

# Structured Nonlinear Feedback Design with Separable Control-Contraction Metrics

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**Abstract**—The abstract goes here.

**Index Terms**—IEEE, IEEEtran, journal, L<sup>A</sup>T<sub>E</sub>X, paper, template.

## I. INTRODUCTION

[1]

a) *Overview.*: The motivation and background needed for this paper are precised in Section ?? . The problem under consideration is formalized in Section ?? . Section II presents the result of this paper. Illustrations of the proposed approach are provided in Section III. The proofs of the results are provided in Section IV. Section V collects final remarks.

b) *Notation.*: Let  $N \in \mathbb{N}$  be a constant value. The notation  $\mathbb{N}_{[1,N]}$  stands for the set  $\{i \in \mathbb{N} : 1 \leq i \leq N\}$ . Let  $c \in \mathbb{R}$  be a constant value. The notation  $\mathbb{R}_{[1,c]}$  (resp.  $\mathbb{R}_{\geq c}$ ) stands for the set  $\{x \in \mathbb{R} : 1 \leq x \leq c\}$  (resp.  $\{x \in \mathbb{R} : x \geq c\}$ ), where  $\diamond$  is a comparison operator, i.e.,  $\diamond \in \{<, \geq, =, \text{etc}\}$ . A matrix  $M \in \mathbb{R}^{n \times n}$  with zero elements except (eventually) those  $m_{ii}, \dots, m_{nn}$  on the diagonal is denoted as  $\text{diag}(m_{ii}, \dots, m_{nn})$ . The notation  $M \succ 0$  (resp.  $M \succeq 0$ ) stands for  $M$  is positive (resp. semi) definite.

The notation  $\mathcal{L}_{\text{loc}}^{\infty}(\mathbb{R}_{\geq 0}, \mathbb{R}^m)$  stands for the class of functions  $u : \mathbb{R} \rightarrow \mathbb{R}^m$  that are locally essentially bounded. Given differentiable functions  $M : \mathbb{R}^n \rightarrow \mathbb{R}^{n \times n}$  and  $f : \mathbb{R}^n \rightarrow \mathbb{R}^n$  the notation  $\dot{M}$  stands for matrix with dimension  $n \times n$  and with  $(i, j)$ -element given by  $\frac{\partial m_{ij}}{\partial x}(x)f(x)$ .

### A. Problem Formulation and Motivation

*Class of systems.* Consider the class of systems described by the differential equation

$$\dot{x}(t) = f(x(t)) + B(x(t))u(t), \quad (1)$$

where, for positive times  $t$ , the *system state*  $x(t)$  and the *system input*  $u(t)$  evolve in the Euclidean spaces  $\mathbb{R}^n$  and  $\mathbb{R}^m$ , respectively. The functions  $f : \mathbb{R}^n \rightarrow \mathbb{R}^n$  and  $B : \mathbb{R}^n \rightarrow \mathbb{R}^m$  are assumed to be smooth, i.e., infinitely differentiable and satisfy  $f(0) = 0$  and  $B(0) = 0$ . From now on the implicit dependence of the function  $f$  and  $B$  on the time  $t$  will be omitted.

A function  $u^* \in \mathcal{L}_{\text{loc}}^{\infty}(\mathbb{R}_{\geq 0}, \mathbb{R}^m)$  is said to be a *input signal or control* for (1). For such a control for (1), and for every *initial condition*  $x^*$ , there exists a solution to (1) ([2]). This solution is defined over an open interval  $(\underline{t}, \bar{t})$ , and is denoted,

at time  $t \in (\underline{t}, \bar{t})$ , by  $X(t, x^*, u^*)$ . This solution is said to be *forward complete* if  $\bar{t} = +\infty$ .

*Stabilizability Notion.* A forward complete  $X(t, x^*, u^*)$  to (1) is said to be *globally exponentially uniformly stabilizable* with rate  $\lambda > 0$  if there exist a constant value  $C > 0$  and a feedback law  $k^* : \mathbb{R}_{\geq 0} \times \mathbb{R}^n \rightarrow \mathbb{R}^m$  such that the inequality

$$|X(t, x^*, u^*) - X(t, x, k^*)| \leq Ce^{-\lambda t}|x^* - x| \quad (2)$$

holds true, for every  $t \geq 0$ , and for every  $x \in \mathbb{R}^n$  ([3]). Note that this is a particular case of *incremental asymptotic stability*. Although this later concept is not in the scope of this work, the interested reader may address [4], [5] for further information.

Note that a stronger condition than the global exponential stabilizability of a particular solution is the requirement that every forward complete solution of the system is globally exponentially stabilizable. This concept is formalized in the following definition recalled from [3].

**Definition 1.** The system (1) is said to be *universally stabilizable* with rate  $\lambda$  if there exists a feedback law  $k^* : \mathbb{R}_{\geq 0} \times \mathbb{R}^n \times \{x^*\} \times \{u^*\} \rightarrow \mathbb{R}^m$  for system (2) that globally exponentially uniformly stabilizes any forward complete solution  $X(\cdot, x^*, u^*)$  to (2).

Note that Definition 1 reduces to the notion of stabilizability of equilibria, when  $x^* = 0$  (for further reading on stabilizability, the reader may address [6]).

At this point, the problem under consideration in this paper can be stated as follows.

### Problem 2.

- 1) Find a feedback law  $k^* : \mathbb{R}_{\geq 0} \times \mathbb{R}^n \times \{x^*\} \times \{u^*\} \rightarrow \mathbb{R}^m$  for system (1) that globally exponentially uniformly stabilizes any forward complete solution  $X(\cdot, x^*, u^*)$  to (1);
- 2) The function  $k^* = (k_1^*, \dots, k_m^*)$  belongs to the set

$$\Xi = \{k^* : \mathbb{R}_{\geq 0} \times \mathbb{R}^n \times \{x^*\} \times \{u^*\} \rightarrow \mathbb{R}^m \mid k_i^* \in \mathcal{K}(i), i \in \mathbb{N}_{[1,n]}\}, \quad (3a)$$

where

$$\mathcal{K}(i) = \{j \in \mathbb{N}_{[1,n]} : k_i^* \text{ depends explicitly on } x_j\}. \quad (3b)$$

The definition of the set  $\mathcal{K}$  encompasses different structures. For instance, when  $m = n$  full decentralization implies that, for each index  $i \in \mathbb{N}_{[1,n]}$ , the component  $k_i^*$  of the function  $k^*$  depends only on  $x_i \in \mathbb{R}$ . This is formalized by letting  $\mathcal{K}(i) = \{i\}$ . Moreover, at points where  $k_i^*$  is differentiable, the explicit dependence on  $x_i$  means that, for every index  $j \in \mathbb{N}_{[1,n]}$  with  $j \neq i$ ,  $\partial k_i^* / \partial x_j \equiv 0$ .

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$$\partial_p M + \frac{\partial^2 M}{\partial x^2} M + \frac{\partial^2 M}{\partial x^2} M$$

$$k(x) = k(kx)?$$

$$k_i$$

$$k_i: x_i \mapsto u_i$$

$$\dot{x} = f(x, t)$$

The property described in item 2 of Problem 2 is particularly relevant for the design feedback laws with a prescribed structure (topology) for network systems rendering it universally stabilizable. Consider the network composed of systems described by the following equation.

$$\dot{x}_i = ?? \quad (4)$$

Section III shows how the approach proposed in this work is employed to design a decentralized controller for the network composed by interconnections of system (4).

### B. Background

*Riemannian metrics and differential formulation.* A Riemannian metric is a positive-definite bilinear form that depends smoothly on  $x \in \mathbb{R}^n$ . In a particular coordinate system, for any pair of vectors  $\delta_0, \delta_1$  of  $\mathbb{R}^n$  the metric is defined as the inner product  $\langle \delta_0, \delta_1 \rangle_x = \delta_0^\top M(x) \delta_1$ , where  $M : \mathbb{R}^n \rightarrow \mathbb{R}^{n \times n}$  is a smooth function. Consequently, local notions of norm  $|\delta_x|_x = \sqrt{\langle \delta_x, \delta_x \rangle_x}$  and orthogonality  $\langle \delta_0, \delta_1 \rangle_x = 0$  can be defined. The metric is said to be *bounded* if there exists constant values  $\underline{M} > 0$  and  $\bar{M} > 0$  such that, for every  $x \in \mathbb{R}^n$ ,  $\underline{M} I \leq M(x) \leq \bar{M} I$ .

Let  $\Gamma(x_0, x_1)$  be the set of piecewise-smooth curves  $\gamma : [0, 1] \rightarrow \mathbb{R}^n$  connecting  $x_0 = \gamma(0)$  to  $x_1 = \gamma(1)$ . The *length* and *energy* of  $\gamma$  are, respectively, defined by the values

$$\ell(\gamma) = \int_0^1 |\gamma'(s)|_{\gamma(s)} ds \quad \text{and} \quad e(\gamma) = \int_0^1 |\gamma'(s)|_{\gamma(s)}^2 ds.$$

The Riemannian distance between  $x_0$  and  $x_1$ , denoted as  $\text{dist}(x_0, x_1)$ , is defined as the curve with the smallest length connecting them. This curve is said to be a *geodesic* and it is the solution to the optimization problem.

$$\text{dist}(x_0, x_1) = \inf_{\gamma \in \Gamma(x_0, x_1)} \ell(\gamma). \quad (5)$$

A suitable framework to deal with exponential convergence of pair of solutions to (1) is provided by the *differential* (also known as variational or prolonged) dynamical system

$$\dot{\delta}_x = A(x, u)\delta_x + B(x)\delta_u, \quad (6)$$

where  $\delta_x$  (resp.  $\delta_u$ ) is a vector of the Euclidean space  $\mathbb{R}^n$  (resp.  $\mathbb{R}^m$ ). More precisely, it is the vector tangent to a piecewise smooth curve connecting a pair of points in  $\mathbb{R}^n$  (resp.  $\mathbb{R}^m$ ). The matrix  $A \in \mathbb{R}^{n \times n}$  has components given, for every  $(x, u) \in \mathbb{R}^n \times \mathbb{R}^m$ , by

$$A_{jk}(x, u) = \frac{\partial [f_j + b_j u_j]}{\partial x_k}(x, u),$$

for indexes  $j, k \in \mathbb{N}_{[1, n]}$ . Similarly to (1), given a control  $\delta_u : \mathbb{R}_{\geq 0} \rightarrow \mathbb{R}^m$ , the solution to (6) computed at time  $t \geq 0$  with  $(x, u) \in \mathbb{R}^n \times \mathbb{R}^m$  and issuing from the initial condition  $\delta_x \in \mathbb{R}^n$  is denoted by  $\Delta_x(t, x, \delta_x, u, \delta_u)$ .

The resulting system composed of Equations (1) and (6) is analyzed on the state space spanned by the vector  $(x, \delta_x) \in \mathbb{R}^n \times \mathbb{R}^n$ .

Lyapunov stability notions of solutions to (6) are similar to those of linear parameter-varying systems (LPVS) (see [7, Ch. 2 and 3] for more information on LPVS).

The importance of the stability of (6) for system (1) can be understood as follows. Let  $\Delta_x(\cdot, x, \delta_x, 0, 0)$  be a solution to (6) and  $X(\cdot, x, 0)$  be a solution to (1). If  $|\Delta_x(t, x, \delta_x, 0, 0)| \rightarrow 0$  exponentially as  $t \rightarrow \infty$ , then these solutions satisfy inequality (2). The interested reader may address [8], [9] and references therein for further details.

A sufficient condition for the stability of (6) is provided by analyzing the derivative of a particular function along the solutions of systems (1) and (6). This function is recalled from [4] and [3].

**Definition 3.** A smooth function  $V : \mathbb{R}^n \times \mathbb{R}^n \rightarrow \mathbb{R}_{\geq 0}$  is said to be a *metric for system (1)* if there exist constant values  $\underline{c} > 0$  and  $\bar{c} > 0$  such that the inequality

$$\underline{c}|\delta_x| \leq V(x, \delta_x) \leq \bar{c}|\delta_x|,$$

holds, for every  $(x, \delta_x) \in \mathbb{R}^n \times \mathbb{R}^n$ . It is said to be a *contraction metric for system (1)* if there exists a value  $\lambda > 0$  such that, for every  $(x, \delta_x) \in \mathbb{R}^n \times \mathbb{R}^n$ , the inequality

$$L_{f+Bx} V(x, \delta_x, 0, 0) \leq -\lambda V(x, \delta_x)$$

holds.

Note that a bounded metric is a contraction metric for system (1). Also, if the bounded metric is a contraction metric for system (1) with  $u \equiv 0$ , then inequality (2) holds. The proof for this claim can be found in [10, Theorem 1], and [11, Theorems 5.7 and 5.33], and [12, Lemma 3.3].

When inputs to systems (1) and (6) are not identically zero, a suitable feedback law and a contraction metric for system (1) need to be found.

This problem is solved by

- 1) Finding a function  $K : \mathbb{R}^n \rightarrow \mathbb{R}^{m \times n}$  and a differentiable metric for system (1) such that the inequality

$$\delta_x^\top (\dot{M} + (A + BK)M + M(A + BK)^\top - 2\lambda M) \delta_x \leq 0,$$

holds, for every  $(x, \delta_x, u) \in \mathbb{R}^n \times \mathbb{R}^n \times \mathbb{R}^m$ ;

- 2) Obtain the function  $k$  by integrating  $K$  along a geodesic in  $\mathbb{R}^n$ .

Note that item 1 is a co-design of a feedback law and a contraction metric. For this reason, the pair of functions  $(k, V)$  satisfying items 1 and 2 is said to be a *contraction pair* for system (1). Item 2 is the construction of the a feedback law for system (1) by integration.

The existence of a particular kind of metric satisfies items 1 and 2. Before presenting this result, the definition of this metric is recalled from [3].

**Definition 4.** A metric for system (1) is said to be a *control-contraction metric for system (1)* if there exists a constant value  $\underline{c} > 0$  such that the condition

$$\delta_x^\top M(x) B(x) = 0 \quad (7a)$$

implies that the inequality

$$\delta_x^\top (\dot{M} + A^\top M + M A) \delta_x \leq -2\lambda \delta_x^\top M \delta_x \quad (7b)$$

holds.



The set of equations (7) is an adaptation of Artstein-Sontag's condition for contraction.

The following result is recalled from [3] and provides a contraction pair for system (1).

**Theorem 5.** *If there exists a control-contraction metric for system (1), then there exists a contraction pair for system (1).*

As remarked in [3], the main advantage to look for control-contraction metric with respect to a control-Lyapunov function is that the former can be formulated in terms of a convex optimization problem [13]. The search for a contraction pair for system (1) can be done in terms of a convex optimization problem.

Step 1 (Offline LMI computation). Consider the change of variables  $\eta = M\delta$  and define the matrix  $W = M^{-1}$ . The set of equations (7) is equivalent (cf. [14, Lemma 11.1]) to the existence of a bounded differentiable function  $W : \mathbb{R}^n \rightarrow \mathbb{R}^{n \times n}$  such that  $W = W^\top \succ 0$  and a function  $Y : \mathbb{R}^n \rightarrow \mathbb{R}^{m \times n}$  satisfying the following linear matrix inequality (LMI)

$$-\dot{W} + AW + WA^\top + BY + (BY)^\top + 2\lambda W \preceq 0, \quad (8)$$

for every  $(x, u) \in \mathbb{R}^n \times \mathbb{R}^m$ .

Step 2 (Online controller integration). Once a solution to the LMI (8) has been found the feedback law for system (1) can be obtained by integration as follows. Let  $u^* : \mathbb{R}_{\geq 0} \rightarrow \mathbb{R}^m$  be a control for system (1) and  $K = YW^{-1}$ , from Hopf-Rinow theorem (cf. [15, Theorem 7.7]), for every  $x_0$  and  $x_1 \in \mathbb{R}^n$ , there exists a geodesic curve  $\gamma : [0, 1] \rightarrow \mathbb{R}^n$  connecting them. This implies that the functions

$$k(t) = u^*(t) + \int_0^1 K(\gamma(s))\gamma'(s) ds, \quad t \geq 0, \quad (9)$$

and  $M = W^{-1}$  are a contraction pair for system (1).

**Contribution.** At this point the two contributions of this paper becomes clear.

First, to impose a particular structure on the matrix  $Y$  satisfying the LMI (8) without imposing any structure on  $W$  is unfeasible, in general.

Second, without imposing any structure on  $W$ , the solution to the optimization problem (5) cannot be distributed. In terms of execution, the feedback law (9) would need to compute a new geodesic at each new time step. This motivates approach proposed in this paper.

## II. RESULTS

**Definition 6.** A control-contraction metric  $M$  for system (1) receives the adjective *sum-separable* if  $M$  has a block-diagonal structure. More precisely, there exist an integer  $N > 0$ , differentiable bounded functions  $M_i : \mathbb{R}^{n_i} \rightarrow \mathbb{R}^{n_i \times n_i}$ , where  $i \in \mathbb{N}_{[1, N]}$ , satisfying  $M_i = M_i^\top \succ 0$  for some integers  $n_i > 0$  such that  $M = (M_1, \dots, M_N)$  and  $n = n_1 + \dots + n_N$ .

Although the requirement of a control-contraction metric  $M$  to have block-diagonal structure may be restrictive, for positive linear time-invariant systems the existence of a symmetric positive definite matrices  $P$  with diagonal structure used as Lyapunov functions is not conservative [16]. Thus, the

question of how restrictive is the requirement of  $M$  be diagonal is open. The main result of the paper is stated below.

**Theorem 7.** *If there exist a differentiable function  $W : \mathbb{R}^n \rightarrow \mathbb{R}^{n \times n}$  such that  $W = W^\top \succ 0$ ,  $W$  is block-diagonal, and a function  $Y \in \Xi$  that is a solution to the LMI (8), then there exists a solution to Problem 2.*

The detailed proof of Theorem 7 is provided in Section IV. Theorem 7 implies that the a control-contraction metric  $M$  for system (7) can be obtained by inverting  $W$ .

Write about the network case

A particular case of Theorem 7 allows the computation of the LMI (8) in parallel. This is formalized in the following result.

**Corollary 8.** *Consider the differentiable function  $T : \mathbb{R}^n \times \mathbb{R}^n \rightarrow \mathbb{R}^{n \times n}$  with elements  $i, j \in \mathbb{N}_{[1, N]}$  defined as*

$$T_{ii} = -\dot{W}_i + A_{ii}W_i + W_iA_{ii}^\top + B_iY_{ii} + (B_iY_{ii})^\top + 2\lambda_iW_i$$

and

$$T_{ij} = A_{ij}W_j + W_iA_{ji} + B_iY_{ij} + (B_iY_{ij})^\top.$$

If, for every index  $i \in \mathbb{N}_{[1, N]}$  there exists a solution to the LMI

$$T_{ii} \preceq 0 \quad (10)$$

such that the matrix  $T$  is row-diagonal dominant, then there exists a solution to Problem 2.

The detailed proof of Corollary 8 is provided in Section IV.

## III. ILLUSTRATION

Here the an example of a network system will be used.

## IV. PROOF OF THE RESULTS

**Proof of Theorem 7.** By assumption, the function  $W : \mathbb{R}^n \rightarrow \mathbb{R}^{n \times n}$  is differentiable,  $W = W^\top \succ 0$ , and it is also block-diagonal. Moreover, the functions  $W$  and  $Y \in \Xi$  is a solution to the LMI (8).

The LMI (8) implies that the inequality

$$\eta^\top (-\dot{W} + AW + WA^\top + BY + (BY)^\top) \eta \leq -2\lambda \eta^\top W \eta \quad (11)$$

holds, for every  $(x, \eta, u) \in \mathbb{R}^n \times \mathbb{R}^n \times \mathbb{R}^m$ . Apply the coordinate change  $\eta = M\delta$  and define the matrices  $W = M^{-1}$  and  $K = YW^{-1}$ , inequality (12) implies that the inequality

$$\delta_x^\top (M + AM + MA^\top + MBK + (MBK)^\top) \delta_x \leq -2\lambda \delta_x^\top M \delta_x \quad (12)$$

holds, for every  $(x, \delta_x, u) \in \mathbb{R}^n \times \mathbb{R}^n \times \mathbb{R}^m$ . Consequently, the condition defined by the set of equations (7) holds. Thus,  $M$  is a sum-separable control-contraction metric for system (1).  $\square$

**Proof of Corollary 8.** a  $\square$

and local dependence!

$$\frac{M_i(x_i)}{M_i}$$

$$\sum_{i=1}^N \delta_i^\top M_i(x_i) \delta_i$$

## V. CONCLUSION

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