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Search for Direct Stop Quark Pair Production in the Single Lepton Channel at 8 TeV

L. Bauerdick, K. Burkett, I. Fisk, Y. Gao, O. Gutsche, B. Hooberman, S. Jindariani, J. Linacre, V. Martinez Outschoorn

Fermilab National Accelerator Laboratory, Batavia, USA

D. Barge, C. Campagnari, A. George, F. Golf, J. Gran, D. Kovalskyi, V. Krutelyov University of California, Santa Barbara, Santa Barbara, USA

W. Andrews, G. Cerati, D. Evans, R. Kelley, I. MacNeill, S. Padhi, Y. Tu, F. Würthwein, V. Welke, A. Yagil, J. Yoo

University of California, San Diego, San Diego, USA

Abstract

This note describes a search for direct stop quark pair production in the single lepton channel using 9.7 fb⁻¹ of pp collision data at $\sqrt{s} = 8$ TeV taken with the CMS detector in 2012. A search for an excess of events over the Standard Model prediction is performed in a sample with a single isolated electron or muon, several jets, missing transverse energy and large transverse mass.

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1 Introduction

This note presents a search for the production of supersymmetric (SUSY) stop quark pairs in events with a single isolated lepton, several jets, missing transverse energy, and large transverse mass. We use the full 2012 data sample, corresponding to an integrated luminosity of 9.7 fb⁻¹. This search is of theoretical interest because of the critical role played by the stop quark in solving the hierarchy problem in SUSY models. This solution requires that the stop quark be light, less than a few hundred GeV and hence within reach for direct pair production. We focus on two decay modes $\tilde{t} \to t\chi_1^0$ and $\tilde{t} \to b\chi_1^+$ which are expected to have large branching fractions if they are kinematically accessible, leading to:

•
$$pp \to \tilde{t}\bar{\tilde{t}} \to t\bar{t}\chi_1^0\chi_1^0$$
, and

•
$$pp \to \tilde{t}\bar{\tilde{t}} \to b\bar{b}\chi_1^+\chi_1^- \to b\bar{b}W^+W^-\chi_1^0\chi_1^0$$
.

Both of these signatures contain high transverse momentum (p_T) jets including two b-jets, and missing transverse energy (E_T^{miss}) due to the invisible χ_1^0 lightest SUSY particles (LSP's). In addition, the presence of two W bosons leads to a large branching fraction to the single lepton final state. Hence we require the presence of exactly one isolated, high p_T electron or muon, which provides significant suppression of several backgrounds that are present in the all-hadronic channel. The largest backgrounds for this signature are semi-leptonic $t\bar{t}$ and W+jets. These backgrounds contain a single leptonically-decaying W boson, and the transverse mass (M_T) of the lepton-neutrino system has a kinematic endpoint requiring $M_T < M_W$. For signal stop quark events, the presence of additional LSP's in the final states allows the M_T to exceed M_W . Hence we search for an excess of events with large M_T . The dominant background in this kinematic region is dilepton $t\bar{t}$ where one of the leptons is not identified, since the presence of two neutrinos from leptonically-decaying W bosons allows the M_T to exceed M_W . Backgrounds are estimated from Monte Carlo (MC) simulation, with careful validation and determination of scale factors and corresponding uncertainties based on data control samples.

The expected stop quark pair production cross section (see Fig. 1) varies between O(10) pb for $m_{\tilde{t}} = 200$ GeV and O(0.01) pb for $m_{\tilde{t}} = 500$ GeV. The critical challenge of this analysis is due to the fact that for light stop quarks ($m_{\tilde{t}} \approx m_t$), the production cross section is large but the kinematic distributions, in particular $M_{\rm T}$, are very similar to SM t \bar{t} production. In this regime it becomes very difficult to distinguish the signal and background. For large stop quark mass the kinematic distributions differ from those in SM t \bar{t} production, but the cross section decreases rapidly, reducing the signal-to-background ratio.

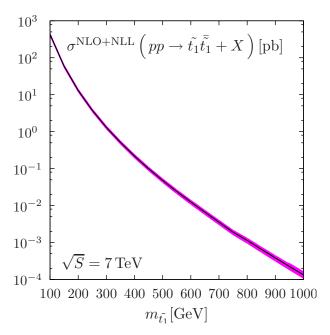


Figure 1: The stop quark pair production cross section in pb, as a function of the stop quark mass. AT SOME POINT WE NEED TO GET A FIGURE FOR 8 TEV CM ENERGY.

2 Overview and Strategy for Background Determination

- THIS SECTION IS NOW MORE OR LESS OK. NEED TO FIX THE "XX" IN FORWARD SECTION REFERENCES]
- We are searching for a $t\bar{t}\chi^0\chi^0$ or $WbW\bar{b}\chi^0\chi^0$ final state (after top decay in the first mode, the final states are actually the same). So to first order this is " $t\bar{t}+$ extra $E_{\rm T}^{\rm miss}$ ".
- We work in the $\ell+$ jets final state, where the main background is $t\bar{t}$. We look for $E_{\mathrm{T}}^{\mathrm{miss}}$ inconsistent with
- $W \to \ell \nu$. We do this by concentrating on the $\ell \nu$ transverse mass (M_T) , since except for resolution effects,
- $M_T < M_W$ for $W \to \ell \nu$. Thus, the initial analysis is simply a counting experiment in the tail of the M_T
- 38 distribution.
- The event selection is one-and-only-one high $p_{\rm T}$ isolated lepton, four or more jets, and some moderate
- 40 $E_{\rm T}^{\rm miss}$ cut. At least one of the jets has to be btagged to reduce W+ jets. The event sample is then
- dominated by $t\bar{t}$, but there are also contributions from W+ jets, single top, dibosons, as well as rare SM
- processes such as ttW.
- The $t\bar{t}$ events in the M_T tail can be broken up into two categories: (i) $t\bar{t} \to \ell + \text{ jets}$ and (ii) $t\bar{t} \to \ell^+\ell^-$
- 44 where one of the two leptons is not found by the second-lepton-veto (here the second lepton can be a
- hadronically decaying τ). For a reasonable M_T cut, say $M_T > 150$ GeV, the dilepton background is of
- order 80% of the total. This is because in dileptons there are two neutrinos from W decay, thus M_T is
- 47 not bounded by M_W . This is a very important point: while it is true that we are looking in the tail of
- M_T , the bulk of the background events end up there not because of some exotic E_T^{miss} reconstruction
- failure, but because of well understood physics processes. This means that the background estimate can
- 50 be taken from Monte Carlo (MC) after carefully accounting for possible data/MC differences.
- 51 In Section XX we will describe the analysis of various Control Regions (CRs) that are used to test the
- Monte Carlo model and, if necessary, to extract data/MC scale factors. In this section we give a general
- description of the procedure. The details of how the final background prediction is assembled are given
- in Section XX.
- The search is performed in a number of signal regions defined by minimum requirements on $E_{
 m T}^{
 m miss}$ and
- M_T . These signal regions are defined in Section XX.
- 57 One general point is that in order to minimize systematic uncertainties, the MC background predictions
- are whenever possible normalized to the bulk of the $t\bar{t}$ data, ie, events passing all of the requirements
- but with $M_T \approx 80$ GeV. This (mostly) removes uncertainties due to $\sigma(t\bar{t})$, lepton ID, trigger efficiency,
- 60 luminosity, etc.

$_{1}$ 2.1 $\ell+$ jets background

- The $\ell+$ jets background is dominated by $t\bar{t} \to \ell+$ jets, but also includes some W+ jets as well as single
- top. The MC input used in the background estimation is the ratio of the number of events with M_T in
- the signal region to the number of events with $M_T \approx 80$ GeV. This ratio is (possibly) corrected by a
- 65 data/MC scale factor obtained from a study of CRs, as outlined below.
- Note that the ratio described above is actually different for $t\bar{t}/\mathrm{single}$ top and W+ jets. This is because
- in W events there is a significant contribution to the M_T tail from very off-shell W. This contribution is
- much smaller in top events because $M(\ell\nu)$ cannot excees $M_{top}-M_b$.
- For W+ jets the ability of the Monte Carlo to model this ratio (R_{wjet}) is tested in a sample of ℓ + jets
- enriched in W+ jets by the application of a b-veto. The equivalent ratio for top events (R_{top}) is validated
- in a sample of well identified $Z \to \ell\ell$ with one lepton added to the $E_{\rm T}^{\rm miss}$ calculation. This sample is well
- suited to testing the resolution effects on the M_T tail, since off-shell effects are eliminated by the Z-mass
- 73 requirement.
- Note that the fact that the ratios are different for $t\bar{t}/\sin \theta$ top and W+ jets introduces a systematic
- 15 uncertainty in the background calculation because one needs to know the relative fractions of these two
- components in $M_T \approx 80 \text{ GeV lepton} + \text{jets sample}$.

77 2.2 Dilepton background

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To suppress dilepton backgrounds, we veto events with an isolated track of $p_T > 10$ GeV. Being the common feature for electron, muon, and one-prong tau decays, this veto is highly efficient for rejecting $t\bar{t}$ to dilepton events. The remaining dilepton background can be classified into the following categories:

- lepton is out of acceptance $(|\eta| > 2.50)$
 - lepton has $p_{\rm T} < 10$ GeV, and is inside the acceptance
 - lepton has $p_{\rm T} > 10$ GeV, is inside the acceptance, but survives the additional isolated track veto

The last category includes 3-prong tau decays as well as electrons and muons from W decay that fail the isolation requirement. Monte Carlo studies indicate that these three components populate the M_T tail in the proportions of roughly 6%, 47%, 47%. We note that at present we do not attempt to veto 3-prong tau decays as they are only 16% of the total dilepton background according to the MC.

The high M_T dilepton backgrounds come from MC, but their rate is normalized to the $M_T \approx 80$ GeV peak. In order to perform this normalization in data, the non- $t\bar{t}$ (eg, W+ jets) events in the M_T peak have to be subtracted off. This also introduces a systematic uncertainty.

There are two types of effects that can influence the MC dilepton prediction: physics effects and instrumental effects. We discuss these next, starting from physics.

First of all, many of our $t\bar{t}$ MC samples (eg: MadGraph) have BR($W \to \ell \nu$) = $\frac{1}{9}$ = 0.1111. PDG says BR($W \to \ell \nu$) = 0.1080 ± 0.0009. This difference matters, so the $t\bar{t}$ MC must be corrected to account for this.

Second, our selection is $\ell+4$ or more jets. A dilepton event passes the selection only if there are two additional jets from ISR, or one jet from ISR and one jet which is reconstructed from the unidentified lepton, e.g., a three-prong tau. Therefore, all MC dilepton $t\bar{t}$ samples used in the analysis must have their jet multiplicity corrected (if necessary) to agree with what is seen in $t\bar{t}$ data. We use a data control sample of well identified dilepton events with $E_{\rm T}^{\rm miss}$ and at least two jets as a template to "adjust" the N_{jet} distribution of the $t\bar{t} \to {\rm dileptons} \ {\rm MC} \ {\rm samples}$.

The final physics effect has to do with the modeling of $t\bar{t}$ production and decay. Different MC models could in principle result in different BG predictions. Therefore we use several different $t\bar{t}$ MC samples using different generators and different parameters, to test the stability of the dilepton BG prediction. All these predictions, **after** corrections for branching ratio and N_{jet} dependence, are compared to each other. The spread is a measure of the systematic uncertainty associated with the $t\bar{t}$ generator modeling.

The main instrumental effect is associated with the efficiency of the isolated track veto. We use tagand-probe to compare the isolated track veto performance in Z+4 jet data and MC, and we extract
corrections if necessary. Note that the performance of the isolated track veto is not exactly the same
on e/μ and on one prong hadronic tau decays. This is because the pions from one-prong taus are often
accompanied by π^0 's that can then result in extra tracks due to phton conversions. We let the simulation
take care of that. Note that JES uncertainties are effectively "calibrated away" by the N_{jet} rescaling
described above.

$_4$ 2.3 Other backgrounds

Other backgrounds are tW, ttV, dibosons, tribosons, Drell Yan. These are small. They are taken from MC with appropriate scale factors for trigger efficiency, etc.

2.4 Future improvements

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Finally, there are possible improvements to this basic analysis strategy that can be added in the future:

- Move from counting experiment to shape analysis. But first, we need to get the counting experiment under control.
- Add an explicit three prong tau veto

- Do something to require that three of the jets in the event be consistent with $t \to Wb, W \to q\bar{q}$. This could help reject some of the dilepton BG in the search for $\tilde{t} \to t\chi^0$, but is not applicable to the $\tilde{t} \to b\chi^+$ search.
- Consider the $M(\ell b)$ variable, which is not bounded by M_{top} in $\widetilde{t} \to b \chi^+$

3 Data Samples

[UPDATE]

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The datasets used for this analysis are summarized in Tables 1 (data) and 2 (MC). The total integrated luminosity is 9.7 fb⁻¹after applying the official good run list. The main Monte Carlo samples are generated with Madgraph, though samples with alternative generators such as Powheg and MC@NLO are also used for the derivation of systematic uncertainties in the tt background prediction. The triggers used to select both the signal and control samples are also summarized in Table. 3.

Dataset Name					
Single Lepton Samples					
/SingleElectron/Run2012A-13Jul2012-v1/AOD					
/SingleMu/Run2012A-13Jul2012-v1/AOD					
/SingleElectron/Run2012B-13Jul2012-v1/AOD					
$/\mathrm{SingleMu}/\mathrm{Run}2012\mathrm{B}$ -13 $\mathrm{Jul}2012$ -v1 $/\mathrm{AOD}$					
/SingleElectron/Run2012C-PromptReco-v*/AOD					
/SingleMu/Run2012C-PromptReco-v*/AOD					
Dilepton Samples (only used for dilepton control region)					
/DoubleElectron/Run2012A-13Jul2012-v1/AOD					
/DoubleMu/Run2012A-13Jul2012-v1/AOD					
$/\mathrm{MuEG/Run}$ 2012A-13Jul2012-v1/AOD					
/DoubleElectron/Run2012B-13Jul2012-v1/AOD					
/DoubleMu/Run2012B-13Jul2012-v1/AOD					
$/\mathrm{MuEG/Run}$ 2012B-13Jul2012-v1/AOD					
/Double Electron/Run 2012 C-Prompt Reco-v*/AOD					
/DoubleMu/Run2012C-PromptReco-v*/AOD					
/MuEG/Run2012C-PromptReco-v*/AOD					

Table 1: Summary of data datasets used.

With Pileup: Processed dataset name is (S3) Summer12_DR53X-PU_S10_START53_V7A-v*/AODSIM (S3) Summer11-PU_S3_START42_V11-v*/AODSIM

Description	Primary Dataset Name	cross-section [pb]
tt	/TTJets_MassiveBinDECAY_TuneZ2Star_8TeV-madgraph-tauola (S3)	225.2
$\mathrm{W} ightarrow \ell u$	/WJetsToLNu_TuneZ2Star_8TeV-madgraph-tauola (S3)	31314.0
WW	/WW_TuneZ2Star_8TeV_pythia6_tauola (S3)	45.6
WZ	/WZ_TuneZ2Star_8TeV_pythia6_tauola (S3)	18.2
ZZ	/ZZ_TuneZ2Star_8TeV_pythia6_tauola (S3)	7.4
t (s-chan)	/T_TuneZ2Star_s-channel_8TeV-powheg-tauola (S3)	3.19
\bar{t} (s-chan)	/Tbar_TuneZ2Star_s-channel_8TeV-powheg-tauola (S3)	1.44
t (t-chan)	/T_TuneZ2Star_t-channel_8TeV-powheg-tauola (S3)	41.92
\bar{t} (t-chan)	/Tbar_TuneZ2Star_t-channel_8TeV-powheg-tauola (S3)	22.65
tW	/T_TuneZ2Star_tW-channel-DR_8TeV-powheg-tauola (S3)	7.87
$ar{t}W$	/Tbar_TuneZ2Star_tW-channel-DR_8TeV-powheg-tauola (S3)	7.87
$Z/\gamma^* \to \ell\ell$	/DYJetsToLL_TuneZ2Star_M-50_8TeV-madgraph-tarball (S3)	3532.8
${ m t}ar{{ m t}}W$	/TTW_TuneZ2Star_8TeV-madgraph (S3)	0.1633
${ m t}ar{ m t} Z$	/TTZ_TuneZ2Star_8TeV-madgraph (S3)	0.139
${ m t}ar{ m t}\gamma$	/TTPhoton_TuneZ2Star_8TeV-madgraph (S3)	0.6545
$\mathrm{WW}\gamma$	/WWPhoton_TuneZ2Star_8TeV-madgraph (S3)	0.177
WWZ	/WWZNoGstar_TuneZ2Star_8TeV-madgraph (S3)	0.0268
WWW	/WWW_TuneZ2Star_8TeV-madgraph (S3)	0.038
WZZ	/WZZNoGstar_TuneZ2Star_8TeV-madgraph (S3)	0.0088
ZZZ	/ZZZNoGstar_TuneZ2Star_8TeV-madgraph (S3)	0.00288
$ \begin{array}{c} \overline{t}\bar{t} \rightarrow t\bar{t}\chi_1^0\chi_1^0 \\ \overline{t}\bar{t} \rightarrow b\bar{b}\chi_1^+\chi_1^- \\ \hline t\bar{t}\ (Q^2\times 2) \end{array} $	/SMS-T2tt_Mstop-225to1200_mLSP-50to1025_8TeV-Pythia6Z (S2)	scan
$\tilde{t}\bar{\tilde{t}} ightarrow bar{b}\chi_1^+\chi_1^-$	/SMS-T2bw_x-0p25to0p75_mStop-50to850_mLSP-50to800_8TeV-Pythia6Z (S2)	scan
$t\bar{t} (Q^2 \times 2)$	/TTjets_TuneZ2Star_scaleup_8TeV-madgraph-tauola (S3)	225.2
$t\bar{t} \ (Q^2 \times 0.5)$	/TTjets_TuneZ2Star_scaledown_8TeV-madgraph-tauola (S3)	225.2
$t\bar{t} \ (x_q > 40 \text{ GeV})$	/TTjets_TuneZ2Star_matchingup_8TeV-madgraph-tauola (S3)	225.2
$t\bar{t} \ (x_q > 10 \text{ GeV})$	/TTjets_TuneZ2Star_matchingdown_8TeV-madgraph-tauola (S3)	225.2
$t\bar{t} \ (m_{\text{top}} = 178.5 \text{ GeV})$	/TTJets_TuneZ2Star_mass178_5_8TeV-madgraph-tauola (S3)	225.2
$t\bar{t} \ (m_{\text{top}} = 166.5 \text{ GeV})$	/TTJets_TuneZ2Star_mass166_5_8TeV-madgraph-tauola (S3)	225.2
$t\bar{t}$	/TT_TuneZ2Star_8TeV-powheg-tauola (S3)	225.2

Table 2: Summary of Monte Carlo datasets used. TO BE UPDATED.

Triggers
Single Muon Sample
HLT IsoMu17 v*
HLT_IsoMu24_v*
HLT_IsoMu30_eta2p1_v*
Single Electron Sample
HLT_Ele25_CaloIdVT_TrkIdT_CentralTriJet30_v*
HLT_Ele25_CaloIdVT_TrkIdT_TriCentralJet30_v*
HLT_Ele25_CaloIdVT_CaloIsoT_TrkIdT_TrkIsoT_TriCentralJet30_v*
HLT_Ele25_CaloIdVT_CaloIsoT_TrkIdT_TrkIsoT_TriCentralPFJet30_v*
Dimuon Sample (only used for dilepton control regions)
HLT_DoubleMu7_v*
HLT_Mu13_Mu7_v*
HLT_Mu13_Mu8_v*
HLT_Mu17_Mu8_v*
Electron-Muon Sample (only used for dilepton control regions)
HLT_Mu17_Ele8_CaloIdL_v*
HLT_Mu8_Ele17_CaloIdL_v*
HLT_Mu17_Ele8_CaloIdT_CaloIsoVL_v*
HLT_Mu8_Ele17_CaloIdT_CaloIsoVL_v*
Dielectron Sample (only used for dilepton control regions)
HLT_Ele17_CaloIdL_CaloIsoVL_Ele8_CaloIdL_CaloIsoVL_v*
HLT_Ele17_CaloIdT_TrkIdVL_CaloIsoVL_TrkIsoVL_Ele8_CaloIdT_TrkIdVL_CaloIsoVL_TrkIsoVL_v
HLT Ele17 CaloIdT CaloIsoVL TrkIdVL TrkIsoVL Ele8 CaloIdT CaloIsoVL TrkIdVL TrkIsoVL v

Table 3: Summary of triggers used. TO BE UPDATED

4 Event Selection

This analysis uses several different control regions in addition to the signal regions. All of these different regions are defined in this section.

6 4.1 Single Lepton Selection

7 [UPDATE SELECTION]

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The single lepton preselection sample is based on the following criteria, starting from the requirements described on https://twiki.cern.ch/twiki/bin/viewauth/CMS/SUSYstop#SINGLE_
LEPTON_CHANNEL

- satisfy the trigger requirement (see Table. 1). Note that the analysis triggers are inclusive single lepton triggers. Dilepton triggers are used only for the dilepton control region.
- select events with one high $p_{\rm T}$ electron or muon, requiring
 - $-p_{\rm T} > 30 \text{ GeV}/c \text{ and } |\eta| < 1.4442(2.4) \text{ for electrons (muons)}$
 - muon ID criteria is based on the 2012 POG recommended tight working point
 - electron ID critera is based on the 2012 POG recommended medium working point
 - PF-based isolation ($\Delta R < 0.3$, $\Delta \beta$ corrected) relative < 0.15 and absolute < 5 GeV
 - $-|p_{\mathrm{T}}(\mathrm{PF}_{\mathrm{lep}}) p_{\mathrm{T}}(\mathrm{RECO}_{\mathrm{lep}})| < 10 \text{ GeV}$
 - $-E/p_{in} < 4$ (electrons only)
- require at least 4 PF jets in the event with $p_T > 30$ GeV within $|\eta| < 2.5$ out of which at least 1 satisfies the CSV medium working point b-tagging requirement
- require moderate $E_{\rm T}^{\rm miss} > 50 \text{ GeV}$

4.2 Signal Region Selection

- 54 [MOTIVATIONAL BLURB ON MET AND MT,
- 155 CAN ADD SIGNAL VS. TTBAR MC PLOT
- 56 ADD SIGNAL YIELDS FOR AVAILABLE POINTS,
- 157 DISCUSS CHOICE SIG REGIONS
- The signal regions (SRs) are selected to improve the sensitivity for the single lepton requirements and cover a range of scalar top scenarios. The $M_{\rm T}$ and $E_{\rm T}^{\rm miss}$ variables are used to define the signal regions and the requirements are listed in Table 4.

Signal Region	Minimum $M_{\rm T}$ [GeV]	Minimum $E_{\mathrm{T}}^{\mathrm{miss}}$ [GeV]
SRA	150	100
SRB	120	150
SRC	120	200
SRD	120	250
SRE	120	300
SRF	120	350
SRG	120	400

Table 4: Signal region definitions based on $M_{\rm T}$ and $E_{\rm T}^{\rm miss}$ requirements. These requirements are applied in addition to the baseline single lepton selection.

Table 5 shows the expected number of SM background yields for the SRs. A few stop signal yields for four values of the parameters are also shown for comparison. The signal regions with looser requirements are sensitive to lower stop masses $M(\tilde{t})$, while those with tighter requirements are more sensitive to higher $M(\tilde{t})$.

Sample	SRA	SRB	SRC	SRD	SRE	SRF	SRG
$t\bar{t} o \ell\ell$	619 ± 9	366 ± 7	127 ± 4	44 ± 2	17 ± 1	7 ± 1	4 ± 1
$t\bar{t} \to \ell + jets \& single top (1\ell)$	95 ± 3	67 ± 3	15 ± 1	6 ± 1	2 ± 1	1 ± 1	1 ± 0
W+jets	29 ± 2	15 ± 2	6 ± 1	3 ± 1	1 ± 0	0 ± 0	0 ± 0
Rare	59 ± 3	38 ± 3	16 ± 2	8 ± 1	4 ± 1	2 ± 0	1 ± 0
Total	802 ± 10	486 ± 8	164 ± 5	62 ± 3	23 ± 2	10 ± 1	6 ± 1

Table 5: Expected SM background contributions, including both muon and electron channels. This is "dead reckoning" MC with no correction. It is meant only as a general guide. The uncertainties are statistical only. ADD SIGNAL POINTS.

4.3 Control Region Selection

166 [1 PARAGRAPH BLURB RELATING BACKGROUNDS (IN TABLE FROM PREVIOUS SECTION)
167 TO INTRODUCE CONTROL REGIONS]

Control regions (CRs) are used to validate the background estimation procedure and derive systematic uncertainties for some contributions. The CRs are selected to have similar kinematics to the SRs, but have a different requirement in terms of number of b-tags and number of leptons, thus enhancing them in different SM contributions. The four CRs used in this analysis are summarized in Table 6.

172 4.4 MC Corrections

73 [UPDATE SECTION]

$_{74}$ 4.4.1 Corrections to Jets and $E_{ m T}^{ m miss}$

75 [UPDATE, ADD FEW MORE DETAILS ON WHAT IS DONE HERE]

The official recommendations from the Jet/MET group are used for the data and MC samples. In particular, the jet energy corrections (JEC) are updated using the official recipe. L1FastL2L3Residual (L1FastL2L3) corrections are applied for data (MC), based on the global tags GR_R_42_V23 (DE-SIGN42_V17) for data (MC). In addition, these jet energy corrections are propagated to the $E_{\rm T}^{\rm miss}$ calculation, following the official prescription for deriving the Type I corrections.

Events with anomalous "rho" pile-up corrections are excluded from the sample since these correspond to events with unphysically large $E_{\rm T}^{\rm miss}$ and $M_{\rm T}$ tail signal region. In addition, the recommended MET filters are applied.

84 4.4.2 Branching Fraction Correction

The leptonic branching fraction used in some of the $t\bar{t}$ MC samples differs from the value listed in the PDG $(10.80 \pm 0.09)\%$. Table. 7 summarizes the branching fractions used in the generation of the various

Selection Criteria	exactly 1 lepton	exactly 2 leptons	1 lepton + isolated track
0 b-tags	CR1) W+Jets dominated: Validate W+Jets $M_{\rm T}$ tail	CR2) apply Z-mass constraint \rightarrow Z+Jets dominated: Validate $t\bar{t} \rightarrow \ell + \text{jets } M_{\text{T}}$ tail comparing data vs. MC "pseudo- M_{T} "	CR3) not used
≥ 1 b-tags	SIGNAL REGION	CR4) Apply Z-mass veto \rightarrow $t\bar{t} \rightarrow \ell\ell$ dominated: Validate "physics" modelling of $t\bar{t} \rightarrow \ell\ell$	CR5) $t\bar{t} \to \ell\ell$, $t\bar{t} \to \ell\tau$ and $t\bar{t} \to \ell$ fake dominated: Validate τ and fake lepton modeling/detector effects in $t\bar{t} \to \ell\ell$

Table 6: Summary of signal and control regions.

tt MC samples. For tt samples with the incorrect leptonic branching fraction, event weights are applied based on the number of true leptons and the ratio of the corrected and incorrect branching fractions.

tt Sample - Event Generator	Leptonic Branching Fraction
Madgraph	0.111
MC@NLO	0.111
Pythia	0.108
Powheg	0.108

Table 7: Leptonic branching fractions for the various $t\bar{t}$ samples used in the analysis. The primary $t\bar{t}$ MC sample produced with Madgraph has a branching fraction that is almost 3% higher than the PDG value.

4.4.3 Lepton Selection Efficiency Measurements

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In this section we measure the identification and isolation efficiencies for muons and electrons in data and MC using tag-and-probe studies. The tag is required to pass the full offline analysis selection and have $p_T > 30$ GeV, $|\eta| < 2.1$, and be matched to the single lepton trigger, HLT_IsoMu24(_eta2p1) for muons and HLT_Ele27_WP80 for electrons. The probe is required to have $|\eta| < 2.1$ and $p_T > 20$ GeV. To measure the identification efficiency we require the probe to pass the isolation requirement, to measure the isolation efficiency we require the probe to pass the identification requirement. The tag-probe pair is required to have opposite-sign and an invariant mass in the range 76–106 GeV. In order to suppress lepton pairs from sources other than Z boson decays, we require the event to have $E_{\mathrm{T}}^{\mathrm{miss}}$ < 30 GeV and no b-tagged jets (CSV loose working point). The muon efficiencies are summarized in Table 8 for inclusive events (i.e. no jet requirements). These efficiencies are displayed in Fig. 2 for several different jet multiplicity requirements. We currently observe good agreement for muons with p_T up to about 200 GeV. For muons with $p_T > 200$ GeV the data efficiency begins to drop, and the effect is especially pronounced for muons with $p_T > 300$ GeV. We are currently investigating the source of this inefficiency. The electron efficiencies are summarized in Table 9 for inclusive events (i.e. no jet requirements). These efficiencies are displayed in Fig. 3 for several different jet multiplicity requirements. In general we observe good agreement between the data and MC identification and isolation efficiencies.

Table 8: Summary of the data and MC muon identification and isolation efficiencies measured with tag-and-probe studies.

MC ID			
p_{T} range [GeV]	$ \eta < 0.8$	$0.8 < \eta < 1.5$	$1.5 < \eta < 2.1$
pri range [dev]			
20 - 30	0.9638 ± 0.0005	0.9590 ± 0.0006	0.9381 ± 0.0008
30 - 40	0.9649 ± 0.0002	0.9612 ± 0.0003	0.9372 ± 0.0005
40 - 50	0.9674 ± 0.0002	0.9651 ± 0.0002	0.9368 ± 0.0004
50 - 60	0.9644 ± 0.0005	0.9589 ± 0.0006	0.9325 ± 0.0009
60 - 80	0.9644 ± 0.0009	0.9586 ± 0.0011	0.9258 ± 0.0019
80 - 100	0.9674 ± 0.0022	0.9602 ± 0.0029	0.9148 ± 0.0053
100 - 150	0.9632 ± 0.0031	0.9621 ± 0.0037	0.9270 ± 0.0068
150 - 200	0.9615 ± 0.0070	0.9519 ± 0.0092	0.8844 ± 0.0213
200 - 300	0.9615 ± 0.0119	0.9353 ± 0.0173	0.8923 ± 0.0384
300 - 10000	0.9667 ± 0.0232	0.9697 ± 0.0298	0.4000 ± 0.1549
MC ISO			
p_{T} range [GeV]	$ \eta < 0.8$	$ 0.8 < \eta < 1.5$	$ 1.5 < \eta < 2.1$
20 - 30	0.8968 ± 0.0007	0.9156 ± 0.0008	0.9301 ± 0.0009
30 - 40	0.9610 ± 0.0002	0.9633 ± 0.0003	0.9706 ± 0.0003
40 - 50	0.9877 ± 0.0001	0.9897 ± 0.0001	0.9912 ± 0.0002
50 - 60	0.9918 ± 0.0002	0.9928 ± 0.0002	0.9939 ± 0.0003
60 - 80	0.9926 ± 0.0004	0.9936 ± 0.0004	0.9948 ± 0.0005
80 - 100	0.9918 ± 0.0012	0.9923 ± 0.0013	0.9933 ± 0.0016
100 - 150	0.9900 ± 0.0016	0.9939 ± 0.0015	0.9927 ± 0.0023
150 - 200	0.9904 ± 0.0036	0.9904 ± 0.0043	0.9950 ± 0.0050
200 - 300	0.9921 ± 0.0056	1.0000 ± 0.0000	0.9831 ± 0.0168
300 - 10000	1.0000 ± 0.0000	1.0000 ± 0.0000	1.0000 ± 0.0000
	1 2:0000 - 0:0000		_ =:0000 <u> </u>
DATA ID			
$p_{\rm T}$ range [GeV]	n < 0.8	0.8 < n < 1.5	$1.5 < \eta < 2.1$
	$ \eta < 0.8$	$0.8 < \eta < 1.5$	
20 - 30	0.9446 ± 0.0005	0.9430 ± 0.0006	0.9203 ± 0.0008
30 - 40	0.9474 ± 0.0003	0.9448 ± 0.0003	0.9237 ± 0.0005
40 - 50	0.9515 ± 0.0002	0.9502 ± 0.0003	0.9252 ± 0.0004
50 - 60	0.9458 ± 0.0005	0.9405 ± 0.0006	0.9163 ± 0.0010
60 - 80			
	0.9457 ± 0.0010	0.9386 ± 0.0013	0.9115 ± 0.0020
80 - 100	0.9393 ± 0.0029	0.9346 ± 0.0035	0.9091 ± 0.0055
100 - 150	0.9355 ± 0.0040	0.9392 ± 0.0045	0.8843 ± 0.0085
150 - 200	0.9526 ± 0.0078	0.9534 ± 0.0099	0.8772 ± 0.0217
200 - 300	0.9017 ± 0.0195	0.9302 ± 0.0194	0.8448 ± 0.0475
300 - 10000	0.7083 ± 0.0656	0.7333 ± 0.1142	0.2000 ± 0.1033
DATA ISO	1		
	$ \eta < 0.8$	$0.8 < \eta < 1.5$	$1.5 < \eta < 2.1$
p_{T} range [GeV]	$ \eta < 0.8$	$0.8 < \eta < 1.5$	$1.5 < \eta < 2.1$
$\frac{p_{\rm T} \text{ range [GeV]}}{20 - 30}$	0.8943 ± 0.0007	0.9144 ± 0.0008	0.9359 ± 0.0008
p_{T} range [GeV]			
$\frac{p_{\rm T} \text{ range [GeV]}}{20 - 30}$ $30 - 40$	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \end{array}$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \end{array}$
$\frac{p_{\rm T} \text{ range [GeV]}}{20 - 30}$ $30 - 40$ $40 - 50$	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \end{array}$	0.9144 ± 0.0008 0.9646 ± 0.0003 0.9903 ± 0.0001	0.9359 ± 0.0008 0.9746 ± 0.0003 0.9920 ± 0.0001
$\begin{array}{c} p_{\mathrm{T}} \; \mathrm{range} \; [\mathrm{GeV}] \\ \hline 20 \; \; 30 \\ 30 \; \; 40 \\ 40 \; \; 50 \\ 50 \; \; 60 \\ \end{array}$	0.8943 ± 0.0007 0.9598 ± 0.0002 0.9870 ± 0.0001 0.9913 ± 0.0002	0.9144 ± 0.0008 0.9646 ± 0.0003 0.9903 ± 0.0001 0.9935 ± 0.0002	0.9359 ± 0.0008 0.9746 ± 0.0003 0.9920 ± 0.0001 0.9952 ± 0.0003
$\begin{array}{c} p_{\mathrm{T}} \; \mathrm{range} \; [\mathrm{GeV}] \\ \hline 20 \; \; 30 \\ 30 \; \; 40 \\ 40 \; \; 50 \\ 50 \; \; 60 \\ \end{array}$	0.8943 ± 0.0007 0.9598 ± 0.0002 0.9870 ± 0.0001 0.9913 ± 0.0002	0.9144 ± 0.0008 0.9646 ± 0.0003 0.9903 ± 0.0001 0.9935 ± 0.0002	0.9359 ± 0.0008 0.9746 ± 0.0003 0.9920 ± 0.0001 0.9952 ± 0.0003
p _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \end{array}$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9920 \pm 0.0001 \\ 0.9952 \pm 0.0003 \\ 0.9952 \pm 0.0005 \end{array}$
p _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \end{array}$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9920 \pm 0.0001 \\ 0.9952 \pm 0.0003 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \end{array}$
p _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \end{array}$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9920 \pm 0.0001 \\ 0.9952 \pm 0.0003 \\ 0.9952 \pm 0.0005 \end{array}$
p _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ \end{array}$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9943 \pm 0.0015 \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9920 \pm 0.0001 \\ 0.9952 \pm 0.0003 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9968 \pm 0.0016 \end{array}$
p _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ \end{array}$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9943 \pm 0.0015 \\ 0.9977 \pm 0.0023 \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9920 \pm 0.0001 \\ 0.9952 \pm 0.0003 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9968 \pm 0.0016 \\ 0.9950 \pm 0.0050 \end{array}$
p _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200 200 - 300	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ 1.0000 \pm 0.0000 \end{array}$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9943 \pm 0.0015 \\ 0.9977 \pm 0.0023 \\ 1.0000 \pm 0.0000 \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9920 \pm 0.0001 \\ 0.9952 \pm 0.0003 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9968 \pm 0.0016 \\ 0.9950 \pm 0.0050 \\ 1.0000 \pm 0.0000 \end{array}$
p _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ \end{array}$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9943 \pm 0.0015 \\ 0.9977 \pm 0.0023 \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9920 \pm 0.0001 \\ 0.9952 \pm 0.0003 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9968 \pm 0.0016 \\ 0.9950 \pm 0.0050 \end{array}$
p _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200 200 - 300 300 - 10000	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ 1.0000 \pm 0.0000 \end{array}$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9943 \pm 0.0015 \\ 0.9977 \pm 0.0023 \\ 1.0000 \pm 0.0000 \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9920 \pm 0.0001 \\ 0.9952 \pm 0.0003 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9968 \pm 0.0016 \\ 0.9950 \pm 0.0050 \\ 1.0000 \pm 0.0000 \end{array}$
p _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200 200 - 300	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ 1.0000 \pm 0.0000 \end{array}$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9943 \pm 0.0015 \\ 0.9977 \pm 0.0023 \\ 1.0000 \pm 0.0000 \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9920 \pm 0.0001 \\ 0.9952 \pm 0.0003 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9968 \pm 0.0016 \\ 0.9950 \pm 0.0050 \\ 1.0000 \pm 0.0000 \end{array}$
p _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200 200 - 300 300 - 10000 Scale Factor ID	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \end{array}$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9943 \pm 0.0015 \\ 0.9977 \pm 0.0023 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9920 \pm 0.0001 \\ 0.9952 \pm 0.0005 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9968 \pm 0.0016 \\ 0.9950 \pm 0.0050 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \end{array}$
$\begin{array}{c} p_{\rm T} \ {\rm range} \ [{\rm GeV}] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ {\rm Scale} \ {\rm Factor} \ {\rm ID} \\ p_{\rm T} \ {\rm range} \ [{\rm GeV}] \\ \hline \end{array}$	$ \begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \eta < 0.8 \\ \end{array} $	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9943 \pm 0.0015 \\ 0.9977 \pm 0.0023 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline 0.8 < \eta < 1.5 \\ \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9920 \pm 0.0001 \\ 0.9952 \pm 0.0005 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9968 \pm 0.0016 \\ 0.9950 \pm 0.0050 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline 1.5 < \eta < 2.1 \\ \end{array}$
$\begin{array}{c} p_{\rm T} \ {\rm range} \ [{\rm GeV}] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ {\rm Scale} \ {\rm Factor} \ {\rm ID} \\ p_{\rm T} \ {\rm range} \ [{\rm GeV}] \\ \hline 20 - 30 \\ \hline \end{array}$	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \eta < 0.8 \\ 0.9801 \pm 0.0007 \\ \end{array}$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9943 \pm 0.0015 \\ 0.9977 \pm 0.0023 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline 0.8 < \eta < 1.5 \\ 0.9833 \pm 0.0009 \\ \hline \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9920 \pm 0.0001 \\ 0.9952 \pm 0.0003 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9968 \pm 0.0016 \\ 0.9950 \pm 0.0050 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline 1.5 < \eta < 2.1 \\ 0.9810 \pm 0.0013 \\ \hline \end{array}$
$\begin{array}{c} p_{\rm T} \ {\rm range} \ [{\rm GeV}] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ {\rm Scale} \ {\rm Factor} \ {\rm ID} \\ p_{\rm T} \ {\rm range} \ [{\rm GeV}] \\ \hline \end{array}$	$ \begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \eta < 0.8 \\ \end{array} $	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9943 \pm 0.0015 \\ 0.9977 \pm 0.0023 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline 0.8 < \eta < 1.5 \\ \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9920 \pm 0.0001 \\ 0.9952 \pm 0.0005 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9968 \pm 0.0016 \\ 0.9950 \pm 0.0050 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline 1.5 < \eta < 2.1 \\ \end{array}$
P _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200 200 - 300 300 - 10000 Scale Factor ID P _T range [GeV] 20 - 30 30 - 40	$ \begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \eta < 0.8 \\ 0.9801 \pm 0.0004 \\ 0.9819 \pm 0.0004 \\ \end{array} $	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9943 \pm 0.0015 \\ 0.9977 \pm 0.0023 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline 0.8 < \eta < 1.5 \\ 0.9833 \pm 0.0009 \\ 0.9829 \pm 0.0005 \\ \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9920 \pm 0.0001 \\ 0.9952 \pm 0.0003 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9968 \pm 0.0016 \\ 0.9950 \pm 0.0050 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline 1.5 < \eta < 2.1 \\ 0.9810 \pm 0.0012 \\ 0.9856 \pm 0.0007 \\ \end{array}$
$\begin{array}{c} p_{\rm T} \ {\rm range} \ [{\rm GeV}] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ Scale \ {\rm Factor} \ {\rm ID} \\ p_{\rm T} \ {\rm range} \ [{\rm GeV}] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ \hline \end{array}$	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ 1.0000 \pm 0.0000 \\ \hline \eta < 0.8 \\ 0.9801 \pm 0.0007 \\ 0.9836 \pm 0.0003 \\ \end{array}$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9943 \pm 0.0015 \\ 0.9977 \pm 0.0023 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline 0.8 < \eta < 1.5 \\ 0.9833 \pm 0.0009 \\ 0.9829 \pm 0.0005 \\ 0.9845 \pm 0.0004 \\ \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9920 \pm 0.0001 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9968 \pm 0.0016 \\ 0.9950 \pm 0.0050 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9810 \pm 0.0012 \\ 0.9856 \pm 0.0007 \\ 0.9875 \pm 0.0006 \\ \end{array}$
$\begin{array}{c} p_{\rm T} \ {\rm range} \ [{\rm GeV}] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ 200 - 300 \\ \hline 300 - 10000 \\ \hline \hline Scale \ {\rm Factor} \ {\rm ID} \\ p_{\rm T} \ {\rm range} \ [{\rm GeV}] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ \hline \end{array}$	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ 1.0000 \pm 0.0000 \\ \hline \eta < 0.8 \\ 0.9801 \pm 0.0007 \\ 0.9819 \pm 0.0004 \\ 0.9836 \pm 0.0003 \\ 0.9808 \pm 0.0007 \end{array}$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9943 \pm 0.0015 \\ 0.9977 \pm 0.0023 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline 0.8 < \eta < 1.5 \\ 0.9833 \pm 0.0009 \\ 0.9829 \pm 0.0005 \\ 0.9845 \pm 0.0004 \\ 0.9808 \pm 0.0009 \\ \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9746 \pm 0.0001 \\ 0.9952 \pm 0.0001 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9968 \pm 0.0016 \\ 0.9950 \pm 0.0050 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline 1.5 < \eta < 2.1 \\ 0.9810 \pm 0.0012 \\ 0.9856 \pm 0.0007 \\ 0.9875 \pm 0.0006 \\ 0.9826 \pm 0.0014 \\ \end{array}$
$\begin{array}{c} p_{\rm T} \ {\rm range} \ [{\rm GeV}] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ Scale \ {\rm Factor} \ {\rm ID} \\ p_{\rm T} \ {\rm range} \ [{\rm GeV}] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ \hline \end{array}$	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ 1.0000 \pm 0.0000 \\ \hline \eta < 0.8 \\ 0.9801 \pm 0.0007 \\ 0.9836 \pm 0.0003 \\ \end{array}$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9943 \pm 0.0015 \\ 0.9977 \pm 0.0023 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline 0.8 < \eta < 1.5 \\ 0.9833 \pm 0.0009 \\ 0.9829 \pm 0.0005 \\ 0.9845 \pm 0.0004 \\ 0.9808 \pm 0.0009 \\ \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9746 \pm 0.0001 \\ 0.9952 \pm 0.0001 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9968 \pm 0.0016 \\ 0.9950 \pm 0.0050 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline 1.5 < \eta < 2.1 \\ 0.9810 \pm 0.0012 \\ 0.9856 \pm 0.0007 \\ 0.9875 \pm 0.0006 \\ 0.9826 \pm 0.0014 \\ \end{array}$
p _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200 200 - 300 300 - 10000 Scale Factor ID p _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ 1.0000 \pm 0.0000 \\ \hline \eta < 0.8 \\ 0.9801 \pm 0.0007 \\ 0.9819 \pm 0.0004 \\ 0.9836 \pm 0.0003 \\ 0.9808 \pm 0.0007 \\ 0.9806 \pm 0.0014 \\ \end{array}$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9943 \pm 0.0015 \\ 0.9977 \pm 0.0023 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline 0.8 < \eta < 1.5 \\ 0.9833 \pm 0.0009 \\ 0.9829 \pm 0.0005 \\ 0.9845 \pm 0.0004 \\ 0.9808 \pm 0.0009 \\ 0.9791 \pm 0.0017 \\ \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9746 \pm 0.0001 \\ 0.9920 \pm 0.0001 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9968 \pm 0.0016 \\ 0.9950 \pm 0.0050 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline 1.5 < \eta < 2.1 \\ 0.9810 \pm 0.0012 \\ 0.9856 \pm 0.0007 \\ 0.9875 \pm 0.0006 \\ 0.9826 \pm 0.0014 \\ 0.9846 \pm 0.0029 \\ \end{array}$
P _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200 200 - 300 300 - 10000 Scale Factor ID P _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \eta < 0.8 \\ \hline 0.9801 \pm 0.0007 \\ 0.9819 \pm 0.0004 \\ 0.9836 \pm 0.0003 \\ 0.9808 \pm 0.0007 \\ 0.9806 \pm 0.0014 \\ 0.9709 \pm 0.0037 \\ \hline \end{array}$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9943 \pm 0.0015 \\ 0.9977 \pm 0.0023 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline 0.8 < \eta < 1.5 \\ 0.9833 \pm 0.0009 \\ 0.9829 \pm 0.0005 \\ 0.9845 \pm 0.0004 \\ 0.9808 \pm 0.0009 \\ 0.9791 \pm 0.0017 \\ 0.9733 \pm 0.0047 \\ \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9746 \pm 0.0001 \\ 0.9920 \pm 0.0001 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9968 \pm 0.0016 \\ 0.9950 \pm 0.0050 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline 1.5 < \eta < 2.1 \\ 0.9856 \pm 0.0012 \\ 0.9856 \pm 0.0007 \\ 0.9856 \pm 0.0007 \\ 0.9826 \pm 0.0014 \\ 0.9846 \pm 0.0029 \\ 0.9937 \pm 0.0084 \\ \hline \end{array}$
$\begin{array}{c} p_{\mathrm{T}} \; \mathrm{range} \; [\mathrm{GeV}] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ \mathbf{Scale} \; \mathrm{Factor} \; \mathrm{ID} \\ p_{\mathrm{T}} \; \mathrm{range} \; [\mathrm{GeV}] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ \hline \end{array}$	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ 1.0000 \pm 0.0000 \\ \hline \eta < 0.8 \\ \hline 0.9801 \pm 0.0007 \\ 0.9819 \pm 0.0004 \\ 0.9836 \pm 0.0003 \\ 0.9808 \pm 0.0007 \\ 0.9806 \pm 0.0014 \\ 0.9709 \pm 0.0037 \\ 0.9713 \pm 0.0052 \\ \hline \end{array}$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9943 \pm 0.0015 \\ 0.9977 \pm 0.0023 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline 0.8 < \eta < 1.5 \\ 0.9833 \pm 0.0009 \\ 0.9829 \pm 0.0005 \\ 0.9845 \pm 0.0004 \\ 0.9808 \pm 0.0009 \\ 0.9791 \pm 0.0017 \\ 0.9762 \pm 0.0060 \\ \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9920 \pm 0.0001 \\ 0.9952 \pm 0.0005 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9950 \pm 0.0050 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9810 \pm 0.0012 \\ 0.9856 \pm 0.0014 \\ 0.9826 \pm 0.0014 \\ 0.9826 \pm 0.0014 \\ 0.9846 \pm 0.0029 \\ 0.9937 \pm 0.0084 \\ 0.9539 \pm 0.0115 \\ \end{array}$
$\begin{array}{c} p_{\mathrm{T}} \; \mathrm{range} \; [\mathrm{GeV}] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ \mathbf{Scale} \; \mathrm{Factor} \; \mathrm{ID} \\ p_{\mathrm{T}} \; \mathrm{range} \; [\mathrm{GeV}] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ \hline \end{array}$	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ 1.0000 \pm 0.0000 \\ \hline \eta < 0.8 \\ \hline 0.9801 \pm 0.0007 \\ 0.9819 \pm 0.0004 \\ 0.9836 \pm 0.0003 \\ 0.9808 \pm 0.0007 \\ 0.9806 \pm 0.0014 \\ 0.9709 \pm 0.0037 \\ 0.9713 \pm 0.0052 \\ \hline \end{array}$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9943 \pm 0.0015 \\ 0.9977 \pm 0.0023 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline 0.8 < \eta < 1.5 \\ 0.9833 \pm 0.0009 \\ 0.9829 \pm 0.0005 \\ 0.9845 \pm 0.0004 \\ 0.9808 \pm 0.0009 \\ 0.9791 \pm 0.0017 \\ 0.9762 \pm 0.0060 \\ \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9920 \pm 0.0001 \\ 0.9952 \pm 0.0005 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9950 \pm 0.0050 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9810 \pm 0.0012 \\ 0.9856 \pm 0.0014 \\ 0.9826 \pm 0.0014 \\ 0.9826 \pm 0.0014 \\ 0.9846 \pm 0.0029 \\ 0.9937 \pm 0.0084 \\ 0.9539 \pm 0.0115 \\ \end{array}$
$\begin{array}{c} p_{\rm T} \ {\rm range} \ [{\rm GeV}] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ 200 - 300 \\ \hline 300 - 10000 \\ \hline \\ Scale \ {\rm Factor} \ {\rm ID} \\ p_{\rm T} \ {\rm range} \ [{\rm GeV}] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ \hline \end{array}$	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \eta < 0.8 \\ 0.9801 \pm 0.0007 \\ 0.9819 \pm 0.0004 \\ 0.9836 \pm 0.0003 \\ 0.9808 \pm 0.0007 \\ 0.9808 \pm 0.0007 \\ 0.9806 \pm 0.0014 \\ 0.9709 \pm 0.0037 \\ 0.9713 \pm 0.0052 \\ 0.9907 \pm 0.0109 \\ \hline \end{array}$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9943 \pm 0.0015 \\ 0.9977 \pm 0.0023 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 0.8 < \eta < 1.5 \\ 0.9833 \pm 0.0009 \\ 0.9829 \pm 0.0005 \\ 0.9845 \pm 0.0004 \\ 0.9808 \pm 0.0009 \\ 0.9791 \pm 0.0017 \\ 0.9733 \pm 0.0047 \\ 0.9762 \pm 0.0060 \\ 1.0017 \pm 0.0142 \\ \hline \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9920 \pm 0.0001 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9958 \pm 0.0016 \\ 0.9950 \pm 0.0050 \\ 1.0000 \pm 0.0050 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9856 \pm 0.0012 \\ 0.9856 \pm 0.0012 \\ 0.9856 \pm 0.0007 \\ 0.9875 \pm 0.0006 \\ 0.9826 \pm 0.0014 \\ 0.9836 \pm 0.0012 \\ 0.9937 \pm 0.0084 \\ 0.9539 \pm 0.0115 \\ 0.9918 \pm 0.0343 \\ \end{array}$
$\begin{array}{c} p_{\rm T} \ {\rm range} \ [{\rm GeV}] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ 200 - 300 \\ \hline 300 - 10000 \\ \hline \\ Scale \ {\rm Factor} \ {\rm ID} \\ p_{\rm T} \ {\rm range} \ [{\rm GeV}] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ 200 - 300 \\ \hline \end{array}$	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ 1.0000 \pm 0.0000 \\ \hline \eta < 0.8 \\ 0.9801 \pm 0.0007 \\ 0.9819 \pm 0.0004 \\ 0.9836 \pm 0.0007 \\ 0.9808 \pm 0.0007 \\ 0.9808 \pm 0.0014 \\ 0.9709 \pm 0.0037 \\ 0.9713 \pm 0.0052 \\ 0.9907 \pm 0.0109 \\ 0.9378 \pm 0.0233 \\ \end{array}$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9943 \pm 0.0015 \\ 0.9977 \pm 0.0023 \\ 1.0000 \pm 0.0000 \\ \hline \\ 0.8 < \eta < 1.5 \\ 0.9833 \pm 0.0009 \\ 0.9829 \pm 0.0005 \\ 0.9845 \pm 0.0004 \\ 0.9808 \pm 0.0009 \\ 0.9791 \pm 0.0017 \\ 0.9733 \pm 0.0047 \\ 0.9762 \pm 0.0060 \\ 1.0017 \pm 0.0142 \\ 0.9946 \pm 0.0278 \\ \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9746 \pm 0.0001 \\ 0.9952 \pm 0.0001 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9968 \pm 0.0016 \\ 0.9950 \pm 0.0050 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9810 \pm 0.0012 \\ 0.9856 \pm 0.0007 \\ 0.9875 \pm 0.0006 \\ 0.9826 \pm 0.0014 \\ 0.9846 \pm 0.0029 \\ 0.9937 \pm 0.0084 \\ 0.9539 \pm 0.0115 \\ 0.9918 \pm 0.0343 \\ 0.9468 \pm 0.0671 \\ \hline \end{array}$
$\begin{array}{c} p_{\rm T} \ {\rm range} \ [{\rm GeV}] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ 200 - 300 \\ \hline 300 - 10000 \\ \hline \\ Scale \ {\rm Factor} \ {\rm ID} \\ p_{\rm T} \ {\rm range} \ [{\rm GeV}] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ \hline \end{array}$	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \eta < 0.8 \\ 0.9801 \pm 0.0007 \\ 0.9819 \pm 0.0004 \\ 0.9836 \pm 0.0003 \\ 0.9808 \pm 0.0007 \\ 0.9808 \pm 0.0007 \\ 0.9806 \pm 0.0014 \\ 0.9709 \pm 0.0037 \\ 0.9713 \pm 0.0052 \\ 0.9907 \pm 0.0109 \\ \hline \end{array}$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9943 \pm 0.0015 \\ 0.9977 \pm 0.0023 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 0.8 < \eta < 1.5 \\ 0.9833 \pm 0.0009 \\ 0.9829 \pm 0.0005 \\ 0.9845 \pm 0.0004 \\ 0.9808 \pm 0.0009 \\ 0.9791 \pm 0.0017 \\ 0.9733 \pm 0.0047 \\ 0.9762 \pm 0.0060 \\ 1.0017 \pm 0.0142 \\ \hline \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9920 \pm 0.0001 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9958 \pm 0.0016 \\ 0.9950 \pm 0.0050 \\ 1.0000 \pm 0.0050 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9856 \pm 0.0012 \\ 0.9856 \pm 0.0012 \\ 0.9856 \pm 0.0007 \\ 0.9875 \pm 0.0006 \\ 0.9826 \pm 0.0014 \\ 0.9836 \pm 0.0012 \\ 0.9937 \pm 0.0084 \\ 0.9539 \pm 0.0115 \\ 0.9918 \pm 0.0343 \\ \end{array}$
$\begin{array}{c} p_{\rm T} \ {\rm range} \ [{\rm GeV}] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ 200 - 300 \\ \hline 300 - 10000 \\ \hline \\ Scale \ {\rm Factor} \ {\rm ID} \\ p_{\rm T} \ {\rm range} \ [{\rm GeV}] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \end{array}$	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ 1.0000 \pm 0.0000 \\ \hline \\ \eta < 0.8 \\ 0.9801 \pm 0.0007 \\ 0.9819 \pm 0.0004 \\ 0.9836 \pm 0.0007 \\ 0.9808 \pm 0.0007 \\ 0.9808 \pm 0.0014 \\ 0.9709 \pm 0.0037 \\ 0.9713 \pm 0.0052 \\ 0.9907 \pm 0.0109 \\ 0.9378 \pm 0.0233 \\ \end{array}$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9943 \pm 0.0015 \\ 0.9977 \pm 0.0023 \\ 1.0000 \pm 0.0000 \\ \hline \\ 0.8 < \eta < 1.5 \\ 0.9833 \pm 0.0009 \\ 0.9829 \pm 0.0005 \\ 0.9845 \pm 0.0004 \\ 0.9808 \pm 0.0009 \\ 0.9791 \pm 0.0017 \\ 0.9733 \pm 0.0047 \\ 0.9762 \pm 0.0060 \\ 1.0017 \pm 0.0142 \\ 0.9946 \pm 0.0278 \\ \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9746 \pm 0.0001 \\ 0.9952 \pm 0.0001 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9968 \pm 0.0016 \\ 0.9950 \pm 0.0050 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9810 \pm 0.0012 \\ 0.9856 \pm 0.0007 \\ 0.9875 \pm 0.0006 \\ 0.9826 \pm 0.0014 \\ 0.9846 \pm 0.0029 \\ 0.9937 \pm 0.0084 \\ 0.9539 \pm 0.0115 \\ 0.9918 \pm 0.0343 \\ 0.9468 \pm 0.0671 \\ \hline \end{array}$
P _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200 200 - 300 300 - 10000 Scale Factor ID P _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200 200 - 300 300 - 10000 Scale Factor ISO	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ 1.0000 \pm 0.0000 \\ \hline \\ \eta < 0.8 \\ 0.9801 \pm 0.0007 \\ 0.9819 \pm 0.0004 \\ 0.9836 \pm 0.0007 \\ 0.9808 \pm 0.0007 \\ 0.9808 \pm 0.0014 \\ 0.9709 \pm 0.0037 \\ 0.9713 \pm 0.0052 \\ 0.9907 \pm 0.0109 \\ 0.9378 \pm 0.0233 \\ \end{array}$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9943 \pm 0.0015 \\ 0.9977 \pm 0.0023 \\ 1.0000 \pm 0.0000 \\ \hline \\ 0.8 < \eta < 1.5 \\ 0.9833 \pm 0.0009 \\ 0.9829 \pm 0.0005 \\ 0.9845 \pm 0.0004 \\ 0.9808 \pm 0.0009 \\ 0.9791 \pm 0.0017 \\ 0.9733 \pm 0.0047 \\ 0.9762 \pm 0.0060 \\ 1.0017 \pm 0.0142 \\ 0.9946 \pm 0.0278 \\ \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9746 \pm 0.0001 \\ 0.9952 \pm 0.0001 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9968 \pm 0.0016 \\ 0.9950 \pm 0.0050 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9810 \pm 0.0012 \\ 0.9856 \pm 0.0007 \\ 0.9875 \pm 0.0006 \\ 0.9826 \pm 0.0014 \\ 0.9846 \pm 0.0029 \\ 0.9937 \pm 0.0084 \\ 0.9539 \pm 0.0115 \\ 0.9918 \pm 0.0343 \\ 0.9468 \pm 0.0671 \\ \hline \end{array}$
P _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200 200 - 300 300 - 10000 Scale Factor ID P _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200 200 - 300 300 - 10000 Scale Factor ISO	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ 1.0000 \pm 0.0000 \\ \hline \\ \eta < 0.8 \\ 0.9801 \pm 0.0007 \\ 0.9819 \pm 0.0004 \\ 0.9836 \pm 0.0003 \\ 0.9808 \pm 0.0003 \\ 0.9808 \pm 0.0004 \\ 0.9366 \pm 0.0014 \\ 0.9709 \pm 0.0037 \\ 0.9713 \pm 0.0052 \\ 0.9907 \pm 0.0109 \\ 0.9378 \pm 0.0233 \\ 0.7328 \pm 0.0701 \\ \hline \end{array}$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9943 \pm 0.0015 \\ 0.9977 \pm 0.0023 \\ 1.0000 \pm 0.0000 \\ \hline \\ 0.8 < \eta < 1.5 \\ 0.9833 \pm 0.0009 \\ 0.9829 \pm 0.0005 \\ 0.9845 \pm 0.0004 \\ 0.9808 \pm 0.0004 \\ 0.9808 \pm 0.0004 \\ 0.9762 \pm 0.0007 \\ 0.9762 \pm 0.0067 \\ 0.0017 \pm 0.0017 \\ 0.9762 \pm 0.0060 \\ 1.0017 \pm 0.0142 \\ 0.9946 \pm 0.0278 \\ 0.7562 \pm 0.1200 \\ \hline \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9746 \pm 0.0001 \\ 0.9952 \pm 0.0001 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9968 \pm 0.0016 \\ 0.9950 \pm 0.0050 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9810 \pm 0.0012 \\ 0.9856 \pm 0.0007 \\ 0.9875 \pm 0.0006 \\ 0.9826 \pm 0.0014 \\ 0.9846 \pm 0.0029 \\ 0.9937 \pm 0.0084 \\ 0.9539 \pm 0.0115 \\ 0.9918 \pm 0.0343 \\ 0.9468 \pm 0.0671 \\ 0.9468 \pm 0.0671 \\ 0.9500 \pm 0.3227 \\ \hline \end{array}$
$\begin{array}{c} p_{\rm T} \ {\rm range} \ [{\rm GeV}] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ Scale \ {\rm Factor} \ {\rm ID} \\ p_{\rm T} \ {\rm range} \ [{\rm GeV}] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ Scale \ {\rm Factor} \ {\rm ISO} \\ p_{\rm T} \ {\rm range} \ [{\rm GeV}] \\ \hline \end{array}$	$ \begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ \eta < 0.8 \\ \hline 0.9801 \pm 0.0007 \\ 0.9819 \pm 0.0004 \\ 0.9836 \pm 0.0003 \\ 0.9808 \pm 0.0007 \\ 0.9806 \pm 0.0014 \\ 0.9709 \pm 0.0037 \\ 0.9713 \pm 0.0052 \\ 0.9907 \pm 0.0109 \\ 0.9378 \pm 0.0233 \\ 0.7328 \pm 0.0701 \\ \hline \\ \eta < 0.8 \\ \hline \end{array} $	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9943 \pm 0.0015 \\ 0.9977 \pm 0.0023 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 0.8 < \eta < 1.5 \\ 0.9833 \pm 0.0009 \\ 0.9829 \pm 0.0005 \\ 0.9845 \pm 0.0004 \\ 0.9808 \pm 0.0009 \\ 0.9791 \pm 0.0017 \\ 0.9733 \pm 0.0047 \\ 0.9762 \pm 0.0042 \\ 0.9946 \pm 0.0278 \\ 0.7562 \pm 0.1200 \\ \hline \\ 0.8 < \eta < 1.5 \\ \hline \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9746 \pm 0.0003 \\ 0.9920 \pm 0.0001 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9950 \pm 0.0016 \\ 0.9950 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9810 \pm 0.0012 \\ 0.9856 \pm 0.0017 \\ 0.9856 \pm 0.0007 \\ 0.9856 \pm 0.0007 \\ 0.9875 \pm 0.0006 \\ 0.9826 \pm 0.0014 \\ 0.9846 \pm 0.0029 \\ 0.9937 \pm 0.0084 \\ 0.9539 \pm 0.0115 \\ 0.9918 \pm 0.0343 \\ 0.99468 \pm 0.0671 \\ 0.5000 \pm 0.3227 \\ \hline \\ 1.5 < \eta < 2.1 \\ \hline \end{array}$
$\begin{array}{c} p_{\rm T} \ {\rm range} \ [{\rm GeV}] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ Scale \ {\rm Factor} \ {\rm ID} \\ p_{\rm T} \ {\rm range} \ [{\rm GeV}] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ Scale \ {\rm Factor} \ {\rm ISO} \\ p_{\rm T} \ {\rm range} \ [{\rm GeV}] \\ \hline \end{array}$	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \eta < 0.8 \\ 0.9801 \pm 0.0007 \\ 0.9819 \pm 0.0004 \\ 0.9836 \pm 0.0003 \\ 0.9808 \pm 0.0007 \\ 0.9806 \pm 0.0014 \\ 0.9709 \pm 0.0037 \\ 0.9713 \pm 0.0052 \\ 0.9907 \pm 0.0109 \\ 0.9378 \pm 0.0233 \\ 0.7328 \pm 0.0701 \\ \hline \eta < 0.8 \\ \hline 0.9971 \pm 0.0011 \\ \hline \end{array}$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9938 \pm 0.0015 \\ 0.9977 \pm 0.0023 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 0.8 < \eta < 1.5 \\ 0.9833 \pm 0.0009 \\ 0.9829 \pm 0.0005 \\ 0.9845 \pm 0.0004 \\ 0.9808 \pm 0.0009 \\ 0.9791 \pm 0.0017 \\ 0.9733 \pm 0.0047 \\ 0.9762 \pm 0.0042 \\ 0.9946 \pm 0.0278 \\ 0.7562 \pm 0.1200 \\ \hline \\ 0.8 < \eta < 1.5 \\ 0.9987 \pm 0.0012 \\ \hline \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9920 \pm 0.0001 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9950 \pm 0.0016 \\ 0.9950 \pm 0.0050 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9856 \pm 0.0012 \\ 0.9856 \pm 0.0012 \\ 0.9856 \pm 0.0007 \\ 0.9856 \pm 0.0007 \\ 0.9856 \pm 0.0004 \\ 0.9826 \pm 0.0014 \\ 0.9826 \pm 0.0014 \\ 0.9837 \pm 0.0084 \\ 0.9539 \pm 0.0115 \\ 0.9937 \pm 0.0084 \\ 0.9539 \pm 0.0115 \\ 0.9918 \pm 0.0343 \\ 0.9468 \pm 0.0671 \\ 0.5000 \pm 0.3227 \\ \hline \\ 1.5 < \eta < 2.1 \\ 1.0062 \pm 0.0012 \\ \hline \end{array}$
$\begin{array}{c} p_{\rm T} \ {\rm range} \ [{\rm GeV}] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ Scale \ {\rm Factor} \ {\rm ID} \\ p_{\rm T} \ {\rm range} \ [{\rm GeV}] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ Scale \ {\rm Factor} \ {\rm ISO} \\ p_{\rm T} \ {\rm range} \ [{\rm GeV}] \\ \hline \end{array}$	$ \begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ \eta < 0.8 \\ \hline 0.9801 \pm 0.0007 \\ 0.9819 \pm 0.0004 \\ 0.9836 \pm 0.0003 \\ 0.9808 \pm 0.0007 \\ 0.9806 \pm 0.0014 \\ 0.9709 \pm 0.0037 \\ 0.9713 \pm 0.0052 \\ 0.9907 \pm 0.0109 \\ 0.9378 \pm 0.0233 \\ 0.7328 \pm 0.0701 \\ \hline \\ \eta < 0.8 \\ \hline \end{array} $	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9943 \pm 0.0015 \\ 0.9977 \pm 0.0023 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 0.8 < \eta < 1.5 \\ 0.9833 \pm 0.0009 \\ 0.9829 \pm 0.0005 \\ 0.9845 \pm 0.0004 \\ 0.9808 \pm 0.0009 \\ 0.9791 \pm 0.0017 \\ 0.9733 \pm 0.0047 \\ 0.9762 \pm 0.0042 \\ 0.9946 \pm 0.0278 \\ 0.7562 \pm 0.1200 \\ \hline \\ 0.8 < \eta < 1.5 \\ \hline \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9746 \pm 0.0003 \\ 0.9920 \pm 0.0001 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9950 \pm 0.0016 \\ 0.9950 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9810 \pm 0.0012 \\ 0.9856 \pm 0.0016 \\ 0.9856 \pm 0.0007 \\ 0.9875 \pm 0.0006 \\ 0.9826 \pm 0.0014 \\ 0.9846 \pm 0.0014 \\ 0.9846 \pm 0.0029 \\ 0.9937 \pm 0.0084 \\ 0.9539 \pm 0.0115 \\ 0.9918 \pm 0.0343 \\ 0.99468 \pm 0.0671 \\ 0.5000 \pm 0.3227 \\ \hline \\ 1.5 < \eta < 2.1 \\ \hline \end{array}$
P _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 200 - 300 300 - 10000 Scale Factor ID P _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200 200 - 300 300 - 10000 Scale Factor ISO P _T range [GeV]	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline & & & & & & & & & & & & & & & & & &$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9943 \pm 0.0015 \\ 0.9977 \pm 0.0023 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 0.8 < \eta < 1.5 \\ 0.9833 \pm 0.0009 \\ 0.9829 \pm 0.0005 \\ 0.9845 \pm 0.0004 \\ 0.9808 \pm 0.0009 \\ 0.9791 \pm 0.0017 \\ 0.9733 \pm 0.0047 \\ 0.9762 \pm 0.0060 \\ 1.0017 \pm 0.0142 \\ 0.9946 \pm 0.0278 \\ 0.7562 \pm 0.1200 \\ \hline \\ 0.8 < \eta < 1.5 \\ 0.9987 \pm 0.0012 \\ 1.0014 \pm 0.0004 \\ \hline \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9746 \pm 0.0003 \\ 0.9920 \pm 0.0001 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9968 \pm 0.0016 \\ 0.9950 \pm 0.0050 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9810 \pm 0.0012 \\ 0.9856 \pm 0.0014 \\ 0.9846 \pm 0.0012 \\ 0.9856 \pm 0.0004 \\ 0.9826 \pm 0.0014 \\ 0.9846 \pm 0.0029 \\ 0.9937 \pm 0.0084 \\ 0.9539 \pm 0.0115 \\ 0.9918 \pm 0.0343 \\ 0.9468 \pm 0.0671 \\ 0.5000 \pm 0.3227 \\ \hline \\ 1.5 < \eta < 2.1 \\ 1.0662 \pm 0.0012 \\ 1.0042 \pm 0.0004 \\ \hline \end{array}$
$\begin{array}{c} p_{\rm T} \ {\rm range} \ [{\rm GeV}] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ 200 - 300 \\ \hline 300 - 10000 \\ \hline \\ Scale \ {\rm Factor} \ {\rm ID} \\ p_{\rm T} \ {\rm range} \ [{\rm GeV}] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ \hline 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ 200 - 300 \\ \hline 300 - 10000 \\ \hline \\ Scale \ {\rm Factor} \ {\rm ISO} \\ p_{\rm T} \ {\rm range} \ [{\rm GeV}] \\ \hline 20 - 30 \\ 30 - 10000 \\ \hline \\ Scale \ {\rm Factor} \ {\rm ISO} \\ p_{\rm T} \ {\rm range} \ [{\rm GeV}] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ \hline \end{array}$	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ 1.0000 \pm 0.0000 \\ \hline \\ \eta < 0.8 \\ 0.9801 \pm 0.0007 \\ 0.9819 \pm 0.0004 \\ 0.9836 \pm 0.0007 \\ 0.9819 \pm 0.0004 \\ 0.9836 \pm 0.0007 \\ 0.9808 \pm 0.0007 \\ 0.9808 \pm 0.0014 \\ 0.9709 \pm 0.0037 \\ 0.9713 \pm 0.0052 \\ 0.9907 \pm 0.0109 \\ 0.9378 \pm 0.0233 \\ 0.7328 \pm 0.0701 \\ \hline \\ \eta < 0.8 \\ \hline \\ 0.9971 \pm 0.0011 \\ 0.9987 \pm 0.0003 \\ 0.9994 \pm 0.0002 \\ \hline \end{array}$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9943 \pm 0.0015 \\ 0.9977 \pm 0.0023 \\ 1.0000 \pm 0.0000 \\ \hline \\ 0.8 < \eta < 1.5 \\ 0.9833 \pm 0.0009 \\ 0.9829 \pm 0.0005 \\ 0.9845 \pm 0.0004 \\ 0.9808 \pm 0.0009 \\ 0.9791 \pm 0.0017 \\ 0.9733 \pm 0.0047 \\ 0.9762 \pm 0.0060 \\ 1.0017 \pm 0.0142 \\ 0.9946 \pm 0.0278 \\ 0.7562 \pm 0.1200 \\ \hline \\ 0.8 < \eta < 1.5 \\ 0.9987 \pm 0.0012 \\ 1.0014 \pm 0.0004 \\ 1.0006 \pm 0.0002 \\ \hline \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9746 \pm 0.0003 \\ 0.9920 \pm 0.0001 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9968 \pm 0.0016 \\ 0.9950 \pm 0.0050 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9810 \pm 0.0012 \\ 0.9856 \pm 0.0007 \\ 0.9875 \pm 0.0006 \\ 0.9826 \pm 0.0007 \\ 0.9875 \pm 0.0006 \\ 0.9826 \pm 0.0014 \\ 0.9846 \pm 0.0029 \\ 0.9937 \pm 0.0084 \\ 0.9539 \pm 0.0115 \\ 0.9918 \pm 0.0343 \\ 0.9468 \pm 0.0671 \\ 0.5000 \pm 0.3227 \\ \hline \\ 1.5 < \eta < 2.1 \\ 1.0062 \pm 0.0012 \\ 1.0042 \pm 0.0004 \\ 1.0008 \pm 0.0002 \\ \end{array}$
P _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 200 - 300 300 - 10000 Scale Factor ID P _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200 200 - 300 300 - 10000 Scale Factor ISO P _T range [GeV]	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ \eta < 0.8 \\ 0.9801 \pm 0.0007 \\ 0.9819 \pm 0.0004 \\ 0.9836 \pm 0.0003 \\ 0.9808 \pm 0.0007 \\ 0.9806 \pm 0.0014 \\ 0.9709 \pm 0.0037 \\ 0.9713 \pm 0.0052 \\ 0.9907 \pm 0.0109 \\ 0.9378 \pm 0.0233 \\ 0.7328 \pm 0.0701 \\ \hline \\ \eta < 0.8 \\ 0.9971 \pm 0.0011 \\ 0.9987 \pm 0.0003 \\ 0.9995 \pm 0.0003 \\ 0.9995 \pm 0.0003 \end{array}$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9943 \pm 0.0015 \\ 0.9977 \pm 0.0023 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 0.8 < \eta < 1.5 \\ 0.9833 \pm 0.0009 \\ 0.9829 \pm 0.0005 \\ 0.9845 \pm 0.0004 \\ 0.9808 \pm 0.0009 \\ 0.9791 \pm 0.0017 \\ 0.9733 \pm 0.0047 \\ 0.9762 \pm 0.0060 \\ 1.0017 \pm 0.0142 \\ 0.9946 \pm 0.0278 \\ 0.7562 \pm 0.1200 \\ \hline \\ 0.8 < \eta < 1.5 \\ 0.9987 \pm 0.0012 \\ 1.0014 \pm 0.0004 \\ \hline \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9746 \pm 0.0003 \\ 0.9920 \pm 0.0001 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9968 \pm 0.0016 \\ 0.9950 \pm 0.0050 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9810 \pm 0.0012 \\ 0.9856 \pm 0.0014 \\ 0.9846 \pm 0.0012 \\ 0.9856 \pm 0.0004 \\ 0.9826 \pm 0.0014 \\ 0.9846 \pm 0.0029 \\ 0.9937 \pm 0.0084 \\ 0.9539 \pm 0.0115 \\ 0.9918 \pm 0.0343 \\ 0.9468 \pm 0.0671 \\ 0.5000 \pm 0.3227 \\ \hline \\ 1.5 < \eta < 2.1 \\ 1.0662 \pm 0.0012 \\ 1.0042 \pm 0.0004 \\ \hline \end{array}$
P _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200 200 - 300 300 - 10000 Scale Factor ID P _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200 200 - 300 300 - 10000 Scale Factor ISO P _T range [GeV]	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ \eta < 0.8 \\ 0.9801 \pm 0.0007 \\ 0.9819 \pm 0.0004 \\ 0.9836 \pm 0.0003 \\ 0.9808 \pm 0.0007 \\ 0.9806 \pm 0.0014 \\ 0.9709 \pm 0.0037 \\ 0.9713 \pm 0.0052 \\ 0.9907 \pm 0.0109 \\ 0.9378 \pm 0.0233 \\ 0.7328 \pm 0.0701 \\ \hline \\ \eta < 0.8 \\ 0.9971 \pm 0.0011 \\ 0.9987 \pm 0.0003 \\ 0.9995 \pm 0.0003 \\ 0.9995 \pm 0.0003 \end{array}$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9938 \pm 0.0011 \\ 0.9943 \pm 0.0015 \\ 0.9977 \pm 0.0023 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 0.8 < \eta < 1.5 \\ 0.9833 \pm 0.0009 \\ 0.9829 \pm 0.0005 \\ 0.9845 \pm 0.0004 \\ 0.9808 \pm 0.0009 \\ 0.9791 \pm 0.0017 \\ 0.9733 \pm 0.0047 \\ 0.9762 \pm 0.0060 \\ 1.0017 \pm 0.0142 \\ 0.9946 \pm 0.0278 \\ 0.7562 \pm 0.1200 \\ \hline \\ 0.8 < \eta < 1.5 \\ 0.9987 \pm 0.0012 \\ 1.0014 \pm 0.0004 \\ 1.0006 \pm 0.0002 \\ 1.0007 \pm 0.0003 \\ \hline \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9746 \pm 0.0003 \\ 0.9920 \pm 0.0001 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9968 \pm 0.0016 \\ 0.9950 \pm 0.0050 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9810 \pm 0.0012 \\ 0.9856 \pm 0.0007 \\ 0.9856 \pm 0.0007 \\ 0.9856 \pm 0.0006 \\ 0.9856 \pm 0.0014 \\ 0.9846 \pm 0.0014 \\ 0.9846 \pm 0.0014 \\ 0.9846 \pm 0.0014 \\ 0.99468 \pm 0.0671 \\ 0.5000 \pm 0.3227 \\ \hline \\ 1.5 < \eta < 2.1 \\ 1.0062 \pm 0.0012 \\ 1.0042 \pm 0.0002 \\ 1.0042 \pm 0.0004 \\ 1.0008 \pm 0.0002 \\ 1.0014 \pm 0.0004 \\ \hline \end{array}$
P _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200 200 - 300 300 - 10000 Scale Factor ID P _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200 200 - 300 300 - 10000 Scale Factor ISO P _T range [GeV]	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \eta < 0.8 \\ 0.9801 \pm 0.0007 \\ 0.9819 \pm 0.0004 \\ 0.9836 \pm 0.0003 \\ 0.9808 \pm 0.0007 \\ 0.9819 \pm 0.0004 \\ 0.9836 \pm 0.0014 \\ 0.9709 \pm 0.0037 \\ 0.9713 \pm 0.0052 \\ 0.9907 \pm 0.0109 \\ 0.9378 \pm 0.0233 \\ 0.7328 \pm 0.0701 \\ \hline \eta < 0.8 \\ \hline 0.9971 \pm 0.0011 \\ 0.9987 \pm 0.0003 \\ 0.9995 \pm 0.0003 \\ 0.9995 \pm 0.0006 \\ \hline \end{array}$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9938 \pm 0.0015 \\ 0.9977 \pm 0.0023 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 0.8 < \eta < 1.5 \\ 0.9833 \pm 0.0009 \\ 0.9829 \pm 0.0005 \\ 0.9845 \pm 0.0004 \\ 0.9808 \pm 0.0009 \\ 0.9791 \pm 0.0017 \\ 0.9733 \pm 0.0047 \\ 0.9762 \pm 0.0060 \\ 1.0017 \pm 0.0142 \\ 0.9946 \pm 0.0278 \\ 0.7562 \pm 0.1200 \\ \hline \\ 0.8 < \eta < 1.5 \\ 0.9987 \pm 0.0012 \\ 1.0014 \pm 0.0004 \\ 1.0014 \pm 0.0004 \\ 1.0006 \pm 0.0002 \\ 1.0007 \pm 0.0003 \\ 0.9994 \pm 0.0006 \\ \hline \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9746 \pm 0.0003 \\ 0.9920 \pm 0.0001 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9950 \pm 0.0050 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9856 \pm 0.0012 \\ 0.9856 \pm 0.0012 \\ 0.9856 \pm 0.0012 \\ 0.9856 \pm 0.0012 \\ 0.9856 \pm 0.0014 \\ 0.9875 \pm 0.0006 \\ 0.9826 \pm 0.0014 \\ 0.9837 \pm 0.0084 \\ 0.9539 \pm 0.0115 \\ 0.9937 \pm 0.0084 \\ 0.9539 \pm 0.0115 \\ 0.9918 \pm 0.0343 \\ 0.9468 \pm 0.0671 \\ 0.5000 \pm 0.3227 \\ \hline \\ 1.5 < \eta < 2.1 \\ 1.0062 \pm 0.0012 \\ 1.0042 \pm 0.0004 \\ 1.0008 \pm 0.0002 \\ 1.0014 \pm 0.0004 \\ 1.0005 \pm 0.0007 \\ \hline \end{array}$
P _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200 200 - 300 300 - 10000 Scale Factor ID P _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200 200 - 300 300 - 10000 Scale Factor ISO P _T range [GeV]	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ 1.0000 \pm 0.0000 \\ \hline \\ \eta < 0.8 \\ 0.9801 \pm 0.0007 \\ 0.9819 \pm 0.0007 \\ 0.9819 \pm 0.0003 \\ 0.9808 \pm 0.0007 \\ 0.9806 \pm 0.0014 \\ 0.9709 \pm 0.0037 \\ 0.9713 \pm 0.0052 \\ 0.9907 \pm 0.0109 \\ 0.9378 \pm 0.0233 \\ 0.7328 \pm 0.0701 \\ \hline \\ \eta < 0.8 \\ \hline \\ 0.9971 \pm 0.0011 \\ 0.9987 \pm 0.0003 \\ 0.9994 \pm 0.0003 \\ 0.9995 \pm 0.0003 \\ 0.9995 \pm 0.0006 \\ 1.0002 \pm 0.0016 \\ \hline \end{array}$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9938 \pm 0.0015 \\ 0.9977 \pm 0.0023 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 0.8 < \eta < 1.5 \\ 0.9833 \pm 0.0009 \\ 0.9829 \pm 0.0005 \\ 0.9845 \pm 0.0009 \\ 0.9829 \pm 0.0005 \\ 0.9845 \pm 0.0009 \\ 0.9791 \pm 0.0017 \\ 0.9733 \pm 0.0047 \\ 0.9762 \pm 0.0060 \\ 1.0017 \pm 0.0142 \\ 0.9946 \pm 0.0278 \\ 0.7562 \pm 0.1200 \\ \hline \\ 0.8 < \eta < 1.5 \\ 0.9987 \pm 0.0012 \\ 1.0014 \pm 0.0004 \\ 1.0006 \pm 0.0002 \\ 1.0007 \pm 0.0003 \\ 0.9994 \pm 0.0006 \\ 1.0015 \pm 0.0017 \\ \hline \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9746 \pm 0.0003 \\ 0.9920 \pm 0.0001 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9968 \pm 0.0016 \\ 0.9950 \pm 0.0050 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9856 \pm 0.0016 \\ 0.9950 \pm 0.0000 \\ \hline \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9810 \pm 0.0012 \\ 0.9856 \pm 0.00014 \\ 0.9826 \pm 0.0014 \\ 0.9839 \pm 0.0015 \\ 0.9937 \pm 0.0084 \\ 0.9539 \pm 0.0015 \\ 0.9937 \pm 0.0084 \\ 0.9539 \pm 0.0115 \\ 0.9918 \pm 0.0343 \\ 0.9468 \pm 0.0671 \\ 0.5000 \pm 0.3227 \\ \hline \\ 1.5 < \eta < 2.1 \\ 1.0062 \pm 0.0012 \\ 1.0042 \pm 0.0004 \\ 1.0008 \pm 0.0002 \\ 1.0014 \pm 0.0004 \\ 1.0005 \pm 0.0007 \\ 1.0010 \pm 0.0022 \\ \hline \end{array}$
P _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200 200 - 300 300 - 10000 Scale Factor ID P _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200 200 - 300 300 - 10000 Scale Factor ISO P _T range [GeV]	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ 1.0000 \pm 0.0000 \\ \hline \\ \eta < 0.8 \\ 0.9801 \pm 0.0007 \\ 0.9819 \pm 0.0007 \\ 0.9819 \pm 0.0003 \\ 0.9808 \pm 0.0007 \\ 0.9806 \pm 0.0014 \\ 0.9709 \pm 0.0037 \\ 0.9713 \pm 0.0052 \\ 0.9907 \pm 0.0109 \\ 0.9378 \pm 0.0233 \\ 0.7328 \pm 0.0701 \\ \hline \\ \eta < 0.8 \\ \hline \\ 0.9971 \pm 0.0011 \\ 0.9987 \pm 0.0003 \\ 0.9994 \pm 0.0003 \\ 0.9995 \pm 0.0003 \\ 0.9995 \pm 0.0006 \\ 1.0002 \pm 0.0016 \\ \hline \end{array}$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9938 \pm 0.0015 \\ 0.9977 \pm 0.0023 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 0.8 < \eta < 1.5 \\ 0.9833 \pm 0.0009 \\ 0.9829 \pm 0.0005 \\ 0.9845 \pm 0.0004 \\ 0.9808 \pm 0.0009 \\ 0.9791 \pm 0.0017 \\ 0.9733 \pm 0.0047 \\ 0.9762 \pm 0.0060 \\ 1.0017 \pm 0.0142 \\ 0.9946 \pm 0.0278 \\ 0.7562 \pm 0.1200 \\ \hline \\ 0.8 < \eta < 1.5 \\ 0.9987 \pm 0.0012 \\ 1.0014 \pm 0.0004 \\ 1.0014 \pm 0.0004 \\ 1.0006 \pm 0.0002 \\ 1.0007 \pm 0.0003 \\ 0.9994 \pm 0.0006 \\ \hline \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9746 \pm 0.0003 \\ 0.9920 \pm 0.0001 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9968 \pm 0.0016 \\ 0.9950 \pm 0.0050 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9856 \pm 0.0016 \\ 0.9950 \pm 0.0000 \\ \hline \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9810 \pm 0.0012 \\ 0.9856 \pm 0.00014 \\ 0.9826 \pm 0.0014 \\ 0.9839 \pm 0.0015 \\ 0.9937 \pm 0.0084 \\ 0.9539 \pm 0.0015 \\ 0.9937 \pm 0.0084 \\ 0.9539 \pm 0.0115 \\ 0.9918 \pm 0.0343 \\ 0.9468 \pm 0.0671 \\ 0.5000 \pm 0.3227 \\ \hline \\ 1.5 < \eta < 2.1 \\ 1.0062 \pm 0.0012 \\ 1.0042 \pm 0.0004 \\ 1.0008 \pm 0.0002 \\ 1.0014 \pm 0.0004 \\ 1.0005 \pm 0.0007 \\ 1.0010 \pm 0.0022 \\ \hline \end{array}$
P _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200 200 - 300 300 - 10000 Scale Factor ID P _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200 200 - 300 300 - 10000 Scale Factor ISO P _T range [GeV]	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ 1.0000 \pm 0.0000 \\ \hline \\ \eta < 0.8 \\ 0.9801 \pm 0.0007 \\ 0.9819 \pm 0.0004 \\ 0.9836 \pm 0.0007 \\ 0.9819 \pm 0.0004 \\ 0.9836 \pm 0.0007 \\ 0.9806 \pm 0.0014 \\ 0.9709 \pm 0.0037 \\ 0.9713 \pm 0.0052 \\ 0.9907 \pm 0.0109 \\ 0.9378 \pm 0.0233 \\ 0.7328 \pm 0.0701 \\ \hline \\ \eta < 0.8 \\ \hline \\ 0.9971 \pm 0.0011 \\ 0.9987 \pm 0.0003 \\ 0.9994 \pm 0.0002 \\ 0.9995 \pm 0.0006 \\ 1.0002 \pm 0.0016 \\ 1.0000 \pm 0.0024 \\ \hline \end{array}$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9938 \pm 0.0015 \\ 0.9977 \pm 0.0023 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 0.8 < \eta < 1.5 \\ 0.9833 \pm 0.0009 \\ 0.9829 \pm 0.0005 \\ 0.9845 \pm 0.0004 \\ 0.9808 \pm 0.0009 \\ 0.9791 \pm 0.0017 \\ 0.9733 \pm 0.0047 \\ 0.9762 \pm 0.0060 \\ 1.0017 \pm 0.0142 \\ 0.9946 \pm 0.0278 \\ 0.7562 \pm 0.1200 \\ \hline \\ \hline \\ 0.8 < \eta < 1.5 \\ 0.9987 \pm 0.0012 \\ 1.0014 \pm 0.0004 \\ 1.0006 \pm 0.0002 \\ 1.0007 \pm 0.0003 \\ 0.9994 \pm 0.0006 \\ 1.0015 \pm 0.00017 \\ 1.0005 \pm 0.0021 \\ \hline \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9746 \pm 0.0003 \\ 0.9920 \pm 0.0001 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9943 \pm 0.0015 \\ 0.9968 \pm 0.0050 \\ 1.0000 \pm 0.0050 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9810 \pm 0.0012 \\ 0.9856 \pm 0.0007 \\ 0.9875 \pm 0.0006 \\ 0.9826 \pm 0.0014 \\ 0.9846 \pm 0.0012 \\ 0.9937 \pm 0.0084 \\ 0.9539 \pm 0.0015 \\ 0.9918 \pm 0.0343 \\ 0.9468 \pm 0.0671 \\ 0.5000 \pm 0.3227 \\ \hline \\ 1.5 < \eta < 2.1 \\ 1.0062 \pm 0.0012 \\ 1.0042 \pm 0.0004 \\ 1.0008 \pm 0.0002 \\ 1.0014 \pm 0.0004 \\ 1.0005 \pm 0.0007 \\ 1.0010 \pm 0.0022 \\ 1.0041 \pm 0.0002 \\ 1.0041 \pm 0.0028 \\ \hline \end{array}$
P _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200 200 - 300 300 - 10000 Scale Factor ID P _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200 200 - 300 300 - 10000 Scale Factor ISO P _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ \eta < 0.8 \\ \hline 0.9801 \pm 0.0007 \\ 0.9819 \pm 0.0004 \\ 0.9836 \pm 0.0003 \\ 0.9808 \pm 0.0007 \\ 0.9808 \pm 0.0007 \\ 0.9806 \pm 0.0014 \\ 0.9709 \pm 0.0037 \\ 0.9709 \pm 0.0109 \\ 0.9378 \pm 0.0233 \\ 0.7328 \pm 0.0701 \\ \hline \\ \eta < 0.8 \\ \hline 0.9971 \pm 0.0011 \\ 0.9987 \pm 0.0003 \\ 0.9995 \pm 0.0003 \\ 0.9995 \pm 0.0003 \\ 0.9995 \pm 0.0006 \\ 1.0002 \pm 0.0016 \\ 1.0002 \pm 0.0016 \\ 1.0000 \pm 0.0024 \\ 1.0068 \pm 0.0042 \\ \hline \end{array}$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9938 \pm 0.0011 \\ 0.9943 \pm 0.0015 \\ 0.9977 \pm 0.0023 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 0.8 < \eta < 1.5 \\ 0.9833 \pm 0.0009 \\ 0.9829 \pm 0.0005 \\ 0.9845 \pm 0.0004 \\ 0.9808 \pm 0.0009 \\ 0.9791 \pm 0.0017 \\ 0.9733 \pm 0.0047 \\ 0.9762 \pm 0.0060 \\ 1.0017 \pm 0.0142 \\ 0.9946 \pm 0.0278 \\ 0.7562 \pm 0.1200 \\ \hline \\ 0.8 < \eta < 1.5 \\ 0.9987 \pm 0.0012 \\ 1.0014 \pm 0.0004 \\ 1.0006 \pm 0.0002 \\ 1.0007 \pm 0.0003 \\ 0.9994 \pm 0.0006 \\ 1.0015 \pm 0.00017 \\ 1.0005 \pm 0.00021 \\ 1.0074 \pm 0.0049 \\ \hline \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9746 \pm 0.0003 \\ 0.9920 \pm 0.0001 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9968 \pm 0.0016 \\ 0.9950 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9810 \pm 0.0012 \\ 0.9856 \pm 0.0007 \\ 0.9856 \pm 0.0007 \\ 0.9875 \pm 0.0006 \\ 0.9826 \pm 0.0014 \\ 0.9846 \pm 0.0014 \\ 0.9846 \pm 0.0014 \\ 0.9937 \pm 0.0084 \\ 0.9539 \pm 0.0115 \\ 0.9918 \pm 0.0343 \\ 0.9468 \pm 0.0671 \\ 0.5000 \pm 0.3227 \\ \hline \\ 1.5 < \eta < 2.1 \\ 1.0062 \pm 0.0012 \\ 1.0042 \pm 0.0004 \\ 1.0008 \pm 0.0002 \\ 1.0014 \pm 0.0004 \\ 1.0005 \pm 0.0007 \\ 1.0010 \pm 0.0022 \\ 1.0041 \pm 0.0022 \\ 1.0041 \pm 0.0028 \\ 1.0000 \pm 0.0071 \\ \hline \end{array}$
P _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200 200 - 300 300 - 10000 Scale Factor ID P _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200 200 - 300 300 - 10000 Scale Factor ISO P _T range [GeV]	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ 1.0000 \pm 0.0000 \\ \hline \\ \eta < 0.8 \\ 0.9801 \pm 0.0007 \\ 0.9819 \pm 0.0004 \\ 0.9836 \pm 0.0007 \\ 0.9819 \pm 0.0004 \\ 0.9836 \pm 0.0007 \\ 0.9806 \pm 0.0014 \\ 0.9709 \pm 0.0037 \\ 0.9713 \pm 0.0052 \\ 0.9907 \pm 0.0109 \\ 0.9378 \pm 0.0233 \\ 0.7328 \pm 0.0701 \\ \hline \\ \eta < 0.8 \\ \hline \\ 0.9971 \pm 0.0011 \\ 0.9987 \pm 0.0003 \\ 0.9994 \pm 0.0002 \\ 0.9995 \pm 0.0006 \\ 1.0002 \pm 0.0016 \\ 1.0000 \pm 0.0024 \\ \hline \end{array}$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9938 \pm 0.0015 \\ 0.9977 \pm 0.0023 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 0.8 < \eta < 1.5 \\ 0.9833 \pm 0.0009 \\ 0.9829 \pm 0.0005 \\ 0.9845 \pm 0.0004 \\ 0.9808 \pm 0.0009 \\ 0.9791 \pm 0.0017 \\ 0.9733 \pm 0.0047 \\ 0.9762 \pm 0.0060 \\ 1.0017 \pm 0.0142 \\ 0.9946 \pm 0.0278 \\ 0.7562 \pm 0.1200 \\ \hline \\ \hline \\ 0.8 < \eta < 1.5 \\ 0.9987 \pm 0.0012 \\ 1.0014 \pm 0.0004 \\ 1.0006 \pm 0.0002 \\ 1.0007 \pm 0.0003 \\ 0.9994 \pm 0.0006 \\ 1.0015 \pm 0.00017 \\ 1.0005 \pm 0.0021 \\ \hline \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9746 \pm 0.0003 \\ 0.9920 \pm 0.0001 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9943 \pm 0.0015 \\ 0.9968 \pm 0.0050 \\ 1.0000 \pm 0.0050 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9810 \pm 0.0012 \\ 0.9856 \pm 0.0007 \\ 0.9875 \pm 0.0006 \\ 0.9826 \pm 0.0014 \\ 0.9846 \pm 0.0012 \\ 0.9937 \pm 0.0084 \\ 0.9539 \pm 0.0015 \\ 0.9918 \pm 0.0343 \\ 0.9468 \pm 0.0671 \\ 0.5000 \pm 0.3227 \\ \hline \\ 1.5 < \eta < 2.1 \\ 1.0062 \pm 0.0012 \\ 1.0042 \pm 0.0004 \\ 1.0008 \pm 0.0002 \\ 1.0014 \pm 0.0004 \\ 1.0005 \pm 0.0007 \\ 1.0010 \pm 0.0022 \\ 1.0041 \pm 0.0002 \\ 1.0041 \pm 0.0028 \\ \hline \end{array}$
P _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200 200 - 300 300 - 10000 Scale Factor ID P _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200 200 - 300 300 - 10000 Scale Factor ISO P _T range [GeV]	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ \eta < 0.8 \\ \hline 0.9801 \pm 0.0007 \\ 0.9819 \pm 0.0004 \\ 0.9836 \pm 0.0003 \\ 0.9808 \pm 0.0007 \\ 0.9806 \pm 0.0014 \\ 0.9709 \pm 0.0037 \\ 0.9713 \pm 0.0052 \\ 0.9907 \pm 0.0109 \\ 0.9378 \pm 0.0233 \\ 0.7328 \pm 0.0701 \\ \hline \\ \eta < 0.8 \\ \hline \\ 0.9971 \pm 0.0011 \\ 0.9987 \pm 0.0003 \\ 0.9995 \pm 0.0003 \\ 0.9995 \pm 0.0003 \\ 0.9995 \pm 0.0006 \\ 1.0002 \pm 0.0016 \\ 1.0002 \pm 0.0016 \\ 1.0002 \pm 0.0012 \\ 1.0080 \pm 0.0057 \\ \hline \end{array}$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9938 \pm 0.0015 \\ 0.9977 \pm 0.0023 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 0.8 < \eta < 1.5 \\ 0.9833 \pm 0.0009 \\ 0.9829 \pm 0.0005 \\ 0.9845 \pm 0.0004 \\ 0.9808 \pm 0.0009 \\ 0.9791 \pm 0.0017 \\ 0.9733 \pm 0.0047 \\ 0.9762 \pm 0.0060 \\ 1.0017 \pm 0.0142 \\ 0.9946 \pm 0.0278 \\ 0.7562 \pm 0.1200 \\ \hline \\ \hline \\ 0.8 < \eta < 1.5 \\ 0.9987 \pm 0.0012 \\ 1.0014 \pm 0.0004 \\ 1.0006 \pm 0.0002 \\ 1.0007 \pm 0.0003 \\ 0.9994 \pm 0.0006 \\ 1.0015 \pm 0.00017 \\ 1.0005 \pm 0.0001 \\ 1.00074 \pm 0.0004 \\ 1.0000 \pm 0.0000 \\ \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9746 \pm 0.0003 \\ 0.9920 \pm 0.0001 \\ 0.9952 \pm 0.0005 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9968 \pm 0.0016 \\ 0.9950 \pm 0.0050 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9810 \pm 0.0012 \\ 0.9856 \pm 0.0014 \\ 0.9856 \pm 0.0007 \\ 0.9875 \pm 0.0006 \\ 0.9826 \pm 0.0014 \\ 0.9846 \pm 0.0029 \\ 0.9937 \pm 0.0084 \\ 0.9539 \pm 0.0115 \\ 0.9918 \pm 0.0343 \\ 0.9468 \pm 0.0671 \\ 0.5000 \pm 0.3227 \\ \hline \\ \\ 1.5 < \eta < 2.1 \\ 1.0062 \pm 0.0012 \\ 1.0042 \pm 0.0004 \\ 1.0008 \pm 0.0002 \\ 1.0014 \pm 0.0004 \\ 1.0005 \pm 0.0007 \\ 1.0010 \pm 0.0022 \\ 1.0041 \pm 0.0028 \\ 1.0000 \pm 0.0071 \\ 1.0172 \pm 0.0174 \\ \hline \end{array}$
P _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200 200 - 300 300 - 10000 Scale Factor ID P _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200 200 - 300 300 - 10000 Scale Factor ISO P _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200	$\begin{array}{c} 0.8943 \pm 0.0007 \\ 0.9598 \pm 0.0002 \\ 0.9870 \pm 0.0001 \\ 0.9913 \pm 0.0002 \\ 0.9921 \pm 0.0004 \\ 0.9920 \pm 0.0011 \\ 0.9900 \pm 0.0017 \\ 0.9972 \pm 0.0020 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ \eta < 0.8 \\ \hline 0.9801 \pm 0.0007 \\ 0.9819 \pm 0.0004 \\ 0.9836 \pm 0.0003 \\ 0.9808 \pm 0.0007 \\ 0.9808 \pm 0.0007 \\ 0.9806 \pm 0.0014 \\ 0.9709 \pm 0.0037 \\ 0.9709 \pm 0.0109 \\ 0.9378 \pm 0.0233 \\ 0.7328 \pm 0.0701 \\ \hline \\ \eta < 0.8 \\ \hline 0.9971 \pm 0.0011 \\ 0.9987 \pm 0.0003 \\ 0.9995 \pm 0.0003 \\ 0.9995 \pm 0.0003 \\ 0.9995 \pm 0.0006 \\ 1.0002 \pm 0.0016 \\ 1.0002 \pm 0.0016 \\ 1.0000 \pm 0.0024 \\ 1.0068 \pm 0.0042 \\ \hline \end{array}$	$\begin{array}{c} 0.9144 \pm 0.0008 \\ 0.9646 \pm 0.0003 \\ 0.9903 \pm 0.0001 \\ 0.9935 \pm 0.0002 \\ 0.9931 \pm 0.0004 \\ 0.9938 \pm 0.0011 \\ 0.9938 \pm 0.0011 \\ 0.9943 \pm 0.0015 \\ 0.9977 \pm 0.0023 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 0.8 < \eta < 1.5 \\ 0.9833 \pm 0.0009 \\ 0.9829 \pm 0.0005 \\ 0.9845 \pm 0.0004 \\ 0.9808 \pm 0.0009 \\ 0.9791 \pm 0.0017 \\ 0.9733 \pm 0.0047 \\ 0.9762 \pm 0.0060 \\ 1.0017 \pm 0.0142 \\ 0.9946 \pm 0.0278 \\ 0.7562 \pm 0.1200 \\ \hline \\ 0.8 < \eta < 1.5 \\ 0.9987 \pm 0.0012 \\ 1.0014 \pm 0.0004 \\ 1.0006 \pm 0.0002 \\ 1.0007 \pm 0.0003 \\ 0.9994 \pm 0.0006 \\ 1.0015 \pm 0.00017 \\ 1.0005 \pm 0.00021 \\ 1.0074 \pm 0.0049 \\ \hline \end{array}$	$\begin{array}{c} 0.9359 \pm 0.0008 \\ 0.9746 \pm 0.0003 \\ 0.9746 \pm 0.0003 \\ 0.9920 \pm 0.0001 \\ 0.9952 \pm 0.0005 \\ 0.9943 \pm 0.0015 \\ 0.9968 \pm 0.0016 \\ 0.9950 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9810 \pm 0.0012 \\ 0.9856 \pm 0.0007 \\ 0.9856 \pm 0.0007 \\ 0.9875 \pm 0.0006 \\ 0.9826 \pm 0.0014 \\ 0.9846 \pm 0.0014 \\ 0.9846 \pm 0.0014 \\ 0.9937 \pm 0.0084 \\ 0.9539 \pm 0.0115 \\ 0.9918 \pm 0.0343 \\ 0.9468 \pm 0.0671 \\ 0.5000 \pm 0.3227 \\ \hline \\ 1.5 < \eta < 2.1 \\ 1.0062 \pm 0.0012 \\ 1.0042 \pm 0.0004 \\ 1.0008 \pm 0.0002 \\ 1.0014 \pm 0.0004 \\ 1.0005 \pm 0.0007 \\ 1.0010 \pm 0.0022 \\ 1.0041 \pm 0.0022 \\ 1.0041 \pm 0.0028 \\ 1.0000 \pm 0.0071 \\ \hline \end{array}$

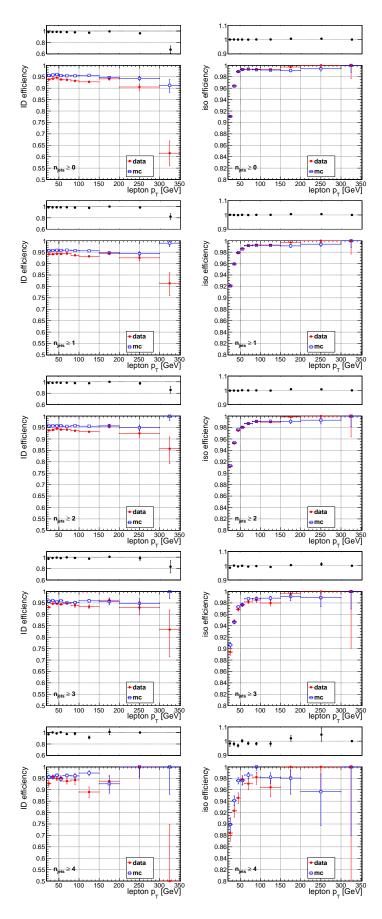


Figure 2: Comparison of the muon identification and isolation efficiencies in data and MC for various jet multiplicity requirements.

Table 9: Summary of the data and MC electron identification and isolation efficiencies measured with tag-and-probe studies. $_$

MC ID		
p_{T} range [GeV]	$ \eta < 1.5$	$1.5 < \eta < 2.1$
20 - 30	0.8156 ± 0.0008	0.6565 ± 0.0019
30 - 40	0.8670 ± 0.0004	0.7450 ± 0.0010
40 - 50	0.8922 ± 0.0003	0.7847 ± 0.0008
50 - 60		0.7956 ± 0.0018
	0.9023 ± 0.0006	
60 - 80	0.9097 ± 0.0011	0.8166 ± 0.0034
80 - 100	0.9203 ± 0.0028	0.8196 ± 0.0090
100 - 150	0.9162 ± 0.0037	0.8378 ± 0.0117
150 - 200	0.9106 ± 0.0087	0.8111 ± 0.0292
200 - 300	0.9304 ± 0.0119	0.9153 ± 0.0363
300 - 10000	0.8684 ± 0.0388	0.8000 ± 0.1789
	0.8084 ± 0.0388	0.8000 ± 0.1789
MC ISO		
p_{T} range [GeV]	$ \eta < 1.5$	$1.5 < \eta < 2.1$
20 - 30	0.9245 ± 0.0006	0.9466 ± 0.0011
30 - 40	0.9682 ± 0.0002	0.9741 ± 0.0004
40 - 50	0.9876 ± 0.0002	0.9883 ± 0.0002
50 - 60	0.9909 ± 0.0002	0.9912 ± 0.0005
60 - 80	0.9916 ± 0.0004	0.9930 ± 0.0008
80 - 100	0.9915 ± 0.0010	0.9908 ± 0.0025
100 - 150	0.9929 ± 0.0012	0.9894 ± 0.0035
150 - 200	0.9919 ± 0.0029	0.9932 ± 0.0068
200 - 300	0.9953 ± 0.0033	1.0000 ± 0.0000
300 - 10000	1.0000 ± 0.0000	1.0000 ± 0.0000
DATA ID		
$p_{\rm T}$ range [GeV]	$ \eta < 1.5$	$1.5 < \eta < 2.1$
$\frac{p_{1} \text{ range [GeV]}}{20 - 30}$	0.8145 ± 0.0008	0.6528 ± 0.0018
30 - 40	0.8676 ± 0.0004	0.7462 ± 0.0010
40 - 50	0.8955 ± 0.0003	0.7922 ± 0.0008
50 - 60	0.9049 ± 0.0006	0.8072 ± 0.0018
60 - 80	0.9110 ± 0.0011	0.8212 ± 0.0035
80 - 100	0.9156 ± 0.0028	0.8358 ± 0.0091
100 - 150	0.9257 ± 0.0036	0.8507 ± 0.0031
150 - 200	0.9186 ± 0.0084	0.8929 ± 0.0292
200 - 300	0.9106 ± 0.0149	0.7576 ± 0.0746
300 - 10000	0.9400 ± 0.0336	1.0000 ± 0.0000
DATA ISO		
$p_{\rm T}$ range [GeV]	1 5	$1.5 < \eta < 2.1$
	$ \eta < 1.5$	0.9419 ± 0.0011
20 - 30	0.9201 ± 0.0006	
30 - 40	0.9667 ± 0.0002	0.9734 ± 0.0004
40 - 50	0.9872 ± 0.0001	0.9892 ± 0.0002
50 - 60	0.9904 ± 0.0002	0.9922 ± 0.0004
60 - 80	0.9923 ± 0.0004	0.9916 ± 0.0009
80 - 100	0.9914 ± 0.0010	0.9921 ± 0.0024
00 - 100	0.0014 1 0.0010	0.0024
100 150	0.0045 0.0011	1 0000 0 0000
100 - 150	0.9945 ± 0.0011	1.0000 ± 0.0000
150 - 200	0.9908 ± 0.0031	1.0000 ± 0.0000
150 - 200 200 - 300	$\begin{array}{c} 0.9908 \pm 0.0031 \\ 0.9941 \pm 0.0042 \end{array}$	$\begin{array}{c} 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \end{array}$
150 - 200	0.9908 ± 0.0031	1.0000 ± 0.0000
150 - 200 200 - 300 300 - 10000	$\begin{array}{c} 0.9908 \pm 0.0031 \\ 0.9941 \pm 0.0042 \end{array}$	$\begin{array}{c} 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \end{array}$
150 - 200 200 - 300 300 - 10000 Scale Factor ID	$ \begin{array}{c} 0.9908 \pm 0.0031 \\ 0.9941 \pm 0.0042 \\ 0.9792 \pm 0.0206 \end{array} $	$\begin{array}{c} 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \end{array}$
$ \begin{array}{r} 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline Scale Factor ID \\ p_T range [GeV] $	$\begin{array}{c} 0.9908 \pm 0.0031 \\ 0.9941 \pm 0.0042 \\ 0.9792 \pm 0.0206 \\ \\ \eta < 1.5 \end{array}$	$ \begin{array}{r} 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \end{array} $ $ 1.5 < \eta < 2.1 $
$ \begin{array}{r} 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline Scale Factor ID \\ p_T range [GeV] \\ 20 - 30 \end{array} $	$\begin{array}{c} 0.9908 \pm 0.0031 \\ 0.9941 \pm 0.0042 \\ 0.9792 \pm 0.0206 \\ \hline \eta < 1.5 \\ 0.9987 \pm 0.0014 \end{array}$	$\begin{array}{c} 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \end{array}$ $\begin{array}{c} 1.5 < \eta < 2.1 \\ 0.9944 \pm 0.0040 \\ \end{array}$
$ \begin{array}{r} 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline Scale Factor ID \\ p_T range [GeV] \\ 20 - 30 \\ 30 - 40 \end{array} $	$\begin{array}{c} 0.9908 \pm 0.0031 \\ 0.9941 \pm 0.0042 \\ 0.9792 \pm 0.0206 \\ \\ \eta < 1.5 \\ 0.9987 \pm 0.0014 \\ 1.0007 \pm 0.0006 \end{array}$	$\begin{array}{c} 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9944 \pm 0.0040 \\ 1.0015 \pm 0.0019 \\ \end{array}$
$ \begin{array}{r} 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline Scale Factor ID \\ p_T range [GeV] \\ 20 - 30 \\ 30 - 40 \\ 40 - 50 \end{array} $	$\begin{array}{c} 0.9908 \pm 0.0031 \\ 0.9941 \pm 0.0042 \\ 0.9792 \pm 0.0206 \\ \\ \hline \eta < 1.5 \\ 0.9987 \pm 0.0014 \\ 1.0007 \pm 0.0006 \\ 1.0036 \pm 0.0005 \\ \end{array}$	$\begin{array}{c} 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9944 \pm 0.0040 \\ 1.0015 \pm 0.0019 \\ 1.0096 \pm 0.0015 \\ \end{array}$
$ \begin{array}{r} 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline Scale Factor ID \\ p_T range [GeV] \\ 20 - 30 \\ 30 - 40 \\ 40 - 50 \end{array} $	$\begin{array}{c} 0.9908 \pm 0.0031 \\ 0.9941 \pm 0.0042 \\ 0.9792 \pm 0.0206 \\ \\ \hline \eta < 1.5 \\ 0.9987 \pm 0.0014 \\ 1.0007 \pm 0.0006 \\ 1.0036 \pm 0.0005 \\ \end{array}$	$\begin{array}{c} 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9944 \pm 0.0040 \\ 1.0015 \pm 0.0019 \\ 1.0096 \pm 0.0015 \\ \end{array}$
$ \begin{array}{r} 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline Scale Factor ID \\ p_T range [GeV] \\ 20 - 30 \\ 30 - 40 \end{array} $	$\begin{array}{c} 0.9908 \pm 0.0031 \\ 0.9941 \pm 0.0042 \\ 0.9792 \pm 0.0206 \\ \\ \eta < 1.5 \\ 0.9987 \pm 0.0014 \\ 1.0007 \pm 0.0006 \end{array}$	$\begin{array}{c} 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9944 \pm 0.0040 \\ 1.0015 \pm 0.0019 \\ \end{array}$
$\begin{array}{c} 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ Scale Factor ID \\ p_T range [GeV] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ \end{array}$	$\begin{array}{c} 0.9908 \pm 0.0031 \\ 0.9941 \pm 0.0042 \\ 0.9792 \pm 0.0206 \\ \hline \\ \eta < 1.5 \\ 0.9987 \pm 0.0014 \\ 1.0007 \pm 0.0006 \\ 1.0036 \pm 0.0005 \\ 1.0029 \pm 0.0010 \\ 1.0014 \pm 0.0018 \\ \end{array}$	$\begin{array}{c} 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9944 \pm 0.0040 \\ 1.0015 \pm 0.0019 \\ 1.0096 \pm 0.0015 \\ 1.0146 \pm 0.0031 \\ 1.0057 \pm 0.0060 \\ \end{array}$
$ \begin{array}{r} 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline Scale Factor ID \\ p_T range [GeV] \\ 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ \end{array} $	$\begin{array}{c} 0.9908 \pm 0.0031 \\ 0.9941 \pm 0.0042 \\ 0.9792 \pm 0.0206 \\ \hline \\ \eta < 1.5 \\ 0.9987 \pm 0.0014 \\ 1.0007 \pm 0.0006 \\ 1.0036 \pm 0.0005 \\ 1.0029 \pm 0.0010 \\ 1.0014 \pm 0.0018 \\ 0.9949 \pm 0.0043 \\ \hline \end{array}$	$\begin{array}{c} 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9944 \pm 0.0040 \\ 1.0015 \pm 0.0019 \\ 1.0096 \pm 0.0015 \\ 1.0146 \pm 0.0031 \\ 1.0057 \pm 0.0060 \\ 1.0197 \pm 0.0158 \\ \end{array}$
$ \begin{array}{r} 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline Scale Factor ID \\ p_T range [GeV] \\ 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ \end{array} $	$\begin{array}{c} 0.9908 \pm 0.0031 \\ 0.9941 \pm 0.0042 \\ 0.9792 \pm 0.0206 \\ \\ \hline \eta < 1.5 \\ 0.9987 \pm 0.0014 \\ 1.0007 \pm 0.0006 \\ 1.0036 \pm 0.0005 \\ 1.0029 \pm 0.0010 \\ 1.0014 \pm 0.0018 \\ 0.9949 \pm 0.0043 \\ 1.0104 \pm 0.0057 \\ \end{array}$	$\begin{array}{c} 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9944 \pm 0.0040 \\ 1.0015 \pm 0.0019 \\ 1.0096 \pm 0.0015 \\ 1.0146 \pm 0.0031 \\ 1.0057 \pm 0.0060 \\ 1.0197 \pm 0.0158 \\ 1.0154 \pm 0.0198 \\ \end{array}$
$\begin{array}{c} 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ Scale Factor ID \\ p_T range [GeV] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ \hline \end{array}$	$\begin{array}{c} 0.9908 \pm 0.0031 \\ 0.9941 \pm 0.0042 \\ 0.9792 \pm 0.0206 \\ \\ \hline \eta < 1.5 \\ 0.9987 \pm 0.0014 \\ 1.0007 \pm 0.0006 \\ 1.0036 \pm 0.0005 \\ 1.0029 \pm 0.0010 \\ 1.0014 \pm 0.0018 \\ 0.9949 \pm 0.0043 \\ 1.0104 \pm 0.0057 \\ 1.0087 \pm 0.0134 \\ \end{array}$	$\begin{array}{c} 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9944 \pm 0.0040 \\ 1.0015 \pm 0.0019 \\ 1.0096 \pm 0.0015 \\ 1.0146 \pm 0.0031 \\ 1.0057 \pm 0.0060 \\ 1.0197 \pm 0.0158 \\ 1.0154 \pm 0.0198 \\ 1.1008 \pm 0.0535 \\ \hline \end{array}$
$\begin{array}{c} 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ Scale Factor ID \\ p_T \ range \ [GeV] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ 200 - 300 \\ \hline \end{array}$	$\begin{array}{c} 0.9908 \pm 0.0031 \\ 0.9941 \pm 0.0042 \\ 0.9792 \pm 0.0206 \\ \hline \\ \eta < 1.5 \\ 0.9987 \pm 0.0014 \\ 1.0007 \pm 0.0006 \\ 1.0036 \pm 0.0005 \\ 1.0029 \pm 0.0010 \\ 1.0014 \pm 0.0018 \\ 0.9949 \pm 0.0043 \\ 1.0104 \pm 0.0057 \\ 1.0087 \pm 0.0134 \\ 0.9786 \pm 0.0203 \\ \end{array}$	$\begin{array}{c} 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9944 \pm 0.0040 \\ 1.0015 \pm 0.0019 \\ 1.0096 \pm 0.0015 \\ 1.0146 \pm 0.0031 \\ 1.0057 \pm 0.0060 \\ 1.0197 \pm 0.0158 \\ 1.0154 \pm 0.0198 \\ 1.1008 \pm 0.0535 \\ 0.8277 \pm 0.0879 \\ \end{array}$
$\begin{array}{c} 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ Scale Factor ID \\ p_T range [GeV] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ \hline \end{array}$	$\begin{array}{c} 0.9908 \pm 0.0031 \\ 0.9941 \pm 0.0042 \\ 0.9792 \pm 0.0206 \\ \\ \hline \eta < 1.5 \\ 0.9987 \pm 0.0014 \\ 1.0007 \pm 0.0006 \\ 1.0036 \pm 0.0005 \\ 1.0029 \pm 0.0010 \\ 1.0014 \pm 0.0018 \\ 0.9949 \pm 0.0043 \\ 1.0104 \pm 0.0057 \\ 1.0087 \pm 0.0134 \\ \end{array}$	$\begin{array}{c} 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9944 \pm 0.0040 \\ 1.0015 \pm 0.0019 \\ 1.0096 \pm 0.0015 \\ 1.0146 \pm 0.0031 \\ 1.0057 \pm 0.0060 \\ 1.0197 \pm 0.0158 \\ 1.0154 \pm 0.0198 \\ 1.1008 \pm 0.0535 \\ \hline \end{array}$
150 - 200 200 - 300 300 - 10000 Scale Factor ID p _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200 200 - 300 300 - 10000	$\begin{array}{c} 0.9908 \pm 0.0031 \\ 0.9941 \pm 0.0042 \\ 0.9792 \pm 0.0206 \\ \hline \\ \eta < 1.5 \\ 0.9987 \pm 0.0014 \\ 1.0007 \pm 0.0006 \\ 1.0036 \pm 0.0005 \\ 1.0029 \pm 0.0010 \\ 1.0014 \pm 0.0018 \\ 0.9949 \pm 0.0043 \\ 1.0104 \pm 0.0057 \\ 1.0087 \pm 0.0134 \\ 0.9786 \pm 0.0203 \\ \end{array}$	$\begin{array}{c} 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9944 \pm 0.0040 \\ 1.0015 \pm 0.0019 \\ 1.0096 \pm 0.0015 \\ 1.0146 \pm 0.0031 \\ 1.0057 \pm 0.0060 \\ 1.0197 \pm 0.0158 \\ 1.0154 \pm 0.0198 \\ 1.1008 \pm 0.0535 \\ 0.8277 \pm 0.0879 \\ \end{array}$
$ \begin{array}{c} 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ Scale Factor ID \\ p_T range [GeV] \\ 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ Scale Factor ISO \\ \hline \end{tabular} $	$\begin{array}{c} 0.9908 \pm 0.0031 \\ 0.9941 \pm 0.0042 \\ 0.9792 \pm 0.0206 \\ \hline \\ \eta < 1.5 \\ 0.9987 \pm 0.0014 \\ 1.0007 \pm 0.0006 \\ 1.0036 \pm 0.0005 \\ 1.0029 \pm 0.0010 \\ 1.0014 \pm 0.0018 \\ 0.9949 \pm 0.0043 \\ 1.0104 \pm 0.0057 \\ 1.0087 \pm 0.0134 \\ 0.9786 \pm 0.0203 \\ 1.0824 \pm 0.0619 \\ \hline \end{array}$	$\begin{array}{c} 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9944 \pm 0.0040 \\ 1.0015 \pm 0.0019 \\ 1.0096 \pm 0.0015 \\ 1.0146 \pm 0.0031 \\ 1.0057 \pm 0.0060 \\ 1.0197 \pm 0.0158 \\ 1.0154 \pm 0.0198 \\ 1.1008 \pm 0.0535 \\ 0.8277 \pm 0.0879 \\ 1.2500 \pm 0.2795 \\ \hline \end{array}$
$ \begin{array}{c} 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ Scale Factor ID \\ p_T range [GeV] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ Scale Factor ISO \\ p_T range [GeV] \\ \hline \end{array} $	$\begin{array}{c} 0.9908 \pm 0.0031 \\ 0.9941 \pm 0.0042 \\ 0.9792 \pm 0.0206 \\ \hline \\ \eta < 1.5 \\ 0.9987 \pm 0.0014 \\ 1.0007 \pm 0.0006 \\ 1.0036 \pm 0.0005 \\ 1.0029 \pm 0.0010 \\ 1.0014 \pm 0.0018 \\ 0.9949 \pm 0.0043 \\ 1.0104 \pm 0.0057 \\ 1.0087 \pm 0.0134 \\ 0.9786 \pm 0.0203 \\ 1.0824 \pm 0.0619 \\ \hline \\ \eta < 1.5 \\ \hline \end{array}$	$\begin{array}{c} 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9944 \pm 0.0040 \\ 1.0015 \pm 0.0019 \\ 1.0096 \pm 0.0015 \\ 1.0146 \pm 0.0031 \\ 1.0057 \pm 0.0060 \\ 1.0197 \pm 0.0158 \\ 1.0154 \pm 0.0198 \\ 1.1008 \pm 0.0535 \\ 0.8277 \pm 0.0879 \\ 1.2500 \pm 0.2795 \\ \hline \\ 1.5 < \eta < 2.1 \\ \hline \end{array}$
$ \begin{array}{c} 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ Scale Factor ID \\ p_T range [GeV] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ Scale Factor ISO \\ p_T range [GeV] \\ \hline 20 - 30 \\ \hline \\ \hline \\ 20 - 30 \\ \hline \end{array} $	$\begin{array}{c} 0.9908 \pm 0.0031 \\ 0.9941 \pm 0.0042 \\ 0.9792 \pm 0.0206 \\ \hline \\ \eta < 1.5 \\ 0.9987 \pm 0.0014 \\ 1.0007 \pm 0.0006 \\ 1.0036 \pm 0.0005 \\ 1.0029 \pm 0.0010 \\ 1.0014 \pm 0.0018 \\ 0.9949 \pm 0.0043 \\ 1.0104 \pm 0.0057 \\ 1.0087 \pm 0.0134 \\ 0.9786 \pm 0.0203 \\ 1.0824 \pm 0.0619 \\ \hline \\ \eta < 1.5 \\ 0.9952 \pm 0.0009 \\ \hline \end{array}$	$\begin{array}{c} 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9944 \pm 0.0040 \\ 1.0015 \pm 0.0019 \\ 1.0096 \pm 0.0015 \\ 1.0146 \pm 0.0031 \\ 1.0057 \pm 0.0060 \\ 1.0197 \pm 0.0158 \\ 1.0154 \pm 0.0198 \\ 1.1008 \pm 0.0535 \\ 0.8277 \pm 0.0879 \\ 1.2500 \pm 0.2795 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9950 \pm 0.0016 \\ \hline \end{array}$
$ \begin{array}{c} 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ Scale Factor ID \\ p_T range [GeV] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ Scale Factor ISO \\ p_T range [GeV] \\ \hline 20 - 30 \\ 30 - 40 \\ \hline \end{array} $	$\begin{array}{c} 0.9908 \pm 0.0031 \\ 0.9941 \pm 0.0042 \\ 0.9792 \pm 0.0206 \\ \\ \hline \eta < 1.5 \\ 0.9987 \pm 0.0014 \\ 1.0007 \pm 0.0006 \\ 1.0036 \pm 0.0005 \\ 1.0029 \pm 0.0010 \\ 1.0014 \pm 0.0018 \\ 0.9949 \pm 0.0043 \\ 1.0104 \pm 0.0057 \\ 1.0087 \pm 0.0134 \\ 0.9786 \pm 0.0203 \\ 1.0824 \pm 0.0619 \\ \hline \eta < 1.5 \\ 0.9952 \pm 0.0009 \\ 0.9984 \pm 0.0003 \\ \hline \end{array}$	$\begin{array}{c} 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9944 \pm 0.0040 \\ 1.0015 \pm 0.0019 \\ 1.0096 \pm 0.0015 \\ 1.0146 \pm 0.0031 \\ 1.0057 \pm 0.0060 \\ 1.0197 \pm 0.0158 \\ 1.0154 \pm 0.0198 \\ 1.1008 \pm 0.0535 \\ 0.8277 \pm 0.0879 \\ 1.2500 \pm 0.2795 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9950 \pm 0.0016 \\ 0.9992 \pm 0.0006 \\ \hline \end{array}$
$ \begin{array}{c} 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ Scale Factor ID \\ p_T range [GeV] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ Scale Factor ISO \\ p_T range [GeV] \\ \hline 20 - 30 \\ \hline \\ \hline \\ 20 - 30 \\ \hline \end{array} $	$\begin{array}{c} 0.9908 \pm 0.0031 \\ 0.9941 \pm 0.0042 \\ 0.9792 \pm 0.0206 \\ \hline \\ \eta < 1.5 \\ 0.9987 \pm 0.0014 \\ 1.0007 \pm 0.0006 \\ 1.0036 \pm 0.0005 \\ 1.0029 \pm 0.0010 \\ 1.0014 \pm 0.0018 \\ 0.9949 \pm 0.0043 \\ 1.0104 \pm 0.0057 \\ 1.0087 \pm 0.0134 \\ 0.9786 \pm 0.0203 \\ 1.0824 \pm 0.0619 \\ \hline \\ \eta < 1.5 \\ 0.9952 \pm 0.0009 \\ \hline \end{array}$	$\begin{array}{c} 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9944 \pm 0.0040 \\ 1.0015 \pm 0.0019 \\ 1.0096 \pm 0.0015 \\ 1.0146 \pm 0.0031 \\ 1.0057 \pm 0.0060 \\ 1.0197 \pm 0.0158 \\ 1.0154 \pm 0.0198 \\ 1.1008 \pm 0.0535 \\ 0.8277 \pm 0.0879 \\ 1.2500 \pm 0.2795 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9950 \pm 0.0016 \\ \hline \end{array}$
$ \begin{array}{c} 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ Scale Factor ID \\ p_T range [GeV] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ Scale Factor ISO \\ p_T range [GeV] \\ \hline 20 - 30 \\ 30 - 40 \\ \hline \end{array} $	$\begin{array}{c} 0.9908 \pm 0.0031 \\ 0.9941 \pm 0.0042 \\ 0.9792 \pm 0.0206 \\ \hline \\ \eta < 1.5 \\ 0.9987 \pm 0.0014 \\ 1.0007 \pm 0.0006 \\ 1.0036 \pm 0.0005 \\ 1.0029 \pm 0.0010 \\ 1.0014 \pm 0.0018 \\ 0.9949 \pm 0.0043 \\ 1.0104 \pm 0.0057 \\ 1.0087 \pm 0.0134 \\ 0.9786 \pm 0.0203 \\ 1.0824 \pm 0.0619 \\ \hline \\ \eta < 1.5 \\ 0.9952 \pm 0.0009 \\ 0.9984 \pm 0.0003 \\ \hline \end{array}$	$\begin{array}{c} 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9944 \pm 0.0040 \\ 1.0015 \pm 0.0019 \\ 1.0096 \pm 0.0015 \\ 1.0146 \pm 0.0031 \\ 1.0057 \pm 0.0060 \\ 1.0197 \pm 0.0158 \\ 1.0154 \pm 0.0198 \\ 1.1008 \pm 0.0535 \\ 0.8277 \pm 0.0879 \\ 1.2500 \pm 0.2795 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9950 \pm 0.0016 \\ 0.9992 \pm 0.0006 \\ \hline \end{array}$
$\begin{array}{c} 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ Scale Factor ID \\ p_T range [GeV] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ Scale Factor ISO \\ p_T range [GeV] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ \hline \end{array}$	$\begin{array}{c} 0.9908 \pm 0.0031 \\ 0.9941 \pm 0.0042 \\ 0.9792 \pm 0.0206 \\ \hline \\ \eta < 1.5 \\ 0.9987 \pm 0.0014 \\ 1.0007 \pm 0.0006 \\ 1.0029 \pm 0.0010 \\ 1.0014 \pm 0.0018 \\ 0.9949 \pm 0.0043 \\ 1.0104 \pm 0.0057 \\ 1.0087 \pm 0.0134 \\ 0.9786 \pm 0.0033 \\ 1.0824 \pm 0.0619 \\ \hline \\ \eta < 1.5 \\ 0.9952 \pm 0.0009 \\ 0.9984 \pm 0.0003 \\ 0.9996 \pm 0.0002 \\ 0.9995 \pm 0.0003 \\ \hline \end{array}$	$\begin{array}{c} 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9944 \pm 0.0040 \\ 1.0015 \pm 0.0019 \\ 1.0096 \pm 0.0015 \\ 1.0146 \pm 0.0031 \\ 1.0057 \pm 0.0060 \\ 1.0197 \pm 0.0158 \\ 1.0154 \pm 0.0198 \\ 1.1008 \pm 0.0535 \\ 0.8277 \pm 0.0879 \\ 1.2500 \pm 0.2795 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9950 \pm 0.0016 \\ 0.9992 \pm 0.0006 \\ 1.0009 \pm 0.0006 \\ 1.0009 \pm 0.0006 \\ \end{array}$
150 - 200 200 - 300 300 - 10000 Scale Factor ID p _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200 200 - 300 300 - 10000 Scale Factor ISO p _T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80	$\begin{array}{c} 0.9908 \pm 0.0031 \\ 0.9941 \pm 0.0042 \\ 0.9792 \pm 0.0206 \\ \hline \\ \eta < 1.5 \\ 0.9987 \pm 0.0014 \\ 1.0007 \pm 0.0006 \\ 1.0036 \pm 0.0005 \\ 1.0029 \pm 0.0010 \\ 1.0014 \pm 0.0018 \\ 0.9949 \pm 0.0043 \\ 1.0104 \pm 0.0057 \\ 1.0087 \pm 0.0134 \\ 0.9786 \pm 0.0203 \\ 1.0824 \pm 0.0619 \\ \hline \\ \eta < 1.5 \\ 0.9952 \pm 0.0009 \\ 0.9984 \pm 0.0003 \\ 0.9996 \pm 0.0002 \\ 0.9995 \pm 0.0002 \\ 0.9995 \pm 0.0003 \\ 1.0006 \pm 0.0005 \\ \hline \end{array}$	$\begin{array}{c} 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9944 \pm 0.0040 \\ 1.0015 \pm 0.0019 \\ 1.0096 \pm 0.0015 \\ 1.0146 \pm 0.0031 \\ 1.0057 \pm 0.0060 \\ 1.0197 \pm 0.0158 \\ 1.0154 \pm 0.0198 \\ 1.1008 \pm 0.0535 \\ 0.8277 \pm 0.0879 \\ 1.2500 \pm 0.2795 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9950 \pm 0.0016 \\ 0.9992 \pm 0.0006 \\ 1.0009 \pm 0.0003 \\ 1.0009 \pm 0.0006 \\ 0.9985 \pm 0.0012 \\ \hline \end{array}$
$ \begin{array}{c} 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ Scale Factor ID \\ p_T range [GeV] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ Scale Factor ISO \\ p_T range [GeV] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ \hline \end{array} $	$\begin{array}{c} 0.9908 \pm 0.0031 \\ 0.9941 \pm 0.0042 \\ 0.9792 \pm 0.0206 \\ \hline \\ \eta < 1.5 \\ 0.9987 \pm 0.0014 \\ 1.0007 \pm 0.0006 \\ 1.0036 \pm 0.0005 \\ 1.0029 \pm 0.0010 \\ 1.0014 \pm 0.0018 \\ 0.9949 \pm 0.0043 \\ 1.0104 \pm 0.0057 \\ 1.0087 \pm 0.0134 \\ 0.9786 \pm 0.0203 \\ 1.0824 \pm 0.0619 \\ \hline \\ \eta < 1.5 \\ 0.9952 \pm 0.0009 \\ 0.9984 \pm 0.0003 \\ 0.9995 \pm 0.0003 \\ 1.0006 \pm 0.0005 \\ 0.9999 \pm 0.0014 \\ \hline \end{array}$	$\begin{array}{c} 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9944 \pm 0.0040 \\ 1.0015 \pm 0.0019 \\ 1.0096 \pm 0.0015 \\ 1.0146 \pm 0.0031 \\ 1.0057 \pm 0.0060 \\ 1.0197 \pm 0.0158 \\ 1.0154 \pm 0.0198 \\ 1.1008 \pm 0.0535 \\ 0.8277 \pm 0.0879 \\ 1.2500 \pm 0.2795 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9950 \pm 0.0016 \\ 0.9992 \pm 0.0006 \\ 1.0009 \pm 0.0006 \\ 1.0009 \pm 0.0006 \\ 0.9985 \pm 0.0012 \\ 1.0013 \pm 0.0035 \\ \hline \end{array}$
150 - 200 200 - 300 300 - 10000 Scale Factor ID p_T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150 150 - 200 200 - 300 300 - 10000 Scale Factor ISO p_T range [GeV] 20 - 30 30 - 40 40 - 50 50 - 60 60 - 80 80 - 100 100 - 150	$\begin{array}{c} 0.9908 \pm 0.0031 \\ 0.9941 \pm 0.0042 \\ 0.9792 \pm 0.0206 \\ \hline \\ \eta < 1.5 \\ 0.9987 \pm 0.0014 \\ 1.0007 \pm 0.0006 \\ 1.0036 \pm 0.0005 \\ 1.0029 \pm 0.0010 \\ 1.0014 \pm 0.0018 \\ 0.9949 \pm 0.0043 \\ 1.0104 \pm 0.0057 \\ 1.0087 \pm 0.0134 \\ 0.9786 \pm 0.0203 \\ 1.0824 \pm 0.0619 \\ \hline \\ \eta < 1.5 \\ 0.9952 \pm 0.0009 \\ 0.9984 \pm 0.0003 \\ 0.9996 \pm 0.0002 \\ 0.9995 \pm 0.0003 \\ 1.0006 \pm 0.0005 \\ 0.9999 \pm 0.0014 \\ 1.0016 \pm 0.0016 \\ \hline \end{array}$	$\begin{array}{c} 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ \hline \\ 0.9944 \pm 0.0040 \\ 1.0015 \pm 0.0019 \\ 1.0096 \pm 0.0015 \\ 1.0146 \pm 0.0031 \\ 1.0057 \pm 0.0060 \\ 1.0197 \pm 0.0158 \\ 1.0154 \pm 0.0198 \\ 1.1008 \pm 0.0535 \\ 0.8277 \pm 0.0879 \\ 1.2500 \pm 0.2795 \\ \hline \\ 1.5 < \eta < 2.1 \\ \hline \\ 0.9950 \pm 0.0016 \\ 0.9992 \pm 0.0006 \\ 1.0009 \pm 0.0006 \\ 1.0009 \pm 0.0006 \\ 0.9985 \pm 0.0012 \\ 1.0013 \pm 0.0035 \\ 1.0108 \pm 0.0036 \\ \hline \end{array}$
$\begin{array}{c} 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ Scale Factor ID \\ p_T range [GeV] \\ 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ Scale Factor ISO \\ p_T range [GeV] \\ 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ \hline \\ 100 - 150 \\ 100 - 150 \\ 100 - 150 \\ 100 - 150 \\ 150 - 200 \\ \hline \end{array}$	$\begin{array}{c} 0.9908 \pm 0.0031 \\ 0.9941 \pm 0.0042 \\ 0.9792 \pm 0.0206 \\ \hline \\ \eta < 1.5 \\ 0.9987 \pm 0.0014 \\ 1.0007 \pm 0.0006 \\ 1.0029 \pm 0.0010 \\ 1.0014 \pm 0.0018 \\ 0.9949 \pm 0.0043 \\ 1.0104 \pm 0.0057 \\ 1.0087 \pm 0.0134 \\ 0.9786 \pm 0.0134 \\ 0.9786 \pm 0.0033 \\ 1.0824 \pm 0.0619 \\ \hline \\ \eta < 1.5 \\ 0.9952 \pm 0.0009 \\ 0.9984 \pm 0.0003 \\ 0.9995 \pm 0.0003 \\ 1.0006 \pm 0.0005 \\ 0.9999 \pm 0.0014 \\ 1.0016 \pm 0.0016 \\ 0.9989 \pm 0.0042 \\ \hline \end{array}$	$\begin{array}{c} 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9944 \pm 0.0040 \\ 1.0015 \pm 0.0019 \\ 1.0096 \pm 0.0015 \\ 1.0146 \pm 0.0031 \\ 1.0057 \pm 0.0060 \\ 1.0197 \pm 0.0158 \\ 1.0154 \pm 0.0198 \\ 1.1008 \pm 0.0535 \\ 0.8277 \pm 0.0879 \\ 1.2500 \pm 0.2795 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9950 \pm 0.0016 \\ 0.9992 \pm 0.0006 \\ 1.0009 \pm 0.0006 \\ 0.9985 \pm 0.0012 \\ 1.0013 \pm 0.0035 \\ 1.0108 \pm 0.0035 \\ 1.0108 \pm 0.0036 \\ 1.0068 \pm 0.0069 \\ \hline \end{array}$
$ \begin{array}{c} 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ Scale Factor ID \\ p_T range [GeV] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ Scale Factor ISO \\ p_T range [GeV] \\ \hline 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ 200 - 300 \\ \hline \end{array} $	$\begin{array}{c} 0.9908 \pm 0.0031 \\ 0.9941 \pm 0.0042 \\ 0.9792 \pm 0.0206 \\ \hline \\ \eta < 1.5 \\ 0.9987 \pm 0.0014 \\ 1.0007 \pm 0.0006 \\ 1.0036 \pm 0.0005 \\ 1.0029 \pm 0.0010 \\ 1.0014 \pm 0.0018 \\ 0.9949 \pm 0.0043 \\ 1.0104 \pm 0.0057 \\ 1.0087 \pm 0.0134 \\ 0.9786 \pm 0.0203 \\ 1.0824 \pm 0.0619 \\ \hline \\ \eta < 1.5 \\ 0.9952 \pm 0.0009 \\ 0.9984 \pm 0.0003 \\ 0.9996 \pm 0.0002 \\ 0.9995 \pm 0.0003 \\ 1.0006 \pm 0.0005 \\ 0.9999 \pm 0.0014 \\ 1.0016 \pm 0.0016 \\ \hline \end{array}$	$\begin{array}{c} 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ \hline \\ 0.9944 \pm 0.0040 \\ 1.0015 \pm 0.0019 \\ 1.0096 \pm 0.0015 \\ 1.0146 \pm 0.0031 \\ 1.0057 \pm 0.0060 \\ 1.0197 \pm 0.0158 \\ 1.0154 \pm 0.0198 \\ 1.1008 \pm 0.0535 \\ 0.8277 \pm 0.0879 \\ 1.2500 \pm 0.2795 \\ \hline \\ 1.5 < \eta < 2.1 \\ \hline \\ 0.9950 \pm 0.0016 \\ 0.9992 \pm 0.0006 \\ 1.0009 \pm 0.0006 \\ 1.0009 \pm 0.0006 \\ 0.9985 \pm 0.0012 \\ 1.0013 \pm 0.0035 \\ 1.0108 \pm 0.0036 \\ \hline \end{array}$
$\begin{array}{c} 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ Scale Factor ID \\ p_T range [GeV] \\ 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ 100 - 150 \\ 150 - 200 \\ 200 - 300 \\ 300 - 10000 \\ \hline \\ Scale Factor ISO \\ p_T range [GeV] \\ 20 - 30 \\ 30 - 40 \\ 40 - 50 \\ 50 - 60 \\ 60 - 80 \\ 80 - 100 \\ \hline \\ 100 - 150 \\ 100 - 150 \\ 100 - 150 \\ 100 - 150 \\ 150 - 200 \\ \hline \end{array}$	$\begin{array}{c} 0.9908 \pm 0.0031 \\ 0.9941 \pm 0.0042 \\ 0.9792 \pm 0.0206 \\ \hline \\ \eta < 1.5 \\ 0.9987 \pm 0.0014 \\ 1.0007 \pm 0.0006 \\ 1.0029 \pm 0.0010 \\ 1.0014 \pm 0.0018 \\ 0.9949 \pm 0.0043 \\ 1.0104 \pm 0.0057 \\ 1.0087 \pm 0.0134 \\ 0.9786 \pm 0.0134 \\ 0.9786 \pm 0.0033 \\ 1.0824 \pm 0.0619 \\ \hline \\ \eta < 1.5 \\ 0.9952 \pm 0.0009 \\ 0.9984 \pm 0.0003 \\ 0.9995 \pm 0.0003 \\ 1.0006 \pm 0.0005 \\ 0.9999 \pm 0.0014 \\ 1.0016 \pm 0.0016 \\ 0.9989 \pm 0.0042 \\ \hline \end{array}$	$\begin{array}{c} 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ 1.0000 \pm 0.0000 \\ \hline 1.0000 \pm 0.0000 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9944 \pm 0.0040 \\ 1.0015 \pm 0.0019 \\ 1.0096 \pm 0.0015 \\ 1.0146 \pm 0.0031 \\ 1.0057 \pm 0.0060 \\ 1.0197 \pm 0.0158 \\ 1.0154 \pm 0.0198 \\ 1.1008 \pm 0.0535 \\ 0.8277 \pm 0.0879 \\ 1.2500 \pm 0.2795 \\ \hline \\ 1.5 < \eta < 2.1 \\ 0.9950 \pm 0.0016 \\ 0.9992 \pm 0.0006 \\ 1.0009 \pm 0.0006 \\ 0.9985 \pm 0.0012 \\ 1.0013 \pm 0.0035 \\ 1.0108 \pm 0.0035 \\ 1.0108 \pm 0.0036 \\ 1.0068 \pm 0.0069 \\ \hline \end{array}$

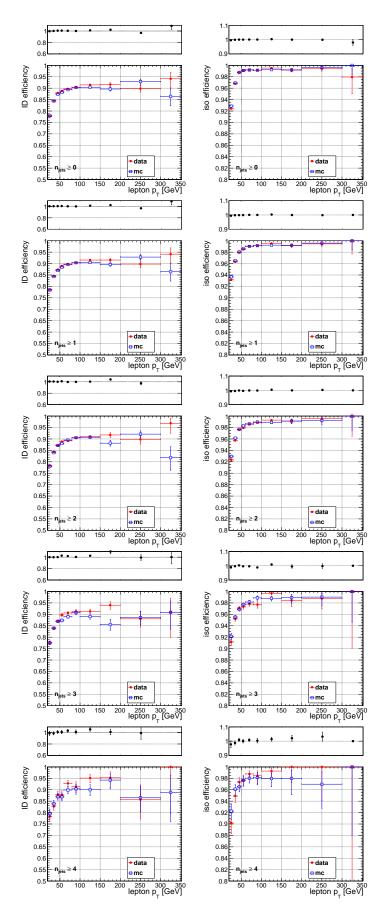


Figure 3: Comparison of the electron identification and isolation efficiencies in data and MC for various jet multiplicity requirements.

206 4.4.4 Trigger Efficiency Measurements

In this section we measure the efficiencies of the single lepton triggers, HLT_IsoMu24(_eta2p1) for muons and HLT_Ele27_WP80 for electrons, using a tag-and-probe approach. The tag is required to pass the full offline analysis selection and have $p_T > 30$ GeV, $|\eta| < 2.1$, and be matched to the single lepton trigger. The probe is also required to pass the full offline analysis selection and have $|\eta| < 2.1$, but the p_T requirement is relaxed to 20 GeV in order to measure the p_T turn-on curve. The tag-probe pair is required to have opposite-sign and an invariant mass in the range 76–106 GeV. The measured trigger efficiencies are displayed in Fig. 4 and summarized in Table 10 (muons) and Table 11 (electrons). These trigger efficiencies will be applied to the MC when used to predict data yields selected by single lepton triggers. [THESE TRIGGER EFFICIENCIES TO BE APPLIED TO MC]

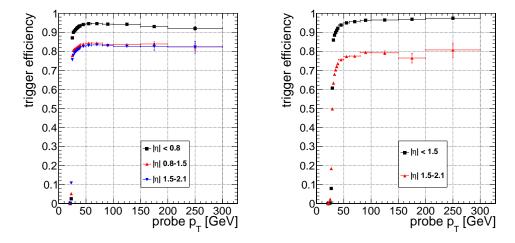


Figure 4: Efficiency for the single muon trigger HLT_IsoMu24(_eta2p1) (left) and single electron trigger HLT_Ele27_WP80 (right) as a function of lepton p_T , for several bins in lepton $|\eta|$.

Table 10: Summary of the single muon trigger efficiency HLT_IsoMu24(_eta2p1). Uncertainties are statistical.

p_{T} range [GeV]	$ \eta < 0.8$	$0.8 < \eta < 1.5$	$1.5 < \eta < 2.1$
20 - 22	0.00 ± 0.000	0.00 ± 0.000	0.00 ± 0.000
22 - 24	0.03 ± 0.001	0.05 ± 0.001	0.11 ± 0.002
24 - 26	0.87 ± 0.002	0.78 ± 0.002	0.76 ± 0.003
26 - 28	0.90 ± 0.001	0.81 ± 0.002	0.78 ± 0.002
28 - 30	0.91 ± 0.001	0.81 ± 0.002	0.79 ± 0.002
30 - 32	0.91 ± 0.001	0.81 ± 0.001	0.80 ± 0.002
32 - 34	0.92 ± 0.001	0.82 ± 0.001	0.80 ± 0.002
34 - 36	0.93 ± 0.001	0.82 ± 0.001	0.81 ± 0.001
36 - 38	0.93 ± 0.001	0.83 ± 0.001	0.81 ± 0.001
38 - 40	0.93 ± 0.001	0.83 ± 0.001	0.82 ± 0.001
40 - 50	0.94 ± 0.000	0.84 ± 0.000	0.82 ± 0.001
50 - 60	0.95 ± 0.000	0.84 ± 0.001	0.83 ± 0.001
60 - 80	0.95 ± 0.001	0.84 ± 0.002	0.83 ± 0.002
80 - 100	0.94 ± 0.002	0.84 ± 0.004	0.83 ± 0.006
100 - 150	0.94 ± 0.003	0.84 ± 0.005	0.83 ± 0.008
150 - 200	0.93 ± 0.006	0.84 ± 0.011	0.82 ± 0.018
>200	0.92 ± 0.010	0.82 ± 0.017	0.82 ± 0.031

Table 11: Summary of the single electron trigger efficiency HLT_Ele27_WP80. Uncertainties are statistical.

$p_{\rm T}$ range [GeV]	$ \eta < 1.5$	$1.5 < \eta < 2.1$
20 - 22	0.00 ± 0.000	0.00 ± 0.000
22 - 24	0.00 ± 0.000	0.00 ± 0.001
24 - 26	0.00 ± 0.000	0.02 ± 0.001
26 - 28	0.08 ± 0.001	0.18 ± 0.003
28 - 30	0.61 ± 0.002	0.50 ± 0.004
30 - 32	0.86 ± 0.001	0.63 ± 0.003
32 - 34	0.88 ± 0.001	0.68 ± 0.003
34 - 36	0.90 ± 0.001	0.70 ± 0.002
36 - 38	0.91 ± 0.001	0.72 ± 0.002
38 - 40	0.92 ± 0.001	0.74 ± 0.002
40 - 50	0.94 ± 0.000	0.76 ± 0.001
50 - 60	0.95 ± 0.000	0.77 ± 0.002
60 - 80	0.96 ± 0.001	0.78 ± 0.003
80 - 100	0.96 ± 0.002	0.80 ± 0.008
100 - 150	0.96 ± 0.002	0.79 ± 0.010
150 - 200	0.97 ± 0.004	0.76 ± 0.026
>200	0.97 ± 0.005	0.81 ± 0.038

²¹⁶ 5 Control Region Studies

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5.1 W+Jets MC Modelling Validation from CR1

The estimate of the uncertainty on this background is based on CR1, defined by applying the full signal selection, including the isolated track veto, but requiring 0 b-tags (CSV medium working point as described in Sec. 4). The sample is dominanted by W+jets and is thus used to validate the MC modelling of this background.

In Table 12 we show the amount that we need to scale the Wjets MC by in order to have agreement between data and Monte Carlo in the M_T peak region, defined as $60 < M_T < 100$ GeV. These scale factors are not terribly important, but it is reassuring that they are not too different from 1. [UPDATE WITH TRIGGER EFFICIENCIES]

Sample	CR1PRESEL	CR1A	CR1B	CR1C	CR1D	CR1E	CR1F	CR1G
$\mu~M_{\mathrm{T}}\text{-SF}$	0.92 ± 0.02	0.97 ± 0.03	0.90 ± 0.04	0.91 ± 0.06	0.93 ± 0.09	0.98 ± 0.13	0.94 ± 0.18	0.96 ± 0.25
e M_{T} -SF	0.94 ± 0.02	0.90 ± 0.04	0.84 ± 0.05	0.80 ± 0.07	0.83 ± 0.10	0.77 ± 0.13	0.86 ± 0.20	0.87 ± 0.29

Table 12: $M_{\rm T}$ peak Data/MC scale factors applied to the single lepton samples and ${\rm t\bar{t}} \to \ell\ell$. The raw MC is used for backgrounds from rare processes. CR1PRESEL refers to a sample with $E_{\rm T}^{\rm miss} > 50$ GeV. The uncertainties are statistical only.

In Table 13 we compare the data and MC yields in the four M_T signal regions and in a looser control region. We also derive the data/MC scale factors SFR_{wjet}^e and SFR_{wjet}^μ . The underlying $E_{\rm T}^{\rm miss}$ and M_T distributions are shown in Fig. 5 and 6

Sample	CR1PRESEL	CR1A	CR1B	CR1C	CR1D	CR1E	CR1F	CR1G
μ MC	480 ± 22	173 ± 5	114 ± 4	40 ± 2	16 ± 1	8 ± 1	4 ± 1	2 ± 1
μ Data	629	238	139	45	12	8	3	2
$\mu \mathrm{Data/MC}$	1.31 ± 0.08	1.37 ± 0.10	1.22 ± 0.11	1.12 ± 0.18	0.75 ± 0.23	0.99 ± 0.37	0.75 ± 0.45	0.96 ± 0.72
e MC	330 ± 8	118 ± 4	79 ± 3	29 ± 2	13 ± 1	5 ± 1	3 ± 1	2 ± 0
e Data	473	174	100	36	16	5	5	2
e Data/MC	1.43 ± 0.07	1.47 ± 0.12	1.27 ± 0.14	1.23 ± 0.22	1.26 ± 0.34	1.07 ± 0.51	1.80 ± 0.91	1.26 ± 0.97
μ+e MC	810 ± 23	291 ± 7	192 ± 5	69 ± 3	29 ± 2	13 ± 1	7 ± 1	4 ± 1
μ+e Data	1102	412	239	81	28	13	8	4
μ+e Data/MC	1.36 ± 0.08	1.42 ± 0.13	1.24 ± 0.15	1.17 ± 0.23	0.97 ± 0.31	1.02 ± 0.51	1.18 ± 0.69	1.09 ± 0.96
μ W MC	300 ± 23	84 ± 5	52 ± 4	20 ± 2	9 ± 2	5 ± 1	3 ± 1	1 ± 1
μ W Data	449 ± 26	149 ± 16	78 ± 12	25 ± 7	5 ± 4	5 ± 3	2 ± 2	1 ± 1
μ W Data/MC	1.50 ± 0.14	1.77 ± 0.21	1.49 ± 0.26	1.25 ± 0.38	0.56 ± 0.39	0.98 ± 0.62	0.60 ± 0.73	0.94 ± 1.14
e W MC	192 ± 8	55 ± 4	36 ± 3	14 ± 2	6 ± 1	3 ± 1	2 ± 1	1 ± 0
e W Data	335 ± 22	111 ± 13	58 ± 10	20 ± 6	10 ± 4	3 ± 2	4 ± 2	1 ± 1
e W Data/MC	1.74 ± 0.14	2.02 ± 0.29	1.58 ± 0.32	1.49 ± 0.50	1.50 ± 0.70	1.10 ± 0.80	2.27 ± 1.55	1.51 ± 1.96
μ+e W MC	493 ± 24	139 ± 6	89 ± 5	33 ± 3	16 ± 2	8 ± 1	4 ± 1	2 ± 1
μ+e W Data	785 ± 59	260 ± 37	135 ± 28	45 ± 16	15 ± 9	8 ± 7	6 ± 5	3 ± 3
μ +e W Data/MC	1.59 ± 0.14	1.87 ± 0.28	1.53 ± 0.33	1.35 ± 0.50	0.95 ± 0.58	1.03 ± 0.83	1.29 ± 1.13	1.16 ± 1.65
SFR_{wjet}	1.48 ± 0.26	1.64 ± 0.38	1.38 ± 0.30	1.26 ± 0.39	0.96 ± 0.45	1.02 ± 0.67	1.23 ± 0.92	1.12 ± 1.31

Table 13: Yields in $M_{\rm T}$ tail comparing the MC prediction (after applying SFs) to data. CR1PRESEL refers to a sample with $E_{\rm T}^{\rm miss} > 50$ GeV and $M_{\rm T} > 150$ GeV. The uncertainties are statistical only.

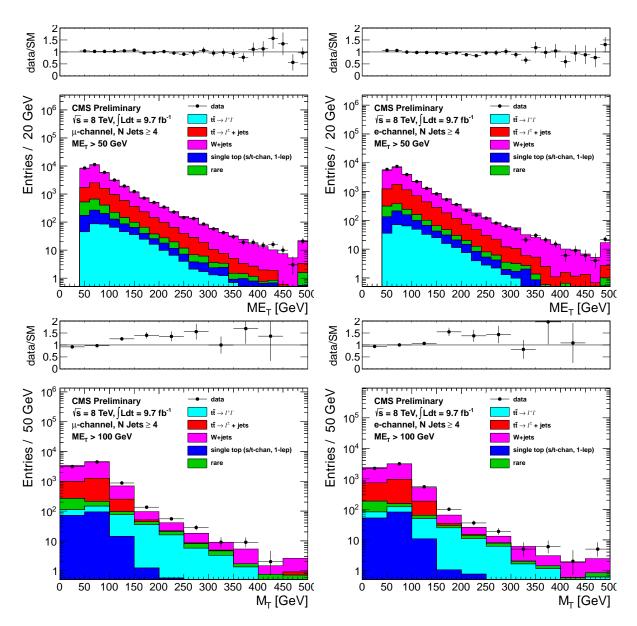


Figure 5: Comparison of the $E_{\rm T}^{\rm miss}$ (top) and $M_{\rm T}$ for $E_{\rm T}^{\rm miss} > 100$ (bottom) distributions in data vs. MC for events with a leading muon (left) and leading electron (right) satisfying the requirements of CR1.

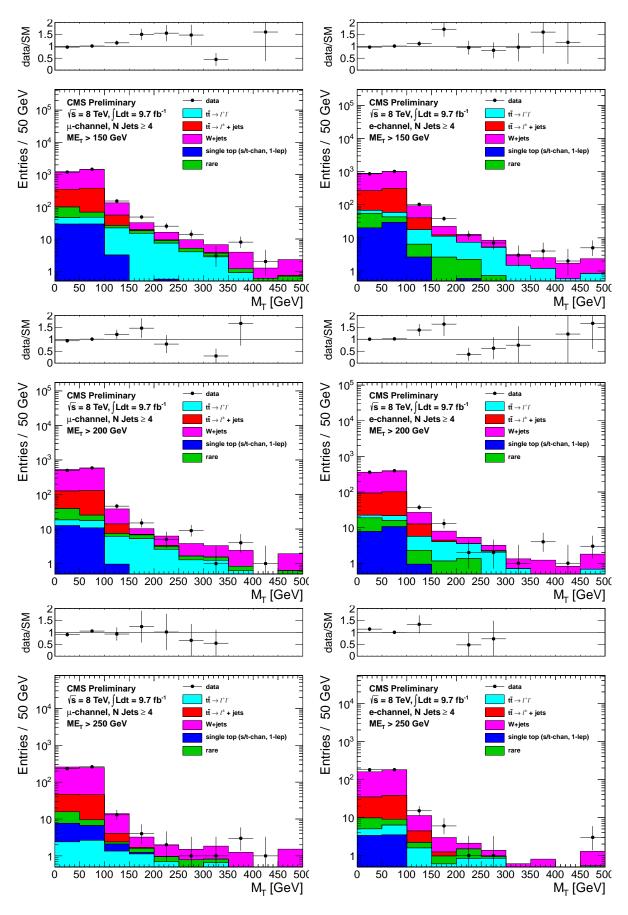


Figure 6: Comparison of the $M_{\rm T}$ distribution in data vs. MC for events with a leading muon (left) and leading electron (right) satisfying the requirements of CR1. The $E_{\rm T}^{\rm miss}$ requirements used are 150 GeV (top), 200 GeV (middle) and 250 GeV (bottom).



Figure 7: Comparison of the $M_{\rm T}$ distribution in data vs. MC for events with a leading muon (left) and leading electron (right) satisfying the requirements of CR1. The $E_{\rm T}^{\rm miss}$ requirements used are 300 GeV (top), 350 GeV (middle) and 400 GeV (bottom).

5.2 Single Lepton Top MC Modelling Validation from CR2

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230 IS THIS GOING TO BE DONE WITH A BVETO OR NOT. IF SO, IS IT GOING TO BE CSVL OR 231 CSVM? NEED TO DISCUSS THIS.

The $M_{\rm T}$ tail for single-lepton top events (tt $\rightarrow \ell$ + jets and single top) is dominated by jet resolution effects. The W cannot be far off-shell because $M_{\rm W} < M_{\rm top}$. The modeling of the $M_{\rm T}$ tail from jet resolution effects is studied using Z+jets data and MC samples. Z events are selection by requiring 2 good leptons (satisfying ID and isolation requirements) and requiring the $M_{\ell\ell}$ to be in the range 81 – 101 GeV. The negative lepton is treated as a neutrino and so is added to the MET: $E_{\rm T}^{\rm miss} \rightarrow p_{\rm T}(\ell^-) + E_{\rm T}^{\rm miss}$, and the $M_{\rm T}$ is recalculated with the positive lepton $M_{\rm T}(\ell^+, E_{\rm T}^{\rm miss})$. The resulting "pseudo- $M_{\rm T}$ " is dominated by jet resolution effects, since no off-shell Z production enters the sample due to the $M_{\ell\ell}$ requirement. This section describes how well the MC predicts the tail of "pseudo- $M_{\rm T}$ ".

The underlying distributions are shown in Fig. 8 and 9. The comparison of data and MC event counts is shown in Table 14. From this table we extract the data to MC scale factors SFR_{top}^e and SFR_{top}^μ .

Sample	CR2PRESEL0	CR2PRESEL1	CR2A	CR2B	CR2C	CR2D	CR2E
MC	36 ± 2	30 ± 2	18 ± 1	30 ± 2	13 ± 1	5 ± 0	2 ± 0
Data	56	43	32	40	21	12	2
Data/MC	1.56 ± 0.23	1.44 ± 0.24	1.77 ± 0.34	1.32 ± 0.22	1.65 ± 0.37	2.65 ± 0.79	0.99 ± 0.71
DY MC	27 ± 2	23 ± 2	14 ± 2	25 ± 3	11 ± 2	3 ± 1	1 ± 1
DY MC DY Data	27 ± 2 47 ± 8	23 ± 2 36 ± 7	14 ± 2 28 ± 6	25 ± 3 35 ± 6	11 ± 2 19 ± 5	3 ± 1 11 ± 3	1 ± 1 1 ± 1
-							

Table 14: Yields in $M_{\rm T}$ tail comparing the $Z+{\rm jets}$ MC prediction (after applying SFs) to data after subtracting the non- $Z+{\rm jets}$ components. CR2PRESEL refers to a sample with $E_{\rm T}^{\rm miss}>50$ GeV and $M_{\rm T}>150$ GeV. The uncertainties are statistical only. NEED TO ADD THE SYMBOLS DEFINED IN THE TEXT FOR THESE SCALE FACTORS. IS THIS GOING TO BE DONE SEPARATELY FOR MUONS AND ELECTRONS??? MAYBE WANT TO REMOVE LAST ENTRIES WHERE STATS ARE VERY LOW

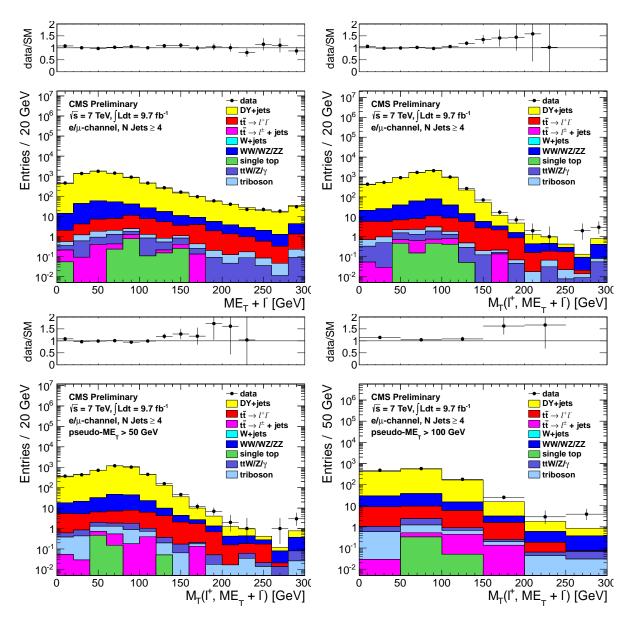


Figure 8: Comparison of the pseudo $E_{\mathrm{T}}^{\mathrm{miss}}$ (top, left), pseudo M_{T} (top, right and bottom) distributions in data vs. MC for events satisfying the requirements of CR2, combining both the muon and electron channels. The pseudo M_{T} distributions are shown before any additional requirements (top, right) and after requiring pseudo $E_{\mathrm{T}}^{\mathrm{miss}}$;50 GeV (bottom, left) and pseudo $E_{\mathrm{T}}^{\mathrm{miss}}$;100 GeV (bottom, right) .

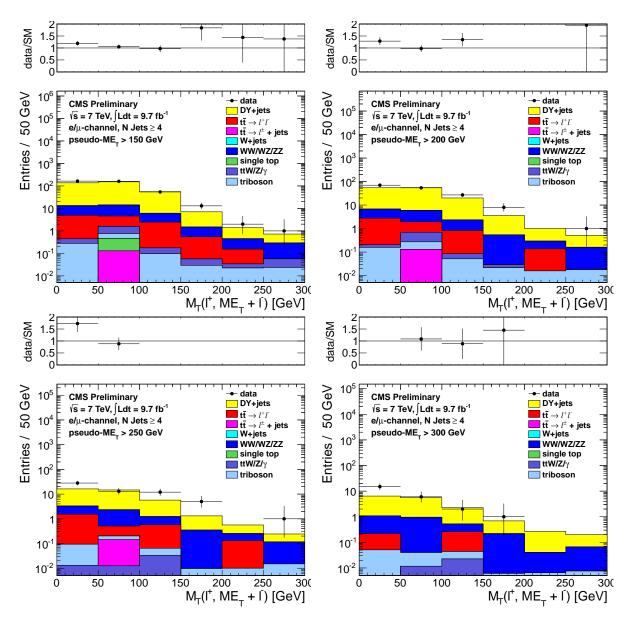


Figure 9: Comparison of the $M_{\rm T}$ distribution in data vs. MC for events satisfying the requirements of CR2, combining both the muon and electron channels. The pseudo- $E_{\rm T}^{\rm miss}$ requirements used are 150 GeV (top, left), 200 GeV (top, right), 250 GeV (bottom, left) and 300 GeV (bottom, right).

5.3 Dilepton studies in CR4

²⁴³ 5.3.1 Modeling of Additional Hard Jets in Top Dilepton Events

²⁴⁴ [THIS SUBSUBSECTION IS DONE...MODULO THE LATEST PLOTS AND THE LATEST NUM-²⁴⁵ BERS IN THE TABLE]

Dilepton $t\bar{t}$ events have 2 jets from the top decays, so additional jets from radiation or higher order contributions are required to enter the signal sample. The modeling of additional jets in $t\bar{t}$ events is checked in a $t\bar{t} \to \ell\ell$ control sample, selected by requiring

- exactly 2 selected electrons or muons with $p_T > 20 \text{ GeV}$
- $\bullet~E_{
 m T}^{
 m miss} > 50~{
 m GeV}$

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- ≥ 1 b-tagged jet
- Z-veto $(|m_{\ell\ell} 91| > 15 \text{ GeV})$

Figure 10 shows a comparison of the jet multiplicity distribution in data and MC for this two-lepton control sample. After requiring at least 1 b-tagged jet, most of the events have 2 jets, as expected from the dominant process $t\bar{t} \to \ell\ell$. There is also a significant fraction of events with additional jets. The 3-jet sample is mainly comprised of $t\bar{t}$ events with 1 additional emission and similarly the \geq 4-jet sample contains primarily $t\bar{t}+\geq 2$ jet events.

It should be noted that in the case of $t\bar{t} \to \ell\ell$ events with a single reconstructed lepton, the other lepton may be mis-reconstructed as a jet. For example, a hadronic tau may be mis-identified as a jet (since no τ identification is used). In this case only 1 additional jet from radiation may suffice for a $t\bar{t} \to \ell\ell$ event to enter the signal sample. As a result, both the samples with $t\bar{t}+1$ jet and $t\bar{t}+2$ jets are relevant for estimating the top dilepton background in the signal region.

Table 15 shows scale factors (K_3 and K_4) used to correct the fraction of events with additional jets in MC to the observed fraction in data. These scale factors are calculated from Fig. 10 as follows:

- $N_2 = \text{data yield minus non-dilepton } t\bar{t} \text{ MC yield for } N_{\text{iets}} \leq 2$
 - $N_3 = \text{data yield minus non-dilepton } t\bar{t} \text{ MC yield for } N_{\text{jets}} = 3$
- $N_4={
 m data\ yield\ minus\ non-dilepton\ tar{t}\ MC\ yield\ for\ N_{
 m jets}\geq 4}$
- $M_2 = \text{dilepton t\bar{t} MC yield for } N_{\text{jets}} \leq 2$
 - $M_3 = \text{dilepton t}\bar{\text{t}} \text{ MC yield for } N_{\text{jets}} = 3$
- $M_4 = \text{dilepton t\bar{t} MC yield for } N_{\text{jets}} \geq 4$

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•
$$SF_2 = N_2/M_2$$

•
$$SF_3 = N_3/M_3$$

•
$$SF_4 = N_4/M_4$$

•
$$K_3 = SF_3/SF_2$$

•
$$K_4 = SF_4/SF_2$$

This insures that $K_3M_3/(M_2+K_3M_3+K_4M_4)=N_3/(N_2+N_3+N_4)$ and similarly for the ≥ 4 jet bin.

Table 15 also shows the values of K_3 and K_4 when the $E_{\rm T}^{\rm miss}$ cut in the control sample definition is changed from 50 GeV to 100 GeV and 150 GeV. These values of K_3 and K_4 are not used in the analysis, but demonstrate that there is no statistically significant dependence of K_3 and K_4 on the $E_{\rm T}^{\rm miss}$ cut.

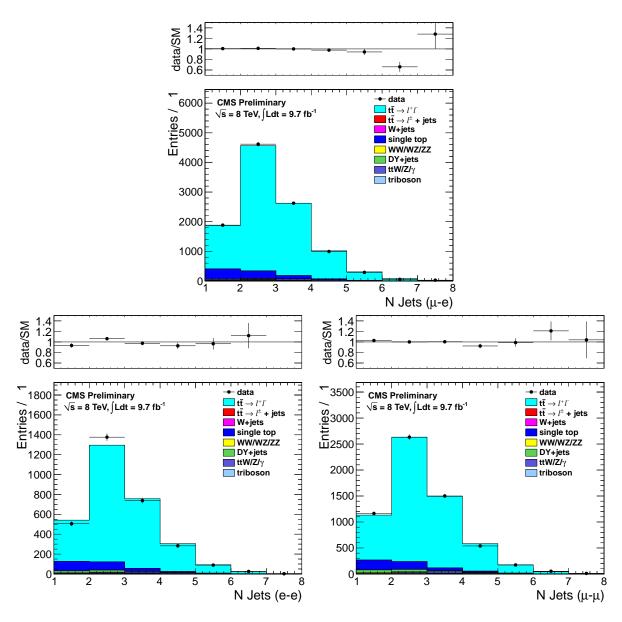


Figure 10: Comparison of the jet multiplicity distribution in data and MC for dilepton events in the e- μ (top), e-e (bottom left) and μ - μ (bottom right) channels.

The factors K_3 and K_4 (derived with the 50 GeV $E_{\rm T}^{\rm miss}$ cut) are applied to the ${\rm t\bar{t}} \to \ell\ell$ MC throughout the entire analysis, i.e. whenever ${\rm t\bar{t}} \to \ell\ell$ MC is used to estimate or subtract a yield or distribution. In order to do so, it is first necessary to count the number of additional jets from radiation and exclude leptons mis-identified as jets. A jet is considered a mis-identified lepton if it is matched to a generator-level second lepton with sufficient energy to satisfy the jet $p_{\rm T}$ requirement ($p_{\rm T} > 30$ GeV). Then ${\rm t\bar{t}} \to \ell\ell$ events that need two radiation jets to enter our selection are scaled by K_4 , while those that only need one radiation jet are scaled by K_3 .

	$E_{\mathrm{T}}^{\mathrm{miss}}$ cut for Data/MC Scale Factor				
Jet Multiplicity Sample	$50 \mathrm{GeV}$	100 GeV	$150 \mathrm{GeV}$		
N jets = 3 (sensitive to $t\bar{t} + 1$ extra jet from radiation)	$K_3 = 0.98 \pm 0.02$	$K_3 = 1.01 \pm 0.03$	$K_3 = 1.00 \pm 0.08$		
N jets ≥ 4 (sensitive to $t\bar{t}+\geq 2$ extra jets from radiation)	$K_4 = 0.94 \pm 0.02$	$K_4 = 0.93 \pm 0.04$	$K_4 = 1.00 \pm 0.08$		

Table 15: Data/MC scale factors used to account for differences in the fraction of events with additional hard jets from radiation in $t\bar{t} \to \ell\ell$ events. The values derived with the 50 GeV $E_{\rm T}^{\rm miss}$ cut are applied to the $t\bar{t} \to \ell\ell$ MC throughout the analysis.

5.3.2 Validation of the "Physics" Modelling of the ${ m tar t} o \ell\ell$ MC in CR4

[THE TEXT IN THIS SUBSECTION IS ESSENTIALLY COMPLETE]

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As mentioned above, $t\bar{t} \to \text{dileptons}$ where one of the leptons is somehow lost constitutes the main background. The object of this test is to validate the M_T distribution of this background by looking at the M_T distribution of well identified dilepton events. We construct a transverse mass variable from the leading lepton and the E_T^{miss} . We distinguish between events with leading electrons and leading muons.

The $t\bar{t}$ MC is corrected using the K_3 and K_4 factors from Section 5.3.1. It is also normalized to the total data yield separately for the $E_{\rm T}^{\rm miss}$ requirements of signal regions A, B, C, and D. These normalization factors are listed in Table 16 and are close to unity.

The underlying $E_{\rm T}^{\rm miss}$ and M_T distributions are shown in Figures 11 and 12. The data-MC agreement is quite good. Quantitatively, this is also shown in Table 17.

Sample	CR4PRESEL	CR4A	CR4B	CR4C	CR4D	CR4E	CR4F
μ Data/MC-SF	1.01 ± 0.03	0.96 ± 0.04	0.99 ± 0.07	1.05 ± 0.13	0.91 ± 0.20	1.10 ± 0.34	1.50 ± 0.67
e Data/MC-SF	0.99 ± 0.03	0.99 ± 0.05	0.91 ± 0.08	0.84 ± 0.13	0.70 ± 0.18	0.73 ± 0.29	0.63 ± 0.38

Table 16: Data/MC scale factors for total yields, applied to compare the shapes of the distributions. The uncertainties are statistical only.

Sample	CR4PRESEL	CR4A	CR4B	CR4C	CR4D	CR4E	CR4F
$\mu \text{ MC}$	256 ± 14	152 ± 11	91 ± 9	26 ± 5	6 ± 2	4 ± 2	2 ± 1
μ Data	251	156	98	27	8	6	4
μ Data/MC SF	0.98 ± 0.08	1.02 ± 0.11	1.08 ± 0.16	1.04 ± 0.28	1.29 ± 0.65	1.35 ± 0.80	2.10 ± 1.72
e MC	227 ± 13	139 ± 11	73 ± 8	21 ± 4	5 ± 2	2 ± 1	1 ± 1
e Data	219	136	72	19	2	1	1
e Data/MC SF	0.96 ± 0.09	0.98 ± 0.11	0.99 ± 0.16	0.92 ± 0.29	0.41 ± 0.33	0.53 ± 0.62	0.76 ± 0.96
μ +e MC	483 ± 19	291 ± 16	164 ± 13	47 ± 7	11 ± 3	6 ± 2	3 ± 2
μ +e Data	470	292	170	46	10	7	5
μ+e Data/MC SF	0.97 ± 0.06	1.00 ± 0.08	1.04 ± 0.11	0.99 ± 0.20	0.90 ± 0.37	1.11 ± 0.57	1.55 ± 1.04

Table 17: Yields in $M_{\rm T}$ tail comparing the MC prediction (after applying SFs) to data. The uncertainties are statistical only.

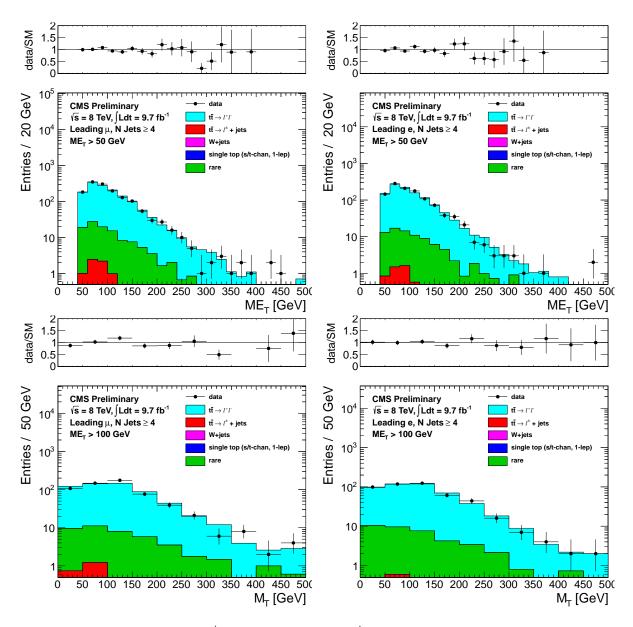


Figure 11: Comparison of the $E_{\rm T}^{\rm miss}$ (top) and $M_{\rm T}$ for $E_{\rm T}^{\rm miss} > 100$ (bottom) distributions in data vs. MC for events with a leading muon (left) and leading electron (right) satisfying the requirements of CR4.

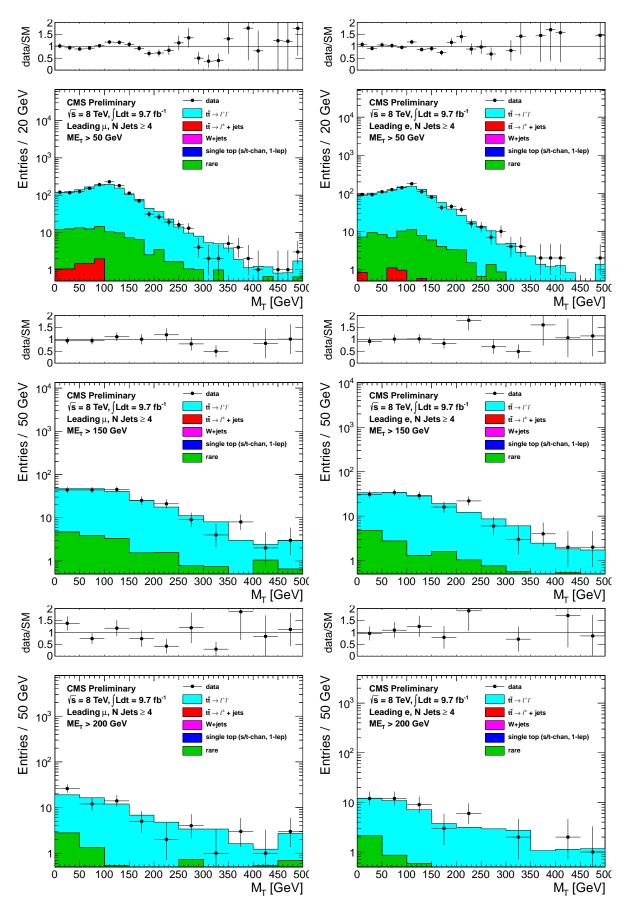


Figure 12: Comparison of the $M_{\rm T}$ distribution in data vs. MC for events with a leading muon (left) and leading electron (right) satisfying the requirements of CR4. The $E_{\rm T}^{\rm miss}$ requirements used are 50 GeV (top), 200 GeV (middle) and 250 GeV (bottom).

²⁹⁹ 5.4 Test of control region with isolated track in CR5

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[NEED TO VERIFY THAT THE DESCRIPTION OF SCALE FACTORS IS CORRECT AND ADD A LITTLE BIT OF DETAIL, AS NOTED IN THE TEXT]

This CR consists of events that pass all cuts but fail the isolated track veto cut. These events (especially in the tail of M_T) are predominantly $t\bar{t}$ dileptons. Thus the test in this control regions is similar to that performed in CR4 and described in Section 5.3.2. There is some non-trivial complementarity because CR5 also includes events with taus and events with electrons or muons below the threshold of the CR4 selection. Also, this test is somewhat sensitive to the simulation of the track isolation requirement, since the number of dilepton events in CR5 depends on the (in)efficiency of that cut.

In CR5 there is also a significant component of $t\bar{t}\to\ell+$ jets, where one of the jets fluctuates to an isolated track. This component dominates at low M_T and is not necessarily well reproduced quantitatively by the simulation. This makes the normalization of the top MC a little bit tricky. We define a "pre-veto" sample as the sample of events that pass all cuts without any isolated track requirements. This sample is dominated by $t\bar{t}\to\ell+$ jets. We normalize the dilepton component of the top MC to that sample (NEED TO EXPLAIN EXACTLY HOW). Next we define a "post-veto" sample as the events that have an isolated track. The $t\bar{t}\to\ell+$ jets component is normalized in this sample (ALSO, NEED TO EXPLAIN HOW, EXACTLY). These normalization factors are summarized in Table 18.

The underlying $E_{\rm T}^{\rm miss}$ and M_T distributions are shown in Figures 13 and 14. The data-MC agreement is quite good. Quantitatively, this is also shown in Table 19.

Sample	CR5PRESEL	CR5A	CR5B	CR5C	CR5D	CR5E	CR5F	CR5G
μ pre-veto $M_{\rm T}$ -SF μ post-veto $M_{\rm T}$ -SF	$1.05 \pm 0.01 \\ 1.25 \pm 0.04$	$1.02 \pm 0.02 \\ 1.17 \pm 0.07$	0.95 ± 0.03 1.05 ± 0.12	0.90 ± 0.05 0.85 ± 0.19	0.98 ± 0.08 0.84 ± 0.30	0.97 ± 0.13 1.07 ± 0.54	0.85 ± 0.18 1.38 ± 1.14	0.92 ± 0.31 0.68 ± 2.05
e pre-veto M_{T} -SF e post-veto M_{T} -SF	$1.01 \pm 0.01 \\ 1.21 \pm 0.04$	$\begin{array}{c} 0.95 \pm 0.02 \\ 1.12 \pm 0.07 \end{array}$	0.95 ± 0.03 1.25 ± 0.14	0.94 ± 0.06 1.17 ± 0.27	0.85 ± 0.09 2.01 ± 0.64	0.84 ± 0.13 1.71 ± 0.99	1.05 ± 0.23 2.79 ± 2.04	1.04 ± 0.33 0.81 ± 1.58

Table 18: $M_{\rm T}$ peak Data/MC scale factors. The pre-veto SFs are applied to the ${\rm t\bar{t}} \to \ell\ell$ sample, while the post-veto SFs are applied to the single lepton samples. The raw MC is used for backgrounds from rare processes. The uncertainties are statistical only.

Sample	CR5PRESEL	CR5A	CR5B	CR5C	CR5D	CR5E	CR5F	CR5G
μ MC	490 ± 9	299 ± 7	155 ± 6	49 ± 3	19 ± 2	7 ± 1	3 ± 1	2 ± 1
μ Data	514	311	167	57	12	4	2	1
μ Data/MC SF	1.05 ± 0.05	1.04 ± 0.06	1.08 ± 0.09	1.17 ± 0.17	0.64 ± 0.20	0.54 ± 0.29	0.66 ± 0.49	0.58 ± 0.62
e MC	405 ± 8	239 ± 7	130 ± 5	43 ± 3	16 ± 2	8 ± 1	6 ± 2	3 ± 1
e Data	427	248	120	38	14	4	3	2
e Data/MC SF	1.06 ± 0.06	1.04 ± 0.07	0.93 ± 0.09	0.89 ± 0.16	0.86 ± 0.25	0.52 ± 0.28	0.54 ± 0.35	0.76 ± 0.60
μ +e MC	894 ± 12	538 ± 10	284 ± 8	92 ± 4	35 ± 3	15 ± 2	9 ± 2	4 ± 1
μ +e Data	941	559	287	95	26	8	5	3
μ+e Data/MC SF	1.05 ± 0.04	1.04 ± 0.05	1.01 ± 0.07	1.04 ± 0.12	0.74 ± 0.16	0.53 ± 0.20	0.58 ± 0.29	0.69 ± 0.43

Table 19: Yields in $M_{\rm T}$ tail comparing the MC prediction (after applying SFs) to data. The uncertainties are statistical only.



Figure 13: Comparison of the $E_{\rm T}^{\rm miss}$ (top) and $M_{\rm T}$ for $E_{\rm T}^{\rm miss} > 100$ (bottom) distributions in data vs. MC for events with a leading muon (left) and leading electron (right) satisfying the requirements of CR5.

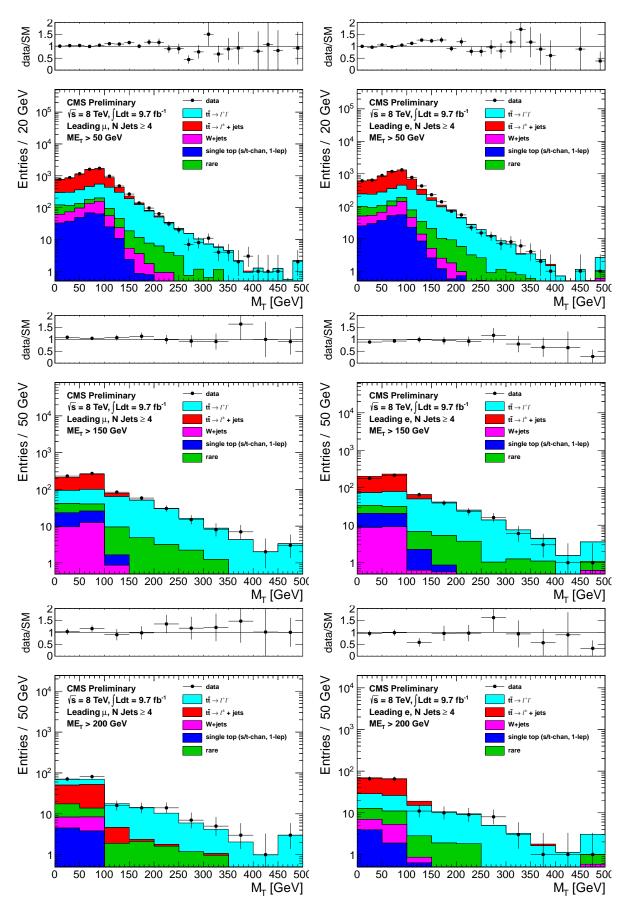


Figure 14: Comparison of the $M_{\rm T}$ distribution in data vs. MC for events with a leading muon (left) and leading electron (right) satisfying the requirements of CR5. The $E_{\rm T}^{\rm miss}$ requirements used are 50 GeV (top), 150 GeV (middle) and 200 GeV (bottom).

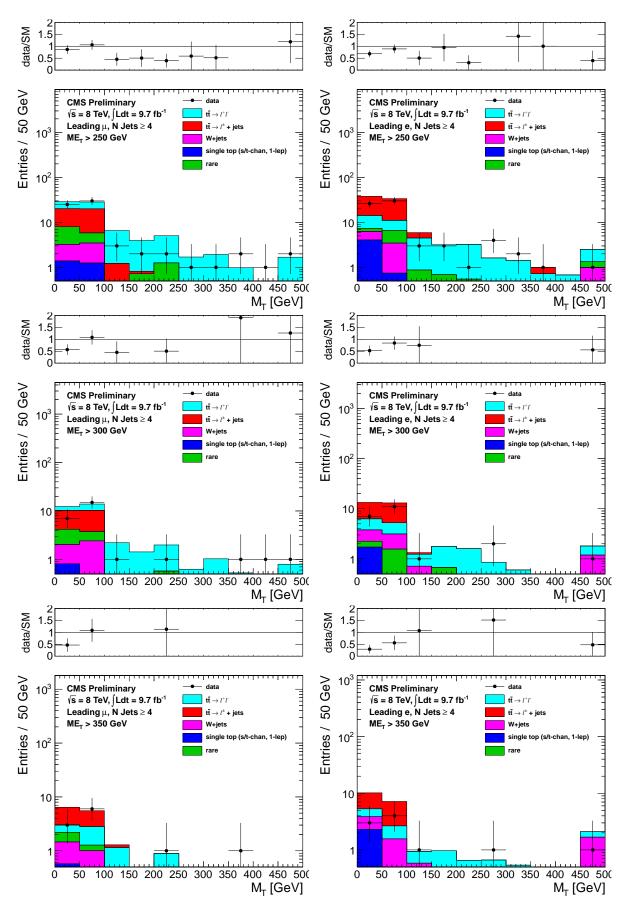


Figure 15: Comparison of the $M_{\rm T}$ distribution in data vs. MC for events with a leading muon (left) and leading electron (right) satisfying the requirements of CR5. The $E_{\rm T}^{\rm miss}$ requirements used are 250 GeV (top), 300 GeV (middle) and 350 GeV (bottom).

318 6 Other Backgrounds

319 Additional background contributions from rare processes include

- $t\bar{t}$ in association with a boson $t\bar{t} + WZ/\gamma^*$
- $Z/\gamma^* + \text{Jets}$
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- triboson WWW/WWZ/WZZ/ZZZ
- dilepton single top tW.

• diboson WW/WZ/ZZ

These backgrounds are small, contributing at the $\sim 5\%$ level and their predictions are taken from MC, normalized to the corresponding cross sections. A 50% systematic uncertainty is assigned for all these backgrounds.

Backgrounds from QCD are expected to be small in the signal regions with large $M_{
m T}$ and $E_{
m T}^{
m miss}$.

7 Tail-to-Peak ratio for lepton + jets top and W events

[FILL IN SOME XX]

An important component of the background calculation is the ratio of the number of events with M_T in the signal region to the number of events with $60 < M_T < 100$ GeV. As discussed in Section 2.1, these ratios are different for W+ jets and top events.

Sample	SRA	SRB	SRC	SRD	SRE	SRF	SRG
R_{top}^{μ}	0.015 ± 0.001	0.035 ± 0.002	0.021 ± 0.002	0.021 ± 0.004	0.025 ± 0.007	0.015 ± 0.009	0.021 ± 0.015
R_{wjet}^{μ}	0.040 ± 0.001	0.071 ± 0.003	0.062 ± 0.004	0.064 ± 0.006	0.065 ± 0.009	0.067 ± 0.012	0.065 ± 0.016
R_{top}^e	0.015 ± 0.001	0.031 ± 0.002	0.026 ± 0.003	0.025 ± 0.005	0.009 ± 0.005	0.021 ± 0.012	0.034 ± 0.024
R_{wjet}^{e}	0.040 ± 0.002	0.075 ± 0.004	0.067 ± 0.005	0.063 ± 0.007	0.061 ± 0.010	0.067 ± 0.015	0.070 ± 0.021

Table 20: Ratio of MC events in the $M_{\rm T}$ -tail over events in the $M_{\rm T}$ -peak for $t\bar{t} \to \ell + {\rm jets}$ (also used for 1-lepton single top) and $W+{\rm jets}$. These are derived before applying the b-tagging requirement.

The MC value of these ratios are shown in Table 20. In addition the studies of CR1 and CR2 (Sections 5.1 and 5.2) lead to data/MC scale factors SFR_{wjets}^e and SFR_{wjets}^μ (Table 13) and SFR_{top}^e and SFR_{top}^μ (Table 14)

342 8 Background Prediction

[THIS IS WHERE THE NUMBERS TO DERIVE THE BACKGROUND ESTIMATES ARE DUMPED AND THE CALCULATION EXPLAINED]

Here we give the details of how we arrive at the background prediction in a given signal region. Here
we concentrate on the method used to arrive at the central value of the background prediction. The
systematic uncertainties will be discussed in Section 9.

As mentioned in Section 2, we normalize the main $t\bar{t}$ background to the M_T peak. This is actually a bit tricky because we want to minimize the effect of the isolated track veto on lepton + jets events, which may not be terribly well reproduced. Thus, we define two normalization region in the M_T peak $(60 < M_T < 100 \text{ GeV})$, one before and one after the application of the isolated track veto.

The dominant dilepton background is normalized to the pre-veto normalization region. A pre-veto scale factor (SF_{pre}) is defined as a common scale factors that needs to be applied to the $t\bar{t}$, single-top, and W+ jets MC to make the data yield in the pre-veto normalization agree with the MC prediction (the small rare MC component is held fixed). Then, the dilepton background prediction is obtained by multiplying the dilepton BG Monte Carlo by SF_{pre} .

The $t\bar{t}$ lepton + jet BG is normalized to post-veto normalization region. A post-veto scale factor (SF_{post}) is defined in (almost) the same way as the pre-veto scale factor. The difference here is that this scale factor applies only to the lepton + jets components and not the dilepton component, since that component is already rescaled by SF_{pre} . This procedure minimizes the reliance on the understanding of the isolated track veto. Then the $t\bar{t}$ lepton + jet BG is obtained by taking the number of MC-predicted $t\bar{t}$ lepton + jets in the post-veto normalization region, scaling it by SF_{post} , multiplying it by the tail-to-peak ratio R_{top} of Table 20, and finally the data-MC scale factor SFR_{top} from Table 14.

The single top background is obtained in exactly the same way as the $t\bar{t}$ lepton + jet BG, using the same tail-to-peak ratio and the same data-MC scale-factor. The W background is done in a similar way, but using a different tail-to-peak ratio (R_{wjets} of Table 20), and a different data-MC scale factor (SFR_{wjet} from Table 13).

Other (small) backgrounds are taken straight from Monte Carlo, as described in Section 6.

Sample	SRA	SRB	SRC	SRD	SRE	SRF	SRG
		Muon					
${ m tar t} o \ell\ell$	371 ± 6	120 ± 4	43 ± 2	17 ± 1	8 ± 1	4 ± 1	1 ± 0
$t\bar{t} \to \ell + jets \& single top (1\ell)$	3666 ± 21	1088 ± 12	355 ± 7	127 ± 4	50 ± 3	22 ± 2	8 ± 1
W+jets	316 ± 8	113 ± 5	46 ± 3	21 ± 2	11 ± 1	5 ± 1	2 ± 1
Rare	117 ± 5	48 ± 3	16 ± 2	6 ± 1	2 ± 1	1 ± 0	1 ± 0
Total	4470 ± 24	1369 ± 13	461 ± 8	171 ± 5	71 ± 3	33 ± 2	13 ± 1
Data	4538	1304	418	168	69	28	12
		Electron					
$t\bar{t} o \ell\ell$	290 ± 6	98 ± 3	35 ± 2	13 ± 1	6 ± 1	3 ± 1	1 ± 0
$t\bar{t} \to \ell + \text{jets \& single top } (1\ell)$	2899 ± 19	861 ± 10	282 ± 6	104 ± 4	42 ± 2	16 ± 2	8 ± 1
W+jets	252 ± 28	87 ± 4	35 ± 3	18 ± 2	8 ± 1	4 ± 1	2 ± 1
Rare	89 ± 5	34 ± 3	15 ± 2	7 ± 1	3 ± 1	0 ± 0	0 ± 0
Total	3530 ± 35	1079 ± 12	367 ± 7	142 ± 5	60 ± 3	24 ± 2	11 ± 1
Data	3358	1022	346	122	51	25	12
	Muor	+Electron C	Combined				
$t \bar t o \ell \ell$	661 ± 9	218 ± 5	78 ± 3	30 ± 2	14 ± 1	7 ± 1	3 ± 1
$t\bar{t} \to \ell + \text{jets \& single top } (1\ell)$	6565 ± 28	1949 ± 16	637 ± 9	231 ± 5	92 ± 4	39 ± 2	16 ± 2
W+jets	568 ± 29	199 ± 6	81 ± 4	38 ± 3	19 ± 2	9 ± 1	4 ± 1
Rare	206 ± 7	82 ± 4	31 ± 3	14 ± 2	5 ± 1	2 ± 0	1 ± 0
Total	8000 ± 42	2448 ± 18	828 ± 11	314 ± 7	131 ± 4	56 ± 3	24 ± 2
Data	7896	2326	764	290	120	53	24

Table 21: Preveto MC and data yields in $M_{\rm T}$ peak region. The n-jets k-factors have been applied to the $t\bar{t} \to \ell\ell$. The uncertainties are statistical only.

Sample	SRA	SRB	SRC	SRD	SRE	SRF	SRG
		Muon					
$\overline{\mathrm{t}} \overline{\mathrm{t}} o \ell \ell$	139 ± 4	46 ± 2	16 ± 1	7 ± 1	3 ± 1	1 ± 0	1 ± 0
$t\bar{t} \to \ell + jets \& single top (1\ell)$	3273 ± 20	974 ± 11	321 ± 6	113 ± 4	45 ± 2	21 ± 2	8 ± 1
W+jets	294 ± 8	105 ± 5	42 ± 3	19 ± 2	10 ± 1	5 ± 1	2 ± 1
Rare	83 ± 4	34 ± 3	11 ± 1	4 ± 1	2 ± 1	1 ± 0	1 ± 0
Total	3789 ± 22	1160 ± 12	391 ± 7	143 ± 4	60 ± 3	28 ± 2	11 ± 1
Data	3790	1098	358	143	59	24	11
		Electron					
$\overline{\mathrm{t}} \overline{\mathrm{t}} o \ell \ell$	116 ± 4	40 ± 2	14 ± 1	5 ± 1	2 ± 0	1 ± 0	1 ± 0
$t\bar{t} \to \ell + jets \& single top (1\ell)$	2595 ± 18	774 ± 10	258 ± 6	97 ± 4	40 ± 2	15 ± 1	7 ± 1
W+jets	236 ± 28	82 ± 4	33 ± 3	17 ± 2	8 ± 1	4 ± 1	2 ± 1
Rare	62 ± 4	23 ± 2	9 ± 1	4 ± 1	2 ± 1	0 ± 0	0 ± 0
Total	3009 ± 34	919 ± 11	315 ± 7	123 ± 4	51 ± 3	21 ± 2	10 ± 1
Data	2788	837	288	92	39	19	10
	Muor	+Electron (Combined				
$\overline{\mathrm{t}} \overline{\mathrm{t}} o \ell \ell$	255 ± 5	86 ± 3	30 ± 2	12 ± 1	5 ± 1	2 ± 1	1 ± 0
$t\bar{t} \to \ell + jets \& single top (1\ell)$	5869 ± 27	1747 ± 15	579 ± 9	209 ± 5	85 ± 3	36 ± 2	15 ± 2
W+jets	529 ± 29	188 ± 6	75 ± 4	36 ± 3	18 ± 2	9 ± 1	4 ± 1
Rare	145 ± 6	58 ± 4	21 ± 2	8 ± 1	3 ± 1	1 ± 0	1 ± 0
Total	6797 ± 40	2079 ± 17	705 ± 10	265 ± 6	111 ± 4	49 ± 3	21 ± 2
Data	6578	1935	646	235	98	43	21

Table 22: MC and data yields in M_T peak region after full selection. The n-jets k-factors have been applied to the $t\bar{t} \to \ell\ell$. The uncertainties are statistical only.

Sample	SRA	SRB	SRC	SRD	SRE	SRF	SRG
		Muon					
${ m tar t} o \ell\ell$	326 ± 6	193 ± 5	66 ± 3	23 ± 2	9 ± 1	4 ± 1	2 ± 1
$t\bar{t} \to \ell + jets \& single top (1\ell)$	54 ± 3	38 ± 2	8 ± 1	3 ± 1	1 ± 1	1 ± 0	0 ± 0
W+jets	17 ± 2	8 ± 1	3 ± 1	2 ± 1	0 ± 0	0 ± 0	0 ± 0
Rare	33 ± 2	23 ± 2	9 ± 1	5 ± 1	3 ± 1	1 ± 0	1 ± 0
Total	430 ± 7	262 ± 6	86 ± 3	33 ± 2	14 ± 1	6 ± 1	4 ± 1
		Electron					
$t\bar{t} o \ell\ell$	261 ± 5	153 ± 4	54 ± 2	19 ± 1	7 ± 1	2 ± 1	1 ± 0
$t\bar{t} \to \ell + jets \& single top (1\ell)$	41 ± 2	28 ± 2	7 ± 1	3 ± 1	1 ± 0	1 ± 0	1 ± 0
W+jets	11 ± 2	7 ± 1	3 ± 1	2 ± 1	0 ± 0	0 ± 0	0 ± 0
Rare	26 ± 2	16 ± 2	7 ± 1	3 ± 1	1 ± 0	0 ± 0	0 ± 0
Total	340 ± 6	204 ± 5	71 ± 3	26 ± 2	8 ± 1	4 ± 1	2 ± 1
	Muon+l	Electron C	ombined				
$t\bar{t} o \ell\ell$	587 ± 8	346 ± 6	120 ± 4	42 ± 2	16 ± 1	7 ± 1	4 ± 1
$t\bar{t} \to \ell + jets \& single top (1\ell)$	95 ± 3	67 ± 3	15 ± 1	6 ± 1	2 ± 1	1 ± 1	1 ± 0
W+jets	29 ± 2	15 ± 2	6 ± 1	3 ± 1	1 ± 0	0 ± 0	0 ± 0
Rare	59 ± 3	38 ± 3	16 ± 2	8 ± 1	4 ± 1	2 ± 0	1 ± 0
Total	770 ± 10	466 ± 7	157 ± 4	59 ± 3	22 ± 2	10 ± 1	6 ± 1

Table 23: MC yields in $M_{\rm T}$ tail region after full selection. The n-jets k-factors have been applied to the $t\bar{t} \to \ell\ell$. The uncertainties are statistical only. Note these values are only used for the rare backgrounds prediction.

Sample	SRA	SRB	SRC	SRD	SRE	SRF	SRG
μ pre-veto $M_{\rm T}$ -SF	1.02 ± 0.02	0.95 ± 0.03	0.90 ± 0.05	0.98 ± 0.08	0.97 ± 0.13	0.85 ± 0.18	0.92 ± 0.31
μ post-veto $M_{\mathrm{T}}\text{-SF}$	1.00 ± 0.02	0.95 ± 0.03	0.91 ± 0.05	1.00 ± 0.09	0.99 ± 0.13	0.85 ± 0.18	0.96 ± 0.31
μ veto $M_{\mathrm{T}}\text{-SF}$	0.98 ± 0.01	0.99 ± 0.01	1.01 ± 0.02	1.02 ± 0.04	1.02 ± 0.06	1.00 ± 0.09	1.04 ± 0.11
e pre-veto $M_{\rm T}$ -SF	0.95 ± 0.02	0.95 ± 0.03	0.94 ± 0.06	0.85 ± 0.09	0.84 ± 0.13	1.05 ± 0.23	1.04 ± 0.33
e post-veto $M_{\mathrm{T}}\text{-SF}$	0.92 ± 0.02	0.91 ± 0.03	0.91 ± 0.06	0.74 ± 0.08	0.75 ± 0.13	0.91 ± 0.22	1.01 ± 0.33
e veto $M_{\mathrm{T}}\text{-SF}$	0.97 ± 0.01	0.96 ± 0.02	0.97 ± 0.03	0.87 ± 0.05	0.89 ± 0.08	0.86 ± 0.11	0.97 ± 0.14

Table 24: $M_{\rm T}$ peak Data/MC scale factors. The pre-veto SFs are applied to the ${\rm t\bar{t}} \to \ell\ell$ sample, while the post-veto SFs are applied to the single lepton samples. The veto SF is shown for comparison across channels. The raw MC is used for backgrounds from rare processes. The uncertainties are statistical only.

9 Systematic Uncertainties on the Background

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DESCRIBE HERE ONE BY ONE THE UNCERTAINTIES THAT ARE PRESENT IN THE SPREADSHHET FROM WHICH WE CALCULATE THE TOTAL UNCERTAINTY. WE KNOW HOW TO DO
THIS AND WE HAVE THE TECHNOLOGY FROM THE 7 TEV ANALYSIS TO PROPAGATE ALL
UNCERTAINTIES CORRECTLY THROUGH. WE WILL DO IT ONCE WE HAVE SETTLED ON
THE INDIVIDUAL PIECES WHICH ARE STILL IN FLUX

In this Section we discuss the systematic uncertainty on the BG prediction. This prediction is assembled from the event counts in the peak region of the transverse mass distribution as well as Monte Carlo with a number of correction factors, as described previously. The final uncertainty on the prediction is built up from the uncertainties in these individual components. The calculation is done for each signal region, for electrons and muons separately.

The choice to normalizing to the peak region of M_T has the advantage that some uncertainties, e.g., 380 luminosity, cancel. It does however introduce complications because it couples some of the uncertainties 381 in non-trivial ways. For example, the primary effect of an uncertainty on the rare MC cross-section is 382 to introduce an uncertainty in the rare MC background estimate which comes entirely from MC. But 383 this uncertainty also affects, for example, the $tt \to dilepton BG$ estimate because it changes the tt384 normalization to the peak region (because some of the events in the peak region are from rare processes). These effects are carefully accounted for. The contribution to the overall uncertainty from each BG source 386 is tabulated in Section 9.8. First, however, we discuss the uncertainties one-by-one and we comment on their impact on the overall result, at least to first order. Second order effects, such as the one described, 388 are also included.

9.1 Statistical uncertainties on the event counts in the M_T peak regions

These vary between XX and XX %, depending on the signal region (different signal regions have different $E_{\rm T}^{\rm miss}$ requirements, thus they also have different M_T regions used as control. Since the major BG, eg, $t\bar{t}$ are normalized to the peak regions, this fractional uncertainty is pretty much carried through all the way to the end. There is also an uncertainty from the finite MC event counts in the M_T peak regions. This is also included, but it is smaller.

$_{6}$ 9.2 Uncertainty from the choice of M_{T} peak region

IN 7 TEV DATA WE HAD SOME SHAPE DIFFERENCES IN THE MTRANS REGION THAT LED
 US TO CONSERVATIVELY INCLUDE THIS UNCERTAINTY. WE NEED TO LOOK INTO THIS
 AGAIN

9.3 Uncertainty on the Wjets cross-section and the rare MC cross-sections

These are taken as 50%, uncorrelated. The primary effect is to introduce a 50% uncertainty on the W+ jets and rare BG background predictions, respectively. However they also have an effect on the other BGs via the M_T peak normalization in a way that tends to reduce the uncertainty. This is easy to understand: if the W cross-section is increased by 50%, then the W background goes up. But the number of M_T peak events attributed to $t\bar{t}$ goes down, and since the $t\bar{t}$ BG is scaled to the number of $t\bar{t}$ events in the peak, the $t\bar{t}$ BG goes down.

$_{407}$ 9.4 Scale factors for the tail-to-peak ratios for lepton + jets top and W events

These tail-to-peak ratios are described in Section 7. They are studied in CR1 and CR2. The studies are described in Sections 5.1 and 5.2), respectively, where we also give the uncertainty on the scale factors.

9.5 Uncertainty on extra jet radiation for dilepton background

As discussed in Section 5.3.1, the jet distribution in $t\bar{t} \to \text{dilepton MC}$ is rescaled by the factors K_3 and K_4 to make it agree with the data. The XX% uncertainties on K_3 and K_4 comes from data/MC statistics. This result directly in a XX% uncertainty on the dilepton BG, which is by far the most important one.

9.6 Uncertainty on the $t\bar{t} \to \ell\ell$ Acceptance

The tt background prediction is obtained from MC, with corrections derived from control samples in data. The uncertainty associated with the theoretical modeling of the tt production and decay is estimated by comparing the background predictions obtained using alternative MC samples. It should be noted that the full analysis is performed with the alternative samples under consideration, including the derivation of the various data-to-MC scale factors. The variations considered are

- Top mass: The alternative values for the top mass differ from the central value by 5 GeV: $m_{\text{top}} = 178.5 \text{ GeV}$ and $m_{\text{top}} = 166.5 \text{ GeV}$.
- Jet-parton matching scale: This corresponds to variations in the scale at which the Matrix Element partons from Madgraph are matched to Parton Shower partons from Pythia. The nominal value is $x_q > 20$ GeV. The alternative values used are $x_q > 10$ GeV and $x_q > 40$ GeV.
- Renormalization and factorization scale: The alternative samples correspond to variations in the scale $\times 2$ and $\times 0.5$. The nominal value for the scale used is $Q^2 = m_{\text{top}}^2 + \sum_{\text{iets}} p_{\text{T}}^2$.
- Alternative generators: Samples produced with different generators include MC@NLO and Powheg (NLO generators) and Pythia (LO). It may also be noted that MC@NLO uses Herwig6 for the hadronisation, while POWHEG uses Pythia6.
- Modeling of taus: The alternative sample does not include Tauola and is otherwise identical to the Powheg sample. This effect was studied earlier using 7 TeV samples and found to be negligible.
- The PDF uncertainty is estimated following the PDF4LHC recommendations[CITE]. The events are reweighted using alternative PDF sets for CT10 and MSTW2008 and the uncertainties for each are derived using the alternative eigenvector variations and the "master equation". In addition, the NNPDF2.1 set with 100 replicas. The central value is determined from the mean and the uncertainty is derived from the 1σ range. The overall uncertainty is derived from the envelope of the alternative predictions and their uncertainties. This effect was studied earlier using 7 TeV samples and found to be negligible.

Sample	Powheg	Madgraph	Mass Up	Mass Down	Scale Up	Scale Down	Match Up	Match Down
SRA	579 ± 10	569 ± 16	591 ± 18	610 ± 22	651 ± 22	537 ± 16	578 ± 18	570 ± 17
SRB	328 ± 7	307 ± 11	329 ± 13	348 ± 15	344 ± 15	287 ± 10	313 ± 13	307 ± 12
SRC	111 ± 4	99 ± 5	107 ± 7	113 ± 8	124 ± 8	95 ± 6	93 ± 6	106 ± 6
SRD	39 ± 2	35 ± 3	41 ± 4	41 ± 5	47 ± 5	33 ± 3	31 ± 3	39 ± 4
SRE	14 ± 1	15 ± 2	17 ± 3	12 ± 3	15 ± 3	13 ± 2	12 ± 2	16 ± 2

Table 25: $t\bar{t} \to \ell\ell$ predictions for alternative MC samples. The uncertainties are statistical only.

Δ/N [%]	Madgraph	Mass Up	Mass Down	Scale Up	Scale Down	Match Up	Match Down
SRA	2	2	5	12	7	0	2
SRB	6	0	6	5	12	5	6
SRC	10	3	2	12	14	16	4
SRD	10	6	6	21	15	19	0
SRE	6	17	15	2	12	17	8

Table 26: Relative difference in $t\bar{t} \to \ell\ell$ predictions for alternative MC samples.

$N\sigma$	Madgraph	Mass Up	Mass Down	Scale Up	Scale Down	Match Up	Match Down
SRA	0.38	0.42	1.02	2.34	1.58	0.01	0.33
SRB	1.17	0.07	0.98	0.76	2.29	0.78	1.11
SRC	1.33	0.37	0.26	1.24	1.82	1.97	0.54
SRD	0.82	0.46	0.38	1.32	1.27	1.47	0.00
SRE	0.32	0.75	0.66	0.07	0.66	0.83	0.38

Table 27: N σ difference in $t\bar{t}\to\ell\ell$ predictions for alternative MC samples.

Av. Δ Evt.	Alt. Gen.	Δ Mass	Δ Scale	Δ Match
SRA	5.0 (1%)	9.6 (2%)	56.8 (10%)	4.4 (1%)
SRB	10.4 (3%)	9.6 (3%)	28.2 (9%)	2.8 (1%)
SRC	5.7 (5%)	3.1 (3%)	14.5 (13%)	6.4 (6%)
SRD	1.9 (5%)	0.1 (0%)	6.9 (18%)	3.6 (9%)
SRE	0.5 (3%)	2.3 (16%)	1.0 (7%)	1.8 (12%)

Table 28: Av. difference in $t\bar{t}\to\ell\ell$ events for alternative sample pairs.

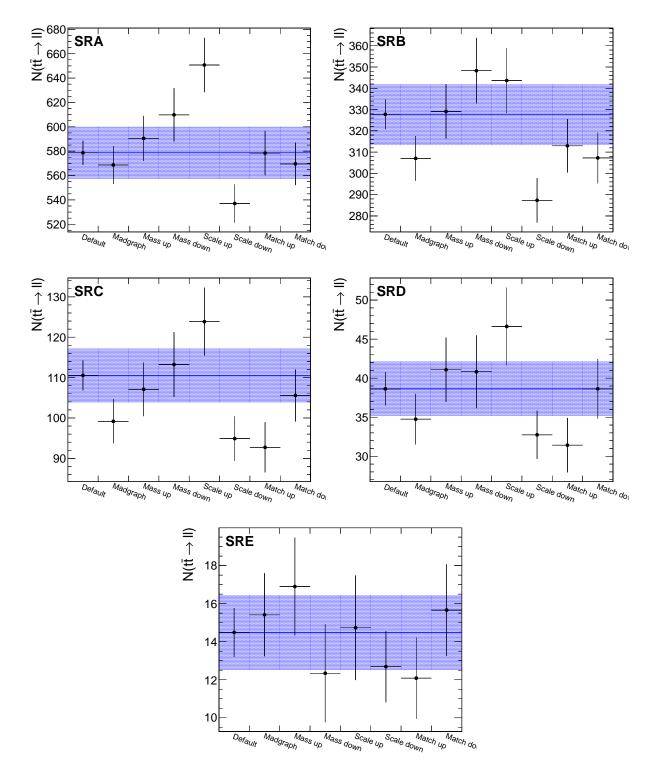


Figure 16: Comparison of the $t\bar{t}\to\ell\ell$ central prediction with those using alternative MC samples. The blue band corresponds to the total statistical error for all data and MC samples. The alternative sample predictions are indicated by the datapoints. The uncertainties on the alternative predictions correspond to the uncorrelated statistical uncertainty from the size of the alternative sample only. [TO BE UPDATED WITH THE LATEST SELECTION AND SFS]

9.7 Uncertainty from the isolated track veto

This is the uncertainty associated with how well the isolated track veto performance is modeled by the Monte Carlo. This uncertainty only applies to the fraction of dilepton BG events that have a second e/ μ or a one prong $\tau \to h$, with $P_T > 10$ GeV in $|\eta| < 2.4$. This fraction is 1/3 (THIS WAS THE 7 TEV NUMBER, CHECK). The uncertainty for these events is XX% and is obtained from Tag and Probe studies of Section 9.7.1

9.7.1 Isolated Track Veto: Tag and Probe Studies

⁴⁴⁶ [EVERYTHING IS 7TEV HERE, UPDATE WITH NEW RESULTS

ADD TABLE WITH FRACTION OF EVENTS THAT HAVE A TRUE ISOLATED TRACK]

Sample	SRA	SRB	SRC	SRD	SRE	SRF	SRG
μ Frac. $t\bar{t} \to \ell\ell$ with true iso. trk.	0.32 ± 0.03	0.30 ± 0.03	0.32 ± 0.06	0.34 ± 0.10	0.35 ± 0.16	0.40 ± 0.24	0.50 ± 0.32
e Frac. $t\bar{t} \to \ell\ell$ with true iso. trk.	0.32 ± 0.03	0.31 ± 0.04	0.33 ± 0.06	0.38 ± 0.11	0.38 ± 0.19	0.60 ± 0.31	0.61 ± 0.45

Table 29: Fraction of $t\bar{t} \to \ell\ell$ events with a true isolated track.

In this section we compare the performance of the isolated track veto in data and MC using tag-andprobe studies with samples of $Z\rightarrow ee$ and $Z\rightarrow \mu\mu$. The purpose of these studies is to demonstrate that the efficiency to satisfy the isolated track veto requirements is well-reproduced in the MC, since if this were not the case we would need to apply a data-to-MC scale factor in order to correctly predict the $t\bar{t} \to \ell\ell$ background. This study addresses possible data vs. MC discrepancies for the efficiency to identify (and reject) events with a second **genuine** lepton (e, μ , or $\tau \to 1$ -prong). It does not address possible data vs. MC discrepancies in the fake rate for rejecting events without a second genuine lepton; this is handled separately in the top normalization procedure by scaling the $t\bar{t} \to \ell + jets$ contribution to match the data in the $M_{\rm T}$ peak after applying the isolated track veto. Furthermore, we test the data and MC isolated track veto efficiencies for electrons and muons since we are using a Z tag-and-probe technique, but we do not directly test the performance for hadronic tracks from τ decays. The performance for hadronic τ decay products may differ from that of electrons and muons for two reasons. First, the τ may decay to a hadronic track plus one or two π^0 's, which may decay to $\gamma\gamma$ followed by a photon conversion. As shown in Figure 19, the isolation distribution for charged tracks from τ decays that are not produced in association with π^0 s are consistent with that from es and μ s. Since events from single prong τ decays produced in association with π^0 s comprise a small fraction of the total sample, and since the kinematics of τ , π^0 and $\gamma \to e^+e^-$ decays are well-understood, we currently demonstrate that the isolation is well-reproduced for electrons and muons only. Second, hadronic tracks may undergo nuclear interactions and hence their tracks may not be reconstructed. As discussed above, independent studies show that the MC reproduces the hadronic tracking efficiency within 4%, leading to a total background uncertainty of less than 0.5% (after taking into account the fraction of the total background due to hadronic τ decays with $p_T > 10$ GeV tracks), and we hence regard this effect as negligible.

The tag-and-probe studies are performed in the full 2011 data sample, and compared with the DYJets madgraph sample. All events must contain a tag-probe pair (details below) with opposite-sign and satisfying the Z mass requirement 76–106 GeV. We compare the distributions of absolute track isolation for probe electrons/muons in data vs. MC. The contributions to this isolation sum are from ambient energy in the event from underlying event, pile-up and jet activitiy, and hence do not depend on the $p_{\rm T}$ of the probe lepton. We therefore restrict the probe $p_{\rm T}$ to be > 30 GeV in order to suppress fake backgrounds with steeply-falling $p_{\rm T}$ spectra. To suppress non-Z backgrounds (in particular $t\bar{t}$) we require $E_{\rm T}^{\rm miss} <$ 30 GeV and 0 b-tagged events. The specific criteria for tags and probes for electrons and muons are:

• Electrons

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- Tag criteria
 - * Electron passes full analysis ID/iso selection
- * $p_{\rm T} > 30 \; {\rm GeV}, |\eta| < 2.1$
 - * Matched to the single electron trigger HLT_Ele27_WP80_v*

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- Probe criteria
484
                   * Electron passes full analysis ID selection
485
                   * p_{\rm T} > 30 {\rm ~GeV}
486
        • Muons
487
              - Tag criteria
488
                   * Muon passes full analysis ID/iso selection
489
                   * p_{\rm T} > 30 \; {\rm GeV}, |\eta| < 2.1
490
                   * Matched to 1 of the 2 single muon triggers
491
                        · HLT_IsoMu30_v*
492
                        · HLT_IsoMu30_eta2p1_v*
493
              - Probe criteria
                   * Muon passes full analysis ID selection
                   * p_{\rm T} > 30 \; {\rm GeV}
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The absolute track isolation distributions for passing probes are displayed in Fig. 17. In general we observe good agreement between data and MC. To be more quantitative, we compare the data vs. MC efficiencies to satisfy absolute track isolation requirements varying from > 1 GeV to > 5 GeV, as summarized in Table 30. In the ≥ 0 and ≥ 1 jet bins where the efficiencies can be tested with statistical precision, the data and MC efficiencies agree within 6%, and we apply this as a systematic uncertainty on the isolated track veto efficiency. For the higher jet multiplicity bins the statistical precision decreases, but we do not observe any evidence for a data vs. MC discrepancy in the isolated track veto efficiency.

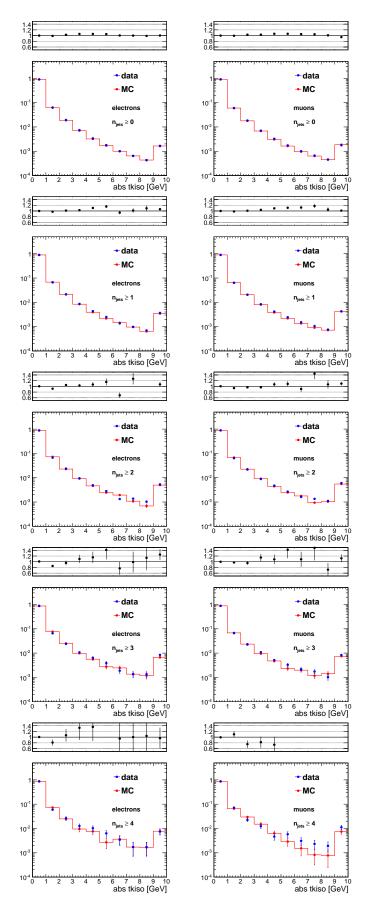


Figure 17: Comparison of the absolute track isolation in data vs. MC for electrons (left) and muons (right) for events with the $N_{\rm jets}$ requirement varied from $N_{\rm jets} \geq 0$ to $N_{\rm jets} \geq 4$.

Table 30: Comparison of the data vs. MC efficiencies to satisfy the indicated requirements on the absolute track isolation, and the ratio of these two efficiencies. Results are indicated separately for electrons and muons and for various jet multiplicity requirements.

	> 1 GeV	> 2 GeV	> 3 GeV	> 4 GeV	> 5 GeV
$e + \ge 0$ jets	0.098 ± 0.0002	0.036 ± 0.0001	0.016 ± 0.0001	0.009 ± 0.0001	0.006 ± 0.0000
data	0.098 ± 0.0002 0.097 ± 0.0002	0.030 ± 0.0001 0.034 ± 0.0001	0.016 ± 0.0001 0.016 ± 0.0001	0.009 ± 0.0001 0.009 ± 0.0001	0.000 ± 0.0000 0.005 ± 0.0000
$^{ m mc}_{ m data/mc}$	0.097 ± 0.0002 1.00 ± 0.00	1.04 ± 0.001	1.04 ± 0.001	1.03 ± 0.001	1.02 ± 0.000
$\mu + \ge 0$ jets	> 1 GeV	> 2 GeV	> 3 GeV	> 4 GeV	> 5 GeV
data	0.094 ± 0.0001	0.034 ± 0.0001	0.016 ± 0.0001	0.009 ± 0.0000	0.006 ± 0.0000
mc	0.093 ± 0.0001	0.033 ± 0.0001	0.015 ± 0.0001	0.009 ± 0.0000	0.006 ± 0.0000
data/mc	1.01 ± 0.00	1.03 ± 0.00	1.03 ± 0.01	1.03 ± 0.01	1.02 ± 0.01
$e + \ge 1 \text{ jets}$	> 1 GeV	> 2 GeV	> 3 GeV	> 4 GeV	> 5 GeV
data	0.110 ± 0.0005	0.044 ± 0.0003	0.022 ± 0.0002	0.014 ± 0.0002	0.009 ± 0.0002
mc	0.110 ± 0.0005	0.042 ± 0.0003	0.021 ± 0.0002	0.013 ± 0.0002	0.009 ± 0.0001
data/mc	1.00 ± 0.01	1.04 ± 0.01	1.06 ± 0.02	1.08 ± 0.02	1.06 ± 0.03
$\mu + \ge 1$ jets	> 1 GeV	> 2 GeV	> 3 GeV	> 4 GeV	> 5 GeV
data	0.106 ± 0.0004	0.043 ± 0.0003	0.023 ± 0.0002	0.014 ± 0.0002	0.010 ± 0.0001
mc	0.106 ± 0.0004	0.042 ± 0.0003	0.021 ± 0.0002	0.013 ± 0.0002	0.009 ± 0.0001
data/mc	1.00 ± 0.01	1.04 ± 0.01	1.06 ± 0.01	1.08 ± 0.02	1.07 ± 0.02
$e + \ge 2 \text{ jets}$	> 1 GeV	> 2 GeV	> 3 GeV	> 4 GeV	> 5 GeV
data	0.117 ± 0.0012	0.050 ± 0.0008	0.026 ± 0.0006	0.017 ± 0.0005	0.012 ± 0.0004
mc	0.120 ± 0.0012	0.048 ± 0.0008	0.025 ± 0.0006	0.016 ± 0.0005	0.011 ± 0.0004
data/mc	0.97 ± 0.01	1.05 ± 0.02	1.05 ± 0.03	1.07 ± 0.04	1.07 ± 0.05
	1 0 77	2 2 7 7	0.017	. ~	F 01 TT
$\mu + \geq 2 \text{ jets}$	> 1 GeV	> 2 GeV	> 3 GeV	> 4 GeV	> 5 GeV
$\frac{\mu + \geq 2 \text{ jets}}{\text{data}}$	0.111 ± 0.0010	0.048 ± 0.0007	0.026 ± 0.0005	0.018 ± 0.0004	0.013 ± 0.0004
data mc	$\begin{array}{c} 0.111 \pm 0.0010 \\ 0.115 \pm 0.0010 \end{array}$	$\begin{array}{c} 0.048 \pm 0.0007 \\ 0.048 \pm 0.0006 \end{array}$	$\begin{array}{c} 0.026 \pm 0.0005 \\ 0.025 \pm 0.0005 \end{array}$	$\begin{array}{c} 0.018 \pm 0.0004 \\ 0.016 \pm 0.0004 \end{array}$	$\begin{array}{c} 0.013 \pm 0.0004 \\ 0.012 \pm 0.0003 \end{array}$
data	0.111 ± 0.0010	0.048 ± 0.0007	0.026 ± 0.0005	0.018 ± 0.0004	0.013 ± 0.0004
data mc	$\begin{array}{c} 0.111 \pm 0.0010 \\ 0.115 \pm 0.0010 \\ 0.97 \pm 0.01 \\ \hline > 1 \ {\rm GeV} \end{array}$	0.048 ± 0.0007 0.048 ± 0.0006 1.01 ± 0.02 > 2 GeV	0.026 ± 0.0005 0.025 ± 0.0005 1.04 ± 0.03 > 3 GeV	0.018 ± 0.0004 0.016 ± 0.0004 1.09 ± 0.04 > 4 GeV	0.013 ± 0.0004 0.012 ± 0.0003 1.09 ± 0.04 > 5 GeV
data mc data/mc	$\begin{array}{c} 0.111 \pm 0.0010 \\ 0.115 \pm 0.0010 \\ 0.97 \pm 0.01 \end{array}$	$0.048 \pm 0.0007 \\ 0.048 \pm 0.0006 \\ 1.01 \pm 0.02$	$0.026 \pm 0.0005 \\ 0.025 \pm 0.0005 \\ 1.04 \pm 0.03$	$0.018 \pm 0.0004 \\ 0.016 \pm 0.0004 \\ 1.09 \pm 0.04$	$0.013 \pm 0.0004 \\ 0.012 \pm 0.0003 \\ 1.09 \pm 0.04$
$\begin{array}{c} \mathrm{data} \\ \mathrm{mc} \\ \mathrm{data/mc} \\ \mathrm{e} + \geq 3 \; \mathrm{jets} \\ \mathrm{data} \\ \mathrm{mc} \end{array}$	$\begin{array}{c} 0.111 \pm 0.0010 \\ 0.115 \pm 0.0010 \\ 0.97 \pm 0.01 \\ \hline > 1 \text{ GeV} \\ 0.123 \pm 0.0031 \\ 0.131 \pm 0.0030 \\ \end{array}$	$\begin{array}{c} 0.048 \pm 0.0007 \\ 0.048 \pm 0.0006 \\ 1.01 \pm 0.02 \\ \\ > 2 \text{ GeV} \\ 0.058 \pm 0.0022 \\ 0.055 \pm 0.0020 \end{array}$	$\begin{array}{c} 0.026 \pm 0.0005 \\ 0.025 \pm 0.0005 \\ 1.04 \pm 0.03 \\ \\ > 3 \text{ GeV} \\ 0.034 \pm 0.0017 \\ 0.030 \pm 0.0015 \end{array}$	$\begin{array}{c} 0.018 \pm 0.0004 \\ 0.016 \pm 0.0004 \\ 1.09 \pm 0.04 \\ \hline > 4 \text{ GeV} \\ 0.023 \pm 0.0014 \\ 0.020 \pm 0.0013 \end{array}$	$\begin{array}{c} 0.013 \pm 0.0004 \\ 0.012 \pm 0.0003 \\ 1.09 \pm 0.04 \\ \hline > 5 \text{ GeV} \\ 0.017 \pm 0.0012 \\ 0.015 \pm 0.0011 \end{array}$
$\begin{array}{c} \text{data} \\ \text{mc} \\ \text{data/mc} \\ \hline \text{e} + \geq 3 \text{ jets} \\ \text{data} \end{array}$	$\begin{array}{c} 0.111 \pm 0.0010 \\ 0.115 \pm 0.0010 \\ 0.97 \pm 0.01 \\ \hline > 1 \text{ GeV} \\ 0.123 \pm 0.0031 \end{array}$	$\begin{array}{c} 0.048 \pm 0.0007 \\ 0.048 \pm 0.0006 \\ 1.01 \pm 0.02 \\ \hline > 2 \text{ GeV} \\ 0.058 \pm 0.0022 \end{array}$	$\begin{array}{c} 0.026 \pm 0.0005 \\ 0.025 \pm 0.0005 \\ 1.04 \pm 0.03 \\ \hline > 3 \text{ GeV} \\ 0.034 \pm 0.0017 \end{array}$	$0.018 \pm 0.0004 0.016 \pm 0.0004 1.09 \pm 0.04 > 4 GeV 0.023 \pm 0.0014$	$\begin{array}{c} 0.013 \pm 0.0004 \\ 0.012 \pm 0.0003 \\ 1.09 \pm 0.04 \\ \hline > 5 \text{ GeV} \\ 0.017 \pm 0.0012 \end{array}$
$\begin{array}{c} \mathrm{data} \\ \mathrm{mc} \\ \mathrm{data/mc} \\ \mathrm{e} + \geq 3 \; \mathrm{jets} \\ \mathrm{data} \\ \mathrm{mc} \end{array}$	$\begin{array}{c} 0.111 \pm 0.0010 \\ 0.115 \pm 0.0010 \\ 0.97 \pm 0.01 \\ \hline > 1 \text{ GeV} \\ 0.123 \pm 0.0031 \\ 0.131 \pm 0.0030 \\ 0.94 \pm 0.03 \\ \hline > 1 \text{ GeV} \\ \end{array}$	$\begin{array}{c} 0.048 \pm 0.0007 \\ 0.048 \pm 0.0006 \\ 1.01 \pm 0.02 \\ \hline > 2 \text{ GeV} \\ 0.058 \pm 0.0022 \\ 0.055 \pm 0.0020 \\ 1.06 \pm 0.06 \\ \hline > 2 \text{ GeV} \end{array}$	$\begin{array}{c} 0.026 \pm 0.0005 \\ 0.025 \pm 0.0005 \\ 1.04 \pm 0.03 \\ \hline > 3 \text{ GeV} \\ 0.034 \pm 0.0017 \\ 0.030 \pm 0.0015 \\ 1.14 \pm 0.08 \\ \hline > 3 \text{ GeV} \\ \end{array}$	$\begin{array}{c} 0.018 \pm 0.0004 \\ 0.016 \pm 0.0004 \\ 1.09 \pm 0.04 \\ \hline > 4 \text{ GeV} \\ 0.023 \pm 0.0014 \\ 0.020 \pm 0.0013 \\ 1.16 \pm 0.10 \\ \hline > 4 \text{ GeV} \end{array}$	$\begin{array}{c} 0.013 \pm 0.0004 \\ 0.012 \pm 0.0003 \\ 1.09 \pm 0.04 \\ \hline > 5 \text{ GeV} \\ 0.017 \pm 0.0012 \\ 0.015 \pm 0.0011 \\ 1.17 \pm 0.12 \\ \hline > 5 \text{ GeV} \end{array}$
$\begin{array}{c} \operatorname{data} \\ \operatorname{mc} \\ \operatorname{data/mc} \\ \end{array}$ $\begin{array}{c} \operatorname{e} + \geq 3 \ \operatorname{jets} \\ \operatorname{data} \\ \operatorname{mc} \\ \operatorname{data/mc} \end{array}$	$\begin{array}{c} 0.111 \pm 0.0010 \\ 0.115 \pm 0.0010 \\ 0.97 \pm 0.01 \\ \hline > 1 \ \mathrm{GeV} \\ 0.123 \pm 0.0031 \\ 0.131 \pm 0.0030 \\ 0.94 \pm 0.03 \\ \hline > 1 \ \mathrm{GeV} \\ 0.121 \pm 0.0025 \\ \hline \end{array}$	$\begin{array}{c} 0.048 \pm 0.0007 \\ 0.048 \pm 0.0006 \\ 1.01 \pm 0.02 \\ \\ > 2 \ \mathrm{GeV} \\ 0.058 \pm 0.0022 \\ 0.055 \pm 0.0020 \\ 1.06 \pm 0.06 \\ \\ > 2 \ \mathrm{GeV} \\ 0.055 \pm 0.0018 \\ \end{array}$	$\begin{array}{c} 0.026 \pm 0.0005 \\ 0.025 \pm 0.0005 \\ 1.04 \pm 0.03 \\ \hline > 3 \text{ GeV} \\ 0.034 \pm 0.0017 \\ 0.030 \pm 0.0015 \\ 1.14 \pm 0.08 \\ \hline > 3 \text{ GeV} \\ 0.033 \pm 0.0014 \\ \hline \end{array}$	$\begin{array}{c} 0.018 \pm 0.0004 \\ 0.016 \pm 0.0004 \\ 1.09 \pm 0.04 \\ \hline > 4 \ GeV \\ 0.023 \pm 0.0014 \\ 0.020 \pm 0.0013 \\ 1.16 \pm 0.10 \\ \hline > 4 \ GeV \\ 0.022 \pm 0.0011 \\ \hline \end{array}$	$\begin{array}{c} 0.013 \pm 0.0004 \\ 0.012 \pm 0.0003 \\ 1.09 \pm 0.04 \\ \hline > 5 \text{ GeV} \\ 0.017 \pm 0.0012 \\ 0.015 \pm 0.0011 \\ 1.17 \pm 0.12 \\ \hline > 5 \text{ GeV} \\ 0.017 \pm 0.0010 \\ \hline \end{array}$
$\begin{array}{c} \operatorname{data} \\ \operatorname{mc} \\ \operatorname{data/mc} \\ \\ e + \geq 3 \text{ jets} \\ \\ \operatorname{data} \\ \operatorname{mc} \\ \\ \operatorname{data/mc} \\ \\ \\ \mu + \geq 3 \text{ jets} \\ \\ \\ \operatorname{data} \\ \\ \operatorname{mc} \\ \\ \end{array}$	$\begin{array}{c} 0.111 \pm 0.0010 \\ 0.115 \pm 0.0010 \\ 0.97 \pm 0.01 \\ \hline > 1 \ \mathrm{GeV} \\ 0.123 \pm 0.0031 \\ 0.131 \pm 0.0030 \\ 0.94 \pm 0.03 \\ \hline > 1 \ \mathrm{GeV} \\ 0.121 \pm 0.0025 \\ 0.120 \pm 0.0024 \\ \end{array}$	$\begin{array}{c} 0.048 \pm 0.0007 \\ 0.048 \pm 0.0006 \\ 1.01 \pm 0.02 \\ \hline > 2 \text{ GeV} \\ 0.058 \pm 0.0022 \\ 0.055 \pm 0.0020 \\ 1.06 \pm 0.06 \\ \hline > 2 \text{ GeV} \\ 0.055 \pm 0.0018 \\ 0.052 \pm 0.0016 \\ \hline \end{array}$	$\begin{array}{c} 0.026 \pm 0.0005 \\ 0.025 \pm 0.0005 \\ 1.04 \pm 0.03 \\ \hline > 3 \text{ GeV} \\ 0.034 \pm 0.0017 \\ 0.030 \pm 0.0015 \\ 1.14 \pm 0.08 \\ \hline > 3 \text{ GeV} \\ 0.033 \pm 0.0014 \\ 0.029 \pm 0.0012 \\ \hline \end{array}$	$\begin{array}{c} 0.018 \pm 0.0004 \\ 0.016 \pm 0.0004 \\ 1.09 \pm 0.04 \\ \hline > 4 \ \mathrm{GeV} \\ 0.023 \pm 0.0014 \\ 0.020 \pm 0.0013 \\ 1.16 \pm 0.10 \\ \hline > 4 \ \mathrm{GeV} \\ 0.022 \pm 0.0011 \\ 0.019 \pm 0.0010 \\ \hline \end{array}$	$\begin{array}{c} 0.013 \pm 0.0004 \\ 0.012 \pm 0.0003 \\ 1.09 \pm 0.04 \\ \hline > 5 \text{ GeV} \\ 0.017 \pm 0.0012 \\ 0.015 \pm 0.0011 \\ 1.17 \pm 0.12 \\ \hline > 5 \text{ GeV} \\ 0.017 \pm 0.0010 \\ 0.014 \pm 0.0009 \\ \hline \end{array}$
$\begin{array}{c} \operatorname{data} \\ \operatorname{mc} \\ \operatorname{data/mc} \\ \\ e + \geq 3 \text{ jets} \\ \operatorname{data} \\ \operatorname{mc} \\ \operatorname{data/mc} \\ \\ \hline \mu + \geq 3 \text{ jets} \\ \\ \operatorname{data} \\ \end{array}$	$\begin{array}{c} 0.111 \pm 0.0010 \\ 0.115 \pm 0.0010 \\ 0.97 \pm 0.01 \\ \hline > 1 \ \mathrm{GeV} \\ 0.123 \pm 0.0031 \\ 0.131 \pm 0.0030 \\ 0.94 \pm 0.03 \\ \hline > 1 \ \mathrm{GeV} \\ 0.121 \pm 0.0025 \\ \hline \end{array}$	$\begin{array}{c} 0.048 \pm 0.0007 \\ 0.048 \pm 0.0006 \\ 1.01 \pm 0.02 \\ \\ > 2 \ \mathrm{GeV} \\ 0.058 \pm 0.0022 \\ 0.055 \pm 0.0020 \\ 1.06 \pm 0.06 \\ \\ > 2 \ \mathrm{GeV} \\ 0.055 \pm 0.0018 \\ \end{array}$	$\begin{array}{c} 0.026 \pm 0.0005 \\ 0.025 \pm 0.0005 \\ 1.04 \pm 0.03 \\ \hline > 3 \text{ GeV} \\ 0.034 \pm 0.0017 \\ 0.030 \pm 0.0015 \\ 1.14 \pm 0.08 \\ \hline > 3 \text{ GeV} \\ 0.033 \pm 0.0014 \\ \hline \end{array}$	$\begin{array}{c} 0.018 \pm 0.0004 \\ 0.016 \pm 0.0004 \\ 1.09 \pm 0.04 \\ \hline > 4 \ GeV \\ 0.023 \pm 0.0014 \\ 0.020 \pm 0.0013 \\ 1.16 \pm 0.10 \\ \hline > 4 \ GeV \\ 0.022 \pm 0.0011 \\ \hline \end{array}$	$\begin{array}{c} 0.013 \pm 0.0004 \\ 0.012 \pm 0.0003 \\ 1.09 \pm 0.04 \\ \hline > 5 \text{ GeV} \\ 0.017 \pm 0.0012 \\ 0.015 \pm 0.0011 \\ 1.17 \pm 0.12 \\ \hline > 5 \text{ GeV} \\ 0.017 \pm 0.0010 \\ \hline \end{array}$
$\begin{array}{c} \operatorname{data} \\ \operatorname{mc} \\ \operatorname{data/mc} \\ \operatorname{e} + \geq 3 \ \operatorname{jets} \\ \operatorname{data} \\ \operatorname{mc} \\ \operatorname{data/mc} \\ \\ \mu + \geq 3 \ \operatorname{jets} \\ \operatorname{data} \\ \operatorname{mc} \\ \operatorname{data/mc} \\ \operatorname{e} + \geq 4 \ \operatorname{jets} \\ \end{array}$	$\begin{array}{c} 0.111 \pm 0.0010 \\ 0.115 \pm 0.0010 \\ 0.97 \pm 0.01 \\ \hline > 1 \ \mathrm{GeV} \\ 0.123 \pm 0.0031 \\ 0.131 \pm 0.0030 \\ 0.94 \pm 0.03 \\ \hline > 1 \ \mathrm{GeV} \\ 0.121 \pm 0.0025 \\ 0.120 \pm 0.0024 \\ 1.01 \pm 0.03 \\ \hline > 1 \ \mathrm{GeV} \\ \end{array}$	$\begin{array}{c} 0.048 \pm 0.0007 \\ 0.048 \pm 0.0006 \\ 1.01 \pm 0.02 \\ \\ > 2 \text{ GeV} \\ 0.058 \pm 0.0022 \\ 0.055 \pm 0.0020 \\ 1.06 \pm 0.06 \\ \\ \\ > 2 \text{ GeV} \\ 0.055 \pm 0.0018 \\ 0.052 \pm 0.0016 \\ 1.06 \pm 0.05 \\ \\ > 2 \text{ GeV} \\ \end{array}$	$\begin{array}{c} 0.026 \pm 0.0005 \\ 0.025 \pm 0.0005 \\ 1.04 \pm 0.03 \\ \hline > 3 \text{ GeV} \\ 0.034 \pm 0.0017 \\ 0.030 \pm 0.0015 \\ 1.14 \pm 0.08 \\ \hline > 3 \text{ GeV} \\ 0.033 \pm 0.0014 \\ 0.029 \pm 0.0012 \\ 1.14 \pm 0.07 \\ \hline > 3 \text{ GeV} \\ \hline \end{array}$	$\begin{array}{c} 0.018 \pm 0.0004 \\ 0.016 \pm 0.0004 \\ 1.09 \pm 0.04 \\ \hline > 4 \text{ GeV} \\ 0.023 \pm 0.0014 \\ 0.020 \pm 0.0013 \\ 1.16 \pm 0.10 \\ \hline > 4 \text{ GeV} \\ 0.022 \pm 0.0011 \\ 0.019 \pm 0.0010 \\ 1.14 \pm 0.08 \\ \hline > 4 \text{ GeV} \\ \hline \end{array}$	$\begin{array}{c} 0.013 \pm 0.0004 \\ 0.012 \pm 0.0003 \\ 1.09 \pm 0.04 \\ \hline > 5 \text{ GeV} \\ 0.017 \pm 0.0012 \\ 0.015 \pm 0.0011 \\ 1.17 \pm 0.12 \\ \hline > 5 \text{ GeV} \\ 0.017 \pm 0.0010 \\ 0.014 \pm 0.0009 \\ 1.16 \pm 0.10 \\ \hline > 5 \text{ GeV} \\ \hline \end{array}$
$\begin{array}{c} \operatorname{data} \\ \operatorname{mc} \\ \operatorname{data/mc} \\ e + \geq 3 \text{ jets} \\ \operatorname{data} \\ \operatorname{mc} \\ \operatorname{data/mc} \\ \hline \mu + \geq 3 \text{ jets} \\ \operatorname{data} \\ \operatorname{mc} \\ \operatorname{data} \\ \operatorname{mc} \\ \operatorname{data/mc} \\ \end{array}$	$\begin{array}{c} 0.111 \pm 0.0010 \\ 0.115 \pm 0.0010 \\ 0.97 \pm 0.01 \\ \hline > 1 \ \mathrm{GeV} \\ 0.123 \pm 0.0031 \\ 0.131 \pm 0.0030 \\ 0.94 \pm 0.03 \\ \hline > 1 \ \mathrm{GeV} \\ 0.121 \pm 0.0025 \\ 0.120 \pm 0.0024 \\ 1.01 \pm 0.03 \\ \hline > 1 \ \mathrm{GeV} \\ 0.129 \pm 0.0080 \\ \hline \end{array}$	$\begin{array}{c} 0.048 \pm 0.0007 \\ 0.048 \pm 0.0006 \\ 1.01 \pm 0.02 \\ \\ > 2 \text{ GeV} \\ 0.058 \pm 0.0022 \\ 0.055 \pm 0.0020 \\ 1.06 \pm 0.06 \\ \\ > 2 \text{ GeV} \\ 0.055 \pm 0.0018 \\ 0.052 \pm 0.0016 \\ 1.06 \pm 0.05 \\ \\ > 2 \text{ GeV} \\ 0.070 \pm 0.0061 \\ \end{array}$	$\begin{array}{c} 0.026 \pm 0.0005 \\ 0.025 \pm 0.0005 \\ 1.04 \pm 0.03 \\ \hline > 3 \text{ GeV} \\ 0.034 \pm 0.0017 \\ 0.030 \pm 0.0015 \\ 1.14 \pm 0.08 \\ \hline > 3 \text{ GeV} \\ 0.033 \pm 0.0014 \\ 0.029 \pm 0.0012 \\ 1.14 \pm 0.07 \\ \hline > 3 \text{ GeV} \\ 0.044 \pm 0.0049 \\ \hline \end{array}$	$\begin{array}{c} 0.018 \pm 0.0004 \\ 0.016 \pm 0.0004 \\ 1.09 \pm 0.04 \\ \hline > 4 \text{ GeV} \\ 0.023 \pm 0.0014 \\ 0.020 \pm 0.0013 \\ 1.16 \pm 0.10 \\ \hline > 4 \text{ GeV} \\ 0.022 \pm 0.0011 \\ 0.019 \pm 0.0010 \\ 1.14 \pm 0.08 \\ \hline > 4 \text{ GeV} \\ 0.031 \pm 0.0042 \\ \hline \end{array}$	$\begin{array}{c} 0.013 \pm 0.0004 \\ 0.012 \pm 0.0003 \\ 1.09 \pm 0.04 \\ \hline > 5 \text{ GeV} \\ 0.017 \pm 0.0012 \\ 0.015 \pm 0.0011 \\ 1.17 \pm 0.12 \\ \hline > 5 \text{ GeV} \\ 0.017 \pm 0.0010 \\ 0.014 \pm 0.0009 \\ 1.16 \pm 0.10 \\ \hline > 5 \text{ GeV} \\ 0.021 \pm 0.0034 \\ \hline \end{array}$
$\begin{array}{c} \operatorname{data} \\ \operatorname{mc} \\ \operatorname{data/mc} \\ e + \geq 3 \; \mathrm{jets} \\ \operatorname{data} \\ \operatorname{mc} \\ \operatorname{data/mc} \\ \mu + \geq 3 \; \mathrm{jets} \\ \operatorname{data} \\ \operatorname{mc} \\ \operatorname{data/mc} \\ e + \geq 4 \; \mathrm{jets} \\ \operatorname{data} \\ \operatorname{mc} \\ \end{array}$	$\begin{array}{c} 0.111 \pm 0.0010 \\ 0.115 \pm 0.0010 \\ 0.97 \pm 0.01 \\ \hline > 1 \ \mathrm{GeV} \\ 0.123 \pm 0.0031 \\ 0.131 \pm 0.0030 \\ 0.94 \pm 0.03 \\ \hline > 1 \ \mathrm{GeV} \\ 0.121 \pm 0.0025 \\ 0.120 \pm 0.0024 \\ 1.01 \pm 0.03 \\ \hline > 1 \ \mathrm{GeV} \\ 0.129 \pm 0.0080 \\ 0.132 \pm 0.0075 \\ \hline \end{array}$	$\begin{array}{c} 0.048 \pm 0.0007 \\ 0.048 \pm 0.0006 \\ 1.01 \pm 0.02 \\ \hline > 2 \ {\rm GeV} \\ 0.058 \pm 0.0022 \\ 0.055 \pm 0.0020 \\ 1.06 \pm 0.06 \\ \hline > 2 \ {\rm GeV} \\ 0.055 \pm 0.0018 \\ 0.052 \pm 0.0016 \\ 1.06 \pm 0.05 \\ \hline > 2 \ {\rm GeV} \\ 0.070 \pm 0.0061 \\ 0.059 \pm 0.0053 \\ \hline \end{array}$	$\begin{array}{c} 0.026 \pm 0.0005 \\ 0.025 \pm 0.0005 \\ 1.04 \pm 0.03 \\ \hline > 3 \text{ GeV} \\ 0.034 \pm 0.0017 \\ 0.030 \pm 0.0015 \\ 1.14 \pm 0.08 \\ \hline > 3 \text{ GeV} \\ 0.033 \pm 0.0014 \\ 0.029 \pm 0.0012 \\ 1.14 \pm 0.07 \\ \hline > 3 \text{ GeV} \\ 0.044 \pm 0.0049 \\ 0.035 \pm 0.0041 \\ \hline \end{array}$	$\begin{array}{c} 0.018 \pm 0.0004 \\ 0.016 \pm 0.0004 \\ 1.09 \pm 0.04 \\ \hline > 4 \ GeV \\ 0.023 \pm 0.0014 \\ 0.020 \pm 0.0013 \\ 1.16 \pm 0.10 \\ \hline > 4 \ GeV \\ 0.022 \pm 0.0011 \\ 0.019 \pm 0.0010 \\ 1.14 \pm 0.08 \\ \hline > 4 \ GeV \\ 0.031 \pm 0.0042 \\ 0.025 \pm 0.0035 \\ \hline \end{array}$	$\begin{array}{c} 0.013 \pm 0.0004 \\ 0.012 \pm 0.0003 \\ 1.09 \pm 0.04 \\ \hline > 5 \ \mathrm{GeV} \\ 0.017 \pm 0.0012 \\ 0.015 \pm 0.0011 \\ 1.17 \pm 0.12 \\ \hline > 5 \ \mathrm{GeV} \\ 0.017 \pm 0.0010 \\ 0.014 \pm 0.0009 \\ 1.16 \pm 0.10 \\ \hline > 5 \ \mathrm{GeV} \\ 0.021 \pm 0.0034 \\ 0.017 \pm 0.0029 \\ \hline \end{array}$
$\begin{array}{c} \operatorname{data} \\ \operatorname{mc} \\ \operatorname{data/mc} \\ e + \geq 3 \; \operatorname{jets} \\ \operatorname{data} \\ \operatorname{mc} \\ \operatorname{data/mc} \\ \mu + \geq 3 \; \operatorname{jets} \\ \operatorname{data} \\ \operatorname{mc} \\ \operatorname{data/mc} \\ e + \geq 4 \; \operatorname{jets} \\ \operatorname{data} \\ \end{array}$	$\begin{array}{c} 0.111 \pm 0.0010 \\ 0.115 \pm 0.0010 \\ 0.97 \pm 0.01 \\ \hline > 1 \ \mathrm{GeV} \\ 0.123 \pm 0.0031 \\ 0.131 \pm 0.0030 \\ 0.94 \pm 0.03 \\ \hline > 1 \ \mathrm{GeV} \\ 0.121 \pm 0.0025 \\ 0.120 \pm 0.0024 \\ 1.01 \pm 0.03 \\ \hline > 1 \ \mathrm{GeV} \\ 0.129 \pm 0.0080 \\ \hline \end{array}$	$\begin{array}{c} 0.048 \pm 0.0007 \\ 0.048 \pm 0.0006 \\ 1.01 \pm 0.02 \\ \\ > 2 \text{ GeV} \\ 0.058 \pm 0.0022 \\ 0.055 \pm 0.0020 \\ 1.06 \pm 0.06 \\ \\ > 2 \text{ GeV} \\ 0.055 \pm 0.0018 \\ 0.052 \pm 0.0016 \\ 1.06 \pm 0.05 \\ \\ > 2 \text{ GeV} \\ 0.070 \pm 0.0061 \\ \end{array}$	$\begin{array}{c} 0.026 \pm 0.0005 \\ 0.025 \pm 0.0005 \\ 1.04 \pm 0.03 \\ \hline > 3 \text{ GeV} \\ 0.034 \pm 0.0017 \\ 0.030 \pm 0.0015 \\ 1.14 \pm 0.08 \\ \hline > 3 \text{ GeV} \\ 0.033 \pm 0.0014 \\ 0.029 \pm 0.0012 \\ 1.14 \pm 0.07 \\ \hline > 3 \text{ GeV} \\ 0.044 \pm 0.0049 \\ \hline \end{array}$	$\begin{array}{c} 0.018 \pm 0.0004 \\ 0.016 \pm 0.0004 \\ 1.09 \pm 0.04 \\ \hline > 4 \text{ GeV} \\ 0.023 \pm 0.0014 \\ 0.020 \pm 0.0013 \\ 1.16 \pm 0.10 \\ \hline > 4 \text{ GeV} \\ 0.022 \pm 0.0011 \\ 0.019 \pm 0.0010 \\ 1.14 \pm 0.08 \\ \hline > 4 \text{ GeV} \\ 0.031 \pm 0.0042 \\ \hline \end{array}$	$\begin{array}{c} 0.013 \pm 0.0004 \\ 0.012 \pm 0.0003 \\ 1.09 \pm 0.04 \\ \hline > 5 \text{ GeV} \\ 0.017 \pm 0.0012 \\ 0.015 \pm 0.0011 \\ 1.17 \pm 0.12 \\ \hline > 5 \text{ GeV} \\ 0.017 \pm 0.0010 \\ 0.014 \pm 0.0009 \\ 1.16 \pm 0.10 \\ \hline > 5 \text{ GeV} \\ 0.021 \pm 0.0034 \\ \hline \end{array}$
$\begin{array}{c} \operatorname{data} \\ \operatorname{mc} \\ \operatorname{data/mc} \\ \operatorname{e} + \geq 3 \operatorname{jets} \\ \operatorname{data} \\ \operatorname{mc} \\ \operatorname{data/mc} \\ \\ \mu + \geq 3 \operatorname{jets} \\ \operatorname{data} \\ \operatorname{mc} \\ \operatorname{data/mc} \\ \operatorname{e} + \geq 4 \operatorname{jets} \\ \operatorname{data} \\ \operatorname{mc} \\ \operatorname{data/mc} \\ \\ \mu + \geq 4 \operatorname{jets} \\ \end{array}$	$\begin{array}{c} 0.111 \pm 0.0010 \\ 0.115 \pm 0.0010 \\ 0.97 \pm 0.01 \\ \hline > 1 \ \mathrm{GeV} \\ 0.123 \pm 0.0031 \\ 0.131 \pm 0.0030 \\ 0.94 \pm 0.03 \\ \hline > 1 \ \mathrm{GeV} \\ 0.121 \pm 0.0025 \\ 0.120 \pm 0.0024 \\ 1.01 \pm 0.03 \\ \hline > 1 \ \mathrm{GeV} \\ 0.129 \pm 0.0080 \\ 0.132 \pm 0.0075 \\ 0.98 \pm 0.08 \\ \hline > 1 \ \mathrm{GeV} \\ \hline \end{array}$	$\begin{array}{c} 0.048 \pm 0.0007 \\ 0.048 \pm 0.0006 \\ 1.01 \pm 0.02 \\ \\ > 2 \text{ GeV} \\ 0.058 \pm 0.0022 \\ 0.055 \pm 0.0020 \\ 1.06 \pm 0.06 \\ \\ \\ > 2 \text{ GeV} \\ 0.055 \pm 0.0018 \\ 0.052 \pm 0.0016 \\ 1.06 \pm 0.05 \\ \\ \\ > 2 \text{ GeV} \\ 0.070 \pm 0.0061 \\ 0.059 \pm 0.0053 \\ 1.18 \pm 0.15 \\ \\ > 2 \text{ GeV} \\ \end{array}$	$\begin{array}{c} 0.026 \pm 0.0005 \\ 0.025 \pm 0.0005 \\ 1.04 \pm 0.03 \\ \hline > 3 \ \mathrm{GeV} \\ 0.034 \pm 0.0017 \\ 0.030 \pm 0.0015 \\ 1.14 \pm 0.08 \\ \hline > 3 \ \mathrm{GeV} \\ 0.033 \pm 0.0014 \\ 0.029 \pm 0.0012 \\ 1.14 \pm 0.07 \\ \hline > 3 \ \mathrm{GeV} \\ 0.044 \pm 0.0049 \\ 0.035 \pm 0.0041 \\ 1.26 \pm 0.20 \\ \hline > 3 \ \mathrm{GeV} \\ \hline \end{array}$	$\begin{array}{c} 0.018 \pm 0.0004 \\ 0.016 \pm 0.0004 \\ 1.09 \pm 0.04 \\ \hline > 4 \ \mathrm{GeV} \\ 0.023 \pm 0.0014 \\ 0.020 \pm 0.0013 \\ 1.16 \pm 0.10 \\ \hline > 4 \ \mathrm{GeV} \\ 0.022 \pm 0.0011 \\ 0.019 \pm 0.0010 \\ 1.14 \pm 0.08 \\ \hline > 4 \ \mathrm{GeV} \\ 0.031 \pm 0.0042 \\ 0.025 \pm 0.0035 \\ 1.24 \pm 0.24 \\ \hline > 4 \ \mathrm{GeV} \\ \hline \end{array}$	$\begin{array}{c} 0.013 \pm 0.0004 \\ 0.012 \pm 0.0003 \\ 1.09 \pm 0.04 \\ \hline > 5 \ \mathrm{GeV} \\ 0.017 \pm 0.0012 \\ 0.015 \pm 0.0011 \\ 1.17 \pm 0.12 \\ \hline > 5 \ \mathrm{GeV} \\ 0.017 \pm 0.0010 \\ 0.014 \pm 0.0009 \\ 1.16 \pm 0.10 \\ \hline > 5 \ \mathrm{GeV} \\ 0.021 \pm 0.0034 \\ 0.017 \pm 0.0029 \\ 1.18 \pm 0.28 \\ \hline > 5 \ \mathrm{GeV} \\ \hline \end{array}$
$\begin{array}{c} \operatorname{data} \\ \operatorname{mc} \\ \operatorname{data/mc} \\ e + \geq 3 \; \operatorname{jets} \\ \operatorname{data} \\ \operatorname{mc} \\ \operatorname{data/mc} \\ \hline \mu + \geq 3 \; \operatorname{jets} \\ \operatorname{data} \\ \operatorname{mc} \\ \operatorname{data/mc} \\ e + \geq 4 \; \operatorname{jets} \\ \operatorname{data} \\ \operatorname{mc} \\ \operatorname{data/mc} \\ \operatorname{data/mc} \\ \end{array}$	$\begin{array}{c} 0.111 \pm 0.0010 \\ 0.115 \pm 0.0010 \\ 0.97 \pm 0.01 \\ \hline > 1 \ \text{GeV} \\ 0.123 \pm 0.0031 \\ 0.131 \pm 0.0030 \\ 0.94 \pm 0.03 \\ \hline > 1 \ \text{GeV} \\ 0.121 \pm 0.0025 \\ 0.120 \pm 0.0024 \\ 1.01 \pm 0.03 \\ \hline > 1 \ \text{GeV} \\ 0.129 \pm 0.0080 \\ 0.132 \pm 0.0075 \\ 0.98 \pm 0.08 \\ \hline > 1 \ \text{GeV} \\ 0.136 \pm 0.0067 \\ \hline \end{array}$	$\begin{array}{c} 0.048 \pm 0.0007 \\ 0.048 \pm 0.0006 \\ 1.01 \pm 0.02 \\ \hline > 2 \ {\rm GeV} \\ 0.058 \pm 0.0022 \\ 0.055 \pm 0.0020 \\ 1.06 \pm 0.06 \\ \hline > 2 \ {\rm GeV} \\ 0.055 \pm 0.0018 \\ 0.052 \pm 0.0016 \\ 1.06 \pm 0.05 \\ \hline > 2 \ {\rm GeV} \\ 0.070 \pm 0.0061 \\ 0.059 \pm 0.0053 \\ 1.18 \pm 0.15 \\ \hline > 2 \ {\rm GeV} \\ 0.064 \pm 0.0048 \\ \hline \end{array}$	$\begin{array}{c} 0.026 \pm 0.0005 \\ 0.025 \pm 0.0005 \\ 1.04 \pm 0.03 \\ \hline > 3 \text{ GeV} \\ 0.034 \pm 0.0017 \\ 0.030 \pm 0.0015 \\ 1.14 \pm 0.08 \\ \hline > 3 \text{ GeV} \\ 0.033 \pm 0.0014 \\ 0.029 \pm 0.0012 \\ 1.14 \pm 0.07 \\ \hline > 3 \text{ GeV} \\ 0.044 \pm 0.0049 \\ 0.035 \pm 0.0041 \\ 1.26 \pm 0.20 \\ \hline > 3 \text{ GeV} \\ 0.041 \pm 0.0039 \\ \hline \end{array}$	$\begin{array}{c} 0.018 \pm 0.0004 \\ 0.016 \pm 0.0004 \\ 1.09 \pm 0.04 \\ \hline > 4 \ \mathrm{GeV} \\ 0.023 \pm 0.0014 \\ 0.020 \pm 0.0013 \\ 1.16 \pm 0.10 \\ \hline > 4 \ \mathrm{GeV} \\ 0.022 \pm 0.0011 \\ 0.019 \pm 0.0010 \\ 1.14 \pm 0.08 \\ \hline > 4 \ \mathrm{GeV} \\ 0.031 \pm 0.0042 \\ 0.025 \pm 0.0035 \\ 1.24 \pm 0.24 \\ \hline > 4 \ \mathrm{GeV} \\ 0.029 \pm 0.0033 \end{array}$	$\begin{array}{c} 0.013 \pm 0.0004 \\ 0.012 \pm 0.0003 \\ 1.09 \pm 0.04 \\ \hline > 5 \text{ GeV} \\ 0.017 \pm 0.0012 \\ 0.015 \pm 0.0011 \\ 1.17 \pm 0.12 \\ \hline > 5 \text{ GeV} \\ 0.017 \pm 0.0010 \\ 0.014 \pm 0.0009 \\ 1.16 \pm 0.10 \\ \hline > 5 \text{ GeV} \\ 0.021 \pm 0.0034 \\ 0.017 \pm 0.0029 \\ 1.18 \pm 0.28 \\ \hline > 5 \text{ GeV} \\ 0.024 \pm 0.0030 \\ \hline \end{array}$
$\begin{array}{c} \operatorname{data} \\ \operatorname{mc} \\ \operatorname{data/mc} \\ e + \geq 3 \; \operatorname{jets} \\ \operatorname{data} \\ \operatorname{mc} \\ \operatorname{data/mc} \\ \mu + \geq 3 \; \operatorname{jets} \\ \operatorname{data} \\ \operatorname{mc} \\ \operatorname{data/mc} \\ e + \geq 4 \; \operatorname{jets} \\ \operatorname{data} \\ \operatorname{mc} \\ \operatorname{data/mc} \\ \mu + \geq 4 \; \operatorname{jets} \\ \operatorname{data} \\ \operatorname{mc} \\ \operatorname{data} \\ \operatorname{mc} \\ \end{array}$	$\begin{array}{c} 0.111 \pm 0.0010 \\ 0.115 \pm 0.0010 \\ 0.97 \pm 0.01 \\ \hline > 1 \ \mathrm{GeV} \\ 0.123 \pm 0.0031 \\ 0.131 \pm 0.0030 \\ 0.94 \pm 0.03 \\ \hline > 1 \ \mathrm{GeV} \\ 0.121 \pm 0.0025 \\ 0.120 \pm 0.0024 \\ 1.01 \pm 0.03 \\ \hline > 1 \ \mathrm{GeV} \\ 0.129 \pm 0.0080 \\ 0.132 \pm 0.0075 \\ 0.98 \pm 0.08 \\ \hline > 1 \ \mathrm{GeV} \\ 0.136 \pm 0.0067 \\ 0.130 \pm 0.0063 \\ \hline \end{array}$	$\begin{array}{c} 0.048 \pm 0.0007 \\ 0.048 \pm 0.0006 \\ 1.01 \pm 0.02 \\ \\ > 2 \ \mathrm{GeV} \\ 0.058 \pm 0.0022 \\ 0.055 \pm 0.0020 \\ 1.06 \pm 0.06 \\ \\ > 2 \ \mathrm{GeV} \\ 0.055 \pm 0.0018 \\ 0.052 \pm 0.0016 \\ 1.06 \pm 0.05 \\ \\ \\ > 2 \ \mathrm{GeV} \\ 0.070 \pm 0.0061 \\ 0.059 \pm 0.0053 \\ 1.18 \pm 0.15 \\ \\ > 2 \ \mathrm{GeV} \\ 0.064 \pm 0.0048 \\ 0.065 \pm 0.0046 \\ \end{array}$	$\begin{array}{c} 0.026 \pm 0.0005 \\ 0.025 \pm 0.0005 \\ 1.04 \pm 0.03 \\ \hline > 3 \ GeV \\ 0.034 \pm 0.0017 \\ 0.030 \pm 0.0015 \\ 1.14 \pm 0.08 \\ \hline > 3 \ GeV \\ 0.033 \pm 0.0014 \\ 0.029 \pm 0.0012 \\ 1.14 \pm 0.07 \\ \hline > 3 \ GeV \\ 0.044 \pm 0.0049 \\ 0.035 \pm 0.0041 \\ 1.26 \pm 0.20 \\ \hline > 3 \ GeV \\ 0.041 \pm 0.0039 \\ 0.035 \pm 0.0034 \\ \hline \end{array}$	$\begin{array}{c} 0.018 \pm 0.0004 \\ 0.016 \pm 0.0004 \\ 1.09 \pm 0.04 \\ \hline > 4 \ GeV \\ 0.023 \pm 0.0014 \\ 0.020 \pm 0.0013 \\ 1.16 \pm 0.10 \\ \hline > 4 \ GeV \\ 0.022 \pm 0.0011 \\ 0.019 \pm 0.0010 \\ 1.14 \pm 0.08 \\ \hline > 4 \ GeV \\ 0.031 \pm 0.0042 \\ 0.025 \pm 0.0035 \\ 1.24 \pm 0.24 \\ \hline > 4 \ GeV \\ 0.029 \pm 0.0033 \\ 0.020 \pm 0.0026 \\ \hline \end{array}$	$\begin{array}{c} 0.013 \pm 0.0004 \\ 0.012 \pm 0.0003 \\ 1.09 \pm 0.04 \\ \hline > 5 \ \mathrm{GeV} \\ 0.017 \pm 0.0012 \\ 0.015 \pm 0.0011 \\ 1.17 \pm 0.12 \\ \hline > 5 \ \mathrm{GeV} \\ 0.017 \pm 0.0010 \\ 0.014 \pm 0.0009 \\ 1.16 \pm 0.10 \\ \hline > 5 \ \mathrm{GeV} \\ 0.021 \pm 0.0034 \\ 0.017 \pm 0.0029 \\ 1.18 \pm 0.28 \\ \hline > 5 \ \mathrm{GeV} \\ 0.024 \pm 0.0030 \\ 0.013 \pm 0.0022 \\ \hline \end{array}$
$\begin{array}{c} \operatorname{data} \\ \operatorname{mc} \\ \operatorname{data/mc} \\ e + \geq 3 \; \operatorname{jets} \\ \operatorname{data} \\ \operatorname{mc} \\ \operatorname{data/mc} \\ \mu + \geq 3 \; \operatorname{jets} \\ \operatorname{data} \\ \operatorname{mc} \\ \operatorname{data/mc} \\ e + \geq 4 \; \operatorname{jets} \\ \operatorname{data} \\ \operatorname{mc} \\ \operatorname{data/mc} \\ \mu + \geq 4 \; \operatorname{jets} \\ \operatorname{data} \\ \operatorname{mc} \\ \operatorname{data/mc} \\ \mu + \geq 4 \; \operatorname{jets} \\ \operatorname{data} \\ \end{array}$	$\begin{array}{c} 0.111 \pm 0.0010 \\ 0.115 \pm 0.0010 \\ 0.97 \pm 0.01 \\ \hline > 1 \ \text{GeV} \\ 0.123 \pm 0.0031 \\ 0.131 \pm 0.0030 \\ 0.94 \pm 0.03 \\ \hline > 1 \ \text{GeV} \\ 0.121 \pm 0.0025 \\ 0.120 \pm 0.0024 \\ 1.01 \pm 0.03 \\ \hline > 1 \ \text{GeV} \\ 0.129 \pm 0.0080 \\ 0.132 \pm 0.0075 \\ 0.98 \pm 0.08 \\ \hline > 1 \ \text{GeV} \\ 0.136 \pm 0.0067 \\ \hline \end{array}$	$\begin{array}{c} 0.048 \pm 0.0007 \\ 0.048 \pm 0.0006 \\ 1.01 \pm 0.02 \\ \hline > 2 \ {\rm GeV} \\ 0.058 \pm 0.0022 \\ 0.055 \pm 0.0020 \\ 1.06 \pm 0.06 \\ \hline > 2 \ {\rm GeV} \\ 0.055 \pm 0.0018 \\ 0.052 \pm 0.0016 \\ 1.06 \pm 0.05 \\ \hline > 2 \ {\rm GeV} \\ 0.070 \pm 0.0061 \\ 0.059 \pm 0.0053 \\ 1.18 \pm 0.15 \\ \hline > 2 \ {\rm GeV} \\ 0.064 \pm 0.0048 \\ \hline \end{array}$	$\begin{array}{c} 0.026 \pm 0.0005 \\ 0.025 \pm 0.0005 \\ 1.04 \pm 0.03 \\ \hline > 3 \text{ GeV} \\ 0.034 \pm 0.0017 \\ 0.030 \pm 0.0015 \\ 1.14 \pm 0.08 \\ \hline > 3 \text{ GeV} \\ 0.033 \pm 0.0014 \\ 0.029 \pm 0.0012 \\ 1.14 \pm 0.07 \\ \hline > 3 \text{ GeV} \\ 0.044 \pm 0.0049 \\ 0.035 \pm 0.0041 \\ 1.26 \pm 0.20 \\ \hline > 3 \text{ GeV} \\ 0.041 \pm 0.0039 \\ \hline \end{array}$	$\begin{array}{c} 0.018 \pm 0.0004 \\ 0.016 \pm 0.0004 \\ 1.09 \pm 0.04 \\ \hline > 4 \ \mathrm{GeV} \\ 0.023 \pm 0.0014 \\ 0.020 \pm 0.0013 \\ 1.16 \pm 0.10 \\ \hline > 4 \ \mathrm{GeV} \\ 0.022 \pm 0.0011 \\ 0.019 \pm 0.0010 \\ 1.14 \pm 0.08 \\ \hline > 4 \ \mathrm{GeV} \\ 0.031 \pm 0.0042 \\ 0.025 \pm 0.0035 \\ 1.24 \pm 0.24 \\ \hline > 4 \ \mathrm{GeV} \\ 0.029 \pm 0.0033 \end{array}$	$\begin{array}{c} 0.013 \pm 0.0004 \\ 0.012 \pm 0.0003 \\ 1.09 \pm 0.04 \\ \hline > 5 \ \mathrm{GeV} \\ 0.017 \pm 0.0012 \\ 0.015 \pm 0.0011 \\ 1.17 \pm 0.12 \\ \hline > 5 \ \mathrm{GeV} \\ 0.017 \pm 0.0010 \\ 0.014 \pm 0.0009 \\ 1.16 \pm 0.10 \\ \hline > 5 \ \mathrm{GeV} \\ 0.021 \pm 0.0034 \\ 0.017 \pm 0.0029 \\ 1.18 \pm 0.28 \\ \hline > 5 \ \mathrm{GeV} \\ 0.024 \pm 0.0030 \\ \hline \end{array}$

fix me: What you have written in the next paragraph does not explain how ϵ_{fake} is measured.
Why not measure ϵ_{fake} in the b-veto region?

506 9.8 Summary of uncertainties

507 .

⁰⁸ THIS NEEDS TO BE WRITTEN

- 10 Results
- 510 11 Conclusion

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A Performance of the Isolation Requirement

The last requirement used in the analysis is an isolated track veto. This selection criteria rejects events containing a track of $p_{\rm T}>10$ GeV with relative track isolation $\sum p_{\rm T}/p_{\rm T}(trk)$ in a cone of size R=0.3<0.1. It may be noted that only tracks consistent with the vertex with highest $\sum p_{\rm T}^2$ are considered in order to reduce the impact of spurious tracks, for example from pileup interactions. This requirement has very good performance. Figure 18 shows the efficiency for rejecting dilepton events compared to the efficiency for selecting single lepton events for various cone sizes and cut values. The chosen working point provides a signal efficiency of $\epsilon(sig)=92\%$ for a background rejection of $\epsilon(bkg)=53\%$ in MC. With "signal" ("background") we are referring to $t\bar{t}\to\ell$ + jets ($t\bar{t}\to\ell\ell$).

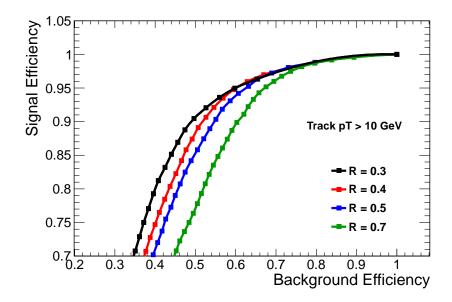


Figure 18: Comparison of the performance in terms of signal (single lepton events) efficiency and background (dilepton events) rejection for various cone sizes and cut values. The current isolation requirement uses a cone of size $\Delta R = 0.3$ and a cut value of 0.1, corresponding to $\epsilon(sig) = 92\%$ for $\epsilon(bkg) = 53\%$. ADD ARROW OR LINE TO INDICATE WORKING POINT.

It should be emphasized that the isolated track veto has a different impact on the samples with a single lepton (mainly $t\bar{t} \to \ell + jets$ and W+jets) and that with two leptons (mainly $t\bar{t} \to \ell \ell$). For the dilepton background, the veto rejects events which have a genuine second lepton. Thus the performance may be understood as an efficiency $\epsilon_{iso\ trk}$ to identify the isolated track. In the case of the single lepton background, the veto rejects events which do not have a genuine second lepton, but rather which contain a "fake" isolated track. The isolated track veto thus effectively scales the single lepton sample by $(1-\epsilon_{fake})$, where ϵ_{fake} is the probability to identify an isolated track with $p_T > 10$ GeVin events which contain no genuine second lepton. It is thus necessary to study the isolated track efficiency $\epsilon(trk)$ and ϵ_{fake} in order to fully characterize the veto performance.

The veto efficiency for dilepton events is calculated using the tag and probe method in Z events. A good lepton satisfying the full ID and isolation criteria and matched to a trigger object serves as the tag. The probe is defined as a track with $p_T > 10$ GeV that has opposite charge to the tag and has an invariant mass with the probe consistent with the Z mass.

Fix me: fkw does not understand why you refer to $p_T > 10$ GeVhere, given that in the very next paragraph you state that this is measured via the absolute track isolation, implying, but not explicitly stating, that a much higher p_T threshold is used to get a clean **Z** signal. ???

The variable used to study the performance of the veto is the absolute track isolation, since it removes the dependence of the isolation variable on the $p_{\rm T}$ of the object under consideration. This is particularly useful because the underlying $p_{\rm T}$ distribution is different for second leptons in $t\bar{t} \to \ell\ell$ events compared to Z events, particularly due to the presence of τ s that have softer decay products. As shown in Figure 19,

the absolute isolation is consistent between Z+4 jet events and $t\bar{t} \to \ell\ell$ events, including leptons from W and τ decays. This supports the notion that the isolation, defined as the energy surrounding the object under consideration, depends only on the environment of the object and not on the object itself. The isolation is thus sensitive to the ambient pileup and jet activity in the event, which is uncorrelated with the lepton $p_{\rm T}$. It is thus justified to use tag and probe in Z+4 jet events, where the jet activity is similar to $t\bar{t} \to \ell\ell$ events in our $N_{\rm jets} > 4$ signal region, in order to estimate the performance of the isolation requirement for the various leptonic categories of $t\bar{t} \to \ell\ell$ events.

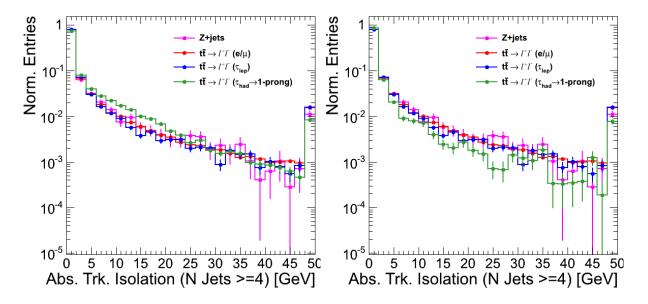


Figure 19: Comparison of absolute track isolation for track probes in Z+4 jet and $t\bar{t}\to\ell\ell$ events for different lepton types. The isolation variables agree across samples, except for single prong τ s, that tend to be slightly less isolated (left). The agreement across isolation distributions is recovered after removing single prong τ events produced in association with π^0 s from the sample (right).

Glossary of abbreviations \mathbf{B}

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R_{wjet}^e, R_{wjet}^\mu, R_{wjet}
     Monte Carlo ratio of W+ jet events in the M_T tail to the M_T peak. Seaparately for electrons and muons,
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     or combined.
     R_{top}^e, R_{top}^\mu, R_{top}
     Monte Carlo ratio of t\bar{t} or single-top \ell+ jets events in the M_T tail to the M_T peak. Separately for
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     electrons and muons, or combined.
     SFR_{wjet}^{e}, SFR_{wjet}^{\mu}, SFR_{wjet}
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     Data/MC scale factors for R_{wjet}^e, R_{wjet}^{\mu}, R_{wjet}
590
591
     SFR_{top}^e, SFR_{top}^\mu, SFR_{top}
592
     Data/MC scale factors for R_{ton}^e, R_{ton}^\mu, R_{ton}
593
594
     K_3 and K_4
595
     Scale factors for t\bar{t} \to \ell\ell events with one or two extra jets from radiation
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 SF_{pre} and SF_{post}

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Scale factors to be applied to MC to normalize to the yields in the M_T control region before and after 599 the application of the isolated track veto. 600