# Robotics: Planning and Navigation - Motion planning for UAV

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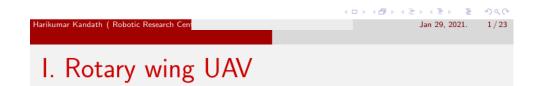




Figure: Multi-rotor VTOL

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#### II. Fixed wing UAV

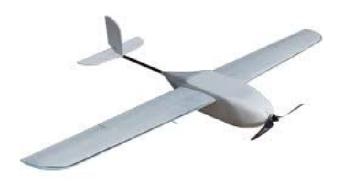


Figure: Fixed wing UAV

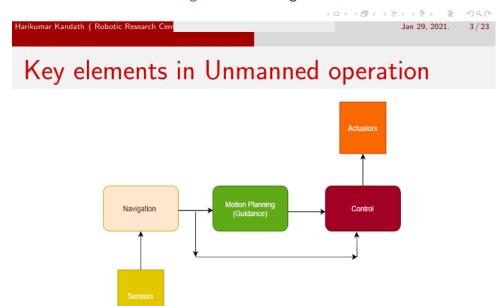


Figure: Navigation, Guidance and Control

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#### Inertial Frame

Position (x, y, z), Velocity  $(v_x, v_y, v_z)$ , Acceleration  $(a_x, a_y, a_z)$ .

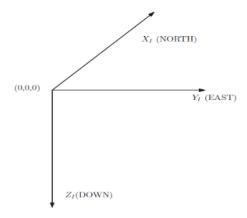


Fig. 1. Diagram showing inertial  $X_I Y_I Z_I$  co-ordinate sytem

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#### Velocity Control

Motion in 2D plane  $(X_I - Y_I)$ .

Altitude (h = -z) is constant, i.e.  $\frac{dh}{dt} = \dot{h} = 0$ . Current position (x, y) and the desired position is  $(x_d, y_d)$ .

$$\frac{dx}{dt} = \dot{x} = v_x \tag{1}$$

$$\frac{dy}{dt} = \dot{y} = v_y \tag{2}$$

Input is  $(v_x, v_y)$  and output is (x, y).

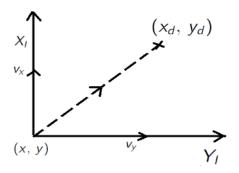
NB: The desired  $(v_x, v_y)$  is tracked by inner loop control system.

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#### Velocity Control - Reaching a point

$$v_x = k(x_d - x) \tag{3}$$

$$v_y = k(y_d - y) \tag{4}$$



#### **Acceleration Control**

$$\frac{dx}{dt} = \dot{x} = v_x \tag{5}$$

$$\frac{dx}{dt} = \dot{x} = v_x \tag{5}$$

$$\frac{d^2x}{dt^2} = \ddot{x} = a_x \tag{6}$$

$$\frac{dy}{dt} = \dot{y} = v_y \tag{7}$$

$$\frac{dy}{dt} = \dot{y} = v_y$$

$$\frac{d^2y}{dt^2} = \ddot{y} = a_y$$
(8)

Reaching a point  $(x_d, y_d)$ .

$$a_x = k_1(x_d - x) - k_2v_x, \ a_y = k_1(y_d - y) - k_2v_y$$
 (9)

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#### **Acceleration Control**

Trajectory (x(t), y(t))

$$\ddot{x} + k_2 \dot{x} + k_1 x = k_1 x_d, \ \ddot{y} + k_2 \dot{y} + k_1 y = k_1 y_d$$
 (10)

At steady-state, 
$$\ddot{x} = \dot{x} = 0 \implies x = x_d$$
 and  $\ddot{y} = \dot{y} = 0 \implies y = y_d$ .

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## Velocity tracking through acceleration control

Desired velocity  $(v_{xd}, v_{yd})$ 

$$\frac{d^2x}{dt^2} = \ddot{x} = \frac{dv_x}{dt} = a_x \tag{11}$$

$$a_{\scriptscriptstyle X} = k_3(v_{\scriptscriptstyle Xd} - v_{\scriptscriptstyle X}) \tag{12}$$

$$\frac{dv_x}{dt} = k_3(v_{xd} - v_x) \tag{13}$$

$$\frac{dv_x}{dt} + k_3 v_x = k_3 v_{xd} \tag{14}$$

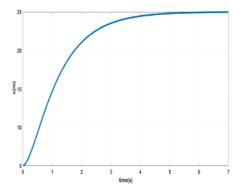
At steady-state  $dv_x/dt = 0 \implies v_x = v_x d_{a}$ 

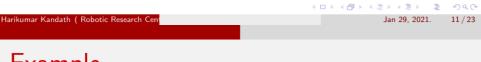
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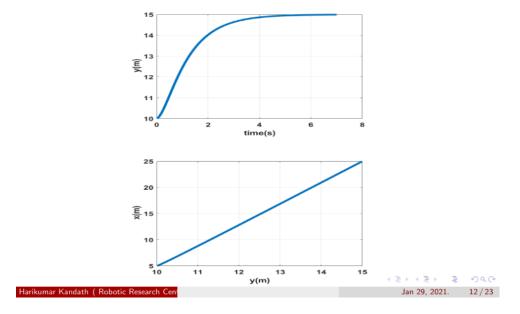
### Example

$$(x, y) = (5, 10), (v_x, v_y) = (1, 0.5), (x_d, y_d) = (25, 15), k_1 = 3, k_2 = 4.$$



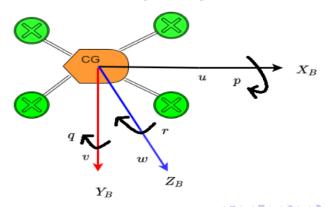


### Example



#### Variables- Body Frame

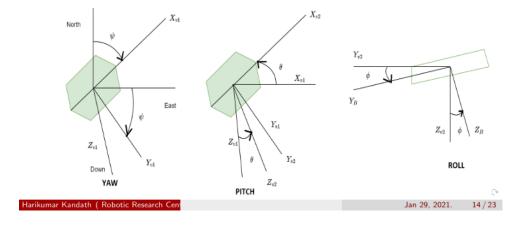
• Velocity:  $V_B = [u, v, w]^T$ • Acceleration:  $\dot{u} = \frac{du}{dt}$ ,  $\dot{v} = \frac{dv}{dt}$ ,  $\dot{w} = \frac{dw}{dt}$ • Angular velocity:  $\Omega = [p, q, r]^T$ 



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#### Euler angles - $\phi$ , $\theta$ , $\psi$

First rotation (i to  $v_1$ )-  $\dot{\phi}=0$ ,  $\dot{\theta}=0$ ,  $\dot{\psi}\neq0$ Second rotation ( $v_1$  to  $v_2$ ) -  $\dot{\phi}=0$ ,  $\dot{\theta}\neq0$ ,  $\dot{\psi}=0$ Third rotation ( $v_2$  to B) -  $\dot{\phi}\neq0$ ,  $\dot{\theta}=0$ ,  $\dot{\psi}=0$ 



#### Euler angles and p,q,r

$$\begin{pmatrix} p \\ q \\ r \end{pmatrix} = \begin{pmatrix} \dot{\phi} \\ 0 \\ 0 \end{pmatrix} + R(\phi)^b_{\nu_2} \begin{pmatrix} 0 \\ \dot{\theta} \\ 0 \end{pmatrix} + R(\phi)^b_{\nu_2} R(\theta)^{\nu_2}_{\nu_1} \begin{pmatrix} 0 \\ 0 \\ \dot{\psi} \end{pmatrix} \quad (15)$$

$$\begin{pmatrix} p \\ q \\ r \end{pmatrix} = \begin{pmatrix} 1 & 0 & -\sin(\theta) \\ 0 & \cos(\phi) & \sin(\phi)\cos(\theta) \\ 0 & -\sin(\phi) & \cos(\phi)\cos(\theta) \end{pmatrix} \begin{pmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{pmatrix} \tag{16}$$

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#### Euler angles and p,q,r

Remark: Rotating about only one of the body axis will directly relate  $\dot{\phi} = p \, (q = r = 0)$ ;  $\dot{\theta} = q \, (\phi = 0, p = r = 0)$  and  $\dot{\psi} = r \, (\phi = \theta = 0, p = q = 0)$ .

$$\begin{pmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{pmatrix} = \begin{pmatrix} 1 & \sin(\phi)\tan(\theta) & \cos(\phi)\tan(\theta) \\ 0 & \cos(\phi) & -\sin(\phi) \\ 0 & \sin(\phi)\sec(\theta) & \cos(\phi)\sec(\theta) \end{pmatrix} \begin{pmatrix} p \\ q \\ r \end{pmatrix}$$
 (17)

why this is important?

Ans. We cannot measure  $\phi, \theta, \psi$  directly using a sensor. But we can always measure p, q, r using 3-axis gyroscope mounted on the UAV and integrate the above to get  $\phi, \theta, \psi$ .

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## Connecting inertial and body axis velocities

How do we use the knowledge of  $\phi$ ,  $\theta$ ,  $\psi$ ?

$$\begin{pmatrix} u \\ v \\ w \end{pmatrix} = R(\phi)_{v_2}^b R(\theta)_{v_1}^{v_2} R(\psi)_i^{v_1} \begin{pmatrix} v_x \\ v_y \\ v_z \end{pmatrix}$$
(18)

$$\begin{pmatrix} v_x \\ v_y \\ v_z \end{pmatrix} = [R(\phi)_{v_2}^b R(\theta)_{v_1}^{v_2} R(\psi)_i^{v_1}]^{-1} \begin{pmatrix} u \\ v \\ w \end{pmatrix}$$
(19)

How do we get u, v, w?

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#### **Equation of Coriolis**

$$V_B = [u, v, w]^T$$
,  $\Omega = [p, q, r]^T$ ,  $F = [F_{XB}, F_{YB}, F_{ZB}]^T$ .

 Equation of Coriolis: Rate of change of a vector (that is defined in a rotating frame )in inertial frame
 Rate of change of the vector in the rotating frame + change due to relative angular velocity between the inertial frame and the rotating frame.

$$\left(\frac{dV_B}{dt}\right)_I = \left(\frac{dV_B}{dt}\right)_B + \Omega \times V_B = \frac{F}{m} \tag{20}$$

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### Translational Dynamics

 $V_B = [u, v, w]^T$ ,  $\Omega = [p, q, r]^T$ ,  $F = [F_{XB}, F_{YB}, F_{ZB}]^T$ .

$$\left(\frac{dV_B}{dt}\right)_I = \left(\frac{dV_B}{dt}\right)_B + \Omega \times V_B = \frac{F}{m}$$
 (21)

$$\dot{u} = rv - qw + \frac{F_{XB}}{m} \tag{22}$$

$$\dot{v} = pw - ru + \frac{F_{YB}}{m} \tag{23}$$

$$\dot{w} = qu - pv + \frac{F_{ZB}}{m} \tag{24}$$

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#### Time-Scale Separation

Basic Idea: Faster variable changes and goes to steady value when compared to the slower variable.

- p,q,r
- $\bullet$   $\phi$ ,  $\theta$ ,  $\psi$
- $\dot{u}$ ,  $\dot{v}$  and  $\dot{w}$   $(a_x, a_y, a_z)$
- u, v, w and  $(v_x, v_y, v_z)$
- x,y,z

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#### Simplification

$$\begin{pmatrix} v_x \\ v_y \\ v_z \end{pmatrix} = R(\phi, \theta, \psi) \begin{pmatrix} u \\ v \\ w \end{pmatrix}$$
 (25)

$$\begin{pmatrix} a_{x} \\ a_{y} \\ a_{z} \end{pmatrix} = R(\phi, \theta, \psi) \begin{pmatrix} \dot{u} \\ \dot{v} \\ \dot{w} \end{pmatrix} + \dot{R}(\phi, \theta, \psi) \begin{pmatrix} u \\ v \\ w \end{pmatrix}$$
(26)

$$\dot{R}(\phi,\theta,\psi)\approx 0$$

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#### Implementation of acceleration command

Compute the desired angles  $\theta_d$ ,  $\phi_d$  and the thrust  $T_d$  for a given  $\psi$  using the below equations. Alternatively, we can also compute desired  $\theta_d$ ,  $\psi_d$ ,  $T_d$  for a given  $\phi$  (or) compute desired  $\phi_d$ ,  $\psi_d$ ,  $T_d$  for a given  $\theta$ .

$$a_{x} = (-\cos\phi\sin\theta\cos\psi - \sin\phi\sin\psi)\frac{T}{m}$$
 (27)

$$a_{y} = (-\cos\phi\sin\theta\sin\psi - \sin\phi\cos\psi)\frac{T}{m}$$
 (28)

$$a_z = g - (\cos\phi\cos\theta)\frac{T}{m} \tag{29}$$

NB: The angles  $\theta$ ,  $\phi$ ,  $\psi$  and the thrust T can be controlled precisely.

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