

2D Elastic Problem

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1 Problem 9.7

Problem 9.7

Repeat Example 9.2 with two triangular elements as shown in Figure 9.19.

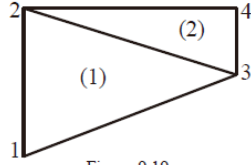


Figure 9.19

Figure 1: Problem 9.7

1.1 Preprocessing, Formation & Assembly

首先写出材料的本构矩阵

$$\mathbf{D} = \frac{E}{1-\nu^2} \begin{pmatrix} 1 & \nu & 0 \\ \nu & 1 & 0 \\ 0 & 0 & \frac{1-\nu}{2} \end{pmatrix}$$

其中, $E = 3 \times 10^7 Pa, \nu = 0.3$, 单元节点标号顺序分别为 (1) $2 \rightarrow 1 \rightarrow 3$ 与 (2) $2 \rightarrow 3 \rightarrow 4$, 于是单元坐标矩阵可写为

$$\begin{pmatrix} \mathbf{x}^{(1)} & \mathbf{y}^{(1)} \end{pmatrix} = \begin{pmatrix} 0 & 1 \\ 0 & 0 \\ 2 & 0.5 \end{pmatrix}$$

$$\begin{pmatrix} \mathbf{x}^{(2)} & \mathbf{y}^{(2)} \end{pmatrix} = \begin{pmatrix} 0 & 1 \\ 2 & 0.5 \\ 2 & 1 \end{pmatrix}$$

由此容易求得单元应变矩阵与 *Jacobi* 矩阵

$$\mathbf{B}^{(1)} = \frac{1}{2} \begin{pmatrix} -0.5 & 0 & -0.5 & 0 & 1 & 0 \\ 0 & 2 & 0 & -2 & 0 & 0 \\ 2 & -0.5 & -2 & -0.5 & 0 & 1 \end{pmatrix}$$

$$\mathbf{B}^{(2)} = \begin{pmatrix} -0.5 & 0 & 0 & 0 & 0.5 & 0 \\ 0 & 0 & 0 & -2 & 0 & 2 \\ 0 & -0.5 & -2 & 0 & 2 & 0.5 \end{pmatrix}$$

$$\mathbf{J}^{(1)} = \begin{pmatrix} -2 & 0.5 \\ -2 & -0.5 \end{pmatrix}$$

$$\mathbf{J}^{(2)} = \begin{pmatrix} -2 & 0 \\ 0 & -0.5 \end{pmatrix}$$

为了计算单元刚度阵，注意到单元内部为常应变状态且 *Jacobi* 矩阵为常数矩阵，因此有

$$\mathbf{K}^e = \frac{|\mathbf{J}^e|}{2} \mathbf{B}^{eT} \mathbf{D} \mathbf{B}^e$$

单元刚度阵的计算结果为

$$\mathbf{K}^{(1)} = 10^7 \times \begin{pmatrix} 1.5399 & -0.5357 & -0.9478 & -0.0412 & -0.4121 & 0.5769 \\ -0.5357 & 3.3688 & 0.0412 & -3.2246 & 0.4945 & -0.1442 \\ -0.9478 & 0.0412 & 1.3599 & 0.5357 & -0.4121 & -0.5769 \\ -0.0412 & -3.2246 & 0.5357 & 3.3688 & -0.4945 & -0.1442 \\ -0.4121 & 0.4945 & -0.4121 & -0.4945 & 0.8242 & 0 \\ 0.5769 & -0.1442 & -0.5769 & -0.1442 & 0 & 0.2885 \end{pmatrix}$$

$$\mathbf{K}^{(2)} = 10^7 \times \begin{pmatrix} 0.4121 & 0 & 0 & 0.4945 & -0.4121 & -0.4945 \\ 0 & 0.1442 & 0.5769 & 0 & -0.5769 & -0.1442 \\ 0 & 0.5769 & 2.3077 & 0 & -2.3077 & -0.5769 \\ 0.4945 & 0 & 0 & 6.5934 & -0.4945 & -6.5934 \\ -0.4121 & -0.5769 & -2.3077 & -0.4945 & 2.7198 & 1.0714 \\ -0.4945 & -0.1442 & -0.5769 & -6.5934 & 1.0714 & 6.7376 \end{pmatrix}$$

组装系统刚度阵时只需要将 $\mathbf{K}^{(1)}$ 和 $\mathbf{K}^{(2)}$ 添加至 $\mathbf{K}(1:6, 1:6)$ 与 $\mathbf{K}(3:8, 3:8)$

处即可，具体为

$$\mathbf{K} = 10^7 \times \begin{pmatrix} 1.3599 & 0.5357 & -0.9478 & 0.0412 & -0.4121 & -0.5769 & 0 & 0 \\ 0.5357 & 3.3688 & -0.0412 & -3.2246 & -0.4945 & -0.1442 & 0 & 0 \\ -0.9478 & -0.0412 & 1.7720 & -0.5357 & -0.4121 & 1.0714 & -0.4121 & -0.4945 \\ 0.0412 & -3.2246 & -0.5357 & 3.5130 & 1.0714 & -0.1442 & -0.5769 & -0.1442 \\ -0.4121 & -0.4945 & -0.4121 & 1.0714 & 3.1319 & 0 & -2.3077 & -0.5769 \\ -0.5769 & -0.1442 & 1.0714 & -0.1442 & 0 & 6.8819 & -0.4945 & -6.5934 \\ 0 & 0 & -0.4121 & -0.5769 & -2.3077 & -0.4945 & 2.7198 & 1.0714 \\ 0 & 0 & -0.4945 & -0.1442 & -0.5769 & -6.5934 & 1.0714 & 6.7376 \end{pmatrix}$$

下面组装右端力向量，将单元 (2) 的 1-4 边上的分布力等效为节点力，有

$$\begin{aligned} t_{x2} &= t_{x4} = 0 \text{ (N)}, \\ t_{y2} &= t_{y4} = -20 \text{ (N)}. \end{aligned}$$

这样就有

$$\mathbf{f} = (0 \ 0 \ 0 \ -20 \ 0 \ 0 \ 0 \ -20)^T.$$

于是就可写系统刚度方程

$$\mathbf{K}\mathbf{d} = \mathbf{f} + \mathbf{r}. \quad (1.1)$$

其中， \mathbf{K}, \mathbf{f} 的具体数值前已给出， \mathbf{d}, \mathbf{r} 的形式如下

$$\begin{aligned} \mathbf{d} &= (0 \ 0 \ 0 \ 0 \ d_{x3} \ d_{y3} \ d_{x4} \ d_{y4})^T, \\ \mathbf{r} &= (r_{x1} \ r_{y1} \ r_{x2} \ r_{y2} \ 0 \ 0 \ 0 \ 0)^T. \end{aligned}$$

1.2 Solution & Postprocessing

这时可直接应用分块降阶法，可依次求得节点位移与约束反力向量如下

$$\mathbf{d} = 10^{-5} \times (0 \ 0 \ 0 \ 0 \ -0.0387 \ -0.6657 \ 0.1235 \ -0.7041)^T, \quad (1.2)$$

$$\mathbf{r} = (40.0000 \ 11.5154 \ -40.0000 \ 28.4846 \ 0 \ 0 \ 0 \ 0)^T \text{ (N)}. \quad (1.3)$$

在与精确解比照后可以知道，与 4Q 单元相比，3T 单元的精度要差很多。

2 Problem 9.8

Problem 9.8

Develop MATLAB finite element program for the three-node constant strain triangular element. Note that in this case, element matrices can be computed without numerical integration. Test the code in one of the following two ways:
(a) against manual calculations for a two-element problem (see Problem 9.7) or
(b) against the MATLAB code for a quadrilateral element provided in chapter 12.
In the latter case, consider very fine meshes (at least 64-element mesh for the problem in Figure 9.14 for quadrilaterals)

Figure 2: Problem 9.8

节点位移与约束反力的计算结果与 **Problem 9.7** 中的结果是一致的。其中，MATLAB 程序改动之处包括

- Preprocessor:
 - `plotmesh` 函数增加 `nen=3` 的判断;
- Formation:
 - `BmatElast2D` 函数增加计算 3T 单元应变矩阵与 *Jacobi* 行列式的分支;
 - `elast2Delem` 函数增加组装 3T 单元刚度阵及体积力向量的分支;
- Postprocessor:
 - `displacements` 函数增加 `nen=3` 的判断;
 - `get_stress` 与 `nodal_stress` 函数增加 3T 常应变单元的应力恢复分支。