

# Rotating Reference Frames



Simplified Frame

$S_0$  = inertial reference frame w/ acceleration  $A$  (capital letters for acc and velocity relative to  $S_0$ )

$S$  = non-inertial reference frame (ex) frame fixed in a railroad car that is moving relative to  $S_0$  w/ velocity  $V$ ,  $A = \dot{V}$

Suppose a passenger is playing catch w/ a ball of mass  $m$   
Consider the motion of the ball measured relative to  $S_0$

Since  $S_0$  is inertial

$$F = m\ddot{r}$$

Ball's position relative to  $S_0$

$F$  is the net force, gravity, air resistance etc...

Now consider the ball's motion relative to the accelerating frame  $S$

$$\ddot{r}_0 = \ddot{r} + V$$

Let's understand why this is the case

$$\begin{aligned} r_0 &= \text{position of ball in inertial frame} \\ r &= \text{position of ball in non-inertial frame} \\ V &= \text{Velocity of car} \end{aligned}$$

$\therefore r_0$  i.e. (ball's velocity relative to ground) =  
(ball's velocity relative to car) + (car's velocity rel to ground)  
makes sense because the persons inside velocity +  
plus the car's velocity is what person on ground  
would see

Now we can take that equation and differentiate it

$$\ddot{r} = \ddot{r}_0 - A$$

and solve for

multiply by  $m$

$$m\ddot{r} = F - mA$$

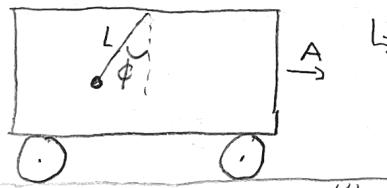
$m\ddot{r}$  = inertial frame's total net force  
eq 9.4

looks totally like a  $F = ma$  for the non-inertial frame except for the extra term  $-mA$ . Call it the inertial force

Inertial force is the force you experience when you accelerate really fast and get pushed into your seat

[another example] Standing on a bus when it suddenly breaks,  $A$  is backward so you feel the  $+mA$  forward and you fall on your face

Example • A pendulum inside a car  $\rightarrow$  find the equilibrium angle  $\phi_{eq}$  and the frequency of small oscillations about  $\phi_{eq}$   
\* in an inertial frame there is just two forces, Tension and weight.  $F = T + mg$



If we choose to work in a non-inertial frame we need  $-mA$  term

$$m\ddot{r} = (T + mg) - mA$$

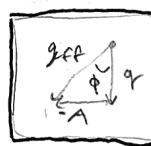
rearranging

$$m\ddot{r} = T + m(g - A)$$

$$g_{eff} = g - A$$

(no  $A$ ) normally it reaches equilibrium

but there is  $A$  it'll be



if at rest  $\ddot{r} = 0$

then  $T = -mg_{eff}$   $\rightarrow$  then from our picture

$$\phi_{eq} = \arctan(\frac{A}{g})$$

Small amplitude frequency for  $\omega = \sqrt{\frac{g}{L}}$  but here  $g_{eff} = g_{eff} = \sqrt{g^2 + A^2}$

Why do this in non-inertial? you could do it in inertial, finding  $\omega_{eff}$  isn't too bad you know  $T + mg = mA$  but  $\omega_{eff}$  of small oscillations is very difficult

$$\omega = \sqrt{\frac{g_{eff}}{L}}$$

TIDES a beautiful result of  $m\ddot{r} = F - mA$

Wrong

Right



a single bulge would have one tide per day when there is two.

An object on earth feels the force of the moon as if it were coming from earth's center

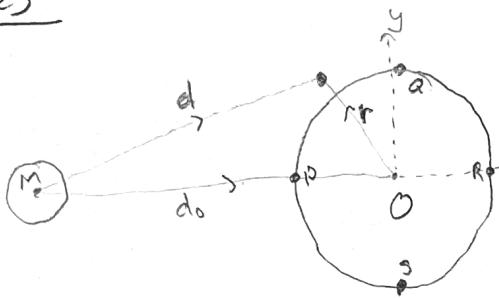
An object on the moon side is pulled by the moon w/ a force that is slightly greater than it would be at the center

On the other side is pulled by the moon that is slightly weaker than it would be which causes another bulge

math explanation on back

# Tides

Using  $m\ddot{r} = F - mA$  we want to figure out the



Forces on mass  
m near earth's  
surface is

- $m_E g$  (gravity of the earth)
- $-\frac{GM_m m}{d^2} \hat{d}$  (gravity of moon)

$F_{\text{tidal}}$  (like buoyant force for ex)

$[F = mg - \frac{G(M_m)m}{d^2} \hat{d} + F_{\text{grav}}] \rightarrow$  But what is  $A$ ? Well this is the car's acceleration it experienced. The car in this situation is the Earth and the acceleration or force it experiences is from the moon

$$[A = -\frac{G M_m}{d_0^2} \hat{d}_0]$$

\* putting it together

\*  $M_m = \text{mass of moon} *$

$$m\ddot{r} = [mg - \frac{G M_m m}{d^2} \hat{d} + F_{\text{grav}}] + \frac{G M_m m}{d^2} \hat{d}$$

(Combine  
 $M_m$  terms)

$$\rightarrow \overset{\text{ex 9.12}}{F_{\text{tidal}}} = -G M_m m \left( \frac{\hat{d}}{d^2} - \frac{\hat{d}_0}{d_0^2} \right) \rightarrow m\ddot{r} = F_{\text{tidal}} + F_{\text{grav}}$$

entire effect of the moon on the motion of any object near earth



distance from  
moon to earth

distance at earth  
surface to moon

[Let's analyze this equation]

At point P,  $d$  and  $d_0$  lie in the same direction,  $d = \vec{r}_P$ ,  $d_0 = \vec{R}_P$ , but  $d_0 > d$

so the first term dominates and the tidal force is toward the moon

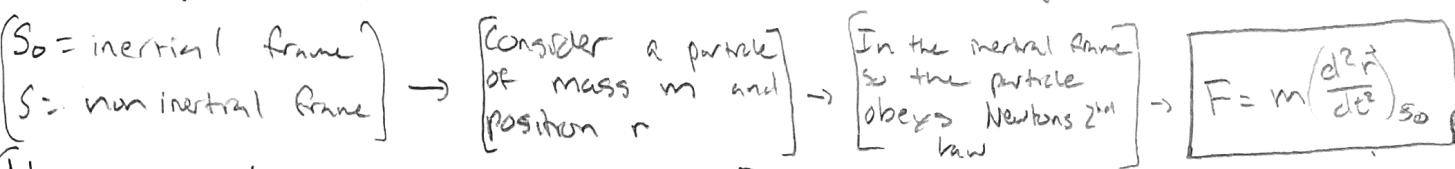
At point R,  $d_0 < d$  so the second term dominates but is negative so it points away from the moon

(so thus you get  
your outward  
bulges)

(could do for point Q, I just know  
they almost cancel except for y-component  
which goes rise to both sides)

## Newton's Second Law in rotating frame S

Assume angular velocity  $\vec{\omega}$  of S relative to  $S_0$  is constant, (good approximation for axis fixed to Earth)



Now we need to find  $F_{\text{inertial}}$  in the non-inertial frame S  $\rightarrow (\text{use relation how we have } \left( \frac{d^2 \vec{r}}{dt^2} \right)_{S_0} = \left( \frac{d}{dt} \right)_{S_0} \left( \frac{d \vec{r}}{dt} \right)_{S_0} + \vec{\omega} \times \vec{r}) \rightarrow \left( \frac{d \vec{r}}{dt} \right)_{S_0} = \left( \frac{d \vec{r}}{dt} \right)_S + \vec{\omega} \times \vec{r})$ , now differentiable.

$$\left( \frac{d^2 \vec{r}}{dt^2} \right)_{S_0} = \left( \frac{d}{dt} \right)_{S_0} \left( \frac{d \vec{r}}{dt} \right)_{S_0} = \left( \frac{d}{dt} \right)_{S_0} \left[ \left( \frac{d \vec{r}}{dt} \right)_S + \vec{\omega} \times \vec{r} \right] \quad (\text{apply Q.30 again}) \rightarrow \left( \frac{d \vec{Q}}{dt} \right)_{S_0} = \left( \frac{d \vec{Q}}{dt} \right)_S + \vec{\omega} \times \vec{Q}$$

$$\left( \frac{d^2 \vec{r}}{dt^2} \right)_{S_0} = \left( \frac{d}{dt} \right)_S \left[ \left( \frac{d \vec{r}}{dt} \right)_S + \vec{\omega} \times \vec{r} \right] + \vec{\omega} \times \left[ \left( \frac{d \vec{r}}{dt} \right)_S + \vec{\omega} \times \vec{r} \right], \quad \begin{matrix} \text{use } d \vec{Q} \\ \text{not } d \vec{r} \\ \text{for non-inertial frame} \end{matrix} \quad \left( \frac{d \vec{Q}}{dt} \right)_S = \vec{Q}$$

\*  $\vec{\omega}$  is constant

$$\left( \frac{d^2 \vec{r}}{dt^2} \right)_{S_0} = \ddot{\vec{r}} + 2\vec{\omega} \times \dot{\vec{r}} + \vec{\omega} \times (\vec{\omega} \times \vec{r}) \quad \leftarrow \vec{r}, \dot{\vec{r}}, \ddot{\vec{r}} \text{ are derived w.r.t. the rotating frame S}$$

$\boxed{\text{apply newtons law and solve for } \ddot{\vec{r}}}$

$$m \ddot{\vec{r}} = \vec{F}_{\text{apparent}} = \vec{F} + 2m \dot{\vec{r}} \times \vec{\omega} + m(\vec{\omega} \times \vec{r}) \times \vec{\omega}$$

last 3 terms aren't forces but purely consequences of the rotation of the body but we can pretend they are forces

$$\boxed{\vec{F}_{\text{cor}} = +2m \dot{\vec{r}} \times \vec{\omega}}$$

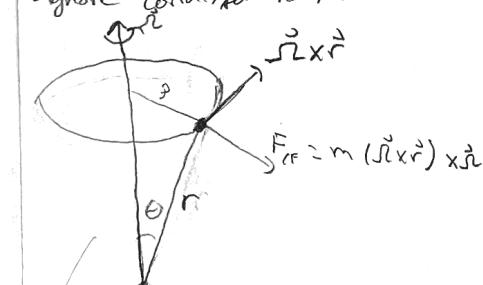
can't be plusses up  
conflicting results

\* check signs of cross product  
flip them

$$\boxed{\vec{F}_{\text{centrifugal}} = +m(\vec{\omega} \times \vec{r}) \times \vec{\omega}}$$

ignore coriolis for now, smaller than  $\vec{F}_{\text{cf}}$

$$\vec{F}_{\text{cf}} = m(\vec{\omega} \times \vec{r}) \times \vec{\omega} = (m \vec{\omega} r \sin \theta) \times \vec{\omega} = m \omega^2 r \sin \theta \hat{\rho} = m r^2 \rho \sin \theta \hat{\rho}$$



A body in free fall to Earth's surface

$$\vec{F}_{\text{ext}} = \vec{F}_{\text{grav}} + \vec{F}_{\text{cf}} = m \vec{g}_0 + m \omega^2 r \sin \theta \hat{\rho}$$

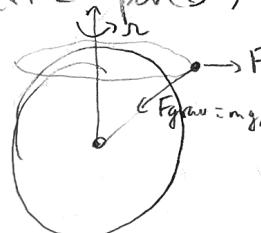
plugging out m,  $\vec{g} = \vec{g}_0 + \omega^2 r \sin \theta \hat{\rho}$

$\sin \theta \text{ b/c } \hat{\rho} = \sin \theta \hat{\phi}$

$$\boxed{\text{Now } g_{\text{grad}} = g \text{ in the direction of } -\vec{r} = g_0 - \omega^2 r \sin^2 \theta}$$

(more like 0.5% change of Earth's gravity)

\* zero at poles,  $g_0 \approx 9.8 \text{ m/s}^2$ , the value of g at the equator is 0.3% less than at the poles



$\vec{g}$  also has a tangential acceleration,  $a_{\text{tan}} = \omega^2 r \sin \theta \cos \theta$

\* zero at poles and equator, max at latitude of  $45^\circ$

$$\alpha_{\text{max}} = \frac{g_{\text{tan}}}{g_{\text{grad}}} = \frac{\omega^2 r}{g_0} = \frac{0.0034}{9.8} = 0.0017 \text{ rad} \approx 0.1^\circ$$



angle between  
radial  
and  
direction  
of  
 $\vec{g}$

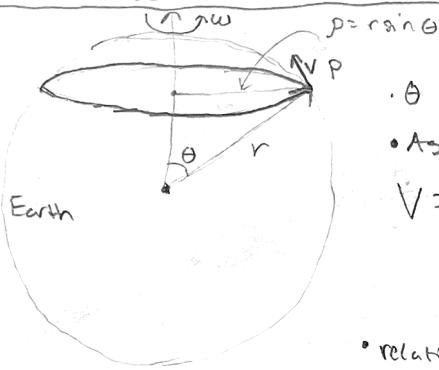
## Angular Velocity Vector

is hard to prove but fairly natural

motion of any body relative to a fixed point  $O$  is a rotation about some axis through  $O$ .

- rotating reference frames and [Euler's theorem]
- concerned w/ rate of rotation or angular velocity,  $\omega = \frac{d\theta}{dt}$  and  $\vec{\omega} = \omega \cdot \hat{e}$
- to get the direction of  $\vec{\omega}$  use the RHTR and curl Angers in direction of spinning
- $\vec{\omega}$  can change in direction and magnitude

## Relation between $\vec{\omega}$ and the linear velocity on the body



•  $\theta$  is the colatitude

• As Earth rotates about its axis "P" is dragged with radius  $p = r \sin \theta$

$$V = \omega p = \omega r \sin \theta \Rightarrow \vec{V} = \vec{\omega} \times \vec{r}$$

↑ distance  
angle/sec

• relation for any vector fixed in the rotating body

If  $\hat{e}$  is a unit vector fixed in Earth then

$$\frac{de}{dt} = \vec{\omega} \times \hat{e}$$

← its rate of change as seen by the non-rotating frame

you can add  $\vec{\omega}$   $\Rightarrow V_{31} = V_{32} + V_{21}$  now let's say w/ same  $\vec{\omega}$  they are rotating  $\rightarrow \vec{\omega}_{31} \times \vec{r} = (\vec{\omega}_{32} \times r) + (\vec{\omega}_{21} \times r) = (\vec{\omega}_{32} + \vec{\omega}_{21}) \times r$

Frame 3 Velocities in relative frames  $\vec{v}_{32}$   $\vec{v}_{21}$   $\vec{\omega}_{32}$   $\vec{\omega}_{21}$   $\vec{\omega}_{31}$   $\vec{\omega}_{31} = \vec{\omega}_{32} + \vec{\omega}_{21}$

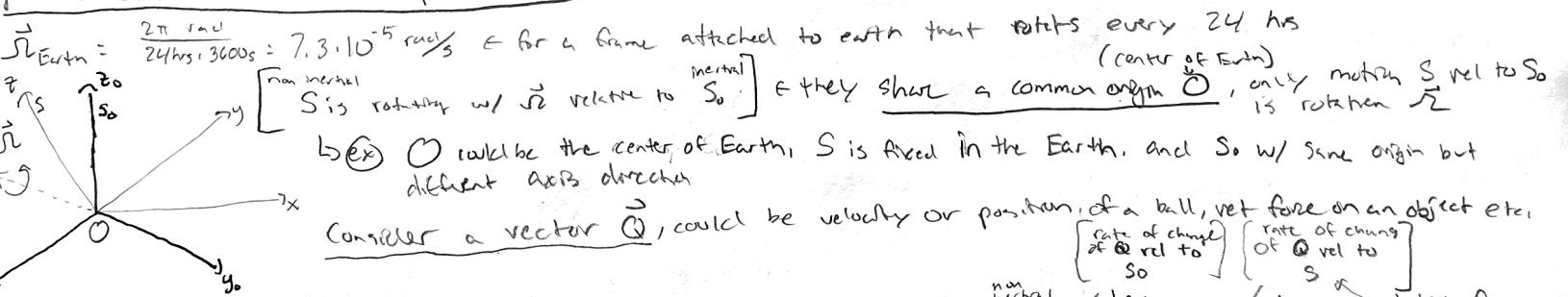
$\vec{\omega}$  for angular velocity, like spinning top

$\vec{A}$  and  $\vec{V}$  for accel and vel of non-inertial frame as well

$\vec{\omega}$  for angular velocity of noninertial, rotating ref frame, relative to which we are calculating the motion of objects

## Time derivatives of rotating ref frame

$S_0$  = inertial frame,  $S$  = non-inertial frame w/ angular velocity  $\vec{\omega}$  rel to  $S_0$



Relate  $\frac{d\vec{Q}}{dt}$  measured in  $S_0$  to the corresponding rate in  $S$ ,  $\left(\frac{d\vec{Q}}{dt}\right)_{S_0}, \left(\frac{d\vec{Q}}{dt}\right)_S$

$$\vec{Q} = Q_1 \hat{e}_1 + Q_2 \hat{e}_2 + Q_3 \hat{e}_3 \quad \text{for example these vectors could be along } \vec{x}, \vec{y}, \vec{z}. \text{ So in frame } S \text{ they are fixed but in } S_0 \text{ they are rotating}$$

Differentiate as seen in frame  $S_0$   $\left(\frac{d\vec{Q}}{dt}\right)_{S_0} = \sum \left(\frac{dQ_i}{dt}\right) \hat{e}_i$

compute w/  $\frac{de}{dt} = \vec{\omega} \times e$

$e_i$  is fixed in  $S$  which is rotating w/ angular velocity  $\vec{\omega}$  relative to  $S_0$

$$\left(\frac{dQ_i}{dt}\right)_{S_0} = \sum \left(\frac{dQ_i}{dt}\right) e_i + \sum Q_i \left(\frac{de_i}{dt}\right)_{S_0}$$

$$\therefore \left(\frac{d\vec{Q}}{dt}\right)_{S_0} = \vec{\omega} \times \vec{Q} + \sum Q_i \left(\frac{de_i}{dt}\right)_{S_0} = \vec{\omega} \times \vec{Q} + \sum Q_i (\vec{\omega} \times \hat{e}_i)$$

$$\left(\frac{d\vec{Q}}{dt}\right)_{S_0} = \left(\frac{d\vec{Q}}{dt}\right)_S + \vec{\omega} \times \vec{Q}$$

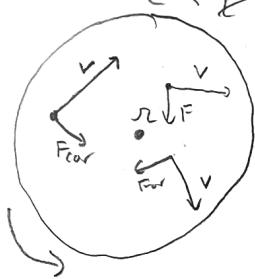
relates derivative of any vector  $\vec{Q}$  measured in inertial frame  $S_0$ , to the corresponding derivative in non-inertial frame  $S$

# The Coriolis Force

$$F_{\text{Cor}} = 2m \vec{\omega} \times \vec{r} = 2m \vec{v} \times \vec{\omega}, \vec{v}$$
 is the object's velocity relative to the rotating frame

↳ Force is always  $\perp$  to the velocity of an object

A turntable



↳ tends to deflect objects to the right in Northern Hemisphere  
If  $\vec{\omega}$  polarity flipped, like in Southern Hemisphere the world deflect to the left +

↳ See John R. Taylor  
example about a puck on a turn table



A cyclone gets started by coriolis

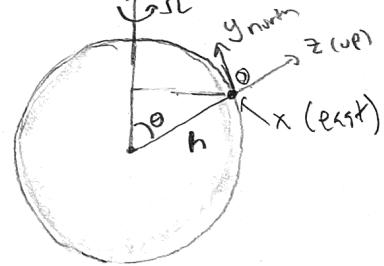
## Free fall w/ coriolis & centrifugal

$$m\ddot{r} = m\vec{g}_0 + \vec{F}_{\text{cp}} + \vec{F}_{\text{cor}} = m\vec{g}_0 + m(\vec{r} \times \vec{\omega}) \times \vec{\omega} + 2m\vec{\omega} \times \vec{r}$$

$$\ddot{r} = (\vec{r} \times \vec{\omega}) \times \vec{\omega} + 2\vec{\omega} \times \vec{r}, \text{ we define } g = g_0 + (\vec{r} \times \vec{\omega}) \times \vec{\omega} = \vec{g}_0 + \frac{r^2}{R^2} R^2 m \vec{\omega}$$

$$\boxed{\ddot{r} = \ddot{g} + 2\vec{\omega} \times \vec{r}}$$

↳ the net force on object doesn't depend on its position  $r$  → lets more the origin to the surface than



↳ [Now position  $P$  is relative to this  $O$ ],  $r = (x, y, z)$

$$\vec{r} = (0, R \sin \theta, R \cos \theta) \text{ then } \vec{r} \times \vec{\omega} = (y R \cos \theta - z R \sin \theta, -x R \cos \theta, x R \sin \theta)$$

$$\begin{bmatrix} \ddot{x} \\ \ddot{y} \\ \ddot{z} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ -g \end{bmatrix} + 2 \begin{bmatrix} y R \cos \theta - z R \sin \theta \\ -x R \cos \theta \\ x R \sin \theta \end{bmatrix}$$

$$\rightarrow \begin{aligned} \ddot{x} &= 0 & \rightarrow x = 0 \\ \ddot{y} &= 0 & \rightarrow y = 0 \\ \ddot{z} &= -g & \rightarrow z = h - \frac{1}{2}gt^2 \end{aligned}$$

zeroth order, no coriolis effects shown

## Next approximation

↳ since zeroth order is a good approx sub it in for original equation you get

$$\begin{aligned} x &= 2Rgt \sin \theta & \rightarrow x = \frac{1}{3}Rgt^3 \sin \theta & \text{t causes the object to deflect in the x-direction (east)} \\ y &= 0 & \rightarrow y = 0 \\ z &= -g & \rightarrow z = h - \frac{1}{2}gt^2 & \text{if an object dropped from it would deflect} \\ & & \approx 2.2 \text{ cm} & \end{aligned}$$

All the information contained in the mass distribution that is needed to solve rotational dynamics problems is contained in the moment of inertia tensor.  
 It relates  $\vec{\omega}$  to  $\vec{L}$

## Motion of Rigid Bodies

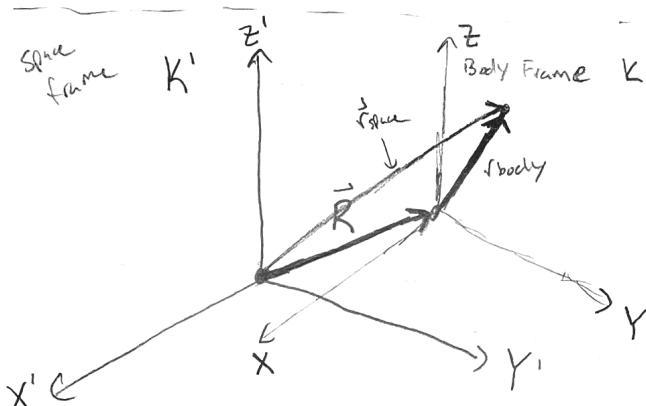
→ quick preliminary info

inertial frame:  $\vec{r}_k^i = \begin{bmatrix} \vec{r}_1 \\ \vec{r}_2 \\ \vec{r}_3 \end{bmatrix}$

rotating coord sys:  $\vec{r}_k = \begin{bmatrix} \vec{r}_1 \\ \vec{r}_2 \\ \vec{r}_3 \end{bmatrix}$

$\vec{r}' = \vec{r}_k$  → inertial frame vector that lies along the  $\vec{i}$  direction  
 $U = \begin{bmatrix} \vec{i} \cdot \vec{i} & \vec{i} \cdot \vec{j} & \vec{i} \cdot \vec{k} \\ \vec{j} \cdot \vec{i} & \vec{j} \cdot \vec{j} & \vec{j} \cdot \vec{k} \\ \vec{k} \cdot \vec{i} & \vec{k} \cdot \vec{j} & \vec{k} \cdot \vec{k} \end{bmatrix}$  → whole vector transforms the inertial frame to the rotating one  
 Function of time  
 $\vec{r}' = U \vec{r}$  inertial frame to rotating frame

take the time derivative:  $\vec{v}'_{\text{fixed}} = \dot{U} \vec{r} + U \vec{v}_{\text{rot}} \rightarrow \vec{v}' = \dot{U} (\underbrace{U^{-1} \vec{r}}_{\vec{r}'}) + U \vec{v} = \dot{U} (U^{-1} \vec{r}') + U \vec{v} = \vec{v}'$   
 (Also recall the proof of)  $\vec{v}' = \vec{v} + \vec{\omega} \times \vec{r}$



using these equations

$$\vec{v}_{\text{space}} = \dot{\vec{r}}_c + \vec{\omega} \times \vec{r}_{\text{body}}$$

[Now we can calculate  $T$ ]  $T = \frac{1}{2} \sum_i m_i v_i^2 = \left( \sum_i m_i \right) \frac{1}{2} \dot{\vec{r}}_c^2 + \vec{\omega} \cdot \vec{\omega} \times \sum_i m_i \vec{r}_i^2 + \frac{1}{2} \sum_i m_i (\vec{\omega} \times \vec{r}_i)^2$

$T = T_{\text{translation}} + T_{\text{rotation}}$   
 $T_{\text{rotational}} = \frac{1}{2} \sum_i m_i (\vec{\omega} \times \vec{r}_i)^2$   
 $T_{\text{translation}} = \frac{1}{2} M \vec{r}_c^2$

$$\vec{a} \cdot \vec{b} = \sum_{\alpha, \beta} a_{\alpha} b_{\beta}$$

$$\vec{a} \cdot \vec{b} = \sum_{i,j} a_{ij} b_{ij}$$

being summed by sum from 1 to 3

Focus on rotational part → Vector identity

$$(\vec{\omega} \times \vec{r})(\vec{\omega} \times \vec{r}) = \vec{\omega} \cdot (\vec{r} \times (\vec{\omega} \times \vec{r})) = \vec{\omega} \cdot (\vec{r}^2 \vec{\omega} - (\vec{\omega} \cdot \vec{r}) \vec{r}) = \vec{r}^2 (\vec{\omega} \cdot \vec{\omega}) - (\vec{\omega} \cdot \vec{r})(\vec{\omega} \cdot \vec{r})$$

$$\hookrightarrow T_{\text{rot}} = \frac{1}{2} \sum_i m_i \left[ \underbrace{\sum_{\alpha=1}^3 r_{i,\alpha}^2}_{\vec{r}^2} \underbrace{\sum_{\beta=1}^3 w_{\beta}^2}_{\vec{\omega} \cdot \vec{\omega}} - \underbrace{\sum_{\alpha=1}^3 r_{i,\alpha} w_{\alpha} \sum_{\beta=1}^3 r_{i,\beta} w_{\beta}}_{\vec{r} \cdot \vec{\omega}}$$

$$\hookrightarrow \sum_{\alpha=1}^3 \sum_{\beta=1}^3 r_{i,\alpha}^2 w_{\beta}^2 \delta_{\alpha \beta} \xrightarrow{\sum_{\alpha=1}^3 \sum_{\beta=1}^3 \sum_{\gamma=1}^3 r_{i,\alpha}^2 w_{\beta} w_{\gamma} \delta_{\beta \gamma}} \xrightarrow{\text{swap indices}} \sum_{\alpha=1}^3 \sum_{\beta=1}^3 \sum_{\gamma=1}^3 r_{i,\alpha}^2 w_{\beta} w_{\gamma} \delta_{\beta \gamma} \xrightarrow{\text{swap all}} \sum_{\alpha=1}^3 \sum_{\beta=1}^3 \sum_{\gamma=1}^3 r_{i,\alpha}^2 w_{\beta} w_{\gamma} \delta_{\alpha \beta}$$

$$\hookrightarrow \sum_{\alpha=1}^3 r_i^2 \sum_{\alpha, \beta} w_{\beta} w_{\alpha} \delta_{\beta \alpha} \rightarrow r_i^2 \sum_{\alpha, \beta} w_{\beta} w_{\alpha} \delta_{\beta \alpha} \quad \text{and RHS} \quad \sum_{\alpha, \beta} r_{i,\alpha} r_{i,\beta} w_{\alpha} w_{\beta} \quad \text{pull out } w_{\alpha} w_{\beta}$$

$$T = \frac{1}{2} \sum_i m_i \left[ \sum_{\alpha, \beta} (r_{i,\alpha}^2 \delta_{\beta \alpha} - r_{i,\alpha} r_{i,\beta}) w_{\alpha} w_{\beta} \right]$$

$$r_i^2 - x_i^2$$

$\alpha = \text{row}$   
 $\beta = \text{column}$

$$r_i^2 = x_i^2 + y_i^2 + z_i^2$$

$$\begin{aligned} I &= x \\ Z &= y \\ Y &= z \end{aligned}$$

Moment of inertia tensor

$$I = \begin{bmatrix} \sum m_i (y_i^2 + z_i^2) - \sum m_i x_i y_i & -\sum m_i x_i z_i & \sum m_i x_i z_i \\ -\sum m_i x_i y_i & \sum m_i (x_i^2 + z_i^2) - \sum m_i y_i z_i & -\sum m_i y_i z_i \\ -\sum m_i x_i z_i & -\sum m_i y_i z_i & \sum m_i (x_i^2 + y_i^2) \end{bmatrix}$$

$$T_{\text{rotation}} = \frac{1}{2} [w_1 \ w_2 \ w_3] [I] \begin{bmatrix} w_1 \\ w_2 \\ w_3 \end{bmatrix}$$

Further

[For each mass point]

$$dI = dm \begin{bmatrix} y^2 + z^2 & -xy & -xz \\ -xy & x^2 + z^2 & -yz \\ -xz & -yz & x^2 + y^2 \end{bmatrix} \quad \text{and } dm = \rho dx dy dz$$

$$\textcircled{e} \quad I_{33} = \iiint \rho(x^2 + y^2) dx dy dz$$

$$U^T I U = \begin{bmatrix} \lambda_1 & 0 & 0 \\ 0 & \lambda_2 & 0 \\ 0 & 0 & \lambda_3 \end{bmatrix} = 0$$

$\lambda_1, \lambda_2, \lambda_3$  are eigenvectors that are the direction cosines of the principal axes

$I$  is symmetric,  $I^T = I$  it is always possible then to find an orthogonal matrix  $U$  that will diagonalize  $I$ . This transformation is called the principle-axis-transformation.

$$I \rightarrow I' = U I U^T = \begin{bmatrix} I'_1 & 0 & 0 \\ 0 & I'_2 & 0 \\ 0 & 0 & I'_3 \end{bmatrix}$$

$I'_k$  are the principle moments of eigenvalues, they are the rotational inertia of the body around each of the axes.  $I'_k$  must be positive

[What if we displace the rotational axis by a constant vector  $\vec{\alpha}$ ]

$$I_{\vec{\alpha}} = I_{cm} + M(\alpha^2 S_{\alpha\beta} - \alpha_x \alpha_y), \text{ if it's parallel to } I_{\vec{\alpha}} = I_{cm} + M\alpha^2$$

moment of inertia

# Moment of Inertia Tensor

considered rotations only about the  $z$ -axis, and gained some useful formulas for those that told us about the angular momentum of the object and its direction.

↳ Specifically for  $z \cdot \alpha \times \beta \rightarrow \vec{L} = (I_{xz}\omega, I_{yz}\omega, I_{zz}\omega)$ , It can also tell you about the kinetic energy in the form of  $T = \frac{1}{2}I\omega^2$ , it's an analogy to mass or resistance to movement, inertia

$$\hookrightarrow \begin{cases} \text{if } L \text{ is constant} \\ \text{the } I = \frac{L}{\omega} \text{ holds} \end{cases} \rightarrow \begin{cases} \text{describes motion \&} \\ \text{a figure skater, as} \\ I \downarrow, \omega \uparrow \end{cases} \rightarrow \begin{cases} \text{As Newton's} \\ \text{Second law} \\ \text{but rotations!} \end{cases} \xrightarrow{\text{z: r} \propto F} I_{z,yz} = I \propto$$

## Angular Momentum for an arbitrary angular velocity

- $\vec{\omega} = \begin{bmatrix} \omega_x \\ \omega_y \\ \omega_z \end{bmatrix}$  two kinds of rotation, rotation about a fixed point and rotation relative to a CM

$$\vec{L} = \sum m_\alpha \vec{r}_\alpha \times \vec{v}_\alpha = \sum m_\alpha \vec{r}_\alpha \times (\vec{\omega} \times \vec{r}_\alpha)$$

$$\vec{r} \times (\vec{\omega} \times \vec{r}) = \begin{bmatrix} \omega_x(y^2 + z^2) - xy\omega_y - xz\omega_z \\ -\omega_x(yx) + (z^2 + x^2)\omega_y - yz\omega_z \\ -\omega_x(zx) - zy\omega_y + (x^2 + y^2)\omega_z \end{bmatrix} = \omega_x \begin{bmatrix} y^2 + z^2 \\ -xy \\ zx \end{bmatrix} + \omega_y \begin{bmatrix} -xy \\ x^2 + z^2 \\ -zy \end{bmatrix} + \omega_z \begin{bmatrix} -xz \\ yz \\ x^2 + y^2 \end{bmatrix}$$

$$m_\alpha \vec{r}_\alpha \times \vec{\omega} \times \vec{r}_\alpha = \omega_x \begin{bmatrix} m_\alpha(y^2 + z^2) \\ -m_\alpha xy_\alpha \\ m_\alpha xz_\alpha \end{bmatrix} + \omega_y \begin{bmatrix} -m_\alpha xy_\alpha \\ m_\alpha(x^2 + y^2) \\ -m_\alpha zy_\alpha \end{bmatrix} + \omega_z \begin{bmatrix} -m_\alpha xz_\alpha \\ -m_\alpha yz_\alpha \\ m_\alpha(x^2 + y^2) \end{bmatrix}$$

scale  $\omega_x$  a certain way  
scale  $\omega_y$  a certain way  
scale  $\omega_z$  a certain way

AS A MATRIX

moments of inertia tensor! cool

$$\begin{bmatrix} L_x \\ L_y \\ L_z \end{bmatrix} = \begin{bmatrix} m_\alpha(y^2 + z^2) & -m_\alpha xy_\alpha & -m_\alpha xz_\alpha \\ -m_\alpha(xy_\alpha) & m_\alpha(x^2 + y^2) & -m_\alpha yz_\alpha \\ m_\alpha(xz_\alpha) & -m_\alpha zy_\alpha & m_\alpha(x^2 + y^2) \end{bmatrix} \begin{bmatrix} \omega_x \\ \omega_y \\ \omega_z \end{bmatrix}$$

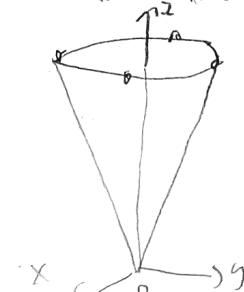
$I$  is symmetric so  
 $I^T$  is the same

$$I = \begin{bmatrix} I_{xx} & I_{xy} & I_{xz} \\ I_{yx} & I_{yy} & I_{yz} \\ I_{zx} & I_{zy} & I_{zz} \end{bmatrix}$$

Last problem on the back!  
all the cross terms are 0.

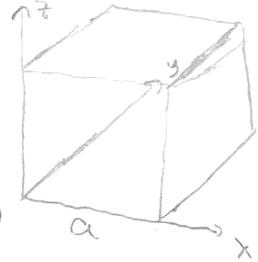
→ just like the mass symmetry example

$$I = \frac{3}{20}M \begin{bmatrix} b^2 + 4h^2 & 0 & 0 \\ 0 & b^2 + 4h^2 & 0 \\ 0 & 0 & 2h^2 \end{bmatrix}$$



cross terms, look for symmetry arguments or calculate it,

# Inertia tensor for a solid cube



a) a solid cube of Mass  $M$  rotating about corner O

$$I_{xx} = \int_0^a dx \int_0^a dy \int_0^a dz \rho(y^2 + z^2), \quad \rho = \frac{M}{\text{Volume}} = \frac{M}{a^3} = \text{constant}$$

$$I_{xx} = \int_0^a \int_0^a \int_0^a \rho(y^2 + z^2) dz dy dx = \rho \int_0^a \int_0^a y^2 z dx + \frac{1}{3} z^3 \Big|_0^a dy dx$$

$$I_{xx} = \rho \int_0^a \int_0^a a y^2 + \frac{1}{3} a^3 dz dx = \rho \int_0^a a y^3 \Big|_0^a + \frac{1}{3} a^3 y^3 \Big|_0^a dx = \rho a \left( \frac{a^4}{3} + \frac{1}{3} a^4 \right)$$

$$I_{xx} = \frac{2}{3} \rho a^5 = \frac{2}{3} M a^2$$

and by symmetry  $I_{yy} = I_{zz} = \frac{2}{3} M a^2$

$$I_{xy} = \int_0^a \int_0^a \int_0^a -\rho xy dz dy dx = -\rho a \int_0^a x y^2 \Big|_0^a dx = -\rho a \int_0^a \frac{a^2}{2} x dx = -\rho a \left( \frac{a^4}{4} \right) = -\frac{Ma^2}{4}$$

by symmetry  $I_{xy} = I_{yx} = I_{zx} = I_{zy} = I_{yz} = I_{xz} = -\frac{Ma^2}{4}$

$$I_{\text{cube}} = \begin{bmatrix} \frac{2}{3} Ma^2 & -\frac{1}{4} Ma^2 & -\frac{1}{4} Ma^2 \\ -\frac{1}{4} Ma^2 & \frac{2}{3} Ma^2 & -\frac{1}{4} Ma^2 \\ -\frac{1}{4} Ma^2 & -\frac{1}{4} Ma^2 & \frac{2}{3} Ma^2 \end{bmatrix} = \frac{Ma^2}{12} \begin{bmatrix} 8 & -3 & -3 \\ -3 & 8 & -3 \\ -3 & -3 & 8 \end{bmatrix}$$

If  $\vec{\omega} = \begin{bmatrix} w \\ 0 \\ 0 \end{bmatrix}$  then  $\vec{L} = \vec{I} \vec{\omega}$

$$\vec{L} = \frac{Ma^2}{12} \begin{bmatrix} 8 & -3 & -3 \\ -3 & 8 & -3 \\ -3 & -3 & 8 \end{bmatrix} \begin{bmatrix} w \\ 0 \\ 0 \end{bmatrix} = \frac{Ma^2}{12} \begin{bmatrix} 8w \\ -3w \\ -3w \end{bmatrix}$$

$$\vec{L} = Ma^2 w \left( \frac{2}{3}, -\frac{1}{4}, -\frac{1}{4} \right)$$

if the cube is rotating about its main diagonal then we get

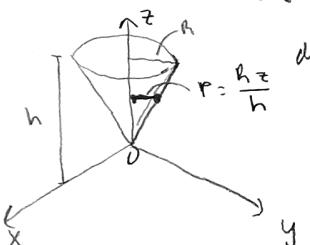
$\hat{u}$  in direction of the rotation along the diagonal

$$\rightarrow \hat{u} = \frac{1}{\sqrt{3}} \begin{bmatrix} 1 \\ 1 \\ 1 \end{bmatrix} \rightarrow \vec{\omega} = |\omega| \hat{u} = \frac{\omega}{\sqrt{3}} \begin{bmatrix} 1 \\ 1 \\ 1 \end{bmatrix}$$

b) If the cube is rotating about its center then we have to map O to the center. Now all of the integrals run from  $-\frac{a}{2}$  to  $\frac{a}{2}$ . If you do so then  $I_{xx} = \frac{1}{6} Ma^2$ ,  $I_{xy} = 0$  = all off diagonals thus

$$I = \frac{1}{6} Ma^2 \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \rightarrow L = \vec{I} \vec{\omega} = \frac{1}{6} Ma^2 \vec{\omega} \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

Rotation about a corner



$$I_{zz} = \iiint (x^2 + y^2) dx dy dz = \iiint \rho^2 dp d\phi dz \quad \text{density } \rho = \frac{Rz}{h} \rightarrow \text{get corner, set radius } Rz \text{ and } dz \text{ count forget } \rho \text{ sign!}$$

$$\hookrightarrow I_{zz} = 2\pi \rho \int_0^h \int_0^{2\pi} \int_0^{Rz/h} p^2 dp d\phi dz = 2\pi \rho \int_0^h \int_0^{2\pi} \frac{R^4 z^2}{20} dz = 2\pi \rho \frac{R^4 z^5}{20} \Big|_0^h = \frac{2\pi \rho R^4 h^4}{20}$$

$$M = \frac{M}{V} = \frac{3M}{\pi R^2 h}$$

$$\hookrightarrow I_{zz} = \frac{3}{10} MR^2$$

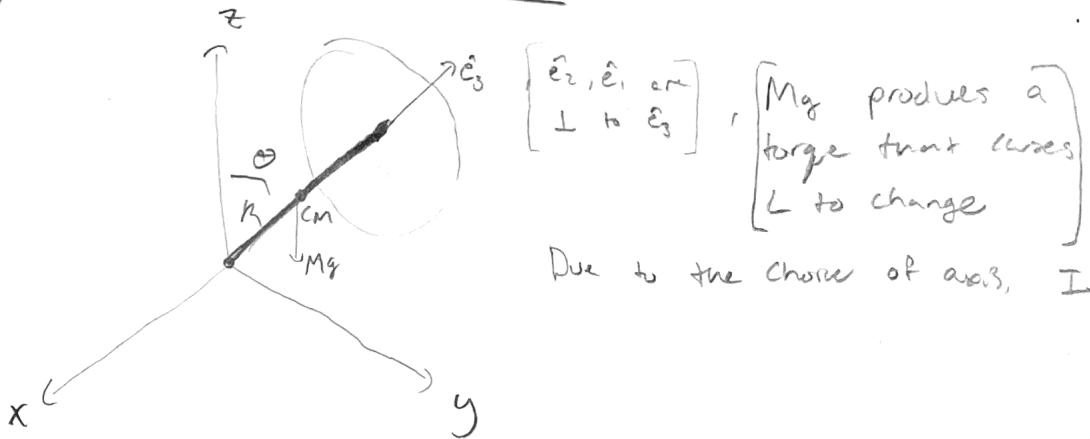
$$\text{Since of rotational symmetries } I_{xx} = I_{yy} = \int_V dV (y^2 + z^2) M = \underbrace{\int_V M y^2 dV}_{(1)} + \underbrace{\int_V M z^2 dV}_{(2)}$$

$$(1) \int_0^h \int_0^{2\pi} \int_0^{Rz/h} M p^2 \sin^2 \phi dp d\phi dz$$

$$(2) \int_0^h \int_0^{2\pi} \int_0^{Rz/h} M z^2 p dp d\phi dz = \frac{3 \cdot 4 h^2}{20} M$$

$$I_{xx} = \frac{3}{20} M (R^2 + 4h^2)$$

## cession of a weak torque



Due to the choice of axes,  $\vec{I} = \begin{bmatrix} I_1 & 0 & 0 \\ 0 & I_2 & 0 \\ 0 & 0 & I_3 \end{bmatrix}$

[First suppose gravity is turned off so it's just spinning about  $\vec{\omega} = \omega \hat{e}_3$ ]  $\rightarrow \vec{L} = I_3 \vec{\omega} = I_3 \omega \hat{e}_3$   $\rightarrow \omega$  has only 3rd component

[Switch gravity back on, which will cause a torque,  $\vec{\tau} = \vec{R} \times \vec{Mg} = \vec{r} = R Mg \sin \theta \hat{e}_3$  (direction L to  $\hat{e}_3$ )]  $\rightarrow$  Existence of a torque implies there will be a change in momentum,  $\vec{L} = \vec{L}'$

[So changing  $\vec{L}$  implies  $\vec{\omega}$  starts to change and]  $\rightarrow$  If torque is small then  $\omega_1, \omega_2$  are small so it's a good approximation  
[ $\omega_1$  and  $\omega_2$  are now no longer 0]

$\hookrightarrow I_3 \omega \dot{e}_3 = \vec{R} \times \vec{Mg}$  and  $\vec{R} = R \hat{e}_3$  and  $\vec{g} = -g \hat{z}$  plug in

$$\hookrightarrow \dot{e}_3 = \frac{R \dot{e}_3}{I_3 \omega} \times (-Mg) \hat{z} = \frac{Mg \hat{z}}{I_3 \omega} \times \overset{\text{constant}}{R \dot{e}_3} = \frac{R Mg}{I_3 \omega} \hat{z} \times \dot{e}_3$$

This says that the axis of the top  $e_3$  rotates w/ angular velocity  $\dot{e}_3$  about the vertical  $\hat{z}$  torque by gravity causes its precess

Space frame

body frame

$\vec{L} = \begin{bmatrix} I_1 \omega_1 \\ I_2 \omega_2 \\ I_3 \omega_3 \end{bmatrix}$ ,  $\left( \frac{d\vec{L}}{dt} \right)_{\text{space}} = \left( \frac{d\vec{L}}{dt} \right)_{\text{body}} + \vec{\omega} \times \vec{L} = \vec{L} + \vec{\omega} \times \vec{L}$  and substituting into J

$$\begin{aligned} \dot{\omega}_1 &= I_1 \ddot{\omega}_1 - (\lambda_2 - \lambda_1) \omega_2 \omega_3 \\ \dot{\omega}_2 &= I_2 \ddot{\omega}_2 - (\lambda_3 - \lambda_1) \omega_3 \omega_1 \\ \dot{\omega}_3 &= I_3 \ddot{\omega}_3 - (\lambda_1 - \lambda_2) \omega_1 \omega_2 \end{aligned}$$

OR if  $\frac{dL}{dt} = 0$  or no net torques  $(\frac{d\vec{L}}{dt})_{\text{space}} = 0 = (\frac{d\vec{L}}{dt})_{\text{body}} + \vec{\omega} \times \vec{L}$

$L_{\text{body}} = \begin{bmatrix} I_1 \omega_1 \\ I_2 \omega_2 \\ I_3 \omega_3 \end{bmatrix}$  then

$$\begin{aligned} I_1 \frac{d\omega_1}{dt} &= \omega_3 L_2 - \omega_2 L_3 = \omega_2 \omega_3 (I_2 - I_3) \\ I_2 \frac{d\omega_2}{dt} &= \omega_1 L_3 - \omega_3 L_1 = \omega_1 \omega_3 (I_3 - I_1) \\ I_3 \frac{d\omega_3}{dt} &= \omega_1 L_1 - \omega_1 L_2 = \omega_1 \omega_2 (I_1 - I_2) \end{aligned}$$

EULER'S EQUATIONS

For Euler equations, often times the torque is very complicated  
more useful when torque is 0.

Case of the spinning top  
the moment of inertia  
always the diagonal  $I_1 = I_2$

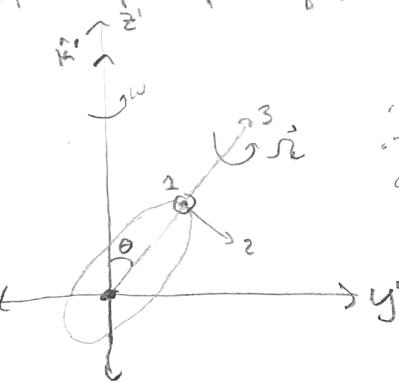
$$\text{thus } I_3 \omega_3 = \tau_3$$

$$\rightarrow \text{thus } I_3 \omega_3 = 0$$

and  $\omega_3$  is a constant

but the torque by law  
 $\tau_3$  is 0. there is no component of torque along  $\hat{e}_3$   
 $c_3$

Spinning top again



most general motion possible for a torque-free top (Symmetry)

• top spins around  $z$  axis w/ constant angular velocity

• top is tilted by an angle  $\theta$

• Define  $z'$  to be along  $L$

• Take a snapshot and define  $y'$  space axis to be in the plane momentarily defined by the  $z$ -axis

$$\vec{\omega}' = \cos\theta \hat{k} + \sin\theta \hat{j} \rightarrow \begin{cases} \text{at } \theta=0 \\ \hat{k}=1 \\ \hat{j}=0 \end{cases} \quad \begin{cases} \text{at } \theta=90^\circ \\ \hat{k}=0 \\ \hat{j}=-1 \end{cases} \quad \text{so } \hat{k}' = \cos\theta \hat{k} - \sin\theta \hat{j}$$

$L = r \times p$  if  $r$  is constant vector  
 $\frac{dL}{dt} = r \times \dot{p} = \tau$  if  $\tau$  is cons.  $L$  is a constant

[No torques on it (gravity  $\vec{g}$   
being neglected)]

$\rightarrow L$  is fixed & no torque  $\rightarrow$   $T$  is fixed & no work of being due

$$\hat{L} = L \hat{k}'$$

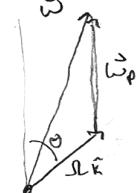
Now for a more fleshed out

• part of the contribution to  $\vec{\omega}$  is due to the spin around  $\hat{e}_3$ ,  $\vec{I}_3 \hat{k}$ . (part of angular momentum)

$\hookrightarrow$  You will see this part after multiplying w/  $\vec{I}$  and  $\vec{I}_3 \vec{z} \hat{k}$  hence

For our picture at an instance  $\vec{I}_3 \vec{z} \hat{k}$  lies in  $z'y'$  plane

$\hookrightarrow$  since we have an  $\vec{\omega}$  and this  $\vec{z} \hat{k}$  there has to be another  $\omega_p$  to bring us to  $\vec{\omega}$



• multiplying  $\omega_p$  by  $\vec{I}$  gets us a meaningful size of angular momentum recall  $I_1 = I_2$

$$\boxed{\text{First}} \quad \vec{\omega}_p = \omega_{p,1} \hat{i} + \omega_{p,2} \hat{j} + \omega_{p,3} \hat{k} \rightarrow \boxed{\text{Now}} \quad \vec{I} \vec{\omega}_p = I_1 (\omega_{p,1} \hat{i} + \omega_{p,2} \hat{j}) + I_3 \omega_{p,3} \hat{k} = L \hat{k}' - I_3 \vec{z} \hat{k}$$

$$\vec{I} = I \hat{e}_3 = \begin{bmatrix} I_1 & 0 & 0 \\ 0 & I_2 & 0 \\ 0 & 0 & I_3 \end{bmatrix}$$

$$\hookrightarrow \vec{I} \vec{\omega}_p = L \hat{k}' - I_3 \vec{z} \hat{k} = (L \cos\theta - I_3 \vec{z}) \hat{k} - L \sin\theta \hat{j}$$

$$L \cos\theta \hat{k} - L \sin\theta \hat{j}$$

Then  $\omega_{p,1} = 0$

$$I_1 \omega_{p,2} = -L \sin\theta$$

$$I_3 \omega_{p,3} = L \cos\theta - I_3 \vec{z}$$

$$L \omega_{p,2} = \frac{FL}{I_1} \sin\theta$$

$$\omega_{p,3} = \left( \frac{L}{I_3} \cos\theta - \vec{z} \cdot \hat{k} \right) \hat{k}$$

$$\text{Recall } T = \frac{1}{2} \vec{\omega}^T \vec{I} \vec{\omega}$$

$$T = \frac{1}{2} \left[ 0, \frac{L}{I_1} \text{ other}, \frac{L}{I_3} \cos\theta \right] \begin{bmatrix} I_1 & 0 & 0 \\ 0 & I_2 & 0 \\ 0 & 0 & I_3 \end{bmatrix} \begin{bmatrix} 0 \\ -\frac{L}{I_1} \sin\theta \\ \frac{L}{I_3} \cos\theta \end{bmatrix}$$

$$\begin{bmatrix} \omega_1 \\ \omega_2 \\ \omega_3 \end{bmatrix} = \begin{bmatrix} \omega_{p,1} \\ \omega_{p,2} \\ \omega_{p,3} \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ SL \end{bmatrix}$$

$$-r \hat{e}_1 + \vec{r} \hat{e}_2 \text{ from}$$

view  
 $\hat{k}'$   
 $\hat{i}$   
 $\hat{j}$   
 $\hat{k}$   
 $\hat{x}_B$  shown  
 for principal  
 axis 3 to  
 get  $\hat{L}$  my  
 way comes  
 out too! G/  
 prime axis 3  
 for body frame  
 and  
 $I_1 = I_2$   
 (diagonal matrix)

o  $\hat{k}' = \cos\theta \hat{k} - \sin\theta \hat{j}$   
 o choose  $\hat{L} = L \hat{k}'$  since it is a constant  
 o  $\vec{\omega}_p = \omega_{p1} \hat{i} + \omega_{p2} \hat{j} + \omega_{p3} \hat{k}$

$\vec{\omega}_p + \vec{\omega}_R = \vec{\omega}$   
 $I_1 \vec{\omega}_p = I_1 (\omega_{p1} \hat{i} + \omega_{p2} \hat{j}) + I_3 \omega_{p3} \hat{k}$   
 and  
 $I_1 \vec{\omega}_p = L \hat{k}' - I_3 \omega_R \hat{k}$   
 $\hat{k}' = \cos\theta \hat{k} - \sin\theta \hat{j} \rightarrow \hat{k}' = (L \cos\theta - I_3 \omega_R) \hat{k} - L \sin\theta \hat{j}$

solve for  
 $\omega_{p1}, \omega_{p2}, \omega_{p3}$   
 then use  
 $\vec{\omega} = \vec{\omega}_p + \vec{\omega}_R$

Now we can plug into  $T = \frac{1}{2} \vec{\omega}^T \vec{I} \vec{\omega} \Rightarrow T = \frac{1}{2} \left[ 0, -\frac{L}{I_1} \sin\theta, \frac{L}{I_3} \cos\theta \right] \begin{bmatrix} I_1 & 0 & 0 \\ 0 & I_1 & 0 \\ 0 & 0 & I_3 \end{bmatrix} \begin{bmatrix} 0 \\ -\frac{L}{I_1} \sin\theta \\ \frac{L}{I_3} \cos\theta \end{bmatrix}$   
 $* T \text{ is a constant then } G \text{ is a constant}$

$\vec{\omega}_p = -L \sin\theta \hat{j} + (L \cos\theta - I_3 \omega_R) \hat{k}$   
 $\vec{\omega}_p = I_1 (\omega_{p1} \hat{i} + \omega_{p2} \hat{j}) + I_3 \omega_{p3} \hat{k}$

\* constant  $\oplus$  means  $\omega_{p1} = 0$  otherwise  $\oplus$  would cause  $\rightarrow$   
 $\omega_{p1} = 0$   
 $\omega_{p2} = -\frac{L}{I_1} \sin\theta$   
 $\hat{k}' \omega_{p3} = \frac{L}{I_3} \cos\theta - \omega_R \rightarrow$  [transformer  $\vec{\omega}_p$ ]  $\rightarrow$

$\vec{\omega}_p = \cos\theta \hat{k}' - \sin\theta \hat{j}'$   
 $\hat{j}' = \cos\theta \hat{j} - \sin\theta \hat{k}'$   
 $\hat{k}' \omega_{p3} = L \left[ \frac{\sin^2\theta}{I_1} + \frac{\cos^2\theta}{I_3} \right] - \omega_R \cos\theta$

Solve for  $\omega_R \rightarrow \omega_R = L \left( \frac{1}{I_1} - \frac{1}{I_3} \right) \cos\theta$   
 now look in space frame  $\vec{\omega}_{px'} = 0$   
 $\vec{\omega}_{py'} = 0$   
 $\vec{\omega}_{pz'} = \text{value}$

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 for pd

$\hookrightarrow \text{So } |\omega_1| = \omega_p \cdot \hat{k}' = L \left( \frac{\sin^2\theta}{I_1} - \frac{\cos^2\theta}{I_3} \right) - \omega_R \cos\theta = L \left( \frac{\sin^2\theta}{I_1} - \frac{\cos^2\theta}{I_3} \right) - L \left( \frac{1}{I_1} - \frac{1}{I_3} \right) \cos^2\theta = \frac{L}{I_1} = |\vec{\omega}_p|$

Calculating the Precession Rate  
 Use EULERS equations:  
 1)  $I_1 \frac{d\omega_1}{dt} = \omega_2 \omega_3 (I_2 - I_3)$   $\frac{d\omega_1}{dt} + \left( \frac{J_3}{I_1} - 1 \right) \omega_2 \omega_3 = 0$   
 2)  $I_2 \frac{d\omega_2}{dt} = \omega_1 \omega_3 (I_3 - I_1)$   $\frac{d\omega_2}{dt} - \left( \frac{J_3}{I_1} - 1 \right) \omega_3 \omega_1 = 0$   
 3)  $I_3 \frac{d\omega_3}{dt} = \omega_1 \omega_2 (I_1 - I_2) = 0$   
 $\omega_1(t=0) = 0$  to make constant  $\omega_1$  easier def  $\rightarrow \phi = 0$ ,  $|\vec{\omega}| = \sqrt{\omega_1^2 + \omega_2^2 + \omega_3^2} = \text{const}$

If we define  $\vec{\omega}_p = \left( \frac{J_3}{I_1} - 1 \right) \omega_3$   
 $\frac{d^2\omega_1}{dt^2} + \omega_p^2 \omega_1 = 0 \rightarrow \omega_1 = A \sin(\omega_p t + \phi)$   
 $\frac{d^2\omega_2}{dt^2} + \omega_p^2 \omega_2 = 0 \rightarrow \omega_2 = A \cos(\omega_p t + \phi)$

$\omega_1^2 + \omega_2^2 = A^2$

\* More notes after will be important?

## Euler Angles

[can convert between space and body coordinates and vice versa]

$$\begin{array}{l} \text{some} \\ \text{body} \\ \text{body} \end{array} \quad r' = U r \quad \left| \begin{array}{l} \text{U must be a} \\ \text{function of 3 params} \end{array} \right.$$

$$\begin{array}{l} \text{body} \\ \text{space} \\ \text{space} \end{array} \quad r = U^{-1} r' \quad \theta, \phi, \psi$$

We are going to use these 3 angles to define a sequence of rotations acting on the body coord which finally converts this coordinate sys into one that has an arbitrary orientation wrt the space coord.

(Step a) Start w/ your space and body coordinates aligned and rotate by an angle  $\phi$  about the z-axis

$$U_1^{-1} = \begin{bmatrix} \cos\phi & \sin\phi & 0 \\ -\sin\phi & \cos\phi & 0 \\ 0 & 0 & 1 \end{bmatrix}, \quad \begin{bmatrix} \text{new} \\ \text{vorts} \\ \text{after} \\ \text{rot} \end{bmatrix} = U_1^{-1} \begin{bmatrix} r_1 \\ r_2 \\ r_3 \end{bmatrix}$$

(Step B) take  $e_3$  which is aligned w/  $\hat{z}$  and rotate it by the angle  $\theta$ .

$$U_2^{-1} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos\theta & \sin\theta \\ 0 & -\sin\theta & \cos\theta \end{bmatrix} \quad \begin{array}{l} \text{when } \hat{e}_1 \text{ gets sent to } \hat{e}'_1 \\ \text{when } \hat{e}_2 \text{ gets sent to } \hat{e}'_2 \\ \text{when } \hat{e}_3 \text{ gets sent to } \hat{e}'_3 \end{array}$$

(Step C) rotate about the  $\hat{e}_1, \hat{e}_2$  plane

$$U_3^{-1} = \begin{bmatrix} \cos\psi & \sin\psi & 0 \\ -\sin\psi & \cos\psi & 0 \\ 0 & 0 & 1 \end{bmatrix} \quad \begin{bmatrix} r_1 \\ r_2 \\ r_3 \end{bmatrix} = U_3 \begin{bmatrix} \text{last} \\ \text{unit} \\ \text{vector} \\ \text{from part} \\ \text{B} \end{bmatrix}$$

But we can do some tricks

Since want in terms of  $\vec{e}_1, \vec{e}_2, \vec{e}_3$  of just  $\vec{e}_1, \vec{e}_2, \vec{e}_3$

$$\vec{w} = w_1 \vec{e}_1 + w_2 \vec{e}_2 + w_3 \vec{e}_3 = \phi \vec{e}_1 + \epsilon \vec{e}_2 + \gamma \vec{e}_3$$

$$(\vec{x}, \vec{y}, \vec{z}) \rightsquigarrow (\vec{e}_1, \vec{e}_2, \vec{e}_3) \rightsquigarrow (\phi, \epsilon, \gamma)$$

WSR2 =  $\phi \vec{e}_3$  whatever we get  $\vec{e}_1, \vec{e}_2, \vec{e}_3$

$w_{\text{step}} = \epsilon \vec{e}_1$  but here the intermediate step

$w_{\text{step}} = \phi \vec{e}_2$  we go from  $\vec{x}, \vec{y}, \vec{z}$  to  $\vec{e}_1, \vec{e}_2, \vec{e}_3$

Find angular velocity of the body rel to space frame

Calculating  $\vec{w}$  in terms of the Euler angles

last column;  $\sin \theta \cos \phi$   
middle column;  $\sin \theta \sin \phi$   
first column;  $\cos \theta$

$$\vec{w} = \begin{bmatrix} \cos \theta \sin \phi + \sin \theta \cos \phi \sin \psi & \sin \theta \sin \phi + \cos \theta \cos \phi \sin \psi \\ \cos \theta \cos \phi - \sin \theta \sin \phi & \sin \theta \cos \phi - \cos \theta \sin \phi \\ \cos \theta \sin \phi & \sin \theta \sin \phi \end{bmatrix}$$

omega plus phi out;

$$\vec{u} = u_1 \vec{u}_1 + u_2 \vec{u}_2 + u_3 \vec{u}_3$$

$$\vec{\omega} = \dot{\phi} \hat{e}_z + \dot{\theta} \hat{e}_x + \dot{\psi} \hat{e}_y$$

\* we want in terms of just  $\hat{e}_1, \hat{e}_2, \hat{e}_3$  but if we just consider the symmetric case where  $I_{xx} = I_{yy}$  we don't have to do this.

$\hookrightarrow$  [The point B]  $\rightarrow$   $\begin{cases} \text{w/ } I_{xx} = I_{yy} \\ \text{any two } \perp \text{ axes in the} \end{cases} \rightarrow \begin{cases} \text{plane of } \hat{e}_1, \hat{e}_2 \\ \text{are also principle axis} \end{cases}$  So!

[We can just get to the point where  $\hat{e}_1', \hat{e}_2', \hat{e}_3'$ ]

note

$$\hat{z}' = \cos\theta \hat{e}_z - \sin\theta \hat{e}_1' \rightarrow \vec{\omega} = (-\dot{\phi} \sin\theta) \hat{e}_1' + \dot{\theta} \hat{e}_2' + (\dot{\psi} + \dot{\phi} \cos\theta) \hat{e}_3'$$

[w/ principle axis]  $\rightarrow L = (I_{xx} \omega_1, I_{yy} \omega_2, I_{zz} \omega_3)$

$$[\text{w/ principle axis}] \rightarrow T = \frac{1}{2} I_{xx} \omega_1^2 + \frac{1}{2} I_{yy} \omega_2^2 + \frac{1}{2} I_{zz} \omega_3^2$$

$$T = \frac{1}{2} I_{xx} (\dot{\phi}^2 \sin^2\theta + \dot{\theta}^2) + \frac{1}{2} I_{zz} (\dot{\psi}^2 + \dot{\phi}^2 \cos^2\theta)$$

\*  $\vec{\omega}$  is not an integrable function

$$\vec{\omega}_{\text{body}} = \begin{pmatrix} \dot{\theta} \cos\psi + \dot{\phi} \sin\psi \sin\theta \\ -\dot{\theta} \sin\psi + \dot{\phi} \cos\psi \sin\theta \\ \dot{\psi} + \dot{\phi} \cos\theta \end{pmatrix}$$

$$\vec{\omega}_{\text{spur}} = \begin{pmatrix} \dot{\theta} \cos\psi + \dot{\phi} \sin\psi \sin\theta \\ \dot{\theta} \sin\psi - \dot{\phi} \cos\psi \sin\theta \\ \dot{\phi} + \dot{\psi} \cos\theta \end{pmatrix}$$

## center of mass

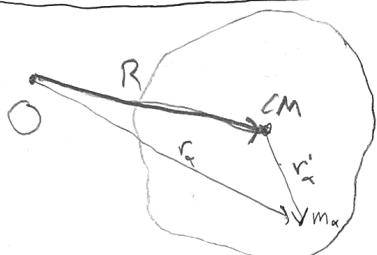
$$\vec{R}_{cm} = \frac{1}{M_{tot}} \cdot (m_1 \vec{r}_1 + \dots + m_N \vec{r}_N) = \frac{1}{M_{tot}} \sum_{\alpha=1}^N m_\alpha \vec{r}_\alpha$$

$\vec{R}_{cm}$  is the weighted average of the positions  $\vec{r}_1, \vec{r}_N$  where  $\vec{r}_\alpha$  is weighted by  $m_\alpha$ .

$$P_{cm} = M_{tot} \dot{\vec{R}}_{cm} \quad \text{and} \quad \vec{R}_{cm} = \frac{1}{M_{tot}} \int r dm = \frac{1}{M_{tot}} \int \vec{r} \rho dV$$

If  $M_{tot}$  is the total mass and  $\vec{R}_{cm}$  is the position of the center mass then

$$\boxed{\vec{F}_{\text{external}} = M_{tot} \ddot{\vec{R}}_{cm}}$$



$$\vec{r}_\alpha = \vec{R} + \vec{r}'_\alpha \quad \rightarrow \quad \vec{r}'_\alpha = \vec{r}_\alpha - \vec{R}$$

$$\vec{l}_\alpha = \vec{r}_\alpha \times \vec{p}_\alpha = \vec{v}_\alpha \times m_\alpha \vec{r}_\alpha$$

$$\vec{L} = \sum \vec{l}_\alpha = \sum \vec{r}_\alpha \times m_\alpha \vec{v}_\alpha = \sum (\vec{R} + \vec{r}'_\alpha) \times m_\alpha (\vec{R} + \vec{r}'_\alpha)$$

## FOIL A

$$\vec{L} = \sum R \times m_\alpha \vec{v}_\alpha + \sum R \times m_\alpha \vec{v}'_\alpha + \sum \vec{r}'_\alpha \times m_\alpha \vec{v}_\alpha + \sum \vec{r}'_\alpha \times m_\alpha \vec{v}'_\alpha$$

$$\hookrightarrow \vec{L} = R \times M \vec{R} + R \times \sum m_\alpha \vec{v}'_\alpha + \underbrace{(\sum m_\alpha \vec{v}'_\alpha) \times \vec{R} + \sum \vec{r}'_\alpha \times m_\alpha \vec{v}'_\alpha}_{\text{center of mass relative to the center of mass which makes } \vec{r}'_\alpha = 0}$$

$$\vec{L} = \underbrace{\vec{R} \times \vec{P}}_{\text{motion of center of mass}} + \underbrace{\sum \vec{r}'_\alpha \times m_\alpha \vec{v}'_\alpha}_{\text{motion relative to the center of mass}}$$

then  $m_\alpha \vec{v}'_\alpha$  is also zero if you differentiate

(ex) Motion of a planet around our sun. This guy asserts the total angular momentum of the planet is the angular momentum of the orbital motion and its angular momentum about its center of mass.

$$\vec{L} = \vec{L}_{\text{orb}} + \vec{L}_{\text{spin}}$$

$$T = \sum_{\alpha=1}^M \frac{1}{2} m_\alpha \vec{r}_\alpha^2 \quad \text{and} \quad \vec{r}_\alpha^2 = \vec{R}^2 + \vec{r}'_\alpha^2 + 2 \vec{R} \cdot \vec{r}'_\alpha \quad \rightarrow \quad T = \underbrace{\frac{1}{2} \sum m_\alpha \vec{R}^2}_{\text{motion of CM}} + \underbrace{\frac{1}{2} \sum m_\alpha \vec{r}'_\alpha^2}_{\text{motion about CM}} + \underbrace{\vec{R} \cdot \sum m_\alpha \vec{r}'_\alpha}_{=0, \text{ find the center of mass rel to CM which makes } \vec{r}'_\alpha = 0}$$

$\hookrightarrow$  potential  
Energy on  
the bicycle

$$U = U^{\text{ext}} + U^{\text{int}}$$

distance between partners  $\alpha$  and  $\beta$

potentials due to external forces      Internal energy

$U^{\text{int}} = \sum_{\alpha < \beta} U_{\alpha\beta}(r_{\alpha\beta})$  ← for a rigid body all of the interparticle distances are fixed. Therefore  $U^{\text{int}}$  is constant, and can be ignored.

[Sum of the potential energies for all pairs of partners]

$L = \sum L_\alpha = \sum m_\alpha r_\alpha \times m_\alpha v_\alpha$  →  $v_\alpha$  are the velocities in which the pieces are being carried in circles by  $\omega$ , then we know  $v_\alpha = \omega \times r_\alpha$

Let's say  $\omega = (0, 0, \omega)$  and  $r_\alpha = (x_\alpha, y_\alpha, z_\alpha)$  →  $\vec{v}_\alpha = \vec{\omega} \times \vec{r}_\alpha = (-\omega y_\alpha, \omega x_\alpha, 0)$

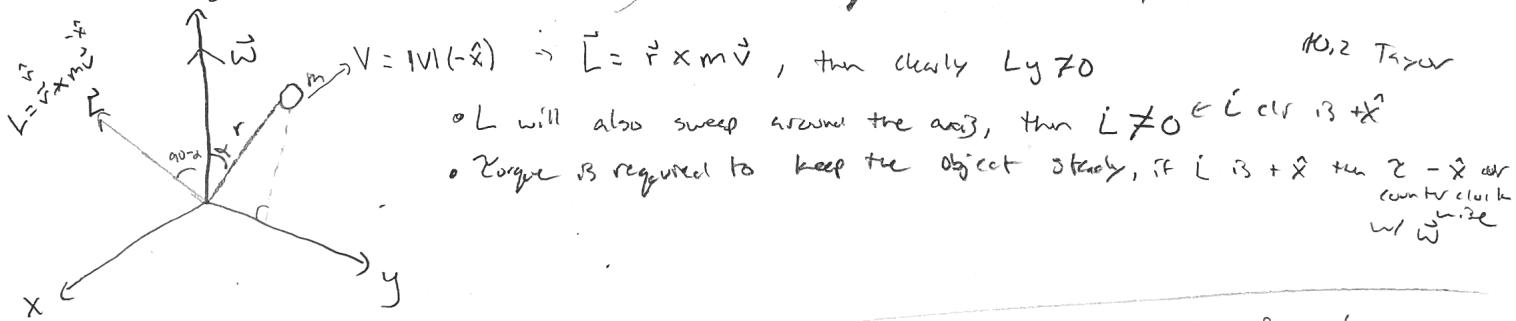
Finally:  $L_\alpha = m_\alpha r_\alpha \times v_\alpha = m_\alpha \omega (-z_\alpha x_\alpha, -z_\alpha y_\alpha, x_\alpha^2 + y_\alpha^2)$

we want angular momentum to look like normal momentum,  $mv$  so  $I_z = \sum m_\alpha p_\alpha^2 \omega$  (like mag)

[Let's calculate components of  $L$ ] →  $L_z = \sum m_\alpha (x_\alpha^2 + y_\alpha^2) \omega = \sum m_\alpha p_\alpha^2 \omega = I_z \omega$

↳ [and T is]  $T = \frac{1}{2} \sum m_\alpha v_\alpha^2 = \frac{1}{2} \sum m_\alpha p_\alpha^2 = \frac{1}{2} I_z \omega^2$   $p_\alpha^2 = \text{distance from z-axis}$   $I_z = \text{usually an integral}$

(Now for  $L_x$  and  $L_y$ )  $L_x = -\sum m_\alpha x_\alpha z_\alpha \omega$  non zero, even though  $\omega$  points in the z-dir  
 $L_y = -\sum m_\alpha y_\alpha z_\alpha \omega$   $L$  may be in a different direction. Thus  $\vec{L} = I \vec{\omega}$  is generally not true!

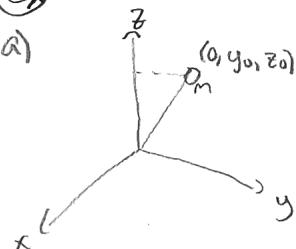


Streamline notation:  $L_x = I_{xz} \omega$  and  $L_y = I_{yz} \omega$  → product of inertia of the body

$$I_z \rightarrow I_{zz} = \sum m_\alpha p_\alpha^2 = \sum m_\alpha (x_\alpha^2 + y_\alpha^2)$$

Thus  $\vec{L} = (I_{xz} \omega, I_{yz} \omega, I_{zz} \omega)$

ex)



b)

$$I_{xz} = -\sum m_\alpha x_\alpha z_\alpha = -\sum m_\alpha x_\alpha \cdot 0 = 0$$

$$I_{yz} = -\sum m_\alpha y_\alpha z_\alpha = -m[y_0 z_0 + y_1(-z_0)] = 0$$

$$I_{zz} = m(0 + y_0^2 + 0 + y_1^2) = my_0^2$$

the two masses mirror each other

c)

every mass can be paired with one across from it as  $(-x_1, -y_1, -z_1)$  to cancel it so  $= 0$

$I_{xz} = -\sum m_\alpha x_\alpha y_\alpha = 0$

$I_{yz} = -\sum m_\alpha y_\alpha z_\alpha = 0$

$I_{zz} = \sum m_\alpha (x_\alpha^2 + y_\alpha^2) = M p_0^2$   $\frac{\text{constant}}{p_0^2}$