1}{2} \sqrt{1 - r_{11} - r_{22} + r_{33}}$$

$$e_3 = \pm \frac{1}{2} \sqrt{1 - r_{11} - r_{22} + r_{33}}$$

$$e_0 = \frac{1}{4} \frac{r_{21} - r_{12}}{r_{22}} \quad e_1 = \frac{1}{4} \frac{r_{31} + r_{13}}{r_{32}} \quad e_2 = \frac{1}{4} \frac{r_{32} + r_{23}}{r_{32}}$$

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