

Prediction of uncertainty of 10-coefficient compressor maps for extreme operating conditions

Howard Cheung

Postdoctoral Research Fellow, Ray W. Herrick Laboratories, School of Mechanical Engineering, Purdue University, 177 S. Russell St., West Lafayette, IN 47907-2031, US

E-mail: cheung@purdue.edu

Christian K. Bach

Assistant Professor, Mechanical and Aerospace Engineering, Oklahoma State University, 218 Engineering North, Stillwater, OK 74078-5016

E-mail: cbach@okstate.edu

Abstract. Empirical compressor maps are a simple and reliable approach for heating and cooling system designers to estimate compressor refrigerant mass flow rate and power consumption quickly. These maps were used for a long time since most compressor manufacturers build the maps with extensive test matrices, leading to good accuracy. However, the situation changes when engineers extrapolate the maps to investigate the compressors performance under extreme operating conditions such as for cold climate heat pump applications or under conditions with system faults. Engineers are not confident on the exact uncertainty of the extrapolation, and often claim that the inaccuracy of their studies is a result of high extrapolation uncertainty. This paper presents a method to estimate the extrapolation uncertainty due to the structure of the test matrix that trains the manufacturer maps and helps the investigators to understand if the extrapolation is the main cause of their inaccuracy. To verify that the method can estimate the uncertainty due to extrapolation, the study builds 10-coefficient compressor maps trained by different test matrices of the same size and different operating points. The maps are used to estimate the compressor performance under different operating points and their estimation uncertainties are compared. The results show that the component of the uncertainty that depends on the structure of the test matrix is small at operating conditions within the test matrix but the uncertainty grows significantly as the estimation becomes further away from the operating conditions within the test matrices.

1. Sources of uncertainty

Uncertainty of the compressor map output is the range where the true value of the map output may be relative to the map output. It consists of multiple components and can be grouped as follows:

- Uncertainty due to inputs
- Uncertainty due to training data
- Uncertainty due to model random error
- Uncertainty due to outputs

1.1. Uncertainty due to inputs

Uncertainty due to inputs is the uncertainty propagated to the map output due to the uncertainty in the inputs to the maps. The inputs to the map (evaporating and condenser temperature) are usually obtained by converting pressure measurement to saturation temperature with refrigerant equations of state, and the estimated saturation temperature contains uncertainty from both the equation of state and the pressure measurement. The equation of state of R22 estimates saturation pressure at an uncertainty of 0.2% [1]. When the equation of state estimates a saturation temperature at a given pressure, this uncertainty is transformed into a component of the uncertainty of the saturation temperature as shown in Eqns. (1) and (2).

$$\frac{\Delta P_{sat,EOS}}{P_{sat}(T)} = 0.002 \quad (1)$$

$$\Delta T_{sat,EOS} = \left| \frac{\partial T_{sat}(P)}{\partial P} \right| \Delta P_{sat,EOS} \quad (2)$$

where $\Delta P_{sat,EOS}$ is the uncertainty of saturation pressure as a result of uncertainty of the equation of state, $P_{sat}(T)$ is the saturation pressure from temperature T , $\Delta T_{sat,EOS}$ is the uncertainty of saturation temperature as a result of uncertainty of the equation of state and $T_{sat}(P)$ is the saturation temperature at pressure P .

The component of the uncertainty due to pressure measurement in saturation temperature values is calculated by Eqn. (3).

$$\Delta T_{sat,mea} = \left| \frac{\partial T_{sat}(P)}{\partial P} \right| \Delta P_{sat,mea} \quad (3)$$

where $\Delta T_{sat,mea}$ is the uncertainty of saturation temperature as a result of pressure measurement and $\Delta P_{sat,mea}$ is the uncertainty of pressure measurement.

The overall uncertainty of the saturation temperature is given by Eqn. (4).

$$\Delta T_{sat} = \sqrt{(\Delta T_{sat,EOS})^2 + (\Delta T_{sat,mea})^2} \quad (4)$$

The uncertainty of the map output propagated from the inputs of condensing temperature and evaporating temperature can be given by Eqn. (5).

$$\Delta \hat{W}_{input} = \sqrt{\left(\frac{\partial \hat{W}}{\partial T_{evap}} \Delta T_{evap} \right)^2 + \left(\frac{\partial \hat{W}}{\partial T_{cond}} \Delta T_{cond} \right)^2} \quad (5)$$

where $\Delta \hat{W}_{input}$ is the uncertainty due to inputs at the map output

1.2. Uncertainty due to training data

Uncertainty due to training data is the uncertainty propagated to the map output from the training data through the map coefficients. This can be understood by considering the estimation of the map coefficients as a function of the training data as Eqn. (6).

$$\hat{\beta} = g(T_{evap,train,1}, \dots, T_{evap,train,n}, T_{cond,train,1}, \dots, T_{cond,train,n}, \dot{W}_{train,1}, \dots, \dot{W}_{train,n}) \quad (6)$$

The uncertainty propagated to the map output through function g and $\hat{\beta}$ in Eqn. (6) is calculated by Eqn. (7).

$$\Delta \hat{W}_{train} = \sqrt{\begin{aligned} &\Sigma_{j=1}^n (\Sigma_{i=1}^m (\frac{\partial \hat{W}}{\partial \beta_i} \frac{\partial \beta_i}{\partial T_{evap,train,j}}) \Delta T_{evap,train,j})^2 \\ &+ \Sigma_{j=1}^n (\Sigma_{i=1}^m (\frac{\partial \hat{W}}{\partial \beta_i} \frac{\partial \beta_i}{\partial T_{cond,train,j}}) \Delta T_{cond,train,j})^2 \\ &+ \Sigma_{j=1}^n (\Sigma_{i=1}^m (\frac{\partial \hat{W}}{\partial \beta_i} \frac{\partial \beta_i}{\partial \dot{W}_{train,j}}) \Delta \dot{W}_{train,j})^2 \end{aligned}} \quad (7)$$

where $\Delta \hat{W}_{train}$ is the uncertainty due to training data at the map output

References

- [1] Taylor B N and Kuyatt C. E. 1994 *NIST Technical Note 1297*