

Introduction to Mobile Robot Control

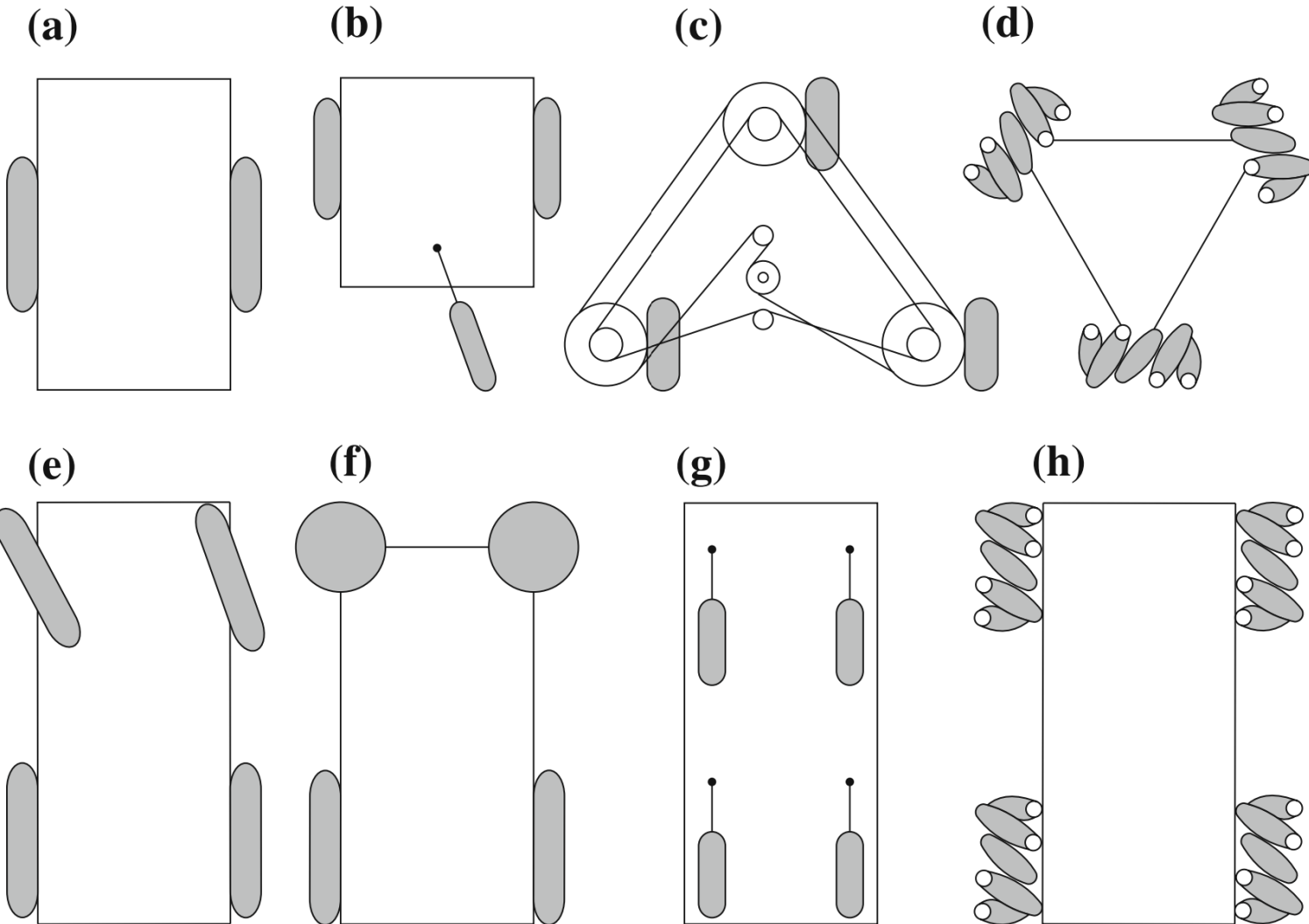
Basics and Advances



Ph.D. Ha Le Nhu Ngoc Thanh
HCMC Univ. of Tech. & Edu.
Faculty of Mechanical Engineering
Mechatronics Dept.

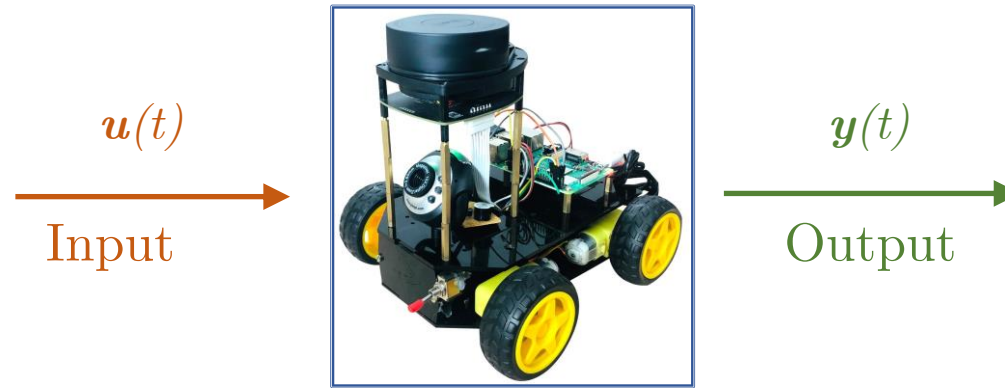
Mobile robot configurations

Mobile Robot Kinematics

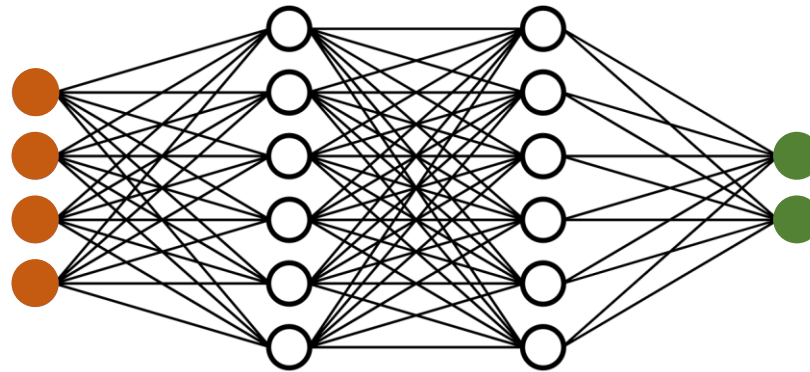


I. System model concept

System model is to use to map the input and output



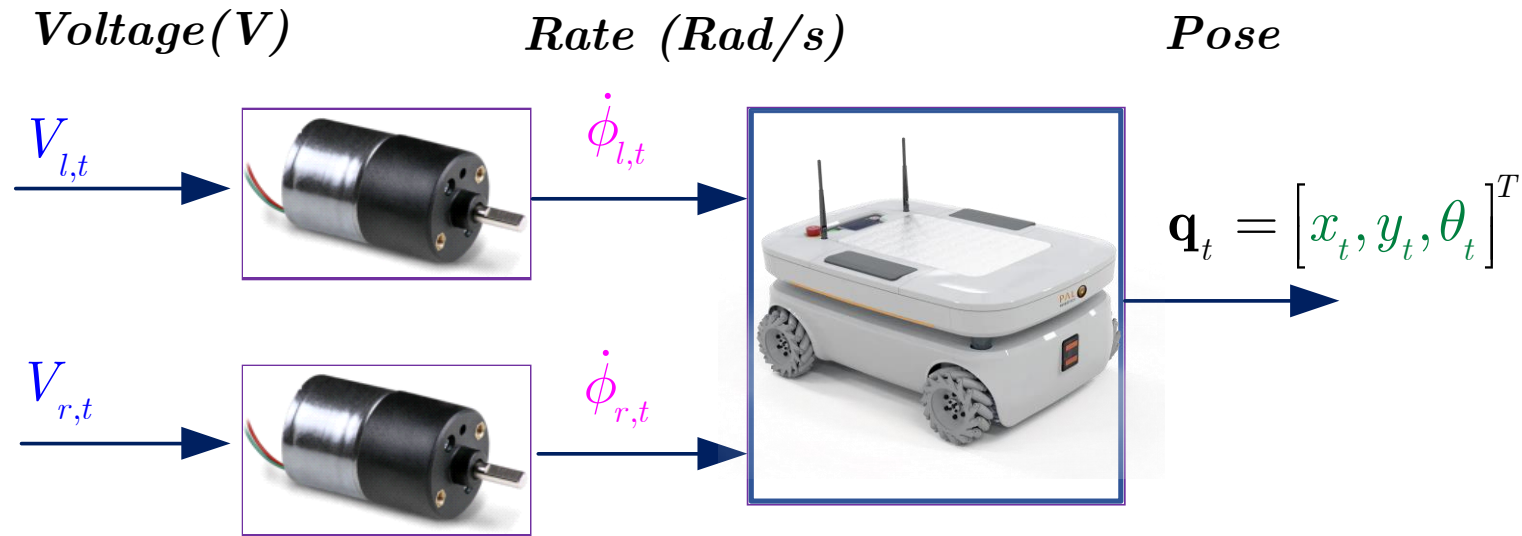
$$\begin{cases} \dot{x}(t) = f(x(t), u(t)) \\ y(t) = g(x(t), u(t)) \end{cases}$$



II. Differential drive WMR

Differential Drive WMR: Motion of each wheel is controlled by a separate DC motor

Model of Differential Drive WMR:



1. Forward kinematics:

Given $\dot{\phi}_1, \dot{\phi}_2, \dots, \dot{\phi}_t$, how will the robot move?

2. Inverse kinematics:

Given a desired movement $\mathbf{q}_1, \mathbf{q}_2, \dots, \mathbf{q}_t$, what commands should we send to the wheels?

$$\dot{\mathbf{q}}_t = f \begin{pmatrix} \dot{\phi}_r \\ \dot{\phi}_l \end{pmatrix} ???$$

$$\begin{pmatrix} \dot{\phi}_r \\ \dot{\phi}_l \end{pmatrix} = f(\dot{\mathbf{q}}_t) ???$$

II. Differential drive WMR

NOTATIONS

World frame: x^w, y^w

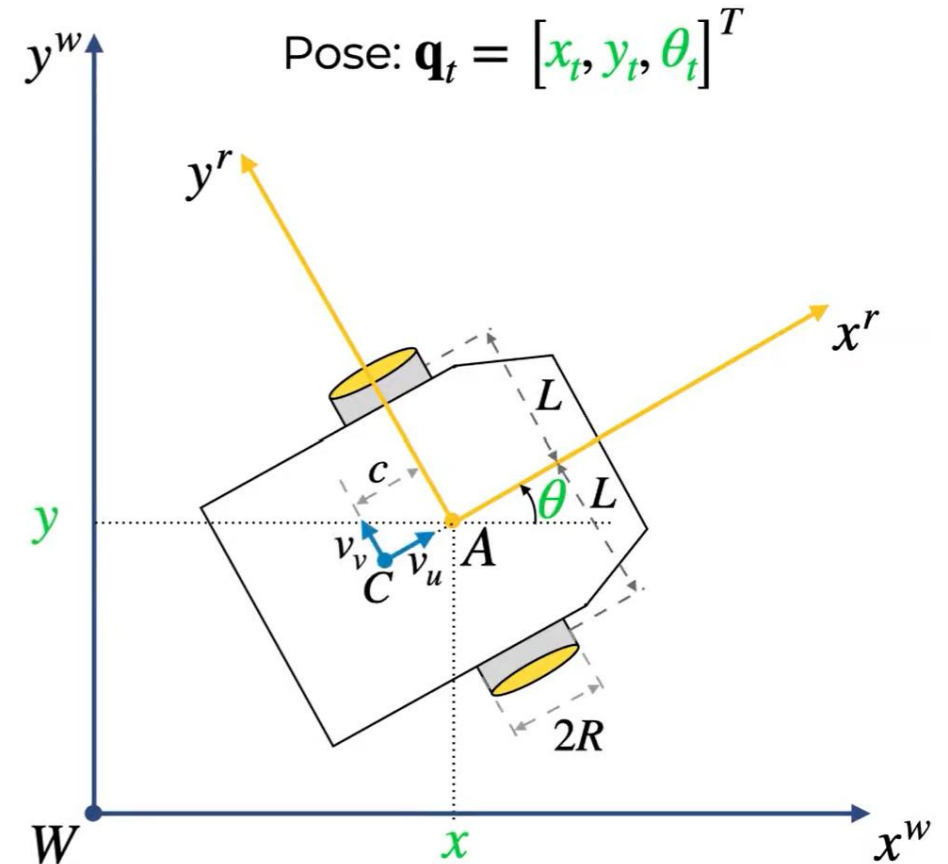
Robot frame: x^r, y^r

⊕ **Assumption 1:** robot is **symmetric** along longitudinal axis (x^r)

- Equidistant wheels (axle length = $2L$)
- Identical wheels ($R_l = R_r = R$)
- Center of mass (C) on x^r at distance c from A (A rotation point)

⊕ **Assumption 2:** robot is rigid body

- Distance between any two points of the robot does not change in time
- In particular $\dot{c} = 0$



Forward kinematics, jacobian matrix?

II. Differential drive WMR

NOTATIONS

Rigid body rotation: $\omega = [0, 0, \dot{\theta}]^T$

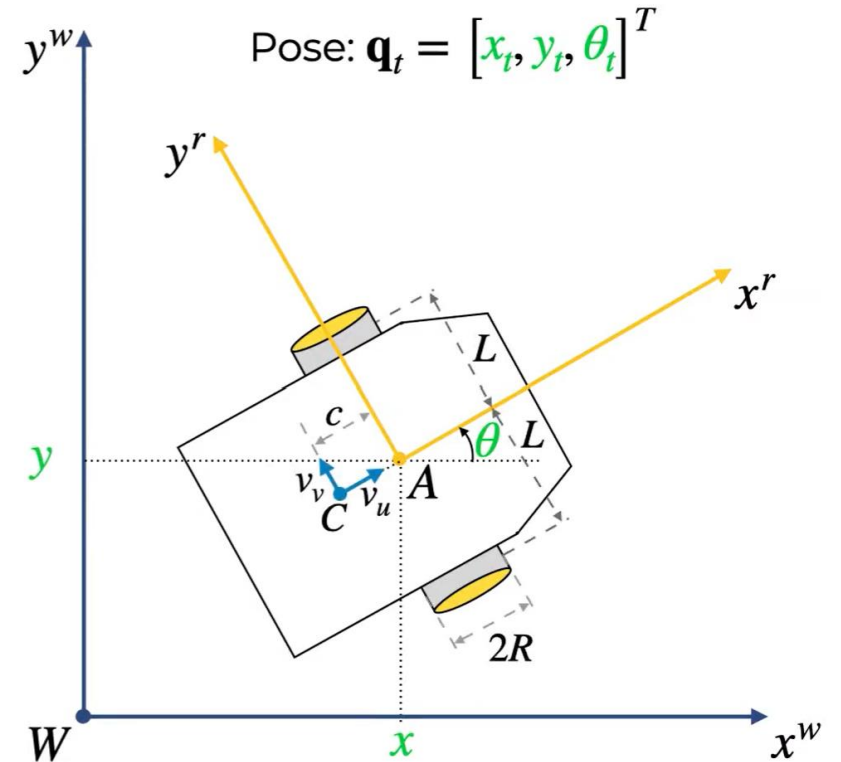
$$\mathbf{v}_A^w = \begin{pmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \end{pmatrix} = {}^wR(z, \theta) \cdot \mathbf{v}_A^r$$

$$= \begin{pmatrix} \cos \theta & -\sin \theta & 0 \\ \sin \theta & \cos \theta & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} v_u \\ v_v - c\dot{\theta} \\ 0 \end{pmatrix} \quad (1)$$

$$\Rightarrow \text{only } x, y \text{ interest} \quad \mathbf{v}_A^w = \begin{pmatrix} \cos \theta & -\sin \theta \\ \sin \theta & \cos \theta \end{pmatrix} \begin{pmatrix} v_u \\ v_v - c\dot{\theta} \end{pmatrix}$$

General kinematic equations : (*include angular rate*)

$$\begin{cases} \dot{x} = v_u \cos \theta - (v_v - c\dot{\theta}) \sin \theta \\ \dot{y} = v_u \sin \theta + (v_v - c\dot{\theta}) \cos \theta \\ \dot{\theta} = \omega \end{cases} \quad (2)$$



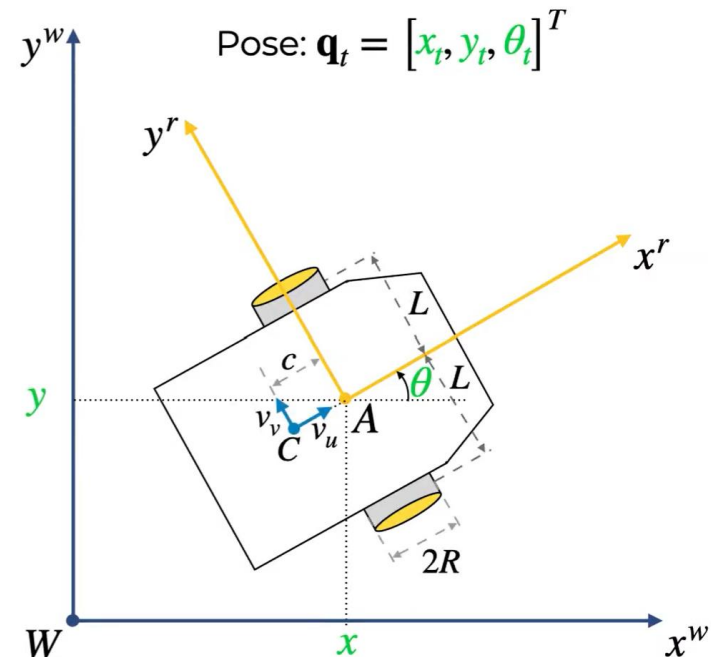
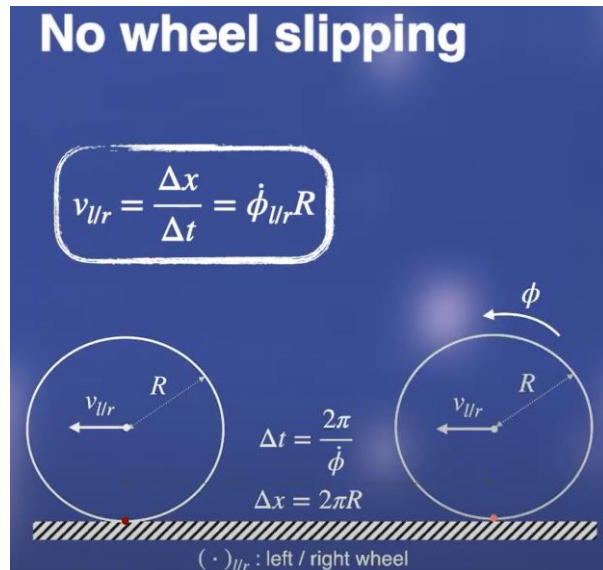
II. Differential drive WMR

Kinematics constraint: Pure rolling

- Assumption: Pure rolling
 - ✓ (1) No moving sideways (skidding): point **A** has null lateral component

$$\mathbf{v}_A^r = \begin{bmatrix} v_u \\ v_v - c\dot{\theta} \end{bmatrix} = \begin{bmatrix} v_u \\ 0 \end{bmatrix}$$

- ✓ (2) No wheel slipping: every a full revolution ($\Delta\phi = 2\pi$), each wheel travels a distance equal to its circumference ($\Delta x = 2\pi R$)



II. Differential drive WMR

No skidding: $v_v - c\dot{\theta} = 0$

find : $\dot{\mathbf{q}}_t = \begin{bmatrix} \dot{x}_t \\ \dot{y}_t \\ \dot{\theta}_t \end{bmatrix} = ?$

$$\xrightarrow[\textcolor{red}{v_A}]{\textcolor{red}{Velocities}} \boxed{\begin{cases} \dot{x} = v_u \cos \theta - \cancel{(v_v - c\dot{\theta}) \sin \theta} \\ \dot{y} = v_u \sin \theta + \cancel{(v_v - c\dot{\theta}) \cos \theta} \\ \dot{\theta} = \omega \end{cases}} \xrightarrow[\textcolor{green}{\dot{\mathbf{q}}_t}]{\textcolor{green}{Pose variation}}$$

let $v_A = v_u$

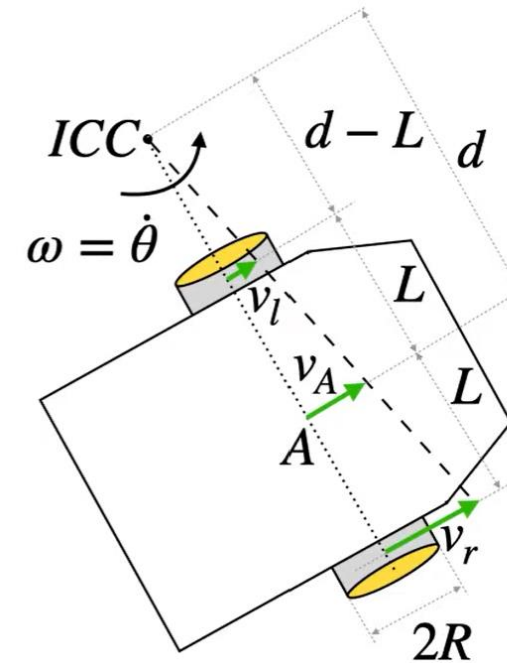
$$\Leftrightarrow \dot{\mathbf{q}}_t = \begin{bmatrix} \dot{x}_t \\ \dot{y}_t \\ \dot{\theta}_t \end{bmatrix} = \begin{bmatrix} \cos \theta_t & 0 \\ \sin \theta_t & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} \textcolor{red}{v_A} \\ \textcolor{red}{\omega_t} \end{bmatrix} \quad (3)$$

II. Differential drive WMR

Instantaneous Center of Curvature (ICC)

No slipping assumption \rightarrow All points in a pure rotation field (centered at ICC) have velocity orthogonal to distance to ICC, how to get v_l , v_A , v_r , d ?

$$\begin{cases} v_l = \omega d - L \\ v_A = \omega d \\ v_r = \omega d + L \end{cases} \quad 4$$
$$\Rightarrow d = L \frac{v_r + v_l}{v_r - v_l}$$



Notes :

1. If $v_r = v_l \Rightarrow$ **no turn** \Rightarrow ICC is underfined
2. If $v_r = -v_l \Rightarrow$ **turn "on itself"** \Rightarrow ICC \equiv A
3. If $v_r = 0$ (or $v_l = 0$) \Rightarrow **turn "on wheel"** $\Rightarrow d = -L$ (or $d = L$)

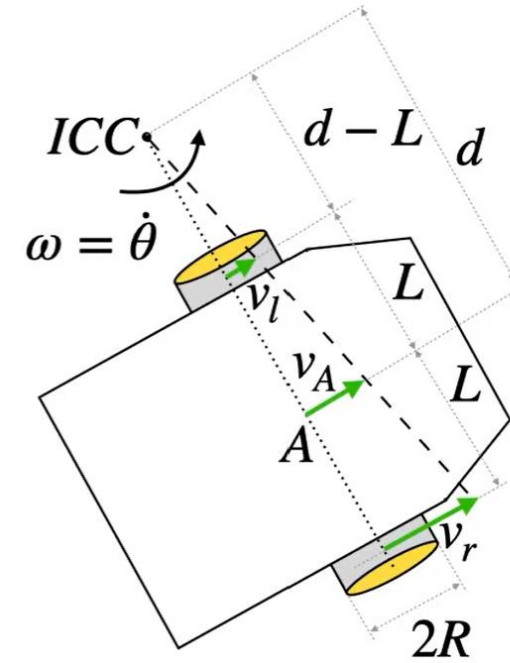
II. Differential drive WMR

Forward kinematics

$$Find : \begin{bmatrix} v_A \\ \omega \end{bmatrix} = \underset{Jacobian}{J} \begin{bmatrix} \dot{\phi}_r \\ \dot{\phi}_l \end{bmatrix}$$

$$4 \Rightarrow \begin{cases} v_r + v_l = 2\omega d \\ v_r - v_l = 2\omega L \end{cases} \Rightarrow \begin{cases} d = L \frac{v_r + v_l}{v_r - v_l} \\ v_A = \omega d = \frac{v_r + v_l}{2} \\ \omega = \frac{v_r - v_l}{2L} \end{cases}$$

$$\begin{aligned} v_r &= \dot{\phi}_r R, v_l = \dot{\phi}_l R \\ \Rightarrow \begin{cases} v_A = \frac{R}{2} \dot{\phi}_r + \dot{\phi}_l \\ \omega = \frac{R}{2L} \dot{\phi}_r - \dot{\phi}_l \end{cases} &\Leftrightarrow \boxed{\begin{bmatrix} v_A \\ \omega \end{bmatrix} = \underbrace{\frac{R}{2} \begin{bmatrix} 1 & 1 \\ 1/L & -1/L \end{bmatrix}}_{Jacobian} \begin{bmatrix} \dot{\phi}_r \\ \dot{\phi}_l \end{bmatrix}} \end{aligned} \quad (5)$$

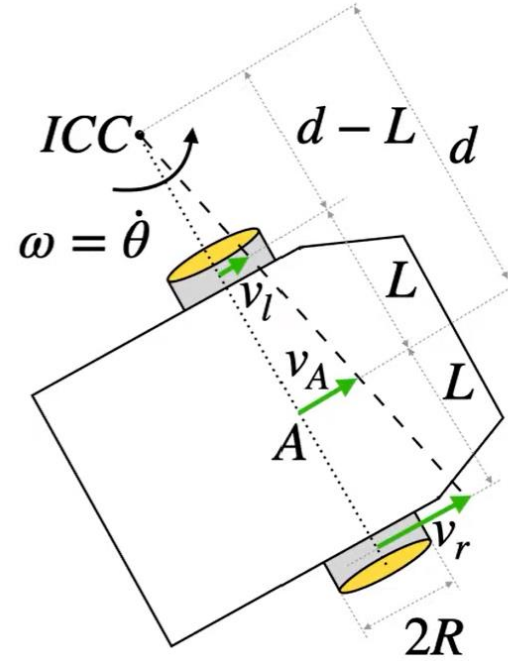


II. Differential drive WMR

Forward kinematics

From (3) & (5)

$$\Rightarrow \dot{\mathbf{q}}_t = \frac{R}{2} \begin{bmatrix} \cos \theta & 0 \\ \sin \theta & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 1 \\ 1/L & -1/L \end{bmatrix} \begin{bmatrix} \dot{\phi}_r \\ \dot{\phi}_l \end{bmatrix}$$

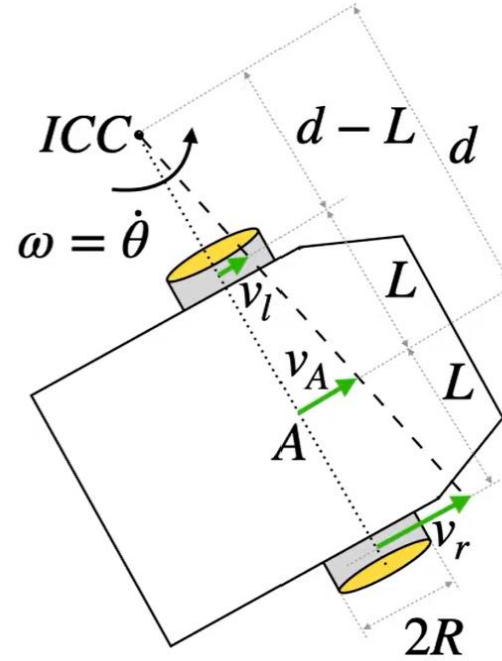


II. Differential drive WMR

Inverse kinematics

From Eq.(5)

$$\Rightarrow \begin{bmatrix} \dot{\phi}_r \\ \dot{\phi}_l \end{bmatrix} = \frac{1}{R} \begin{bmatrix} 1 & L \\ 1 & -L \end{bmatrix} \begin{bmatrix} v_A \\ \omega \end{bmatrix} \quad (6)$$

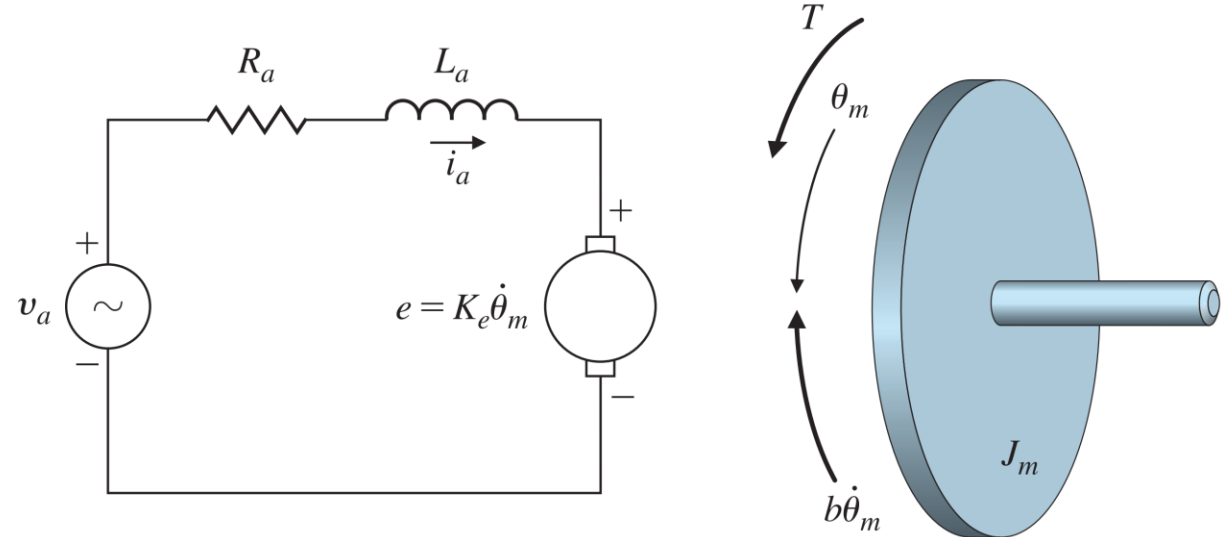
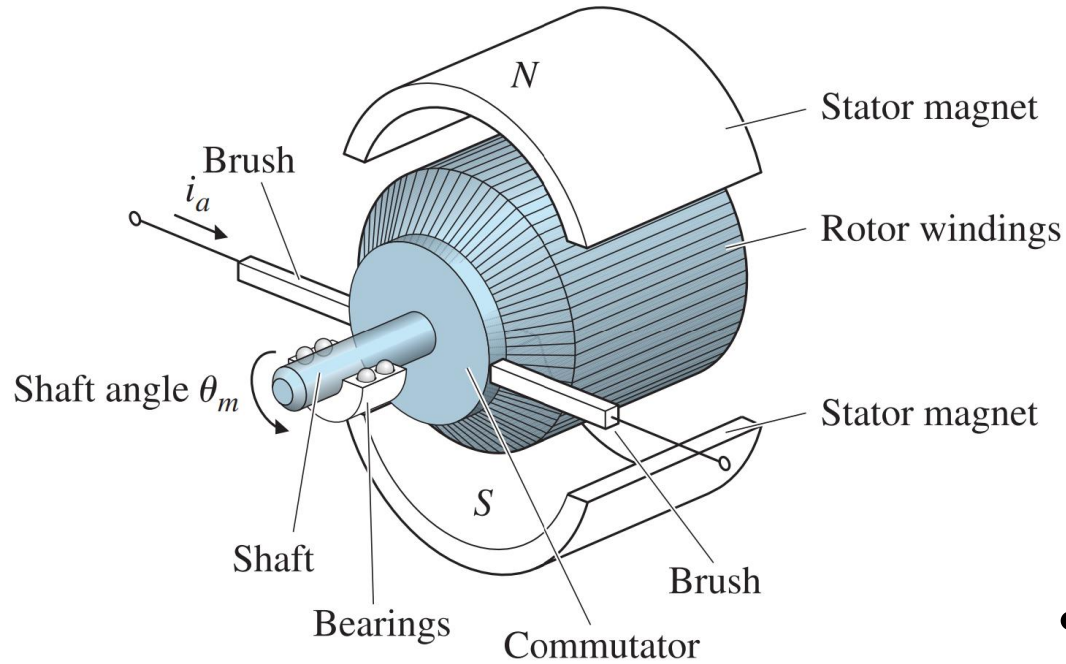


$$\text{where } \begin{bmatrix} \dot{x}_t \\ \dot{y}_t \\ \dot{\theta}_t \end{bmatrix} = \begin{bmatrix} \cos \theta_t & 0 \\ \sin \theta_t & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} v_A \\ \omega_t \end{bmatrix}$$

II. Differential drive WMR

DC motor model

Reference: Franklin, "Feedback Control of Dynamic Systems" 8th Edition, Pearson 2020



*The generated electromotive force (emf) works against the applied armature voltage, it is called the **back emf**.*

- The torque T on the rotor in terms of the armature current i_a : $\boxed{T = K_t i_a}$, $K_t \left[\frac{N}{A} \right]$: torque const
- The express of **back emf** voltage e in terms of the shaft's rotational velocity $\dot{\theta}_m$: $\boxed{e = K_e \dot{\theta}_m}$, $K_e \left[\frac{V}{rad/s} \right]$: electric const
- $K_t = K_e$, but unit are different needing to translate to a certain

II. Differential drive WMR

DC motor model

Reference: Franklin, "Feedback Control of Dynamic Systems" 8th Edition, Pearson 2020

- Electrical subsystem (Kirchhoff's law):

$$L_a \frac{di_a}{dt} + R_a i_a = v_a - K_e \dot{\theta}_m \quad (7)$$

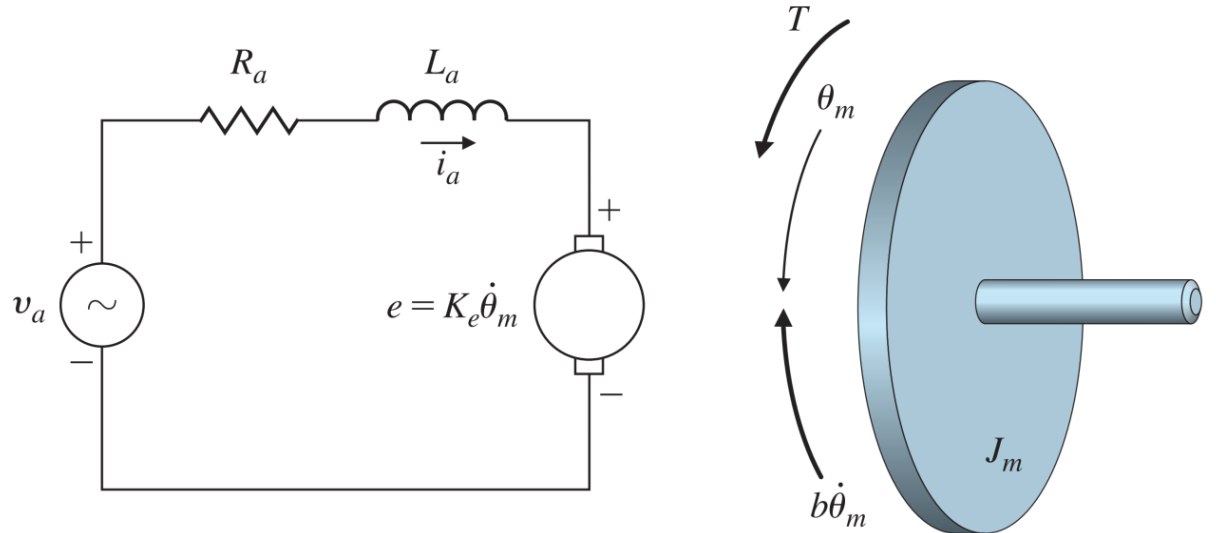
- Mechanical subsystem (Newton's law):

$$J_m \ddot{\theta}_m + b \dot{\theta}_m = K_t i_a \quad (8)$$

where J_m is inertia, and b viscous friction coefficient

$$(7) \Rightarrow i_a = \frac{v_a - K_e \dot{\theta}_m}{R_a}, \quad (L_a: \text{be neglected})$$

In many cases the relative effect of the *inductance* is negligible compared with the mechanical motion



II. Differential drive WMR

DC motor model

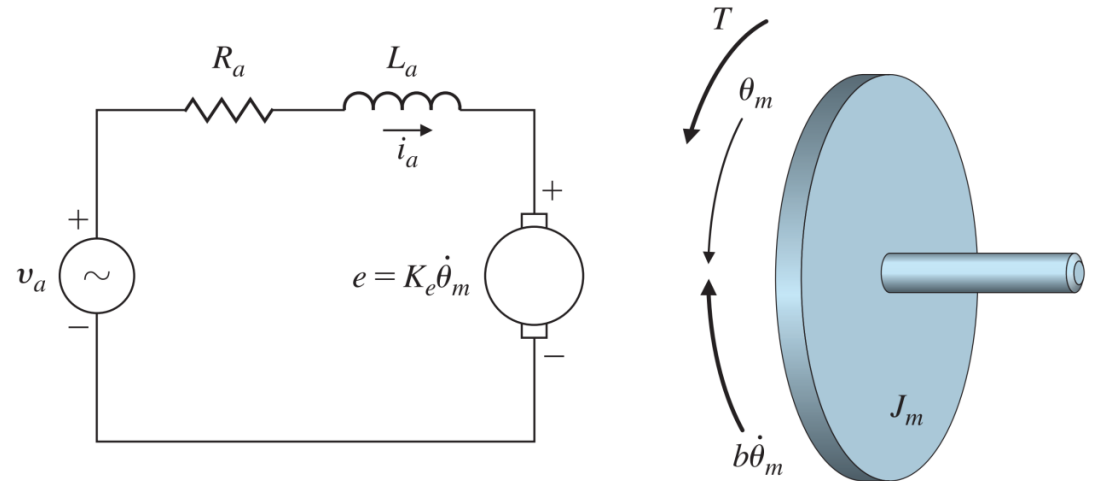
Reference: Franklin, "Feedback Control of Dynamic Systems" 8th Edition, Pearson 2020

$$(8) \Rightarrow \boxed{J_m \ddot{\theta}_m + \left(b + \frac{K_t K_e}{R_a}\right) \dot{\theta}_m = \frac{K_t}{R_a} v_a} \quad (ODE)$$

$$\xrightarrow{\text{Laplace}} G(s) = \frac{\Theta_m(s)}{V_a(s)} = \frac{\frac{K_t}{R_a}}{J_m s^2 + \left(b + \frac{K_t K_e}{R_a}\right) s}$$

$$\Rightarrow \boxed{G(s) = \frac{K}{s \tau s + 1}} \quad (TF)$$

$$\text{where } K = \frac{K_t}{bR_a + K_t K_e}, \tau = \frac{R_a J_m}{bR_a + K_t K_e}$$

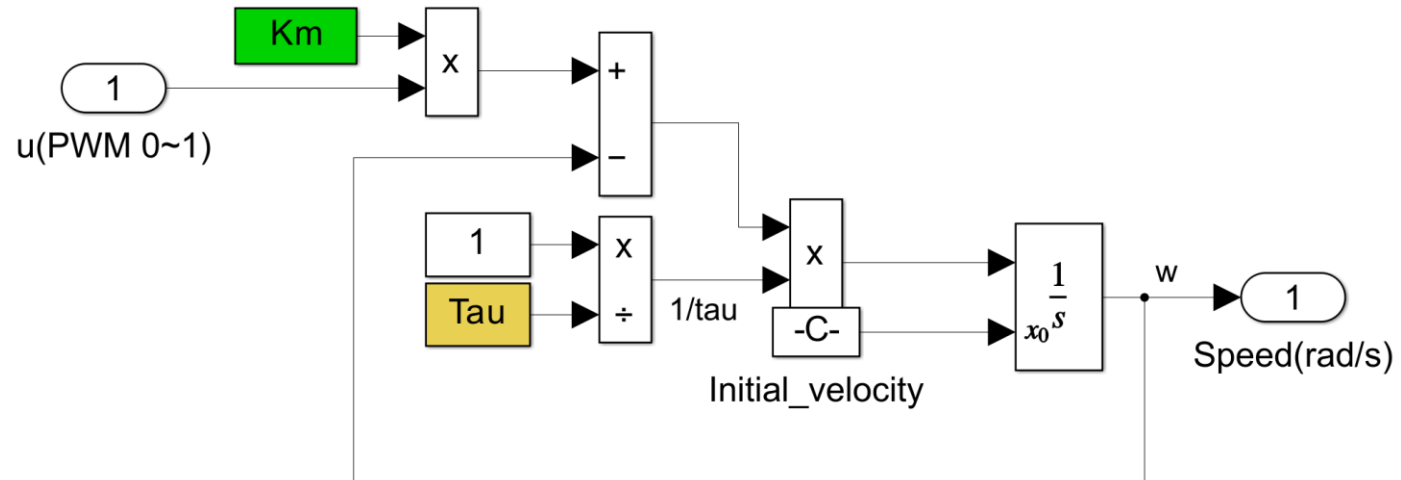


In many cases, a transfer function between the motor input and the output speed ($\omega = \dot{\theta}_m$) is required:

$$\boxed{\frac{\Omega(s)}{V_a(s)} = s \frac{\Theta_m(s)}{V_a(s)} = \frac{K}{\tau s + 1}}$$

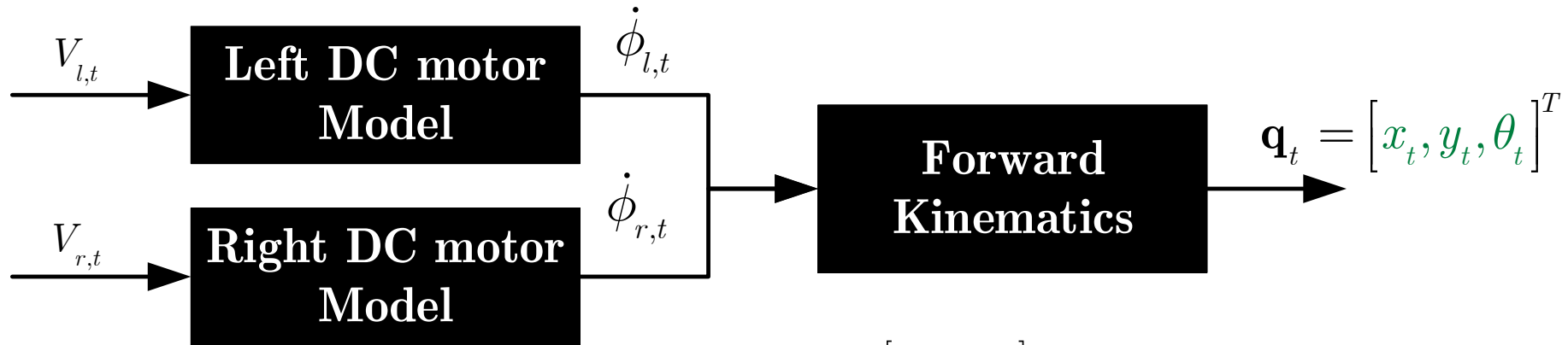
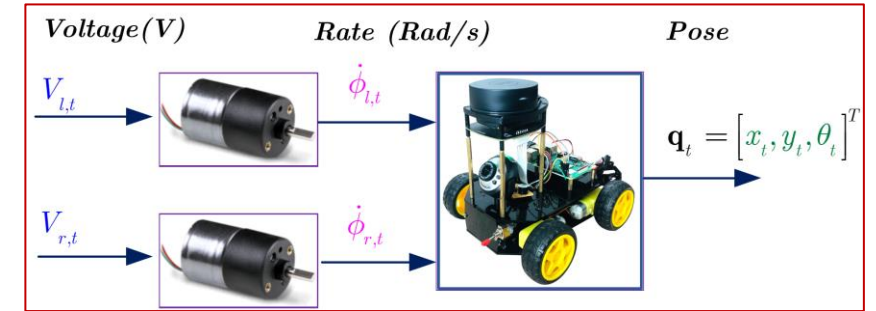
II. Differential drive WMR

DC motor model



II. Differential drive WMR

DC motor model

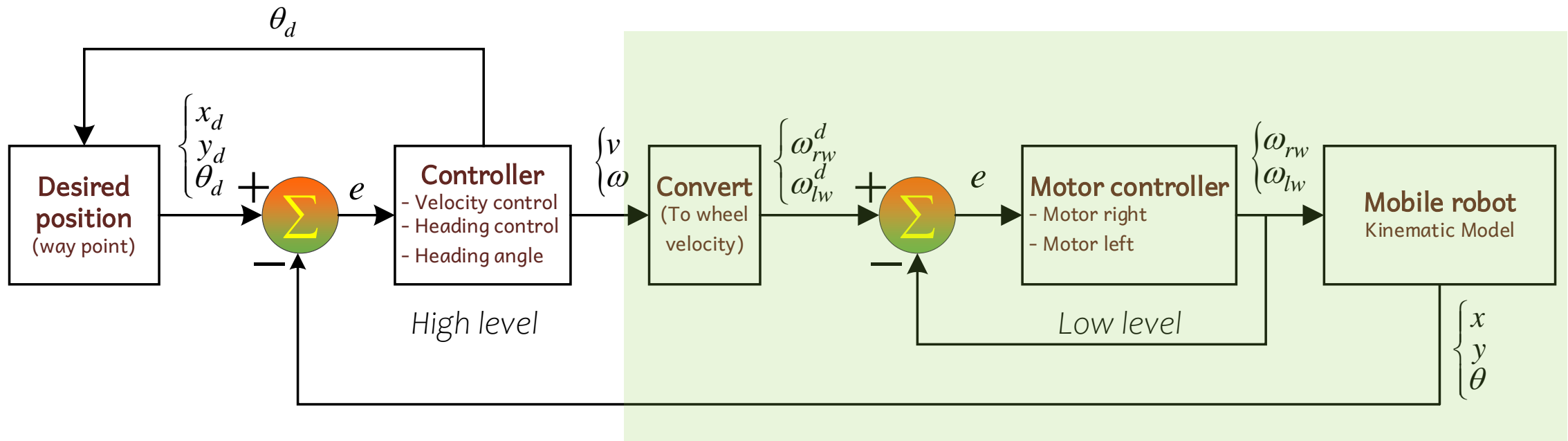


$$\frac{\Omega(s)}{V_a(s)} = \frac{K}{\tau s + 1}$$

$$\dot{\mathbf{q}}_t = \frac{R}{2} \begin{bmatrix} \cos \theta & 0 \\ \sin \theta & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 1 \\ 1/L & -1/L \end{bmatrix} \begin{bmatrix} \dot{\phi}_r \\ \dot{\phi}_l \end{bmatrix}$$

Controller design – PID controller (basic)

- + Controller: v and ω
- + From controller v and ω , it can be generated to ω_{rw}^d and ω_{lw}^d



Controller design

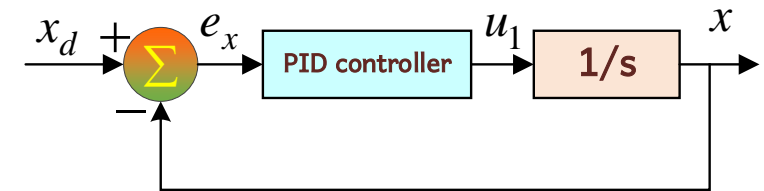
$$\text{From : } \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{\theta} \end{bmatrix} = \frac{R}{2} \begin{bmatrix} \cos \theta & 0 \\ \sin \theta & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 1 \\ 1/L & -1/L \end{bmatrix} \begin{bmatrix} \dot{\phi}_r \\ \dot{\phi}_l \end{bmatrix} \Rightarrow \begin{cases} \dot{x} = \frac{R}{2} \omega_{rw} + \omega_{lw} \cos \theta \\ \dot{y} = \frac{R}{2} \omega_{rw} + \omega_{lw} \sin \theta \\ \dot{\theta} = \frac{R}{2} \left(\frac{\omega_{lw} + \omega_{rw}}{L} \right) \end{cases}$$

+ Position (x,y) controller u

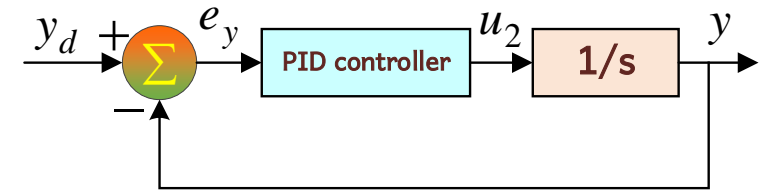
Let give a controller as follows:

$$u = \begin{bmatrix} u_1 \\ u_2 \\ u_3 \end{bmatrix} = \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{\theta} \end{bmatrix} = \begin{bmatrix} PID \ x_d - x \\ PID \ y_d - y \\ PID \ \theta_d - \theta \end{bmatrix} = \begin{bmatrix} K_1 \ x_d - x \\ K_2 \ y_d - y \\ K_3 \ \theta_d - \theta \end{bmatrix}$$

Controller for x axis: $\dot{x} = u_1$

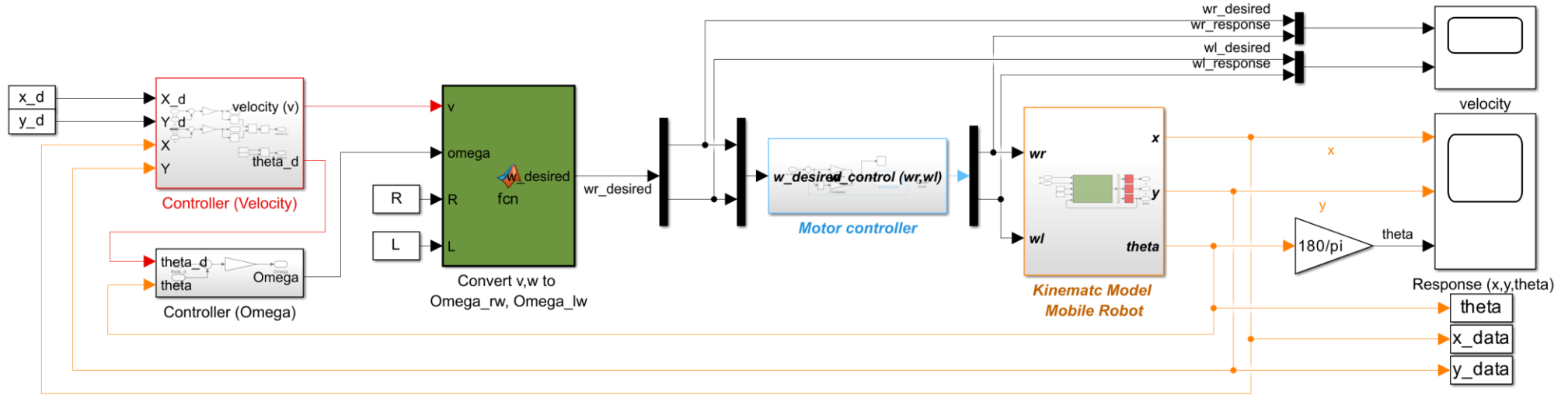


Controller for y axis : $\dot{y} = u_2$



Controller design

Simulation:

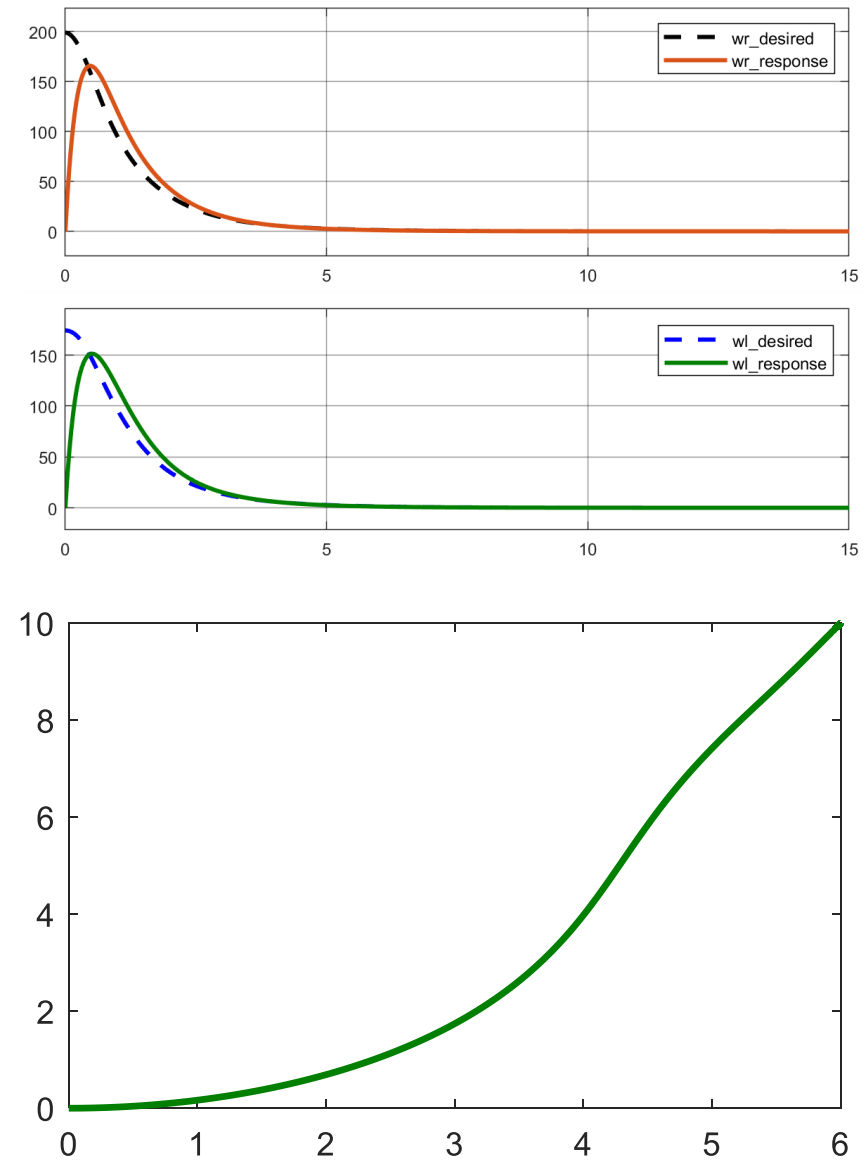
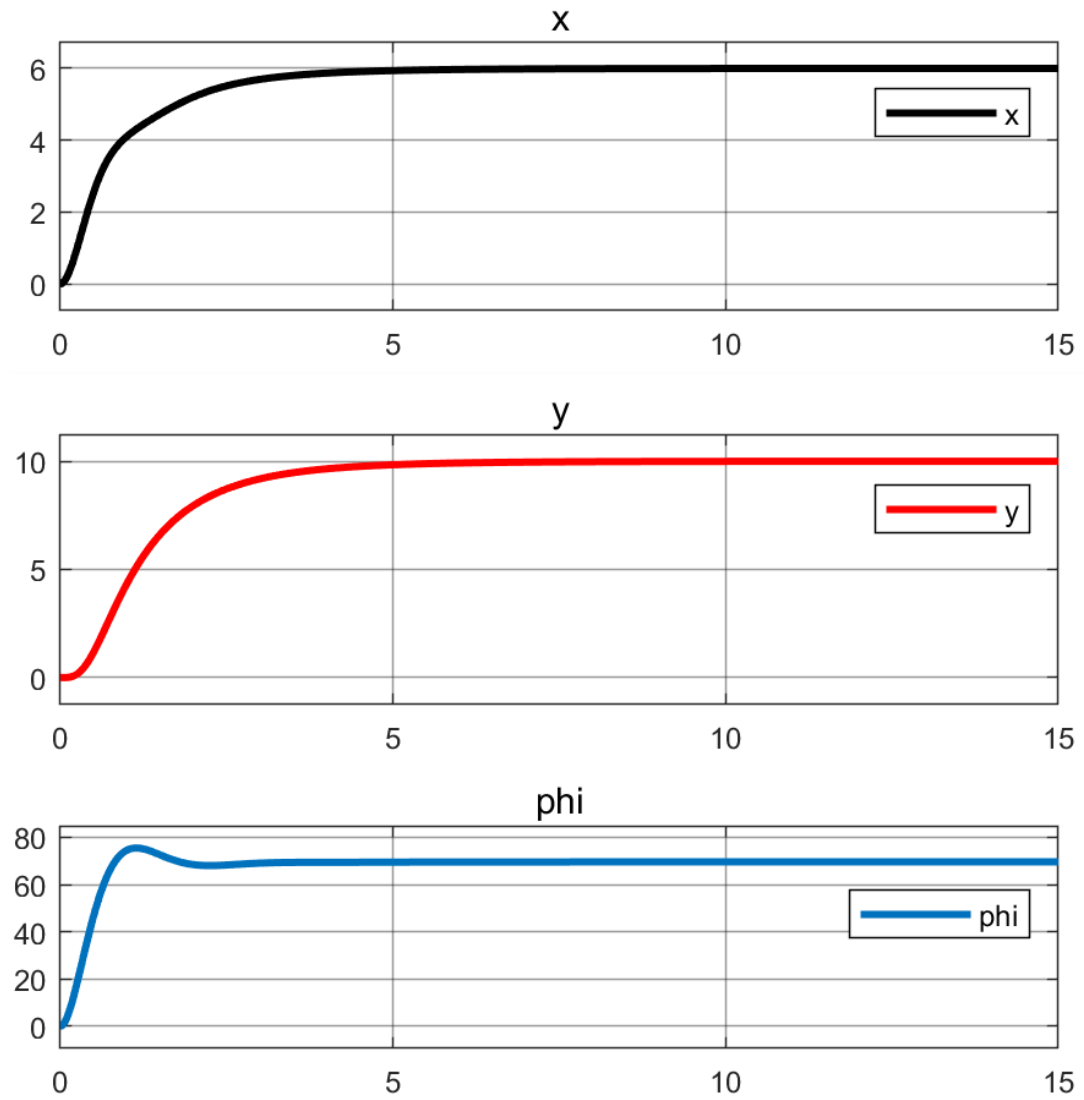


```
clc; clear all; close all;  
R=0.05 %5cm  
L=0.2 %40cm  
x_Init=0  
y_Init=0  
phi_Init=0*pi/180  
%% setpoint  
x_d=6  
y_d=10  
%% Motor Dynamics  
Km=500;  
Tau = 2;
```

```
%% mobile robot control  
kpx=0.8  
kpy=0.8  
kptheta=3  
%% motor control  
kp=0.02  
ki=0.015
```

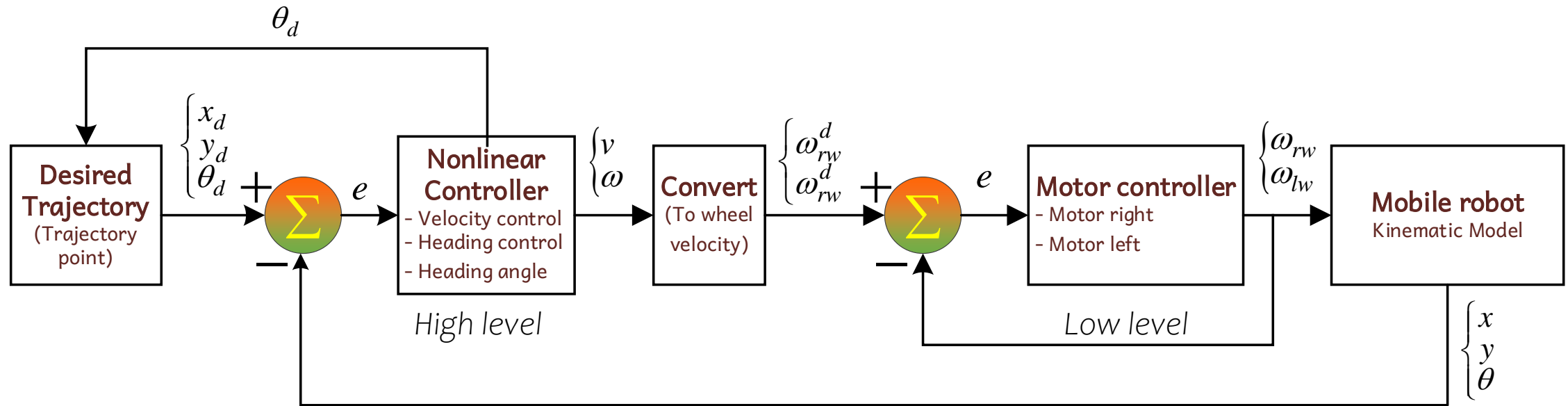
Controller design

Simulation:

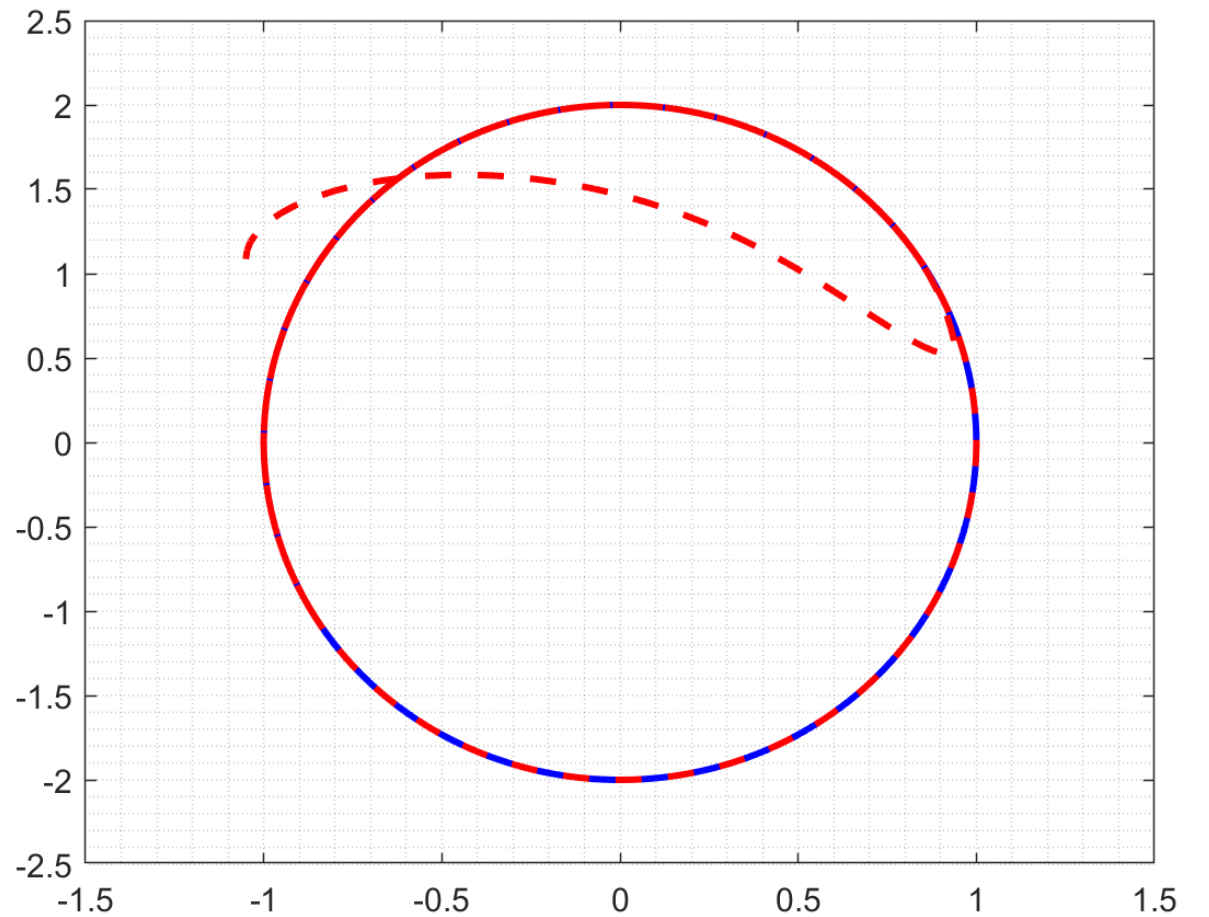
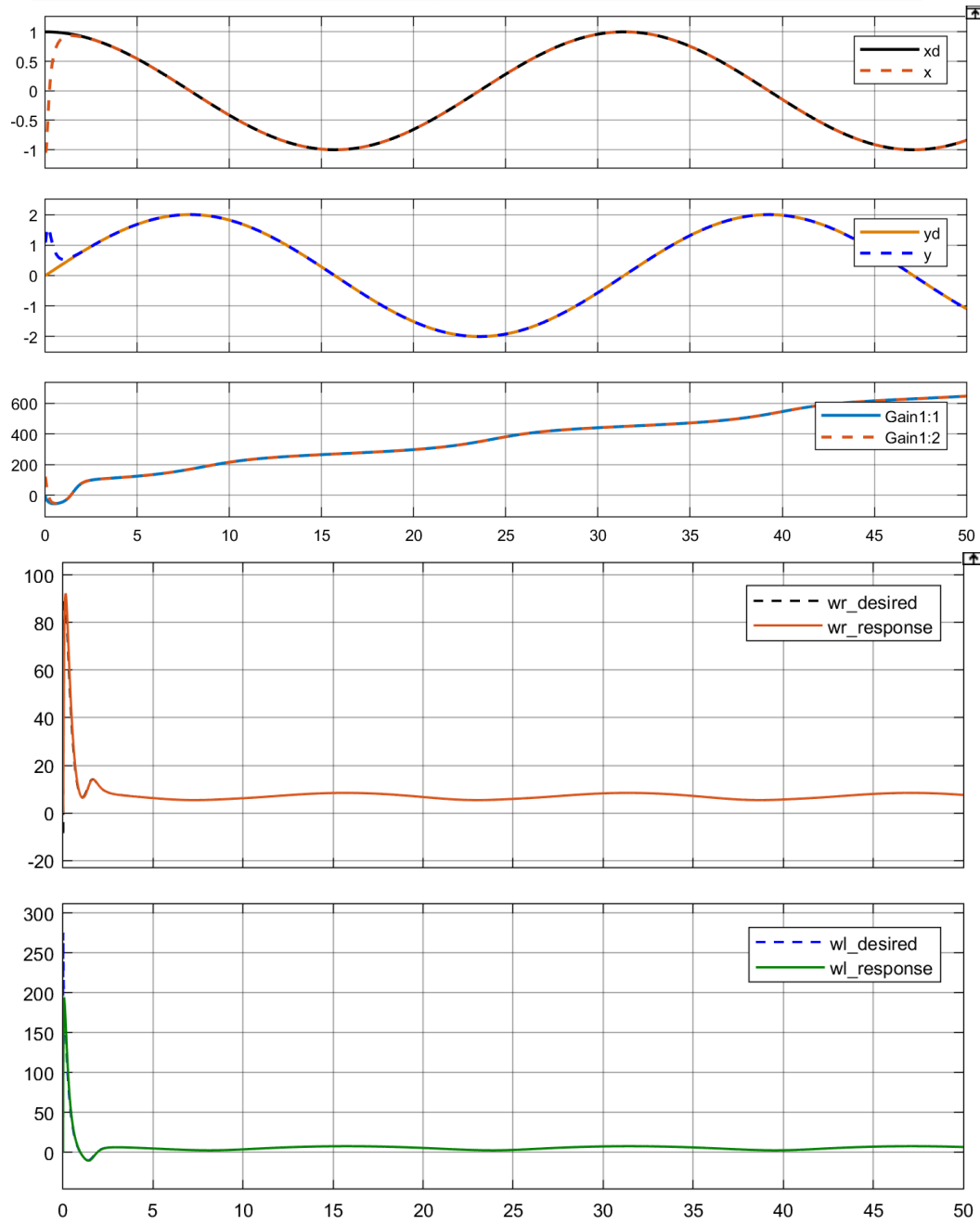


Controller design – Linear, Nonlinear Tracking Control

- + Controller: v and ω
- + From controller v and ω , it can be generated to ω_{rw}^d and ω_{lw}^d



Controller design – Linear Tracking Control



Controller design – Linear Tracking Control

