

Structured Nonlinear Feedback Design with Separable Control-Contraction Metrics

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Abstract—In this paper, input-affine nonlinear systems are considered. The problem under consideration is to design structured (for instance, decentralized or distributed) controllers for this class of systems. Although control-Lyapunov functions are the natural candidate to design these feedback laws, in terms of dynamical programming, the search for these functions is non-convex [1]. On the other hand, control-contraction metrics provide controllers that render pairs of solutions exponentially converge to each other. Moreover, the search for a structured controller and a suitable metric can be formulated in terms of a convex optimization problem. Under block-diagonal dominance conditions, this convex optimization problem can also be distributed. An example illustrates the approach for a network system.

Index Terms—Nonlinear Systems, Feedback Design, Contraction Theory, Distributed Control, Network Systems

I. INTRODUCTION

Over the years, methods for the design of controllers for dynamical systems has developed different techniques, according to the vector field that describes the system structure. The main concept employed for the control of dynamic systems is the Lyapunov's stability theory [2], [3]. In terms of computation, controller design problems are often translated in terms of dynamic programming.

For linear systems, controller design methods include H_∞ optimization [4] and LQR [5]. The design problems are usually formulated in terms of linear matrix inequalities (LMIs) and semidefinite programming [6], [7]. In the case of nonlinear systems, design approaches include high-gain [8], backstepping [9], and forwarding [10]. These methods depend on the structure of the vector field and may fail to be applied when appropriate conditions are not met [11]. In terms of numerical computation, often the techniques employed for feedback synthesis include sum-of-squares (SOS) optimization [12].

For those systems described by input-affine differential equations, the existence of a control-Lyapunov function (CLF) satisfying the so-called *small control property* provides a “universal” formula for a stabilizing feedback law [13], [14]. However, by the time that this paper was submitted, systematic methods for the search of a CLF were known only for particular systems within this class (see, for instance, [15]). In addition to the lack of a general systematic approach, the search for a CLF in terms of numerical optimization leads to a problem that is not necessarily convex nor connected [1].

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An alternative to CLFs is provided by the so-called control-contraction metrics (CCMs). One of the main advantages of CCMs over CLFs is that the feedback law is obtained by solving a convex optimization problem [16], due to the fact that the differential / variational formulation of the system is considered. The obtained controller makes every solution of the closed-loop system exponentially converge to a prescribed trajectory (see a precise definition below). This stability notion is related to contraction theory (an incremental stability property [17], [18], [19], [20], [21]) which can be traced back to the work [22].

The drawback of methods such as CCMs, H_∞ optimization and LQR is that, when the system under consideration has several states (large scale), it does not scale well. This is due to the fact that the stability verification of a system with n states may require a function with n^2 terms (see [23] for the case of linear systems and Lyapunov functions).

Large-scale systems may appear in the form of interconnection of smaller components, for example, in applications such as traffic networks [24], pipe networks [25] and sensor networks [26]. For such systems, a property often sought is the ability to augment or to reduce the size of the network without computing the controller for all subsystems, i.e., to make the controller scalable. In some cases, this property is satisfied by designing controllers with particular structures (see [27], [28] for distributed controllers).

In terms of dynamic programming, the problem of design controllers having an arbitrary structure is known to be NP-hard [29], [30], for linear systems. Consequently, for nonlinear systems the problem is very challenging.

In the case of linear systems whose solutions evolve in the positive orthant (positive systems), the problem of design a structured stabilizing feedback law has been addressed in [30]. Also, the authors show that the existence of such a controller is equivalent to the existence of Lyapunov function with a diagonal structure. The importance of this result for large-scale systems is highlighted in [23], where sparsity is explored to reduce the number of LMIs to be solved.

For nonlinear systems described by a non-fully connected graph, the design of structured controllers could be simplified by choosing structured Lyapunov functions (see [31] and references therein). However, the search for a general Lyapunov function is a non-trivial problem by itself [32]. The case can be even worse, when structural constraints are considered.

For this reason, the structured design of feedback laws for nonlinear systems is investigated with CCMs satisfying structural constraints, in this work. The systems under consideration are continuously differentiable and affine in the input. One of the key elements employed to design these

controllers is the concept of a Riemannian metric (see the definition below) which is employed, similarly to Lyapunov functions, to measure the exponential convergence of pairs of solutions. Employing CCMs that can be decomposed into the sum of smaller elements, the design of a structured feedback law allowing exponential convergence of solutions is obtained in two steps.

The first step consists of an off-line computation. The original system is extended with its *differential / variational* formulation (see definition below). The exponential convergence is reformulated in terms of stability of the origin for the extended system. This stability problem is written in terms of a convex optimization problem under the prescribed structural constraint. The solution consists of a pair of matrices: the Riemannian metric and the *differential / variational* feedback law. The second step consists of an on-line integration. The obtained *differential / variational* controller is integrated along geodesics (see definition below).

Although this method is applicable to systems described a strongly connected graph, it is particularly useful for **such systems**, as the number of equations needed to verify stability is smaller.

At this point, the contributions of this work can be highlighted. First, using the methodology for synthesis of CCMs introduced in [16] and imposing a (block-)diagonal structure constraint, a feedback law with **suitable** structure is obtained for nonlinear systems. Second, because the CCM has a (block-)diagonal structure, the computation of the on-line integration phase, which corresponds to an optimization problem, can be distributed. Third, when the system is described a non-strongly connected graph, the structure imposed on the CCM allows to reduce the number of equations needed to verify stability. Note that the proposed method provides an explicit formula for the controller, since it is constructive.

Other works related to analysis under structural constraints to achieve exponential convergence of solutions do exist in the literature. These are mostly related to network systems. For contraction analysis, see [33] for analysis according to different network topologies and [34] for transversal contraction analysis. This paper contrast with these works mainly in two points: 1) A methodology for the design of structured controllers is proposed; 2) Due the formulation of the stabilization problem as a convex optimization problem, not only an explicit formula of a structured controller is obtained but also a metric.

a) *Overview.*: The motivation and the problem formulation are provided in Section I-A. The background needed for this paper is stated in Section I-B. Section II presents the result of this paper. Illustrations of the proposed approach are provided in Section III. The proofs of the results are provided in Section IV. Section V collects final remarks.

b) *Notation.*: Let $N \in \mathbb{N}$ be a constant value. The notation $\mathbb{N}_{[1,N]}$ stands for the set $\{i \in \mathbb{N} : 1 \leq i \leq N\}$. Let $c \in \mathbb{R}$ be a constant value. The notation $\mathbb{R}_{[1,c]}$ (resp. $\mathbb{R}_{\diamond c}$) stands for the set $\{x \in \mathbb{R} : 1 \leq x \leq c\}$ (resp. $\{x \in \mathbb{R} : x \diamond c\}$, where \diamond is a comparison operator, i.e., $\diamond \in \{<, \geq, =, \text{etc}\}$). A matrix $M \in \mathbb{R}^{n \times n}$ with zero elements except (possibly) those m_{ii}, \dots, m_{nn} on the diagonal

is denoted as $\text{diag}(m_{ii}, \dots, m_{nn})$. The notation $M \succ 0$ (resp. $M \succeq 0$) stands for M being positive (resp. semi)definite.

The notation $\mathcal{L}_{\text{loc}}^{\infty}(\mathbb{R}_{\geq 0}, \mathbb{R}^m)$ stands for the class of functions $u : \mathbb{R} \rightarrow \mathbb{R}^m$ that are locally essentially bounded. Given differentiable functions $M : \mathbb{R}^n \rightarrow \mathbb{R}^{n \times n}$ and $f : \mathbb{R}^n \rightarrow \mathbb{R}^n$ the notation $\partial_f M$ stands for matrix with dimension $n \times n$ and with (i, j) element given by $\frac{\partial m_{ij}}{\partial x}(x)f(x)$. The notation f' stands for the total derivative of f .

A. Problem Formulation and Motivation

Class of systems. Consider the class of systems described by the differential equation

$$\dot{x}(t) = f(x(t)) + B(x(t))u(t), \quad (1)$$

where, for positive times t , the system state $x(t)$ and the system input variable $u(t)$ evolve in the Euclidean spaces \mathbb{R}^n and \mathbb{R}^m , respectively. The functions $f : \mathbb{R}^n \rightarrow \mathbb{R}^n$ and $B : \mathbb{R}^n \rightarrow \mathbb{R}^m$ are assumed to be smooth, i.e., infinitely differentiable and satisfy $f(0) = 0$ and $B(0) = 0$. From now on the dependence of on the time t will be omitted.

A function $u^* \in \mathcal{L}_{\text{loc}}^{\infty}(\mathbb{R}_{\geq 0}, \mathbb{R}^m)$ is said to be an *input signal or control* for (1). For such a control for (1), and for every *initial condition* x^* , there exists a unique solution to (1) ([35]) that is denoted by $X(t, x^*, u^*)$, when computed at time t . This solution is defined over an open interval (\bar{t}, \bar{t}) , and it is said to be *forward complete* if $\bar{t} = +\infty$.

Stabilizability Notion. A forward complete solution $X^*(\cdot, x^*, u^*)$ to (1) is said to be *globally exponentially uniformly stabilizable* with rate $\lambda > 0$ if there exist a constant value $C > 0$ and a feedback law $k^* : \mathbb{R}_{\geq 0} \times \mathbb{R}^n \rightarrow \mathbb{R}^m$, denoted as $k^*(\cdot, \cdot, X^*, u^*)$, such that the inequality

$$|X(t, x^*, u^*) - X(t, x, k^*)| \leq Ce^{-\lambda t} |x^* - x| \quad (2)$$

holds true, for every $t \geq 0$, and for every $x \in \mathbb{R}^n$ ([16]). Note that this not is a particular case of *incremental asymptotic stability*, the interested reader may address [21], [36] for further information on this stability concept.

Note that a stronger condition than the global exponential stabilizability of a particular solution is the requirement that every forward complete solution of the system is globally exponentially stabilizable. This concept is formalized in the following definition recalled from [16].

Definition 1. The system (1) is said to be *universally stabilizable* with rate λ if there exists a static feedback law k^* for system (2) that globally exponentially uniformly stabilizes any forward complete solution $X^*(\cdot, \cdot, u^*)$ to (1).

Note that Definition 1 reduces to the notion of stabilizability of equilibria, when $x^* = 0$ (for further reading on stabilizability, the reader may address [37]).

For each component $i \in \mathbb{N}_{[1,m]}$ of the feedback law $k^* = (k_1^*, \dots, k_m^*)^T$, denote the set of indexes

$$\mathcal{K}(i) = \{j \in \mathbb{N}_{[1,n]} : k_i^* \text{ depends explicitly on } x_j\}.$$

The definition of the set $\mathcal{K}(\cdot)$ encompasses different structures. For instance, when $m = n$, full decentralization implies that, for each index $i \in \mathbb{N}_{[1,n]}$, the component k_i^* of the

function k^* depends only on x_i . This is formalized by letting $\mathcal{K}(i) = \{i\}$. Moreover, at points where k_i^* is differentiable, the explicit dependence on x_i means that, for every index $j \in \mathbb{N}_{[1,n]}$ with $j \neq i$, $\partial k_i^* / \partial x_j \equiv 0$.

Define also the set of feedback laws

$$\Xi = \{k^* : \mathbb{R}_{\geq 0} \times \mathbb{R}^n \rightarrow \mathbb{R}^m : k_i^* \text{ has the property } \mathcal{K}(i)\}.$$

At this point, the problem under consideration in this paper can be stated as follows.

Problem 2.

- 1) Find a feedback law $k^* : \mathbb{R}_{\geq 0} \times \mathbb{R}^n \rightarrow \mathbb{R}^m$ for ~~system (1) that globally exponentially uniformly stabilizes any forward complete solution $X(\cdot, x^*, u^*)$ to (1);~~
- 2) The function $k^* = (k_1^*, \dots, k_m^*)$ belongs to the set Ξ .

The property described in item 2 of Problem 2 is particularly relevant for the design feedback laws with a prescribed structure (topology) ~~for network systems rendering it universally stabilizable.~~ Consider the network composed of systems described by the following equation.

$$\begin{cases} \dot{x}_i &= -x_i - x_i^3 + y_i^2 + 0.01(x_{i-1}^3 - 2x_i^3 + x_{i+1}^3) \\ \dot{y}_i &= u_i, \end{cases} \quad (3)$$

~~Section III shows how the approach proposed in this work is employed to design a decentralized controller for the network composed by interconnections of system (3).~~

B. Background

Riemannian metrics and differential formulation. A Riemannian metric is a positive-definite bilinear form that depends smoothly on $x \in \mathbb{R}^n$. In a particular coordinate system, for any pair of vectors δ_0, δ_1 of \mathbb{R}^n the metric is defined as the inner product $\langle \delta_0, \delta_1 \rangle_x = \delta_0^\top M(x) \delta_1$, where $M : \mathbb{R}^n \rightarrow \mathbb{R}^{n \times n}$ is a smooth function. Consequently, local notions of norm $|\delta_x|_x = \sqrt{\langle \delta_x, \delta_x \rangle_x}$ and orthogonality $\langle \delta_0, \delta_1 \rangle_x = 0$ can be defined. The metric is said to be *bounded* if there exists constant values $\underline{m} > 0$ and $\bar{m} > 0$ such that, for every $x \in \mathbb{R}^n$, $\underline{m}I_n \leq M(x) \leq \bar{m}I_n$, where $I_n \in \mathbb{R}^{n \times n}$ is the identity matrix.

Let $\Gamma(x_0, x_1)$ be the set of piecewise-smooth curves $\gamma : [0, 1] \rightarrow \mathbb{R}^n$ connecting $x_0 = \gamma(0)$ to $x_1 = \gamma(1)$. The *length* and *energy* of γ are, respectively, defined by the values

$$\ell(\gamma) = \int_0^1 |\gamma'(s)|_{\gamma(s)} ds \text{ and } e(\gamma) = \int_0^1 |\gamma'(s)|_{\gamma(s)}^2 ds.$$

The Riemannian distance between x_0 and x_1 , denoted as $\text{dist}(x_0, x_1)$, is defined as the curve with the smallest length connecting them. This curve is said to be a *geodesic* and it is the solution to the optimization problem.

$$\text{dist}(x_0, x_1) = \inf_{\gamma \in \Gamma(x_0, x_1)} \ell(\gamma). \quad (4)$$

A suitable notion to deal with exponential convergence of pair of solutions to (1) is provided by the *differential* (also known as variational or prolonged) dynamical system

$$\dot{\delta}_x = A(x, u)\delta_x + B(x)\delta_u, \quad (5)$$

where δ_x (resp. δ_u) is a vector of the Euclidean space \mathbb{R}^n (resp. \mathbb{R}^m). More precisely, it is the vector tangent to a piecewise smooth curve connecting a pair of points in \mathbb{R}^n (resp. \mathbb{R}^m). The matrix $A \in \mathbb{R}^{n \times n}$ has components given, for every $(x, u) \in \mathbb{R}^n \times \mathbb{R}^m$, by

$$A_{jk}(x, u) = \frac{\partial [f_j + b_j u_j]}{\partial x_k}(x, u)$$

for indexes $j, k \in \mathbb{N}_{[1,n]}$.

The resulting system composed of Equations (1) and (5) is analyzed on the state space spanned by the vector $(x, \delta_x) \in \mathbb{R}^n \times \mathbb{R}^n$.

Similarly to (1), given a control δ_u for system (5), the solution to (5) computed at time $t \geq 0$ with $(x, u) \in \mathbb{R}^n \times \mathbb{R}^n$ and issuing from the initial condition $\delta_x \in \mathbb{R}^n$ is denoted by $\Delta_x(t, x, \delta_x, u, \delta_u)$.

Lyapunov stability notions of solutions to (5) are similar to those of linear parameter-varying systems (LPVS) (see [38, Ch. 2 and 3] for more information on LPVS).

The importance of the stability of (5) for system (1) can be understood as follows. Given fixed controls u and δu for systems (1) and (5), respectively. If every solution $|\Delta_x(t, x, \delta_x, u, \delta u)| \rightarrow 0$ exponentially as $t \rightarrow \infty$, then every pair of solutions to (1) converge to each other exponentially. The interested reader may address [18], [20] and references therein for further details.

A sufficient condition for the stability of (5) is provided by analyzing the derivative of a particular function along the solutions of systems (1) and (5). This function is recalled from [21] and [16].

Definition 3. A smooth function $V : \mathbb{R}^n \times \mathbb{R}^n \rightarrow \mathbb{R}_{\geq 0}$ is said to be a *metric for system (1)* if there exist constant values $\underline{c} > 0$ and $\bar{c} > 0$ such that the inequality

$$\underline{c}|\delta_x|^2 \leq V(x, \delta_x) \leq \bar{c}|\delta_x|^2, \quad (6a)$$

holds, for every $(x, \delta_x) \in \mathbb{R}^n \times \mathbb{R}^n$. Given fixed controls u and δu for systems (1) and (5), respectively. A metric system (1) receives the adjective *contraction* if there exists a value $\lambda > 0$ such that the inequality

$$\frac{dV}{dt}(X(t, x, u), \Delta(t, x, \delta_x, u, \delta u)) \leq -\lambda V(x, \delta_x) \quad (6b)$$

holds, for every pair $(x, \delta_x) \in \mathbb{R}^n \times \mathbb{R}^n$.

Note that a bounded Riemannian metric defined, for every $(x, \delta_x) \in \mathbb{R}^n \times \mathbb{R}^n$, as $V(x, \delta_x) = |\delta_x|_x^2$ and satisfying the set of inequalities (6) is a contraction metric for system (1). With an abuse of concept, from now the bounded Riemannian metric defined above will be called simply as *metric*.

The existence a contraction metric for system (1) with $u \equiv 0$ implies that every two solutions of this system converge to each other exponentially. The proof of this claim can be found in [39, Theorem 1], and [40, Theorems 5.7 and 5.33], and [41, Lemma 3.3].

For the class of systems considered in this paper, the following kind of metric is of interest, since it also allows the design a feedback law for system (5).

Definition 4 ([16]). A metric for system (1) is said to be a *control-contraction metric for system (1)* if there exists a constant value $\lambda > 0$ such that the condition

$$\delta_x^\top M(x)B(x) = 0 \quad (7a)$$

implies that the inequality

$$\delta_x^\top (\dot{M} + A^\top M + MA)\delta_x \leq -2\lambda \delta_x^\top M \delta_x \quad (7b)$$

holds, where $\dot{M} := \partial_{f+Bu}M$.

The set of equations (7) is an adaptation of Artstein-Sontag's condition for exponential convergence of solutions. Given a control-contraction metric for system (1), Finsler's lemma (cf. [42, Lemma 11.1]) provides stabilizing a feedback law of the form $\delta_u = K\delta_x$ for system (5) defined for every $\delta_x \in \mathbb{R}^n$, where $K : \mathbb{R}^n \times \mathbb{R}^m \rightarrow \mathbb{R}^{n \times m}$.

The following result is recalled from [16] and provides a feedback law for system (1) given a feedback law for system (5).

Theorem 5. *If there exists a control-contraction metric for system (1), then a feedback law that is a solution to item 1 of Problem 2 is obtained by integrating the feedback law for system (5).*



As remarked in [16] (the main advantage to look for control-contraction metric with respect to a control-Lyapunov function is that the former case can be formulated in terms of a convex optimization problem while the later is non-convex [1]. The steps to obtain a control to system (1) that solves item 1 of Problem 2 are shown below.

Step 1 (Offline MI computation). Consider the change of variables $\eta = M\delta$ and define the matrix $W = M^{-1}$. The set of equations (7) is equivalent (cf. [42, Lemma 11.1]) to the existence of a bounded differentiable function $W : \mathbb{R}^n \rightarrow \mathbb{R}^{n \times n}$ such that $W = W^\top \succ 0$ and a function $Y : \mathbb{R}^n \times \mathbb{R}^m \rightarrow \mathbb{R}^{m \times n}$ satisfying the following matrix inequality (MI)

$$-\dot{W} + AW + WA^\top + BY + (BY)^\top + 2\lambda W \preceq 0, \quad (8)$$

that is linear on the matrix variables W and Y , for every $(x, u) \in \mathbb{R}^n \times \mathbb{R}^m$. Consequently, $M = W^{-1}$ is a control-contraction metric for system (1).

Step 2 (Online controller integration). The feedback law for system (1) can be obtained by integration as follows. Let $u^* : \mathbb{R}_{\geq 0} \rightarrow \mathbb{R}^m$ be a control for system (1) and $K = YW^{-1}$, from Hopf-Rinow theorem (cf. [43, Theorem 7.7]), for every x_0 and $x_1 \in \mathbb{R}^n$, there exist a smooth geodesic curve $\gamma : [0, 1] \rightarrow \mathbb{R}^n$ connecting them. This implies that the solution k^* to the integral equation

$$k^*(t, s) = u^*(t) + \int_0^s K(\gamma(\sigma), k^*(t, \sigma))\gamma'(\sigma) d\sigma, \quad (9)$$

where $s \in [0, 1]$, is a feedback law for system (1).

Motivation. From the above steps, even if the problem of imposing a particular structure on Y to correspond to the constraints of Problem 2 was tractable, the integration of the controller would not necessarily satisfy these constraints. This is due to the fact that the solutions to the optimization problem (4) can not be distributively computed.

Contribution. In this paper, these limitations are addressed by imposing a block-diagonal structure over W . Moreover, when W is row-diagonal dominant, not only the solutions to the optimization problem (4) can be computed in parallel but also the MI (8).

II. RESULTS

Definition 6. A control-contraction metric V for system (1) receives the adjective *sum-separable* if M has a block-diagonal structure.

Definition 6 implies that there exist integers $N > 1$ and $n_i > 0$ such that $n_1 + \dots + n_N = n$. Also, there exist smooth bounded functions $M_i : \mathbb{R}^{n_i} \rightarrow \mathbb{R}^{n_i \times n_i}$ satisfying $M_i = M_i^\top \succ 0$, for every index $i \in \mathbb{N}_{[1, N]}$, and the equation

$$V(x, \delta_x) = \sum_{i=1}^N \delta_{x_i}^\top M_i(x_i) \delta_{x_i} = \sum_{i=1}^N V_i(x_i),$$

for every $(x_i, \delta x_i) \in \mathbb{R}^{n_i} \times \mathbb{R}^{n_i}$.

In other words, a sum-separable metric is the case in which the metric V for system (1) is decomposed into a sum of components V_i , where $i \in \mathbb{N}_{[1, N]}$, each one of these components depend only on i -th component of the the system state x , i.e., $x_i \in \mathbb{R}^{n_i}$. The concept behind this definition is similar to the notion of sum-separable Lyapunov functions (see [31]).

To solve item 2 of Problem 2, the structure on the feedback defined in Equation (9) is obtained by imposing a a suitable constraint on the function Y to be satisfied together with the MI (8).

For each index $i \in \mathbb{N}_{[1, N]}$, define the sets

$$\mathcal{K}_Y(i) = \{j \in \mathbb{N}_{[1, N]} \setminus \mathcal{K}(i) : Y_{ij} \equiv 0\}$$

and

$$\Xi_Y = \{Y : \mathbb{R}^n \times \mathbb{R}^m \rightarrow \mathbb{R}^{m \times n} : \text{the } i\text{-th row } Y_i$$

has the properties $\mathcal{K}_Y(i)$ and $\mathcal{K}(i)\}$.

Note that the set $\mathcal{K}_Y(i)$ is the set index for which the corresponding columns of the row-vector Y_i are zero. By definition, this set is the complement of $\mathcal{K}(i)$. Consequently, given an index $j \in \mathcal{K}_Y$ and W is diagonal, the i -th line of the vector $YW^{-1}\delta_x$ does not depend on j -th component of the vector δ_x . As remarked in [30], the constraint “ $Y \in \Xi_Y$ ” is linear.

Theorem 7. *If there exist a smooth functions $W : \mathbb{R}^n \rightarrow \mathbb{R}^{n \times n}$ and $Y : \mathbb{R}^n \times \mathbb{R}^m \rightarrow \mathbb{R}^{m \times n}$ such that, for every $(x, \delta x, u) \in \mathbb{R}^n \times \mathbb{R}^n \times \mathbb{R}^m$, $W = W^\top \succ 0$, W is block-diagonal, $Y \in \Xi_Y$ and the pair (W, Y) is a solution to the MI (8), then there exists a solution to Problem 2.*

The detailed proof of Theorem 7 is provided in Section IV.

Although Theorem 7 provides a methodology to design distributed controllers, *a priori* the computation of the MI (8) cannot be done in parallel. The next result provides sufficient conditions to solve each component (8) independently, and according to the structure defined by the set Ξ . Before present

it, the following concept of block-diagonally dominant matrix is recalled from [44].

Consider the smooth function $T : \mathbb{R}^n \times \mathbb{R}^m \rightarrow \mathbb{R}^{n \times n}$ with elements $i, j \in \mathbb{N}_{[1, N]}$ defined as

$$T_{ii} = -\dot{W}_i + A_{ii}W_i + W_iA_i^\top + B_iY_{ii} + (B_iY_{ii})^\top + 2\lambda_i W_i \quad (11a)$$

and

$$T_{ij} = A_{ij}W_j + W_iA_{ji} + B_iY_{ij} + (B_jY_{ji})^\top. \quad (11b)$$

Definition 8. The matrix T is said to be *block-diagonally dominant* if the inequality

$$|T_{ii}^{-1}|^{-1} \geq \sum_{\substack{j=1 \\ j \neq i}}^N |T_{ij}|, \quad (12)$$

holds, for every index $i \in \mathbb{N}_{[1, N]}$ and for every $(x, u) \in \mathbb{R}^n \times \mathbb{R}^m$.

Corollary 9. If there exist a smooth functions $W : \mathbb{R}^n \rightarrow \mathbb{R}^{n \times n}$ and $Y : \mathbb{R}^n \times \mathbb{R}^m \rightarrow \mathbb{R}^{m \times n}$ such that, for every $(x, \delta x, u) \in \mathbb{R}^n \times \mathbb{R}^n \times \mathbb{R}^m$, $W = W^\top \succ 0$, W is block-diagonal, $Y \in \Xi_Y$ and the pair (W, Y) is a solution to the MI (8).

$$T_{ii} \leq 0 \quad (13)$$

for every index $i \in \mathbb{N}_{[1, N]}$, and the matrix T is diagonally dominant, then pair of matrices W and Y is a solution to the MI (8).

The detailed proof of Corollary 9 is provided in Section IV.

A. Discussion

Although the requirement of a sum-separable structure seems to be restrictive, for some classes of systems this structure is equivalent to the (possibly local) stability of the origin.

For monotone systems (i.e., systems for which the some order of initial conditions is preserved along the flow of the vector field) described by a vector field that is continuously differentiable and whose gradient matrix is Hurwitz at the origin, there exists a sum-separable Lyapunov function in a neighborhood of the origin [31, Theorem 3.4].

For linear time-invariant systems with the property that solutions starting in the positive orthant remain in the positive orthant (also known as positive systems), the stability of the origin is equivalent to the existence of a quadratic Lyapunov function described by a matrix $P = P^\top \succ 0$ with diagonal structure [30].

Based on these paragraphs, the question of how restrictive is the requirement of M to have a block-diagonal structure is open. As mentioned before, the main advantage to look for control-contraction metric with respect to a control-Lyapunov function is that the former case can be formulate in terms of a convex optimization problem while the later is non-convex [1].

III. ILLUSTRATION

A case where structured controller design is important is on distributed design for network systems.

Let $N > 0$ be a constant integer, for each index $i \in \mathbb{N}_{[1, N]}$, consider the following graph that described the network re-

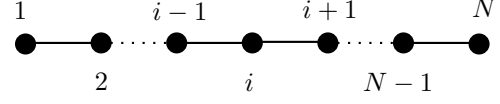


Figure 1. Graph describing the network composed of systems of the form (3).

sulting of connecting agents whose dynamics is described by the system

$$\begin{cases} \dot{x}_i &= -x_i - x_i^3 + y_i^2 + 0.01(x_{i-1}^3 - 2x_i^3 + x_{i+1}^3) \\ \dot{y}_i &= u_i, \end{cases} \quad (3)$$

where for convenience $x_0 = x_1$ and $x_N = x_{N+1}$.

For each index $i \in \mathbb{N}_{[1, N]}$, define the vectors $q_i = (x_i, y_i)$, $\check{q}_i = (x_{i-1}, x_{i+1})$ and let $q = (q_1, \dots, q_N)$. Denote also

$$f_i(q_i, \check{q}_i) = \begin{bmatrix} -x_i - x_i^3 + y_i^2 + 0.01(x_{i-1}^3 - 2x_i^3 + x_{i+1}^3) \\ 0 \end{bmatrix}$$

$$B_i = [0, 1]^\top.$$

Note that system (3) is not feedback linearizable in the sense of [45], because the vector fields

$$B = \text{diag}(B_1, \dots, B_N),$$

$$\frac{\partial f}{\partial q} B - \frac{\partial B}{\partial q} f = \text{diag} \left(\begin{bmatrix} 2y_1 \\ 0 \end{bmatrix}, \dots, \begin{bmatrix} 2y_N \\ 0 \end{bmatrix} \right)$$

are not linearly independent when $y_1 = \dots = y_N = 0$. Furthermore, due to the quadratic term on y , the only action of the controller on the x -subsystem is capable of is to move the x -component of solution to (3) towards the positive semi-axis. In other words, the controller cannot reduce the value of the x -component.

When $N \geq 6$ and Y is a full matrix with elements described by polynomials, the MI (8) could not be solved with the optimization parser Yalmip [46], [47] and the solver Mosek running on an Intel Core i7, 8GB RAM, Microsoft Windows 10 and on Matlab 2015b. A reason for this issue is the dependence of each element of the matrix Y on the variable q . Another reason is the need to verify if the matrix (8) is negative definite. When no structural constraints are imposed on Y , this verification can lead n^2 equations to be solved. This motivates the approach proposed in this paper.

To show the advantages of the method proposed in this paper, a benchmark was run for a network composes by $N = 4$ systems and in three scenarios, according to the constraints imposed on the matrix Y . Namely, the unconstrained case, the “neighbor case”, and the fully decentralized (diagonal) case. For the two latter cases, it was possible to consider up to $N = 256$ systems for the “neighbor case” and up to $N = 512$ systems for the fully decentralized (diagonal) case.

In all cases, the matrix W was required to have a block-diagonal structure as follows

$$W = \text{diag}(W_a, W_b, W_b, W_a),$$

the definition of the matrices W_a and W_b differs, according to each case considered.

In the first one, no constraints were imposed on the matrix Y and it was defined as a full matrix. ~~Note that~~

The parser took 98 seconds to solve the MI (8). The components of the matrix W and the matrix Y that form a solution to (8) are

$$W_a = \text{diag}(1.27, 1.53), \quad W_b = \text{diag}(1.08, 1.53)$$

and the matrix Y has the structure shown in Equation (14) with elements

$$\begin{aligned} \bar{Y}_{ij}(q) &= -3y_i - 0.08x_i y_i \\ \underline{Y}_{ij}(q) &= -2 + 0.009x_i - 1.2 \sum_{k=1}^4 y_k^2 + x_k^2. \end{aligned}$$

For the remaining cases, the constraints imposed on the matrix Y such that the matrix of the left-hand-side of the MI (8) is given by

$$\text{diag} \left(\begin{bmatrix} T_{11} & T_{12} \\ T_{12}^\top & T_{22} \end{bmatrix}, \dots, \begin{bmatrix} T_{(N-1)(N-1)} & T_{(N-1)N} \\ T_{(N-1)N}^\top & T_{NN} \end{bmatrix} \right).$$

This implies that sparsity can be exploited to decrease the number of verifications.

In the “neighbor” case, the constraint imposed on the matrix Y was that each line of this matrix should depend on the system i and on its neighbors. The set \mathcal{K} is defined, for each index $i = 2, 3$, as $\mathcal{K}(i) = \{i-1, i, i+1\}$, $\mathcal{K}(1) = \{1, 2\}$ and $\mathcal{K}(4) = \{3, 4\}$. Consequently, for each index $i \in \mathbb{N}_{[1,4]}$, the non-identically zero elements of the i -th line of the matrix Y depend on the variables q_{i-1} , q_i and q_{i+1} (note that, for convenience $q_0 = q_1$ and $q_5 = q_4$).

The time taken by the parser to solve the MI (8), in this case, was 3.5 seconds. The components of the matrix W and the matrix Y that form a solution to the (8) are

$$W_a = \text{diag}(1.32, 1.7) \quad \text{and} \quad W_b = \text{diag}(1.2, 1.6).$$

and the matrix Y has the structure shown in Equation (15) with elements

$$Y_{ij}(q_i, \check{q}_i) = -3.3y_i - 0.09x_i y_i$$

for pair of indexes (i, j) given as $(1, 1)$, $(2, 3)$, $(3, 5)$ and $(4, 6)$. Also,

$$\begin{aligned} Y_{12}(q_i, \check{q}_i) &= -2.8 - 0.01x_1 - 2(y_1^2 + y_2^2 + x_1^2 + x_2^2) \\ Y_{24}(q_i, \check{q}_i) &= -3 - 2(y_1^2 + y_2^2 + y_3^2 + x_1^2 + x_2^2 + x_3^2) \\ Y_{36}(q_i, \check{q}_i) &= -3 - 2(y_2^2 + y_3^2 + y_4^2 + x_2^2 + x_3^2 + x_4^2) \\ Y_{48}(q_i, \check{q}_i) &= -2.5 - 0.01x_4 - 1.5(y_3^2 + y_4^2 + x_3^2 + x_4^2) \end{aligned}$$

In the last case, the fully decentralized scenario has been considered. The time taken by the parser to solve the MI (8) was 2.6 seconds. In this case, $\mathcal{K}_Y(i) = \{j \in \mathbb{N}_{[1,N]} \setminus \mathcal{K}(i) : Y_{ij} \equiv 0\}$, where $\mathcal{K}(i) = \{i\}$. Imposing $Y \in \Xi_Y$ and solving

the MI (8) the following components the matrices W and Y were obtained

$$\begin{aligned} W &= \text{diag}(W_a, W_b, W_b, W_a), \\ Y &= \text{diag}(Y_1, Y_2, Y_3, Y_4) \end{aligned}$$

where

$$W_a = \text{diag}(1.4, 1.6), \quad W_b = \text{diag}(1.2, 1.6)$$

and, for each index $i = 1, 4$,

$$Y_i(q_i) = [-3.1y_i + 0.06x_i y_i, -3.6 - 0.02x_i - 2.3y_i^2 - 2.4x_i^2]$$

and, for each index $i = 2, 3$,

$$Y_i(q_i) = [-3.1y_i, -3.8 - 2.1y_i^2 - 2.2x_i^2].$$

Figure 2 shows a plot of the time taken by parser to the MI (8) for the three cases considered in this illustration: unconstrained, “neighbor” (the feedback law of system i depends only on q_i and \check{q}_i) and fully decentralized (the feedback law of system i depends on q_i only).

From the graph shown in Figure 2, for $N = 1, 2$, the time taken by the parser to solve the MI (8) of the same order of magnitude for the three cases. However, as the number of systems increases, the unconstrained case takes more time to be solved than the “neighbor”-constrained case which, in turn, takes more time than the fully decentralized-constrained case. The time difference between the two latter cases can be explained by fact that, for the “neighbor” case, each element of Y was defined as a polynomial of second degree on the variables q_i and \check{q}_i . While, for the fully decentralized case, Y was defined as a polynomial of second degree on the variable q_i only.

Regarding the on-line integration phase, since the matrices W computed in each case are constant for each index $i \in \mathbb{N}_{[1,4]}$, the geodesic curve connecting the origin to a point $q_i \in \mathbb{R}^2$ is a straight line: $\gamma_i(s) = sq_i$, for $s \in [0, 1]$. For each case, and for each index $i \in \mathbb{N}_{[1,4]}$, the feedback law given by the formula

$$k = \int_0^1 Y(sq)W^{-1}q ds.$$

Given the structure of the matrices Y and W , each line $i \in \mathbb{N}_{[1,4]}$ has the following structure

$$k_i = \begin{cases} \int_0^1 Y_i(sq)W_i^{-1}q_i ds, & \text{if unconstrained} \\ \int_0^1 Y_i(sq_i, \check{s}q_i)W_i^{-1}q_i ds, & \text{if “neighbor”} \\ \int_0^1 Y_i(sq_i)W_i^{-1}q_i ds, & \text{if fully decentralized.} \end{cases}$$

Moreover, the computed feedback law k globally exponentially uniformly stabilizes the origin for the network resulting from the interconnection of systems (3).

(solves Pg. 2)

$$Y(q) = \begin{bmatrix} \bar{Y}_{11}, & \bar{Y}_{12}, & -0.004y_1, & 0, & -0.04y_1 - 0.003x_3y_1, & 0.005y_1y_3, & -0.006y_1 + 0.001x_4y_1, & 0 \\ -0.006y_2, & 0, & \bar{Y}_{23}, & \bar{Y}_{24}, & -0.009y_2 - 0.001x_3y_2, & 0, & -0.04y_2 - 0.004x_4y_2, & 0.005y_2y_4 \\ -0.04y_3 - 0.004x_1y_3, & 0, & -0.008y_3 + 0.001x_2y_3, & 0, & \bar{Y}_{35}, & \bar{Y}_{36}, & -0.006y_3, & 0 \\ -0.006y_4 + 0.001x_1y_4, & 0, & -0.04 - 0.003x_2y_4, & 0, & -0.004y_4, & 0, & \bar{Y}_{47}, & \bar{Y}_{48} \end{bmatrix} \quad (14)$$

$$Y(q) = \begin{bmatrix} Y_{11}, & Y_{12}, & -0.001y_1, & 0, & 0, & 0, & 0, & 0 \\ -0.001(y_2 + x_1y_2), & 0, & Y_{23}, & Y_{24}, & -0.003y_2, & 0, & 0, & 0 \\ 0, & 0, & -0.002y_3, & 0, & Y_{35}, & Y_{36}, & -0.002y_3, & 0 \\ 0, & 0, & 0, & 0, & -0.003y_4, & 0, & Y_{47}, & Y_{48} \end{bmatrix} \quad (15)$$

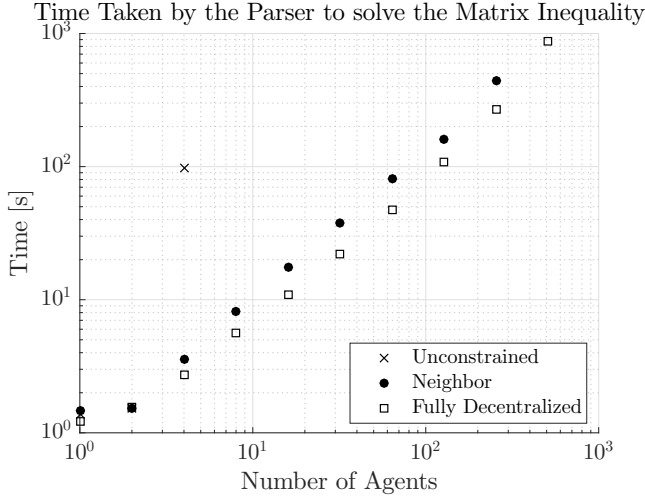


Figure 2. Time take by the parser to solve the MI (8) for the three cases under consideration. The number of agents started with one system and double each time. Axes are on log scale.

only 9 h, 356 in 512

IV. PROOF OF THE RESULTS

Proof of Theorem 7. By assumption, the functions $W : \mathbb{R}^n \rightarrow \mathbb{R}^{n \times n}$ and $Y : \mathbb{R}^n \times \mathbb{R}^m$ is a solution to the MI (8). Apply the coordinate change $\eta = M\delta$ and define the matrices $W = M^{-1}$ and $K = YW^{-1}$. Since W is diagonal, the structure of Y is preserved and, consequently, $K \in \Xi_Y$.

The MI (8) implies that the inequality

$$\delta_x^\top \left(\dot{M} + (A + BK)M + M(A + BK)^\top - 2\lambda M \right) \delta_x \leq 0$$

holds, for every $(x, \delta_x, u) \in \mathbb{R}^n \times \mathbb{R}^n \times \mathbb{R}^m$. Consequently, the condition defined by the set of equations (7) holds. Thus, M is a sum-separable control-contraction metric for system (1).

It now remains to integrate $K\delta_x$ to obtain a feedback law for system (1) satisfying the constraints of Problem 2. Because M is a block-diagonal matrix, the length of any curve $\varphi : [0, 1] \rightarrow \mathbb{R}^n$ satisfies the following equation

$$\ell(\varphi) = \int_0^1 \sqrt{\sum_{i=1}^N \varphi'_i(s_i)^\top M_i(\varphi_i(s_i)) \varphi'_i(s_i)} ds. \quad (16)$$

Since M is positive definite, the minimum of Equation (16) corresponds to a minimum of each component $i \in \mathbb{N}_{[1, N]}$. More precisely,

$$\gamma = \arg \inf \ell(\varphi) \Leftrightarrow \gamma_i = \arg \inf e(\varphi_i), \quad \forall i \in \mathbb{N}_{[1, N]}.$$

Consequently

This implies that the minimization of Equation (16) can be computed separately.

From Hopf-Rinow theorem (cf. [43, Theorem 7.7]), for every index $i \in \mathbb{N}_{[1, N]}$, and for every x_i and $x_i^* \in \mathbb{R}^{n_i}$, there exists a solution to the optimization problem

$$\gamma_i = \arg \inf_{\varphi_i \in \Gamma(x_i^*, x_i)} e(\varphi_i).$$

This solution is a geodesic smooth curve $\gamma_i : [0, 1] \rightarrow \mathbb{R}^{n_i}$ connecting x_i to $x_i^* \in \mathbb{R}^{n_i}$.

From the definition of the tangent vectors δ_x and δ_u , given an input u^* for system (1), a feedback for system (1) that solves item 1 of Problem 2 is given by Equation (9).

From the fundamental theorem of calculus, Equation (9) is equivalent to the differential equation

$$\frac{dk^*}{ds}(t, s) = K(\gamma(s), k^*(t, s))\gamma'(s) =: \bar{K}(t, s, k^*). \quad (17)$$

which has a unique solution defined of a maximal interval of existence, for every initial condition, due to the smoothness of the functions K and γ . It remains to show that this interval of existence can be extended on $[0, 1]$. In other words, to show that there exist no $\bar{s} \in [0, 1]$ such that $k^*(t, s) \rightarrow \infty$, as $s \rightarrow \bar{s}$.

To show that a solution k^* is defined on the whole interval $[0, 1]$, the result [35, Theorem 2.12] is employed. This theorem states that, if the vector field has a linear growth with respect to the variable k^* , then the solutions to (17) are defined on the whole interval $[0, 1]$.

Since the vector field \bar{K} is smooth, it also Lipschitz. This implies that, for every fixed $t \geq 0$, and for every $S > 0$, there exists constants $c_1(S)$ and $c_2(S)$ such that the inequality

$$|\bar{K}(t, s, k^*)| \leq c_1(S) + c_2(S)|k^*|$$

holds, for every $(s, k^*) \in [-S, S] \times \mathbb{R}^m$. Applying [35, Theorem 2.12] pointwisely at $t \geq 0$, implies that a solution k^* to (17) is defined for every $s \in [0, 1]$.

Note that, due to the structure of the matrix K , the feedback law k^* defined in Equation (9) solves item 2 of Problem 2, i.e., $k^* \in \Xi$. Furthermore, the computation of a solution to Equation (17) can be partially distributed, because each line of the matrix K will depend only on specific components of the vector φ^t .

This concludes the proof of Theorem 7. \square

Proof of Corollary 9. By assumption, the pair of matrices W and Y is a solution to the MI (13) and the matrix T with components defined by the set of equations (11) is block-diagonally dominant.

Equation (12) together with the fact that $|I_{n_i}| \leq |T_{ii}||T_{ii}^{-1}|$ implies that the inequality

$$\sum_{\substack{j=1 \\ j \neq i}}^N |T_{ij}| \leq |T_{ii}| \quad (18)$$

holds, for every index $i \in \mathbb{N}_{[1,N]}$.

For every $\delta_\eta \in \mathbb{R}^n$, consider the product $\delta_\eta^\top T \delta_\eta$. Each line $i \in \mathbb{N}_{[1,N]}$ of this product is given by

$$\delta_{\eta_i}^\top [T_{i1} \cdots T_{i(i-1)} \quad T_{ii} \quad T_{i(i+1)} \cdots T_{iN}] \delta_\eta.$$

Inequalities (18) and (13) imply that the inequalities

$$\sum_{\substack{j=1 \\ j \neq i}}^N \delta_{\eta_i}^\top T_{ij} \delta_{x_j} \leq \delta_{\eta_i}^\top T_{ii} \delta_{\eta_i} \leq 0$$

hold, for every $\delta_\eta \in \mathbb{R}^n$. Consequently, the inequality $\delta_\eta^\top T \delta_\eta \leq 0$ holds, for every $\delta_\eta \in \mathbb{R}^n$. This later inequality is equivalent to the MI (8). This concludes the proof of Corollary 9. \square

V. CONCLUSION

In this work, input-affine nonlinear systems were considered. The ~~considered~~ problem was the design of structured feedback laws. The methodology employed for synthesis was based on control-contraction metrics which provides a controller ensuring exponential convergence of pairs of solutions.

In terms of dynamic programming, employing control-contraction metrics allows one to formulate the search for the controller as a convex optimization problem. Although this is one of its main advantages in ~~comparison to~~ the search of control-Lyapunov functions, it does not scale well.

For systems described by a non-fully connected graph, the approach presented in this paper exploits ~~the~~ sparsity to design feedback laws with a prescribed structure. More precisely, by imposing a block-diagonal structure on the matrix describing the metric, a ~~structured~~ controller can be synthesized. Moreover, the on-line integration phase can be done in parallel, because each block defines a metric to the corresponding component of the state space where the geodesic is computed by optimization.

The authors plan to extend this work for the synthesis of event-based controllers, and the analysis of disturbances ~~like~~ time delays.

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REFERENCES

- [1] A. Rantzer, "A dual to Lyapunov's stability theorem", *Syst. & contr. lett.*, vol. 42, pp. 161–168, 2001.
- [2] N. P. Bhatia and G. P. Szegő, *Stability theory of dynamical systems*, ser. Classics in Mathematics. Springer, 1970.
- [3] N. Rouche, P. Habets, and M. Laloy, *Stability theory by Liapunov's direct methods*, ser. Applied mathematical sciences. Springer, 1977, vol. 22.
- [4] J. C. Doyle, B. A. Francis, and A. R. Tannenbaum, *Feedback control theory*. Macmillan Coll Div, 1992.
- [5] J. P. Hespanha, *Linear systems theory*. Princeton University Press, 2009.

- [6] S. Boyd, L. El Ghaoui, E. Feron, and V. Balakrishnan, *Linear matrix inequalities in system and control theory*, ser. Studies in Applied Mathematics. Society for Industrial and Applied Mathematics (SIAM), 1994, vol. 15.
- [7] G. E. Dullerud and F. Paganini, *A Course in Robust Control Theory*. Springer, 2000.
- [8] F. Gognard, R. Sepulchre, and G. Bastin, "Global stabilization of feedforward systems with exponentially unstable Jacobian linearization", *Syst. & contr. lett.*, vol. 37, no. 2, pp. 107–115, 1999.
- [9] M. Krstić, I. Kanellakopoulos, and P. V. Kokotović, *Nonlinear and adaptive control design*. Wiley, 1995.
- [10] F. Mazenc and L. Praly, "Adding integrations, saturated controls, and stabilization for feedforward systems", *IEEE Trans. Autom. Control*, vol. 41, no. 11, pp. 1559–1578, 1996.
- [11] H. Stein Shiromoto, V. Andrieu, and C. Prieur, "Relaxed and hybridized backstepping", *IEEE Trans. Autom. Control*, vol. 58, no. 12, pp. 3236–3241, 2013.
- [12] P. A. Parrilo, "Semidefinite programming relaxations for semi-algebraic problems", *Mathematical programming*, vol. 96, no. 2, pp. 293–320, 2003.
- [13] E. D. Sontag, "A Lyapunov-Like Characterization of Asymptotic Controllability", *SIAM J. Control Optim.*, vol. 21, no. 3, pp. 462–471, 1983.
- [14] —, "A 'universal' Construction of Artstein's Theorem on Nonlinear Stabilization", *Syst. & Contr. Lett.*, 1989.
- [15] F. Mazenc and M. Malisoff, "Further Constructions of Control-Lyapunov Functions and Stabilizing Feedbacks for Systems Satisfying the Jurdjevic–Quinn Conditions", *IEEE Trans. Autom. Control*, vol. 51, no. 2, pp. 360–365, 2006.
- [16] I. R. Manchester and J.-J. E. Slotine, "Control contraction metrics and universal stabilizability", in *Proceedings of the 19th IFAC world congress*, vol. 19, Cape Town, South Africa, 2014, pp. 8223–8228.
- [17] D. Angeli, "A Lyapunov approach to incremental stability properties", *IEEE Trans. Autom. Control*, vol. 47, no. 3, pp. 410–421, 2002.
- [18] W. Lohmiller and J.-J. Slotine, "On contraction analysis for nonlinear systems", *Automatica*, vol. 34, no. 6, pp. 683–696, 1998.
- [19] B. S. Rüffer, N. van de Wouw, and M. Mueller, "Convergent systems vs. incremental stability", *Sys.*, vol. 62, no. 3, pp. 277–285, 2013.
- [20] E. D. Sontag, "Contractive systems with inputs", in *Perspectives in mathematical system theory, control, and signal processing*, Springer, 2010, pp. 217–228.
- [21] F. Forni and R. Sepulchre, "A Differential Lyapunov Framework for Contraction Analysis", *IEEE transactions on automatic control*, vol. 59, no. 3, pp. 614–628, 2014.
- [22] D. C. Lewis, "Metric properties of differential equations", *American journal of mathematics*, vol. 71, no. 2, pp. 294–312, 1949.
- [23] A. Rantzer, "Scalable control of positive systems", *European journal of control*, vol. 24, pp. 72–80, 2015.
- [24] C. Canudas de Wit, F. Morbidi, L. Leon Ojeda, A. Y. Kibangou, I. Bellicot, and P. Bellemain, "Grenoble Traffic Lab: An Experimental Platform for Advanced Traffic Monitoring and Forecasting", *IEEE Control Systems Magazine*, vol. 35, no. 3, pp. 23–39, 2015.
- [25] C. de Persis and C. S. Kallesoe, "Pressure regulation in nonlinear hydraulic networks by positive and quantized controls", *IEEE transactions on control systems technology*, vol. 19, no. 6, pp. 1371–1383, 2011.
- [26] M. Pajic, S. Sundaram, G. J. Pappas, and R. Mangharam, "The wireless control network: A new approach for control over networks", *IEEE Trans. Autom. Control*, vol. 56, no. 10, pp. 2305–2318, 2011.
- [27] D. Điljak, *Decentralized Control of Complex Systems*. Academic Press, 1991.

- [28] H. Bai, M. Arcak, and J. Wen, *Cooperative control design: A systematic, passivity-based approach*, ser. Communications and Control Engineering. Springer, 2011, vol. 89.
- [29] V. Blondel and J. N. Tsitsiklis, “NP-Hardness of Some Linear Control Design Problems”, *SIAM J. Control Optim.*, vol. 35, no. 6, pp. 2118–2127, 1997.
- [30] T. Tanaka and C. Langbort, “The bounded real lemma for internally positive systems and h-infinity structured static state feedback”, *IEEE Trans. Autom. Control*, vol. 56, no. 9, pp. 2218–2223, 2011.
- [31] G. Dirr, H. Ito, A. Rantzer, and B. S. Rüffer, “Separable lyapunov functions for monotone systems: Constructions and limitations”, *Discrete and continuous dynamical systems series b (DCDS-B)*, vol. 20, no. 8, pp. 2497–2526, 2015.
- [32] M. Malisoff and F. Mazenc, *Constructions of strict lyapunov functions*. Springer, 2009.
- [33] Z. Aminzare and E. D. Sontag, “Synchronization of diffusively-connected nonlinear systems: Results based on contractions with respect to general norms”, *IEEE transactions on network science and engineering*, vol. 1, no. 2, pp. 91–106, 2014.
- [34] V. Andrieu, B. Jayawardhana, and L. Praly, “Transverse exponential stability and applications”, *IEEE Trans. Autom. Control*, 2016, (to appear).
- [35] G. Teschl, *Ordinary differential equations and dynamical systems*. American Mathematical Society, 2012, vol. 1XX.
- [36] F. Forni and R. Sepulchre, “Differential analysis of nonlinear systems: Revisiting the pendulum example”, in *Proceedings of the 53rd IEEE conference on decision and control*, 2014, pp. 3848–3859.
- [37] A. Bacciotti, *Local stabilizability of nonlinear control systems*. World Scientific Publishing Company, 1992.
- [38] C. Briat, *Linear parameter-varying and time-delay systems*. Springer, 2015.
- [39] D. C. Lewis, “Differential equations referred to a variable metric”, *American journal of mathematics*, vol. 73, no. 1, pp. 48–58, 1951.
- [40] S. Reich and D. Shoikhet, *Nonlinear semigroups, fixed points, and geometry of domains in banach spaces*. Imperial College Press, 2005.
- [41] G. Isac and S. Z. Nemeth, *Scalar and asymptotic scalar derivatives: Theory and applications*. Springer, 2008, vol. 13.
- [42] G. Calafiore and L. El Ghaoui, *Optimization models*. Cambridge University Press, 2014.
- [43] W. M. Boothby, *An introduction to differentiable manifolds and Riemannian geometry*. Academic Press, 1986.
- [44] C.-Y. Zhang, Y.-T. Li, and F. Chen, “On schur complement of block diagonally dominant matrices”, *Linear algebra and its applications*, vol. 414, no. 2-3, pp. 533–546, 2006.
- [45] A. Isidori, *Nonlinear control systems*, ser. Communications and Control Engineering. Springer, 1995.
- [46] J. Löfberg, “YALMIP : A toolbox for modeling and optimization in MATLAB”, in *Proceedings of the IEEE international symposium on computer aided control systems design*, Taipei, Rep. of China, 2004, pp. 284–289.
- [47] —, “Pre- and post-processing sum-of-squares programs in practice”, *IEEE Trans. Autom. Control*, vol. 54, no. 5, pp. 1007–1011, 2009.