Cvičení č. 11 - Aposteriorní odhad chyby (metoda ZZ)

Z MKP řešení plyne

$$u^{MKP}(x) = N(x)r$$

$$\sigma^{MKP}(x) = DB(x)r$$
,

kde B obsahuje derivace interpolačních funkcí. Předpokládáme, že skutečnému průběh napětí je bližší průběh

$$\sigma^*(x) = N(x)r_{\sigma}$$

Koeficienty r_σ určíme tak, aby chyba mezi přibližným napětím σ^{MKP} a "vylepšeným napětím" σ^* ve smyslu nejmenších čtverců byla co nejmenší

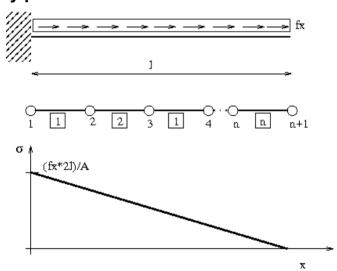
$$\int_{\Omega} \left(\sigma^* - \sigma^{MKP}
ight)^T \left(\sigma^* - \sigma^{MKP}
ight) \; d\Omega o min.$$

Odtud po úpravách obdržíme (viz. přednáška):

$$\left(\int_{\Omega} N^T N \, d\Omega
ight) r_{\sigma} = \left(\int_{\Omega} N^T \sigma^{MKP} \, d\Omega
ight)$$

$$Ar_{\sigma}=b$$

Příklad 1: tažený tlačený prut



A dále budeme uvažovat $f_x=1$, l=3 , EA=1

Analytické řešení:

Staticky určitá kce, průběh napětí určíme z podmínky rovnováhy $\sigma(x)=f_x(l-x)/A, \;\; x\in (0,l)$

Pusun určíme integrací deformace: $u(x)=\int_0^x\sigma(s)/Eds=\left[(f_xls-f_xs^2/2)/(EA)\right]_0^x=-(f_x/EA)*(-x^2/2-lx)$

Řešení MKP

```
In [3]: #pocet prvku na delku
         n = 5
         1 = 3/n;
         E = 1;
         A = 1;
         # mkp reseni
         ki = (E*A/1)*[1 -1; -1 1];
         fi = [1^2/(2*1) 1^2/(2*1)];
         K = zeros (n+1);
         F = zeros (n+1, 1);
         for i=1:n
             loc = [i i+1];
             K(loc, loc) += ki;
             F(loc)+= fi';
         endfor
         u = K(2:n+1, 2:n+1) \setminus (F(2:n+1,1));
         U = [0; u]
         #plot analytical solution
         hold on;
         x = 0:0.1:3;
         plot (x, -x.^2/2+3*x, "b;u;", x, -x+3, "r;N;")
         sig = zeros(n,1);
         #evaluate stress and plot obtained solution
         for i=1:n
            eps = (U(i+1)-U(i))/1;
             sig(i) = E*eps;
             N = A*E*eps;
             plot ([(i-1)*l i*l], [U(i) U(i+1)], "b--")
plot ([(i-1)*l i*l], [N N], "r--")
         endfor
```

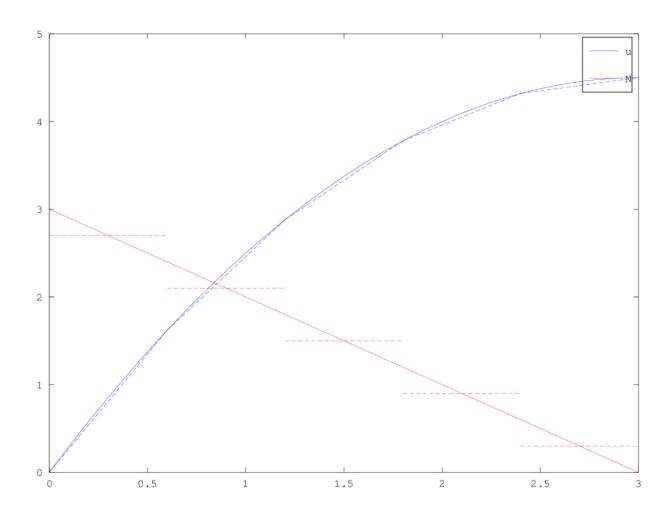
0.00000

1.62000

2.88000

3.78000

4.32000 4.50000



Určení vyhlazeného napětí σ^*

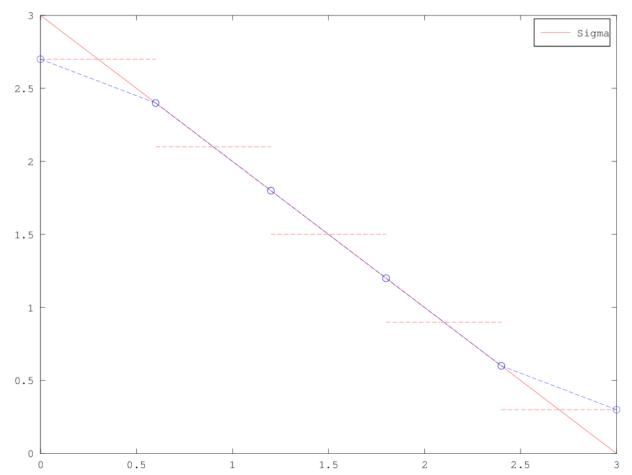
$$A^e = \int_l egin{bmatrix} N_1 \ N_2 \end{bmatrix} egin{bmatrix} N_1 & N_2 \end{bmatrix} \, dx = egin{bmatrix} l/3 & l/6 \ l/6 & l/3 \end{bmatrix} = egin{bmatrix} l/2 \ & l/2 \end{bmatrix}$$

$$b^e = \int N^T \sigma^e \; dx = \left\{ egin{aligned} \sigma^e l/2 \ \sigma^e l/2 \end{array}
ight\}$$

Pro uzlové hodnoty vyhlazeného napětí pak platí $Ar_{\sigma}^{=}b$

kde A se získá lokalizací A_i , b lokalizaci b_i .

```
In [4]: # evaluate recovered stresses
        Ai = [1/2, 0; 0, 1/2];
        bi = [1/2;1/2];
        A = zeros(n+1);
        B = zeros(n+1,1);
        for i=1:n
            loc = [i i+1];
            A(loc, loc) += Ai;
            B(loc)+= sig(i)*bi;
        endfor
        sig2 = A \B;
        #plot analytical solution
        hold on;
        x = 0:0.1:3;
        plot (x, -x+3, "r;Sigma;")
        #plot recovered stresses
        hold on;
        for i=1:n
            plot ([(i-1)*l i*l], [sig(i) sig(i)], "r--")
            plot ([(i-1)*l i*l], [sig2(i) sig2(i+1)], "o--")
        endfor
```



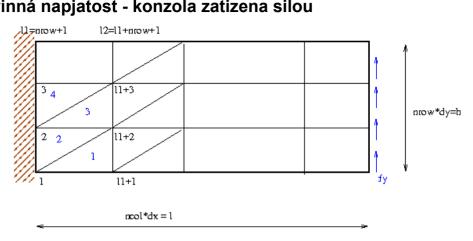
Odhad chyby

$$|e|=\int_{\Omega}rac{1}{E(x)}\Big(\sigma_x^*(x)-\sigma_x^{mkp}(x)\Big)^2dx.$$

$$|e| = \sum_e \int_{l_e} rac{1}{E(x)} \Big(\sigma_x^*(x) - \sigma_x^{mkp}(x)\Big)^2 dx.$$

```
In [5]: # numericka integrace
        w = [1.0; 1.0];
        xi=[-1./sqrt(3); 1/sqrt(3)];
        #prispevek do chyby po elementech
        e = zeros(n,1);
        err = 0.0;
        hold on;
        for i=1:n
            for ip=1:2
                sig2xi = (1-xi(ip))/2*sig2(i)+(1+xi(ip))/2*sig2(i+1);
                dsig = sig2xi-sig(i);
                e(i) += (dsig^2/E)*w(ip)*1/2;
            endfor
            err = err+e(i);
        endfor
        err
        for i=1:n
            plot ([(i-1)*l i*l], [e(i) e(i)], "o--")
        e =
           0.018000
           0.018000
           0.018000
           0.018000
           0.018000
        err = 0.090000
            0.02
          0.0195
           0.019
          0.0185
           0.018 💠
          0.0175
           0.017
          0.0165
           0.016
                 0
                               0.5
                                               1
                                                             1.5
                                                                              2
                                                                                            2.5
                                                                                                            3
```

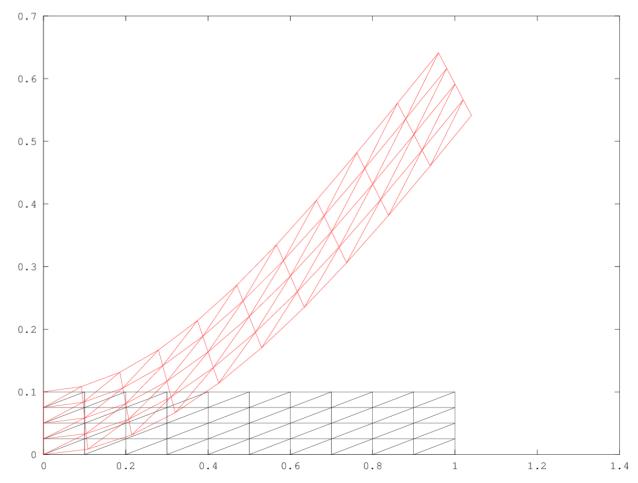
Příklad 2: Rovinná napjatost - konzola zatizena silou



E = 3000 I=1.0, h=0.1

Pozn: Řešení úlohy MKP není zveřejněno.

```
In [7]: # zobrazeni site
        hold on;
        sig;
        triplot(enodes,x,y,'k')
        triplot(enodes,xnew,ynew,'r')
        #for ie=1:nelem
             trimesh(enodes(ie,:),xnew(enodes(ie,:)),ynew(enodes(ie,:)),[sig(ie,1),sig(ie,1),sig(ie,1)])
        #endfor
```



Odhad chyby

Výpočet vyhlazených napětí

$$A^e = \int_{A_e} N^T N dA = \int_{A_e} egin{bmatrix} N_1 \ N_2 \ N_3 \end{bmatrix} egin{bmatrix} N_1 & N_2 & N_3 \end{bmatrix} dA$$

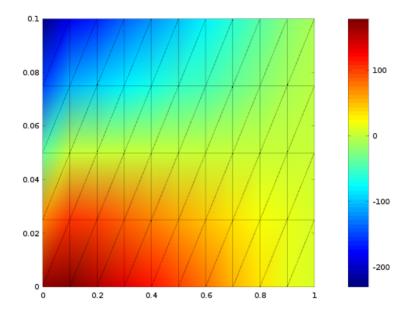
$$b_i = \int_{A_e} N^T \sigma dA = \int_{A_e} egin{bmatrix} N_1 \ N_2 \ N_3 \end{bmatrix} \sigma(x) dx$$

$$Ar_{\sigma^*}=b$$

```
In [8]: function [Ai, bi] = plane_stress_reco (xe,ye,sig)
            # numericka integrace
            W = [0.26014666666; 0.26014666666; 0.26014666666; -0.28125];
            xi=[0.2, 0.2; 0.6, 0.2; 0.2, 0.6; 0.333333333, 0.333333333];
            Ae=(1/2)*((xe(2)*ye(3)-xe(3)*ye(2))-(xe(1)*ye(3)-xe(3)*ye(1))+(xe(1)*ye(2)-xe(2)*ye(1))) ;
            AAi=zeros(3);
            Ai=zeros(3);
            bi=zeros(3,3); #prava strana pro 3 komponenty napeti
            for ip = 1:4
                Ni=[xi(ip,1), xi(ip,2), 1-xi(ip,1)-xi(ip,2)]; # bazove funkce
                AAi = AAi + Ni'*Ni*w(ip)*2*Ae;
                bi = bi+Ni'*sig*w(ip)*2*Ae;
            endfor
            for i=1:3
                Ai(i,i)=sum(AAi(i,:));
            endfor
        end
        # evaluate recovered stresses
        A = zeros(nnodes);
        B = zeros(nnodes,3);
        for en=1:nelem
            xe = [x(enodes(en,:))];
            ye = [y(enodes(en,:))];
            [Ai,bi] = plane_stress_reco (xe,ye,sig(en,:));
            lm = [enodes(en,1), enodes(en,2), enodes(en,3)]; #kodova cisla odpovidaji cislum uzlu
            A(lm, lm) += Ai;
            B(lm,[1,2,3]) += bi;
        endfor
        sig2 = A \ B
        if (0)
            hold on;
            caxis ("auto")
            colorbar;
            for en=1:nelem
                xe = [x(enodes(en,:)); x(enodes(en,1))];
                ye = [y(enodes(en,:)); y(enodes(en,1))];
                sig2e = [sig2(enodes(en,:),1); sig2(enodes(en,1),1)];
                 patch (xe, ye, sig2e);
            endfor
        endif
```

1.7218e+02	8.3082e+00	9.6599e+00
7.6158e+01	5.3983e+00	4.4783e+01
-3.8137e+01	-2.5533e+00	4.4558e+01
-1.5283e+02	-1.0527e+01	4.4393e+01
-2.3074e+02	-2.3074e+01	1.1516e+02
1.7892e+02	6.4295e-01	-2.6171e+01
1.1051e+02	1.7933e+00	8.4175e+00
1.9143e+00	-2.5754e-01	9.2766e+00
-1.0632e+02	-2.4918e+00	7.9001e+00
-1.8312e+02	-8.8015e+00	4.0493e+01
1.5869e+02	3.5503e-01	-2.2594e+01
9.8389e+01	-1.6859e+00	8.0161e+00
2.1021e+00	-1.6623e+00	9.7197e+00
-9.4360e+01	-1.7128e+00	8.2875e+00
-9.4360E+01 -1.6286e+02	-3.0333e+00	3.5981e+01
1.3870e+02	1.5161e-01	-1.8919e+01
8.6325e+01	-1.6739e+00	8.1711e+00
2.0146e+00	-1.6998e+00	9.6890e+00
-8.2309e+01	-1.6958e+00	8.1974e+00
-1.4265e+02	-2.7036e+00	3.2204e+01
1.1861e+02	-5.0728e-02	-1.5266e+01
7.4282e+01	-1.6730e+00	8.1861e+00
2.0074e+00	-1.6751e+00	9.6924e+00
-7.0266e+01	-1.6754e+00	8.1866e+00
-1.2254e+02	-2.4861e+00	2.8535e+01
9.8515e+01	-2.5346e-01	-1.1616e+01
6.2236e+01	-1.6730e+00	8.1864e+00
2.0075e+00	-1.6730e+00	9.6921e+00
-5.8221e+01	-1.6729e+00	8.1863e+00
-1.0245e+02	-2.2812e+00	2.4886e+01
7.8418e+01	-4.5632e-01	-7.9659e+00
5.0190e+01	-1.6731e+00	8.1863e+00
2.0076e+00	-1.6731e+00	9.6921e+00
-4.6175e+01	-1.6730e+00	8.1863e+00
-8.2352e+01	-2.0785e+00	2.1236e+01
5.8322e+01	-6.5940e-01	-4.3150e+00
3.8145e+01	-1.6746e+00	8.1871e+00
2.0080e+00	-1.6750e+00	9.6920e+00
-3.4129e+01	-1.6731e+00	8.1853e+00
-6.2257e+01	-1.8758e+00	1.7585e+01
3.8217e+01	-8.6687e-01	-6.6091e-01
2.6097e+01	-1.6769e+00	8.1966e+00
2.0150e+00	-1.6772e+00	9.6951e+00
-2.2082e+01	-1.6739e+00	8.1733e+00
-4.2168e+01	-1.6730e+00	1.3933e+01
1.8098e+01	-1.5020e+00	3.0253e+01
1.4038e+01	-1.7895e+00	8.1952e+00
	-1.5587e+00	9.6894e+00
2.0173e+00		
-1.0016e+01	-1.4535e+00	8.1699e+00
-2.2076e+01	-1.4645e+00	1.0284e+01
1.2078e+01	-1.7451e+00	3.0195e+00
8.0066e+00	-2.1230e+00	7.7018e+00
2.0061e+00	-1.6627e+00	9.6658e+00
-3.9772e+00	-1.2099e+00	8.6548e+00
-8.9892e+00	-1.0215e+00	8.4720e+00

Prubeh napeti σ_x^*



Odhad chyby

$$||e||=\int \left(\sigma^{st}(x)-\sigma^{MKP}(x)
ight)^{T}D^{-1}\left(\sigma^{st}(x)-\sigma^{MKP}(x)
ight)d\Omega$$

```
In [9]: # numericka integrace
        w = [0.26014666666; 0.26014666666; 0.26014666666; -0.28125];
        xi=[0.2, 0.2; 0.6, 0.2; 0.2, 0.6; 0.333333333, 0.333333333];
        #prispevek do chyby po elementech
        e = zeros(nelem,1);
        err = 0.0;
        sig
        for en=1:nelem
            sig2e = [sig2(enodes(en,1),:); sig2(enodes(en,2),:);sig2(enodes(en,3),:)];
            xe = [x(enodes(en,:))];
            ye = [y(enodes(en,:))];
            Ae=(1/2)*((xe(2)*ye(3)-xe(3)*ye(2))-(xe(1)*ye(3)-xe(3)*ye(1))+(xe(1)*ye(2)-xe(2)*ye(1))) ;
            [ke,dbe,de,be] = plane_stress(xe,ye,E,nu) ; # de
            for ip=1:4
                xiip = [xi(ip,1), xi(ip,2), 1-xi(ip,1)-xi(ip,2)];
                sig2xi = xiip*sig2e;# napeti v integracnim bode
                dsig = sig2xi-sig(en,:); #rozdil sigma_*-sigma_mkp
                e(en) += (dsig)*inv(de)*dsig'*w(ip)*Ae*2;
            endfor
            err = err+e(en);
        endfor
        err
```

```
2.2973e+02
             5.1542e+00 -9.4548e+01
1.1462e+02
             1.1462e+01
                           1.1387e+02
             4.7427e+00
                         -9.2630e+01
1.1395e+02
-9.8909e-02
            -9.8909e-03
                          1.1311e+02
2.8302e-01
             3.8094e+00
                         -9.2980e+01
-1.1459e+02
            -1.1459e+01
                          1.1354e+02
-1.1315e+02
              2.9511e+00
                          -9.5525e+01
-2.3074e+02
             -2.3074e+01
                           1.1516e+02
 2.0505e+02
              4.3949e+00
                          -8.4683e+01
1.0199e+02
             -7.6203e+00
                           1.0072e+02
1.0312e+02
             3.7080e+00
                          -8.1568e+01
-3.4434e-01
            -6.6868e+00
                           1.0467e+02
6.3556e-01
             3.1122e+00
                          -8.1496e+01
-1.0294e+02
            -6.5129e+00
                          1.0499e+02
-1.0203e+02
             2.5426e+00
                          -8.4465e+01
-2.0548e+02
             -6.2815e+00
                           1.0184e+02
 1.8120e+02
              3.8000e+00
                          -7.3744e+01
 8.9806e+01
             -7.1298e+00
                           9.0646e+01
9.0837e+01
             3.1833e+00
                          -7.0663e+01
-4.7322e-01
            -6.6514e+00
                          9.3648e+01
4.4925e-01
             2.5733e+00
                          -7.0585e+01
-9.0775e+01
            -6.0289e+00
                          9.3655e+01
-8.9975e+01
             1.9711e+00
                          -7.3524e+01
-1.8107e+02
            -5.3610e+00
                           9.0567e+01
1.5708e+02
              3.1939e+00
                          -6.2788e+01
 7.7811e+01
             -6.5391e+00
                           7.9774e+01
7.8723e+01
              2.5852e+00
                          -5.9708e+01
                           8.2721e+01
-4.2705e-01
            -5.9431e+00
3.6496e-01
             1.9770e+00
                          -5.9639e+01
-7.8663e+01
            -5.3380e+00
                           8.2652e+01
-7.7993e+01
             1.3690e+00
                          -6.2581e+01
-1.5690e+02
            -4.7210e+00
                           7.9568e+01
1.3293e+02
             2.5856e+00
                          -5.1836e+01
 6.5825e+01
             -5.9316e+00
                           6.8826e+01
 6.6616e+01
             1.9773e+00
                          -4.8757e+01
-3.6530e-01
            -5.3236e+00
                           7.1769e+01
3.0396e-01
             1.3689e+00
                          -4.8688e+01
-6.6555e+01
            -4.7150e+00
                          7.1700e+01
-6.6008e+01
             7.6057e-01
                          -5.1631e+01
-1.3274e+02
            -4.1062e+00
                          6.8619e+01
1.0878e+02
             1.9772e+00
                          -4.0886e+01
 5.3840e+01
             -5.3232e+00
                           5.7875e+01
 5.4509e+01
              1.3688e+00
                          -3.7806e+01
-3.0422e-01
             -4.7148e+00
                           6.0818e+01
2.4330e-01
             7.6045e-01
                          -3.7738e+01
-5.4449e+01
             -4.1063e+00
                          6.0749e+01
-5.4023e+01
             1.5210e-01
                          -4.0681e+01
-1.0859e+02
             -3.4980e+00
                          5.7669e+01
8.4624e+01
             1.3686e+00
                          -2.9936e+01
4.1855e+01
             -4.7148e+00
                           4.6924e+01
4.2403e+01
             7.5960e-01
                          -2.6855e+01
-2.4340e-01
             -4.1064e+00
                          4.9867e+01
             1.5130e-01
                          -2.6787e+01
1.8238e-01
-4.2342e+01
            -3.4981e+00
                          4.9798e+01
-4.2038e+01
            -4.5623e-01
                          -2.9730e+01
-8.4441e+01
            -2.8897e+00
                          4.6719e+01
6.0471e+01
             7.5991e-01
                          -1.8983e+01
 2.9871e+01
            -4.1067e+00
                           3.5974e+01
3.0296e+01
              1.4457e-01
                          -1.5901e+01
-1.8118e-01
             -3.4988e+00
                           3.8917e+01
1.2217e-01
             -4.6533e-01
                          -1.5837e+01
-3.0235e+01
            -2.8904e+00
                           3.8848e+01
-3.0052e+01
            -1.0634e+00
                          -1.8785e+01
-6.0291e+01
            -2.2815e+00
                          3.5768e+01
3.6304e+01
             1.3911e-01
                          -8.0244e+00
             -3.4996e+00
1.7875e+01
                           2.5025e+01
1.8179e+01
             -4.6381e-01
                          -4.9058e+00
-1.0865e-01
             -2.8959e+00
                           2.7971e+01
7.5071e-02
             -1.0587e+00
                          -4.8791e+00
-1.8113e+01
            -2.2889e+00
                           2.7900e+01
-1.8051e+01 -1.6614e+00 -7.9038e+00
```

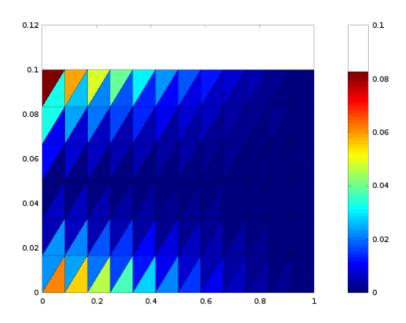
```
-3.6161e+01 -1.6742e+00
                        2.4817e+01
1.2078e+01 -1.7451e+00
                         3.0195e+00
                         1.4081e+01
5.9122e+00 -2.9001e+00
6.0298e+00 -1.7237e+00
                         6.0050e+00
-7.1441e-02 -2.2888e+00
                         1.6990e+01
5.9889e-02 -9.7554e-01
                         6.0021e+00
-6.0300e+00 -1.6692e+00
                         1.6958e+01
-5.9616e+00 -9.8495e-01
                         3.0042e+00
-1.2017e+01 -1.0580e+00
                        1.3940e+01
```

e =

- 1.0268e-02
- 8.1590e-03
- 1.3137e-02
- 6.2613e-03
- 1.3016e-02
- 6.4484e-03
- 1.5302e-02
- 3.2585e-03
- 6.2711e-03
- 1.0400e-02
- 8.1474e-03
- 9.2370e-03
- 8.1153e-03
- 9.3210e-03
- 9.7814e-03
- 6.3693e-03
- 4.8997e-03
- 8.2860e-03
- 6.2832e-03
- 7.2454e-03
- 6.2813e-03 7.2292e-03
- 7.5861e-03 4.9375e-03
- 3.6814e-03
- 6.2708e-03
- 4.6739e-03
- 5.4983e-03
- 4.6647e-03
- 5.4849e-03
- 5.6564e-03
- 3.7171e-03
- 2.6369e-03 4.5332e-03
- 3.2973e-03
- 3.9937e-03
- 3.2894e-03
- 3.9830e-03
- 4.0134e-03
- 2.6681e-03 1.7669e-03
- 3.0776e-03
- 2.1601e-03
- 2.7300e-03
- 2.1538e-03
- 2.7211e-03
- 2.6524e-03
- 1.7925e-03
- 1.0715e-03
- 1.9038e-03
- 1.2627e-03
- 1.7063e-03
- 1.2581e-03 1.6991e-03
- 1.5730e-03
- 1.0914e-03
- 5.5086e-04
- 1.0114e-03
- 6.0532e-04 9.2250e-04
- 6.0229e-04

9.1727e-04 7.7534e-04 5.6490e-04 2.0461e-04 4.0079e-04 1.8672e-04 3.7867e-04 1.8629e-04 3.7522e-04 2.6127e-04 2.1316e-04 5.3013e-06 8.1341e-05 1.0145e-05 7.4529e-05 1.1178e-05 6.4665e-05 2.8891e-05 2.7579e-05

err = 0.30338



Vývoj chyby pro různé hustoty sítě

Deleni	h (char rozmer prvku = $\sqrt{\overline{A_e}}$)	w(l)	$\sigma_x(0)$	e
4x10	0.05	0.541	-230.7	0.303
6x20	0.029	0.961	-422.7	0.265
8x25	0.022	1.074	-476.1	0.20
10x30	0.018	1.1453	-510.8	0.16
15x40	0.013	1.226	-552.7	0.08

```
In [10]: h=[0.05;0.029;0.022; 0.018; 0.013];
    e=[0.303;0.256; 0.20; 0.16; 0.08];
    w=[0.541; 0.961; 1.074; 1.145; 1.226];
    s=[-230.7; -422.7; -476.1; -510.8; -552.7];
    subplot(1,3,1)
    plot (h,e)
    subplot(1,3,2)
    plot (h,w)
    subplot(1,3,3)
    plot (h,s)
```

