

THERMODYNAMICS

PH332

①

2 STATISTICAL MECHANICS

Feb 6, 2019

Thermodynamics

- macroscopic properties of system P, V, T, etc
- and w/ system that are large enough that microscopic fluctuations can be ignored

Stat mech

- individual states of atoms / microscopic states of particles in system & uses statistics to describe macroscopic behavior

- This course focuses on systems of large numbers of particles.
? → how large?

Large? 1 mole $\rightarrow N_A = 6.022 \times 10^{23}$ particles \rightarrow Avogadro's #

- Why need statistics? \rightarrow Ex. Say we want to count # of particles in a mole of water.

$$3\text{GHz} \rightarrow 3 \times 10^9 \text{ s}^{-1} \text{ count rate} \Rightarrow 2 \times 10^{14} = 6.4 \times 10^6 \text{ yrs.}$$

→ needs stats models...

What is a mole?

\rightarrow A mole is the amount of matter that contains as matter as 12g of ^{12}C

Molar Mass

M: mass of 1 mole of a substance in grams.

$$\begin{aligned} \text{Ex } M_{^{12}\text{C}} &= 12 \text{ g/mol} & M_{\text{H}_2\text{O}} &= 18 \text{ g/mol} \\ M_{\text{He}} &= 4 \text{ g/mol} \end{aligned}$$

Temperature

\rightarrow always use K. Don't use Fahrenheit.

Fahrenheit scale \rightarrow Freezing point of water: 32°F
Boiling point of water: 212°F

Celsius \rightarrow

0°C

100°C

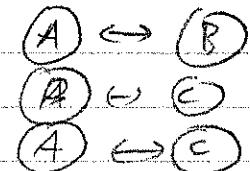
$${}^\circ\text{F} = 32 + \frac{9}{5} {}^\circ\text{C}$$

$$T_{(K)} = T_{(C)} + 273.15$$

What is temperature?

[0th law of thermodynamics]

{ If A is in thermoequilibrium with B
 but C is in thermoequilibrium with C
 then $T_A = T_C$
 → "thermoequilibrium" ≡ same T.



Temperature: a measure of how likely it is for a system to give up energy to another system. Generally, higher T → more likely to give off energy

Feb 8, 2019

Ideal Gas Law

$$PV = nRT$$

$$PV = NkT$$

n: # of moles R: Gas constant 8.31 J/mole

N: # of particles k_B : Boltzmann Constant $= 1.38 \times 10^{-23} \text{ J/K}$

$$\therefore nR = Nk_B$$

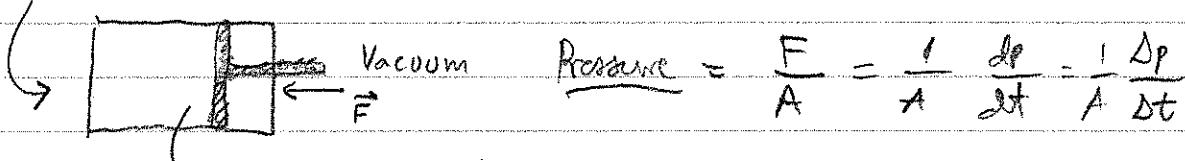
Note $N = nN_A$ so

$$R = N_A k_B$$

$$k_B = \frac{R}{N_A}$$

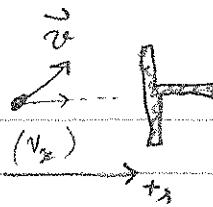
Assumptions: point-like particles, don't interact

How does Temperature T of ideal gas relate to its KE?



* assume perfectly elastic collisions

(1) Change in momentum of single particle.



$$\Delta p = mv_f - mv_i$$

$$= -mv_x - mv_x = -2mv_x$$

$\therefore \Delta p_{\text{piston}} = 2mv_x$

(2) # of collisions?



assume N molecules in volume V

$$\rightarrow \text{density} = \frac{N}{V} = \frac{N}{V}$$

$\therefore \# \text{ of collisions} = \frac{N}{V} \cdot (v_x A)$

$\therefore \# \text{ collision/sec} = \frac{N(v_x A)}{V}$

(3) Force on piston $F = \frac{\Delta P}{\Delta t} = \left(2mv_x\right) \left(\frac{Nv_x A}{V}\right)$

$$= 2mv_x^2 \frac{NA}{V}$$

$\therefore P = \frac{F}{A} = 2mv_x^2 \frac{N}{V}$

Now, corrections. Not all particles have the same v_x

$\rightarrow \langle v_x^2 \rangle$ instead of v_x^2 . Also, $1/2$ of particles are moving in the other direction ($-v_x$) \rightarrow divide by 2

$\therefore P = m \langle v_x^2 \rangle \frac{N}{V}$

$$\text{Now } v^2 = v_x^2 + v_y^2 + v_z^2$$

$\Rightarrow PV = m \langle v_x^2 \rangle N$

\Rightarrow Assume $\langle v_z^2 \rangle$ equal

$$\Rightarrow \frac{\langle v^2 \rangle}{3} = \langle v_x^2 \rangle$$

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$$\text{So } PV = NkT = \frac{1}{3}m\langle v^2 \rangle N = \frac{2}{3}\left[\frac{1}{2}m\langle v^2 \rangle\right]N$$

$$\text{So } kT = \frac{2}{3}\langle KE \rangle$$

$$\text{So } \langle KE \rangle = \frac{3kT}{2}$$

Average speed of the particles?

$$\text{Naively } \frac{1}{2}m\langle v^2 \rangle = \frac{3}{2}kT \quad (\text{g}), \text{ not } M = m/N_A$$

$$\rightarrow \langle v^2 \rangle = \frac{3kT}{m}$$

But this is Not $\langle v \rangle$

$$\text{So } v_{rms} = \sqrt{\langle v^2 \rangle} = \sqrt{\frac{3kT}{m}}$$

$$\langle v \rangle = \sqrt{\langle v_x^2 \rangle + \langle v_y^2 \rangle + \langle v_z^2 \rangle}$$

We will (can) show that

$$\text{Part } \langle v^2 \rangle = \sqrt{\langle v_x^2 \rangle + \langle v_y^2 \rangle + \langle v_z^2 \rangle}$$

v_{rms}

$$\langle v \rangle = \sqrt{\frac{8kT}{\pi m}} < v_{rms}$$

Ex Find rms v of N_2 molecule at room temp. $\approx 300K$

$$v_{rms} = \sqrt{\frac{3k \cdot 300}{28/N_A}} \approx$$

$$\text{or } v_{rms} = \sqrt{\frac{3kT}{m}} = \sqrt{\frac{3nRT}{NM}} = \sqrt{\frac{3RT}{M}} \approx \sqrt{\frac{3 \cdot 8.31 \text{ J/moleK} \cdot 300}{28 \text{ g/mol}}} \approx$$

$$\text{Now } 28 \text{ g/mol} = 28 \times 10^{-3} \text{ kg/mol} \rightarrow v_{rms} = 517 \text{ m/s}$$

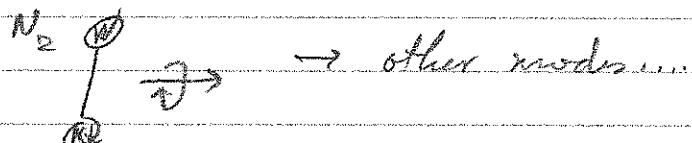
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What's the total thermal energy of a gas? or internal

$$U = \frac{3}{2} kT \cdot N = \langle KE \rangle N \rightarrow \text{but only true for monotonic ideal gas}$$

→ like noble gas.

Why? Degrees of freedom



If translational motion is not the only contributing factor

→ [Equipartition theorem]

{ → At some temp T, the average energy for every quadratic degree of freedom = $\frac{1}{2} kT$
 ex. $\frac{1}{2} m(v^2)$

So

$$U_{\text{thermal}} = Nf \frac{1}{2} kT \quad f = \# \text{ of quadratic df}$$

Degrees of freedom?

→ for a gas

↳ translational : x, y, z (3 df)

↳ Rotational : how many axes of rotation introduce a symmetry?

Ex → (2 df)

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Ex $\text{O}_2 \rightarrow (3 \text{ df})$

• vibrational (1) $\text{m} - \text{n} \rightarrow$ classical mech tells us this

$\langle \text{KE} \rangle = \langle \text{PE} \rangle$ for SHO \rightarrow 2 degrees of freedom, both quadratic.

at normal temp

\rightarrow small effect. Most diatomic molecules only have (5) df at typical room temp, so vibr. df are frozen out.

$$\rightarrow U_{\text{internal N}_2} \approx N \left(\frac{3+2+0}{2} \right) kT$$

Feb 11, 2019

[Heat = Work]

Exchange is energy

Last time

$$U = \frac{f}{2} N \cdot kT$$

{ Heat (Q) \rightarrow spontaneous flow of energy from one system to another due to a ΔT }

so $\boxed{\text{if } \Delta T \neq 0, \text{ then } Q \neq 0 \text{ (Heat) Spontaneously}}$

Work

(W) non-spontaneous transfer of energy

\rightarrow need an "agent" to transfer energy

Heat & Work are not intrinsic to system. \rightarrow they're processes.

Compression work



$$P = \frac{F}{A}$$

positive, since $\Delta x < 0$

$$W_{\text{on gas}} = -F \Delta x = -PA \Delta x = -P \Delta V$$

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$$\text{So } W_{\text{noncons}} = -P\Delta V$$

\Rightarrow We should use differentials, but they are not exact diff. because of path-dependence.

$$W = \int_p \vec{F} \cdot d\vec{r}$$

A differential is exact if $\exists f = f(x, y)$ such that

$$df = \left(\frac{\partial f}{\partial x} \right)_y dx + \left(\frac{\partial f}{\partial y} \right)_x dy$$

\rightarrow True for conservative vector fields $\vec{v} = \nabla f$

$$A = \frac{\partial f}{\partial x}$$

In other words, $df = Adx + Bdy$ exact diff. if $B = \frac{\partial f}{\partial y}$

$$\vec{J} \times [A, B] = \begin{vmatrix} \frac{\partial f}{\partial x} & \frac{\partial f}{\partial y} \\ \frac{\partial f}{\partial x} & \frac{\partial f}{\partial y} \end{vmatrix} = \frac{\partial^2 f}{\partial x \partial y} - \frac{\partial^2 f}{\partial y \partial x} = 0$$

\Rightarrow Can we Euler's test to determine if we have an exact diff.

$$\text{let } df = Adx + Bdy$$

\checkmark check if $\frac{\partial A}{\partial y} = \frac{\partial B}{\partial x} \rightarrow$ Yes! \rightarrow Exact

\checkmark No! \rightarrow Not exact

\checkmark Inexact differentials are written as \rightarrow dW or ds

\hookrightarrow path-dependence!

- ◻ Exact differentials can become exact by multiplying by some integrating factor.

e.g. $\frac{dw}{P} = dV \rightarrow$ volume $dV \rightarrow$ exact diff

$\left\{ \frac{dq}{T} = ds \right. \rightarrow$ entropy $ds \rightarrow$ exact diff

- ◻ If Q & W are the only ways energy is transferred, then conservation of energy

$$\boxed{\Delta U = Q + W_{on}} \rightarrow 1^{\text{st}} \text{ law of thermodynamics}$$

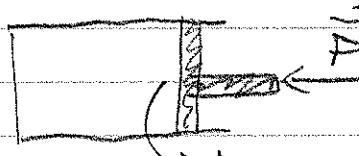
Q : heat added to system, W : work done on system

In differential \rightarrow $\boxed{dU = \delta Q + \delta W_{on} = \delta Q - \delta W_{by}}$

Units of energy $\rightarrow 1 \text{ J} \rightarrow 1 \text{ kg m/s}^2$

$1 \text{ cal} \rightarrow 4,186 \text{ J}$

$1 \text{ cal} \rightarrow$ # heat needed to raise 1g of H₂O by 1°C or 1K



$$W_{on} = -F \Delta x = -PAV$$

(let $P \rightarrow P(V)$)

$x \quad \Delta x$

Before, we assumed that P is constant over the process \rightarrow assumed piston movement was slow

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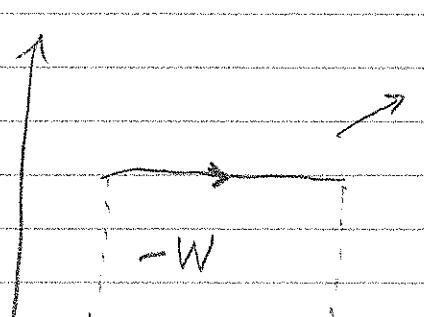
Quasi-static process → slow process, allow P to equilibrate

$$\rightarrow W_m = -PV \quad \text{or} \quad dW_m = PdV$$

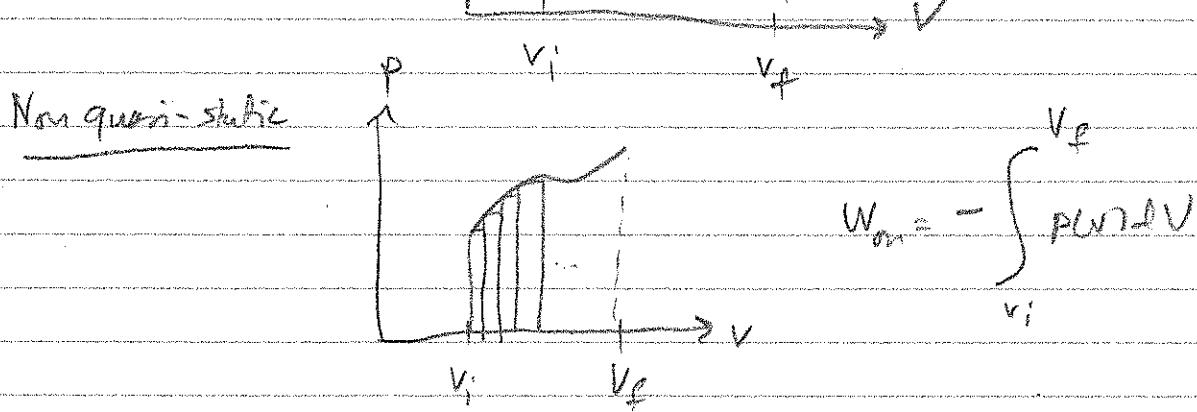
N.B. There is heat flow in quasi-static process

Q We often consider infinitesimal changes that are each quasistatic
so their integral

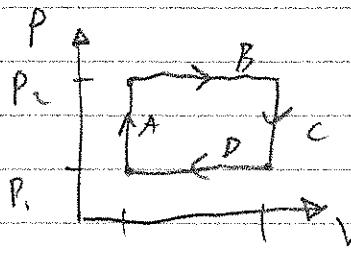
$$W_m = - \int_{V_1}^{V_2} PV dV$$

P-V diagram 

quasistatic



Example of PV diagram Interpreting PV diagrams



An ideal diatomic gas (N_e)

For steps $A \rightarrow D \rightarrow$ we want to determine
 W_m , Q_{add} , ΔU , and $W_{total\ air}$, Q_{tot}

H.N.2

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	A	B	C	D	E
W_m	0	$P_2(V_1 - V_2)$	0	$P_1(V_2 - V_1)$	< 0
Q	$\sum v_i (P_2 - P_1)$	$\frac{3}{2} P_2 (V_2 - V_1)$:	:	> 0
ΔU	$\sum v_i (P_2 - P_1)$	$\frac{5}{2} P_2 (V_2 - V_1)$:	:	0

A: $W = 0$, $\Delta U = \frac{f}{2} NkT = \frac{f}{2} Nk \frac{PV}{NkT} = \frac{f}{2} PV$

So $\Delta U_A = \frac{f}{2} V_f \Delta P$

$$\Delta U = Q + W$$

B $\Delta U = \frac{5}{2} P \Delta V = \frac{5}{2} P_2 (V_2 - V_1)$

$$Q = \Delta U - W = \sum P_i (V_2 - V_1) - P_2 (V_1 - V_2)$$

Note $\left\{ \begin{array}{l} W_{on, total} < 0 \\ Q > 0 \\ \Delta V = 0 \end{array} \right\}$

Feb 12, 2019 Quasistatic review "slow" \rightarrow so that system can equilibrate
 \rightarrow pressure is uniform over system

$$W_{on} = -F \Delta x \rightarrow -P \Delta V$$

Not-quasistatic "fast" \rightarrow pressure depends on position

Compressing of an ideal gas

→ "slow" compression such that
 Isothermal compression $\rightarrow T = \text{constant}$

Temp doesn't increase

$$\Delta U = W_{on} + Q_{add} \rightarrow Q \text{ leaves system} \rightarrow \Delta U = 0$$

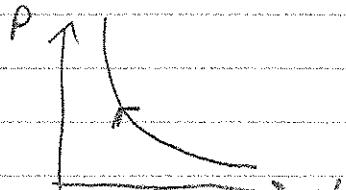
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Adiabatic compression \rightarrow "fast" compression. So fast that no heat can escape.

$$\dot{Q} = 0 \quad \text{so} \quad \Delta U = W_{\text{in}} + Q_{\text{add}} = W_{\text{in}}$$

\rightarrow Temp increases

P-V diagram



Isothermal process \rightarrow Quasistatic

$$W_{\text{in}} = - \int_{V_i}^{V_f} p(V)dV = - \int_{V_i}^{V_f} \frac{NkT}{V} dV \quad \rightarrow PV = \text{const}$$

$$= - NkT \int_{V_i}^{V_f} \frac{dV}{V}$$

$$W_{\text{in}} = - NkT \ln \left(\frac{V_f}{V_i} \right)$$

\rightarrow Work done on system
in isothermal compression.

Since T does not increase, how much heat is lost?

$$\downarrow$$

$$\dot{Q} = W_{\text{in}} + Q_{\text{add}} = 0 \quad \text{or} \quad W_{\text{in}} = Q_{\text{out}}$$

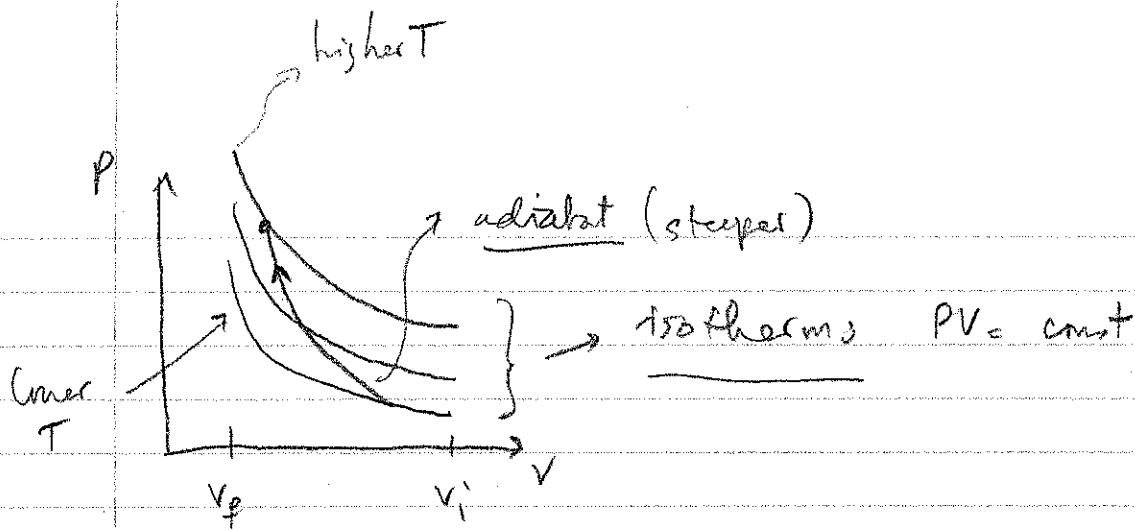
$$\therefore Q_{\text{add}} = - W_{\text{in}} = NkT \ln \left(\frac{V_f}{V_i} \right)$$

Adiabatic process \rightarrow fast

Assume quasistatic process ... $\Delta U = W_{\text{in}} + Q_{\text{add}}$

By definition of adiabatic $\rightarrow Q = 0$

$$\therefore \Delta U = W_{\text{in}}$$



Q How do different parameters change during adiabatic compression?

C Ideal gas $\Delta U = \frac{W}{n} + Q = W_n$

$$U = \frac{f}{2} NkT \rightarrow dU = \frac{f}{2} Nk dT = dW = -PdV$$

$$\int \frac{f}{2} Nk dT = - \frac{NkT}{V} dV$$

$$\int \frac{f}{2} \frac{dT}{T} = - \int \frac{dV}{V}$$

$$\int \frac{f}{2} \ln\left(\frac{T_f}{T_i}\right) = - \ln\left(\frac{V_f}{V_i}\right)$$

$$\left(\frac{T_f}{T_i}\right)^{\frac{f}{2}} = + \left(\frac{V_f}{V_i}\right)^{-1} \rightarrow V_i T_i^{\frac{f}{2}} = T_f^{\frac{f}{2}} V_f$$

$$\boxed{VT^{\frac{f}{2}} \rightarrow \text{constant}}$$

\rightarrow adiabatic compression/expansion of ideal gas

$$T = \frac{PV}{Nk} \rightarrow V \cdot \left(\frac{PV}{Nk}\right)^{\frac{f}{2}} \rightarrow \text{constant} \quad \left\{ \rightarrow PV^{1+\frac{2}{f}} = \text{constant} \right.$$

$$\rightarrow P^{\frac{f}{2}} V^{1+\frac{f}{2}} \rightarrow \text{constant} \quad \left\{ \text{Call } \gamma = 1 + \frac{2}{f} = \frac{f+2}{f} \right.$$

$$\rightarrow P^{\gamma} V^{\gamma} = \text{constant}$$

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We call $\gamma \rightarrow$ "adiabatic exponent" $\gamma = \frac{f+2}{f}$

$$\gamma = \frac{f+2}{f} \quad \left\{ \begin{array}{l} PV^\gamma = \text{constant} \\ VT^{\frac{1}{\gamma}-1} = \text{constant} \end{array} \right\}$$

Now, pressure & temp.

$$\hookrightarrow V^\gamma P = \text{constant} \quad \sqrt[V]{T^{\frac{1}{\gamma}-1}} = \text{constant}$$

$$\therefore (V^\gamma P)(V^{\frac{1}{\gamma}-1} T^{\frac{1}{\gamma}-1})$$

$$= PT^{\frac{1}{\gamma}-1} \text{ constant}$$

$$\therefore \boxed{PT^{\frac{1}{\gamma}-1} \text{ constant}}$$

Ex Diesel engine (no spark plugs...)

atm air is quickly compressed to $1/20$ original volume
 \rightarrow Estimate temp of air in cylinder

$$\text{well } \frac{V_f}{V_i} = \frac{1}{20} \rightarrow \text{assume ideal gas (diatomic} \rightarrow f=5)$$

$$\text{Ok } VT^{\frac{1}{\gamma}-1} = \text{constant}$$

$$\hookrightarrow \left(\frac{T_f}{T_i} \right)^{\frac{1}{\gamma}-1} = \left(\frac{1}{20} \right)^{-1} = 20$$

$$\approx 20 \approx 300$$

$$\therefore T_f = \sqrt[5/2]{20 T_i} = \sqrt[5/2]{20} T_i$$

$$\therefore \boxed{T_f \approx 1000k > 700^\circ C}$$

\rightarrow hot enough to ignite Diesel without spark plug.

Heat capacity

↳ the amount of heat necessary to raise a substance by 1°C

$$C = \frac{Q}{\Delta T}$$

$$Q = C\Delta T = mc\Delta T$$

Specific heat capacity

$$c = \frac{C}{m}$$

But recall → $Q_n = \Delta U - W_m$: limiting case $\rightarrow W = 0$
 → no change in V

get heat capacity at constant volume, $-C_V$

not the most physical

$$C_V = \frac{\Delta U - W}{\Delta T} = \frac{\Delta U}{\Delta T} = \left(\frac{\partial U}{\partial T} \right)_{V \text{ constant}}$$

Ex for 1g of H_2O $C_V = 1 \text{ cal/K}$

Feb 13, 2019

Heat Capacity

$$\begin{aligned} &\rightarrow W = 0, \Delta V = 0 \rightarrow C_V = \frac{\Delta U - W}{\Delta T} = \left(\frac{\partial U}{\partial T} \right)_{V \text{ const}} \\ &\text{limiting cases} \quad \left. \begin{array}{l} \text{Constant volume} \\ \text{Constant pressure} \end{array} \right\} \end{aligned}$$



Heat capacity at constant pressure

$$C_P = \frac{Q}{\Delta T} = \frac{\Delta U - W}{\Delta T} = \left(\frac{\Delta U - (-P\Delta V)}{\Delta T} \right)_{P \text{ const}}$$

$$C_P = \left(\frac{\partial U}{\partial T} + P \frac{\partial V}{\partial T} \right)_{P \text{ const}}$$

→ heat needed to compensate for expansion

$$\text{Note } \left(\frac{\partial U}{\partial T} \right)_P \approx \left(\frac{\partial U}{\partial T} \right)_V \rightarrow$$

(energy loss at work due to recession)

Suppose we have a system that obeys equipartition theorem

$$U = \frac{f N k T}{2}$$

Then

$$C_V = \left(\frac{\partial U}{\partial T} \right)_{V, \text{constant}} = \frac{f N k}{2}$$

if we can measure C_V
then we can find f.

[Ex]



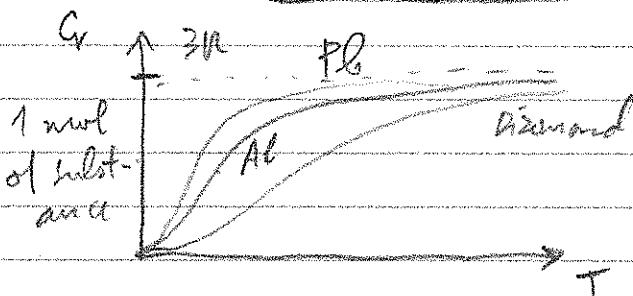
Consider solids/crystal

no rotation/translation

→ only of is rotation.

→ Solid should have 6 d.f.s

$$\therefore C_V = \frac{6 N k}{2} = 3 N k = 3 n R \quad \text{for solid}$$



Heat capacity at constant pressure for ideal gas

$$C_p = \left(\frac{\partial V}{\partial T} \right)_p + \left(P \frac{\partial V}{\partial T} \right)_p$$

↓ always eq. partition

$$\downarrow = \frac{f N k}{2} + P \frac{\partial}{\partial T} \left[\frac{N k T}{P} \right]$$

$$+ n R = C_p + N k = C_p = \frac{f}{2} N k + N k$$

$$\text{Recall } r = \frac{f+2}{f} > 1 + \frac{2}{f}$$

$$\downarrow = \left(\frac{f+1}{2} \right) N k$$

$$\rightarrow \gamma - 1 = \frac{2}{f}$$

$$\boxed{C_p = \frac{\gamma}{\gamma-1} N k}$$

$$\frac{f+1}{2} = \frac{1}{\gamma-1} + 1$$

Recall the Adiabatic exponent γ

Definition

$$\gamma \equiv \frac{C_p}{C_V} = \frac{C_V + nR}{C_V} = \frac{f/2 + 1}{f/2} = \frac{2+f}{f}$$

Example of heat capacity

■ Heat capacity of a star

Well $U_{\text{pot}} = -\frac{GMm}{r}$ $KE = \frac{1}{2}mv^2$ $v = \sqrt{\frac{GM}{r}}$

$\therefore k = \frac{1}{2}m \frac{GM}{r}$

Virial Theorem

$$\rightarrow U_{\text{tot}} = U_{\text{pot}} + KE = \frac{1}{2}m \frac{GM}{r} - \frac{GMm}{r} = -\frac{1}{2} \frac{GMm}{r}$$

$$\downarrow -2KE \quad \rightarrow U_{\text{tot}} = -k = \frac{1}{2} \frac{GMm}{r}$$

Star { It goes (3 df) \rightarrow quadratic

{ obeys eq. part. then $k = \frac{1}{2}mv^2 = \frac{f}{2}NkT = \frac{3}{2}NkT$

$\therefore U_{\text{tot}} = -\frac{3}{2}NkT$

$\hookrightarrow C_V = \left(\frac{\partial u}{\partial T} \right)_V = -\frac{3}{2}Nk \rightarrow$ negative heat capacity

\hookrightarrow So, as a star radiates Σ , it gets fatter.

Latent heat → useful for phase transitions.

e.g. melting ice Solid \rightarrow liquid \rightarrow Vapor

Note Temperature stays constant during phase transitions.

→ need to know how much heat is needed to complete phase transitions.

$$\text{latent heat } \{ L = \frac{Q}{m} \}$$

• Assume that $P = \text{constant}$ over phase transitions

• Assume that no other work besides expansion/compression

Ex latent heat of fusion

$$\begin{aligned} \text{H}_2\text{O}(s) &\rightarrow \text{H}_2\text{O}(l) \quad L_f = 333 \text{ J/g} \gg C_f \\ \text{H}_2\text{O}(l) &\rightarrow \text{H}_2\text{O}(g) \quad L_v = 2260 \text{ J/g} \gg C_v \end{aligned}$$

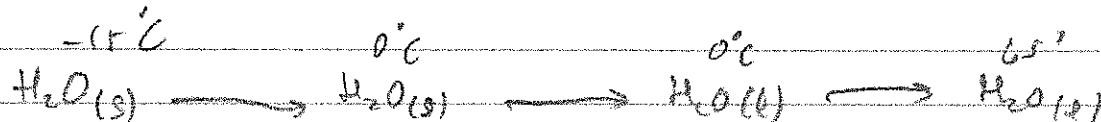
Ex 200g cup of tea that is @ boiling pt (212°F , 100°C)

I want to cool down to drink - 150°F , 65°C
How much ice do we want?

$$T_{\text{ice}} = -15^\circ\text{C} \quad C_{\text{ice}} = 0.5 \text{ cal/g/C}$$

$$C_{\text{H}_2\text{O}(l)} = 1 \text{ cal/g} \quad L_f = 80 \text{ cal/g}$$

$$\begin{aligned} \text{(lost heat)} &= m_{\text{ice}} \Delta T C_{\text{H}_2\text{O}} = 200 (100 - 15) 1 \text{ cal} \\ &= 7000 \text{ cal} \end{aligned}$$



$$\begin{aligned} Q_{\text{cool}} &= m C_p \Delta T + L \cdot m + m C_D \Delta T \end{aligned}$$

Q $m = \frac{7000 \text{ cal}}{C_{\text{ice}}(0 - (-15)) + L + (65 - 0) C_{\text{H}_2\text{O}(\ell)}} \approx 46 \text{ g of ice}$

Feb 15, 2019

Enthalpy

→ total heat content of a system

$$H \equiv U + PV$$

→ used for constant P processes

H is used for constant-pressure processes.

Ex Add heat to a system at constant pressure. Then U, V, H change.

So $H + \Delta H = U + \Delta U + P(V + \Delta V)$

$$H + \Delta H = \underbrace{(U + PV)}_H + (\Delta U + P\Delta V)$$

So $\boxed{\Delta H = \Delta U + P\Delta V} \rightarrow @ \text{constant pressure.}$

First law if $\Delta U = Q + (-P\Delta V) \rightsquigarrow + W_{\text{other}}$ → compression work

Then $\Delta H = \Delta U + P\Delta V = Q + W_{\text{other}}$

So

$$\boxed{\Delta H = Q_{\text{add}} + W_{\text{other}}} \rightsquigarrow \text{true for constant P processes.}$$

Heat capacity at constant pressure

$$\boxed{C_p = \left(\frac{\partial H}{\partial T}\right)_p}$$

Examples ΔH for boiling H_2O (phase transition)

$\Delta H = 40660 \text{ J/mol}$ at 1 atm, 298K

$$\Delta H = \frac{40660 \text{ J/mol}}{18 \text{ g/mol}} \approx 2260 \text{ J/g} = L_{H_2O}$$

↳ latent heat of vaporization

How much work is needed to create space for the vapor

$$V_f \approx 0 \quad V_f \approx \frac{nRT}{P} = \frac{RT}{P} \quad (n=1)$$

$$\therefore \Delta V = \frac{RT}{P} \rightarrow W = PDV = RT = \frac{8.314 \text{ J}}{\text{mol} \cdot \text{K}} \cdot 298 \text{ K}$$

$$\approx 3100 \text{ J}$$

Statistics

Random Walk problem



$$\begin{cases} P(\text{left}) = P(\text{right}) = 1-p = q \\ P(\text{right}) = p \end{cases}$$

Final position $x = ml$ after N total steps where N_m are integers: $-N \leq m \leq N$

$\therefore P_N(m) = \text{Probability of finding our drunk at } x=ml \text{ after } N \text{ steps.}$

$$\left. \begin{array}{l} \text{let } n_R = \# \text{ steps to R} \\ n_L = \# \text{ steps to L} \end{array} \right\} \quad N = n_R + n_L$$

$$\text{And } m = n_R - n_L = n_R - (N - n_R) = -N + 2n_R$$

The probability of any sequence of steps (ass. independent) is

$$P^{n_R} (1-p)^{n_L} = P^{n_R} (1-p)^{N-n_R} \quad \text{the products}$$

But there are many ways of taking N steps with $n_R = n_L$

The number of ways is called "Multiplicity", Ω

↳ "No. of microstates"

$$\Omega = \frac{N!}{n_R! n_L!} = C^N_{n_R}$$

Say there are N objects $\rightarrow N!$ permutations. But this is only true for distinguishable objects, since order matters.

What about the # of ways N objects can be arranged into n_R spaces? where $n_R < N$

$$\Omega = \frac{N!}{(N-n_R)! n_R!} = \frac{N!}{(N-n_R+1)(N-n_R+2)\dots(N-n_R+n_R)!}$$

If we have indistinguishable objects, we have all $n_R!$ ways of arranging N into n_R spaces are the same \rightarrow divide them out

$$\rightarrow \frac{N!}{(N-n_R)! n_R!} = \frac{N!}{n_R! n_L!}$$

\rightarrow For indistinguishable objects, use combinations... Total multiplicity of outcomes

$$\Omega(n_R) = \frac{N!}{n_R! (N-n_R)!} = \binom{N}{n_R}$$

(21)

$$\hookrightarrow P_N(n_R, n_L) = \binom{N}{n_R} p^{n_R} (1-p)^{N-n_R}$$

or other notation

$$\hookrightarrow W_N(n_R) = \binom{N}{n_R} p^{n_R} (1-p)^{N-n_R} \rightarrow \text{same thing}$$

\hookrightarrow Binomial distribution

$$\textcircled{a} \quad \sum_{n=0}^N W_N(n) = 1 \quad \textcircled{b} \quad E(n) = Np \quad \textcircled{c} \quad V_n = Np(1-p)$$

Ex 18.2019Binomial Distribution

$$P_N(n) = \binom{N}{n} p^n q^{N-n}$$

$$\sum_{n=0}^N P_N(n) = 1$$

$$\text{More generally, } \sum_{n=0}^N W_N(n) = (p+q)^N$$

Example Roll 4 dice

$$P(\text{one of 4 is } \square) = \binom{4}{1} \left(\frac{1}{6}\right)^1 \left(\frac{5}{6}\right)^{4-1} = 1 - \left(\frac{5}{6}\right)^4 \approx 39\%$$

Example Roll 2 1's, 4 dice

$$P_4(2) = \binom{4}{2} \left(\frac{1}{6}\right)^2 \left(\frac{5}{6}\right)^{4-2} = \left(\frac{5}{6}\right)^2 \frac{1}{6} \approx 12\%$$

Note High multiplicity, don't not likely outcome.

Random Walk

$$x = ml$$

 $n=0$

What is the probability that we're back at $m=0$ after N steps?

(a) If N is even?

(b) If N is odd?

$$P_N(m) = \frac{N!}{n_R!(N-n_R)!} p^{n_R} (1-p)^{N-n_R}$$

$$N = n_R + n_L$$

$$m = n_R - n_L$$

$$= \frac{(n_R + n_L)!}{n_R! n_L!} p^{n_R} (1-p)^{N-n_R}$$

$$\text{So } N = 2n_L - m$$

$$= \frac{N!}{(\frac{N+m}{2})! (\frac{N-m}{2})!} p^{\frac{N+m}{2}} (1-p)^{\frac{N-m}{2}}$$

Assume that $p = 1-p = \frac{1}{2}$

So

$$P_N(m) = \frac{N!}{(\frac{N+m}{2})! (\frac{N-m}{2})!} \cdot \left(\frac{1}{2}\right)^N$$

So $P_N(m=0) = \frac{N!}{(\frac{N}{2})! (\frac{N}{2})!} \left(\frac{1}{2}\right)^N \Rightarrow \text{if } N \text{ even}$

If N is odd, then $m \neq 0$ since $N = 2n_L - m$

So $\boxed{P_N(m=0) = 0}$

odd even odd

Determination of mean value

Random walk with $N = 2$ steps. Let's say after 2 steps, drunk finds \$ and picks it up.

(@)	$x = -2l$	\$1
(@)	$x = 0$	\$5
(@)	$x = 2l$	\$20

Question on average, how much \$ would you pick up?

Well $P_1(-2l) = ?$, $P_2(2l) = ?$, $P_2(0) = ?$

$$\rightarrow P_2(0) = \frac{1}{2} \quad \left. \begin{array}{l} P_1(-2l) = P_2(2l) = \frac{1}{4} \end{array} \right\} \text{"by inspection"}$$

Let $f(m)$ be the amount of \$ at location m .

In general, $\langle x \rangle = E(x) = \sum_{x=0}^{\infty} x \cdot P(x)$

$$\overline{x} = \frac{\sum_{i=0}^{\infty} P(x_i) x_i}{\sum_{i=1}^{\infty} P(x_i)}$$

But since we're dealing w probabilities, $\sum P(x_i) = 1$

Mean value of f_m

$$E[f(u)] = \sum_{i=0}^{\infty} f(u_i) P(u_i)$$

(24)

$$\text{Note } E[f(u) + g(u)] = E(f(u)) + E(g(u))$$

$$\text{If } sE(f(u)) = E(sf(u)), \quad s \in \mathbb{R}$$

→

So

 $\frac{1}{4}$

$$\text{Ex: average, } E(\$) = \frac{1}{4} \cdot 1 + \frac{1}{2} \cdot 5 + \frac{1}{2} \cdot 20$$



$$= \frac{1}{4} + \frac{5}{2} + 10$$

 $\$1 \quad \$5 \quad \$20$

$$= \$ \frac{50}{4} (10 + \frac{11}{4})$$

On average, how far away from the average are we?

$$\rightarrow E(u - E(u)) = ? = E(u) - \overline{E(u)} = 0$$

What about $E((u - E(u))^2)$?

(Second moment about the mean? → Variance)

$$\Delta u^2 = \sigma^2 = E[(u - E(u))^2]$$

$$= E(u^2) - 2E(u)\overline{E(u)} + E(\overline{E(u)})^2$$

$$\boxed{\text{Var}(u) = E(u^2) - \overline{E(u)}^2}$$

$$\text{Standard deviation} \rightarrow \sqrt{\text{Var}(u)} = \sigma = \sqrt{E(u^2) - \overline{E(u)}^2}$$

Mean values - Random Walk problem

Feb 19,
2019

Recall

$$P_N(n_R) = \frac{N!}{n_R!(N-n_R)!} p^{n_R} q^{N-n_R}$$

$$\mathbb{E}[f(n_R)] = \sum_{n_R=0}^N f(n_R) P_N(n_R)$$

↳

Merge & steps to the right

$$\mathbb{E}[n_R] = \sum_{n_R=0}^N n_R P(n_R) = \sum_{n_R=0}^N n_R \frac{N!}{n_R!(N-n_R)!} p^{n_R} q^{N-n_R}$$

$$\text{Notice } n_R p^{n_R} = p \frac{\partial}{\partial p} (p^n)$$

$$\mathbb{E}[n_R] = \sum_{n_R=0}^N \frac{N!}{n_R!(N-n_R)!} p \frac{\partial}{\partial p} (p^{n_R}) q^{N-n_R}$$

$$= p \frac{\partial}{\partial p} \sum_{n_R=0}^N \frac{N!}{n_R!(N-n_R)!} p^{n_R} q^{N-n_R}$$

$$= p \frac{\partial}{\partial p} (p+q)^N$$

$$= p \cdot N \frac{\partial}{\partial p} (p+q)^{N-1}$$

But $p+q=1$

↳ $\boxed{\mathbb{E}[n_R] = pN}$

Similarly

$$\boxed{\mathbb{E}[n_L] = qN = N(1-p)}$$

$$\left. \begin{aligned} \mathbb{E}[n] &= \mathbb{E}[n_R - n_L] \\ &= \mathbb{E}[n_R] - \mathbb{E}[n_L] \\ &= N(p-q) \end{aligned} \right\}$$

$$\text{So } E(n) = N(p-q)$$

→ If $p=q$, then $E(n) = 0$.

(Variance)

$(pn)^2$

$$\text{Var}(n_R) = E(n_R^2) - E(n_R)^2$$

$$E(n_R^2) = \sum_{n_R=0}^N n_R^2 p(n_R)$$

$$= \sum_{n_R=0}^N n_R^2 \frac{N!}{n_R!(N-n_R)!} p^{n_R} q^{N-n_R}$$

$$\rightarrow \text{Same trick as before ... } n_R^2 p^{n_R} = n_R p \frac{\partial}{\partial p} p^{n_R} = p \frac{\partial}{\partial p} (n_R p^{n_R})$$

$$E(n_R^2) = \sum_{n_R=0}^N \binom{N}{n_R} \left(p \frac{\partial}{\partial p} \right)^2 p^{n_R} q^{N-n_R} = \left(p \frac{\partial}{\partial p} \right)^2 p^{n_R}$$

$$= \sum_{n_R=0}^N \binom{N}{n_R} \left(p \frac{\partial}{\partial p} \right)^2 p^{n_R} q^{N-n_R}$$

$$= \left(p \frac{\partial}{\partial p} \right)^2 \sum_{n_R=0}^N \binom{N}{n_R} p^{n_R} q^{N-n_R}$$

$$= \left(p \frac{\partial}{\partial p} \right)^2 \{ p+q \}^N$$

$$= \left[p \frac{\partial}{\partial p} \right] \left(p + N(p+q)^{N-1} \right)$$

$$q+p=1 \rightarrow = p \left[N(p+q)^{N-1} + pN(N-1)(p+q)^{N-2} \right]$$

$$= pN + p^2 N(N-1) = pN + (pn)^2 - p^2 N$$

$$\text{So } \text{Var}(n_R) = pN + (qN)^2 - p^2N - (pqN)^2$$

$$= pN(1-p)$$

$$\boxed{\text{Var}(n_R) = Npq}$$

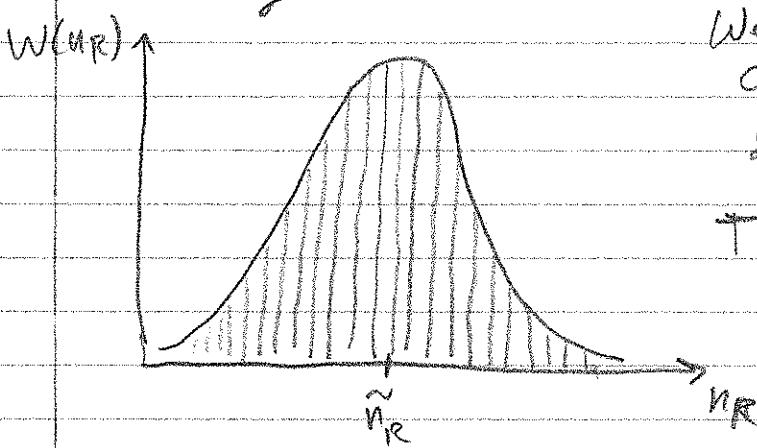
Relative Width of a distribution

$$\frac{\sigma_{n_R}}{E(n_R)} = \frac{\sigma_{n_R}}{Np} = \frac{\sqrt{Npq}}{Np} = \frac{\sqrt{q}}{\sqrt{Np}} = \boxed{\frac{\sqrt{q}}{\sqrt{Np}}}$$

where $p=q$, $\frac{\sigma_{n_R}}{E(n_R)} = \frac{1}{\sqrt{N}}$

→ relative width is $\propto \frac{1}{\sqrt{N}}$ ($p \neq q$ in general)

For large N , there's a well defined peak or a well-defined peak in $W(n_R) \propto n_R = \tilde{n}_R$, where \tilde{n}_R is the most likely value.



We can treat this as a continuous function as $N \rightarrow \infty$

To find \tilde{n}_R as a fn. of N, p, q , we need to look for

here

$$\frac{dW(n_R)}{dn_R} = 0$$

Instead of evaluating $\frac{dW}{dn_R}$, we'll do

$\frac{d}{dn_R} \ln(W(n_R))$ since it has the same \tilde{n}_R & is a more gradually varying fn. of n_R

$$\frac{dW_{nR}}{dn_R} = 0 = \frac{d\ln(W(n_R))}{dn_R}$$

B Taylor series expansion around \tilde{n}

$$\rightarrow f(x) \approx f(a) + \frac{f'(a)}{1}(x-a) + \frac{f''(a)}{2!}(x-a)^2 + \dots$$

\rightarrow We want to expand $\ln(W(n))$ around \tilde{n} .

$$n_R = \tilde{n} + \varepsilon \quad (\varepsilon \ll \tilde{n}) \quad \text{let's work with } n \neq n_R$$

$$\ln(W(n)) = \ln(W(\tilde{n})) + \frac{d}{dn} \ln(W(n)) \Big|_{\tilde{n}} \cdot \varepsilon + \frac{1}{2} \frac{d^2}{dn^2} \ln(W(n)) \Big|_{\tilde{n}} \varepsilon^2$$

0 since \tilde{n} most likely ...

$$= \ln(W(\tilde{n})) + \frac{1}{2} \frac{d^2}{dn^2} \ln(W(n)) \Big|_{\tilde{n}} \varepsilon^2$$

$$\text{So } W(n) \approx W(\tilde{n}) \cdot \exp \left[\frac{1}{2} \frac{d^2}{dn^2} \ln W(n) \Big|_{\tilde{n}} \varepsilon^2 \right]$$

Next $\frac{d\ln W(n)}{dn} = \frac{d}{dn} \cdot \left(\ln \left[\binom{N}{n} p^n q^{N-n} \right] \right)$

$$= \frac{d}{dn} \left[\ln(N!) - \ln(n!) - \ln((N-n)!) + n \ln p + (N-n) \ln q \right]$$

* Note that

$$\boxed{\frac{d}{dx} \ln x! \approx \ln x}$$

for large X

$$\text{So } \frac{d}{dn} \ln(W(n)) \Big|_{\tilde{n}} = -\ln \tilde{n} + \ln(N-\tilde{n}) + \ln p + \ln q$$

(29)

Result

$$W(n) = w(\tilde{n}) \exp \left[\frac{1}{2} (n - \tilde{n})^2 \frac{d^2 \ln W}{dn^2} \Big|_{\tilde{n}} \right]$$

$$\frac{d \ln W}{dn} \Big|_{\tilde{n}} = -\ln \tilde{n} + \ln(N-\tilde{n}) + \ln p - \ln q$$

$$e^{d\ln W} = (N-\tilde{n})^{\tilde{n}} \cdot \tilde{n}^{N-\tilde{n}} \cdot p^{\tilde{n}} \cdot q^{N-\tilde{n}}$$

$$e^{\sigma^2} = e^{\ln \left(\frac{(N-\tilde{n})^{\tilde{n}}}{\tilde{n}^{N-\tilde{n}}} \cdot p^{\tilde{n}} \cdot q^{N-\tilde{n}} \right)} = E(n)$$

$$\underline{\text{S}} \quad 1 = \frac{(N-\tilde{n})^{\tilde{n}}}{\tilde{n}^{N-\tilde{n}}} \Rightarrow \boxed{\tilde{n} = \frac{Np}{p+q} = \frac{Np}{N}}$$

Now, evaluate $\frac{d^2 \ln W}{dn^2} \Big|_{\tilde{n}}$

$$\frac{d^2 \ln W}{dn^2} = \frac{d}{dn} \left(\frac{d \ln W}{dn} \right) = \frac{d}{dn} \left[-\ln \tilde{n} + \ln(N-\tilde{n}) + \ln p - \ln q \right]$$

$$= -\frac{1}{\tilde{n}} + \frac{1}{N-\tilde{n}} \Big|_{\tilde{n}} = \frac{-N+n-n}{n(N-n)} \Big|_{\tilde{n}}$$

$$\underline{\text{S}} \quad \frac{d^2 \ln W}{dn^2} \Big|_{\tilde{n}} = \frac{-N}{\tilde{n}(N-\tilde{n})} = \frac{-N}{N_p(N-N_p)} = \frac{-1}{N_p(1-p)}$$

$$\boxed{\frac{d^2 \ln W}{dn^2} \Big|_{\tilde{n}} = \frac{-1}{N_p q}} \rightarrow > 0$$

Finally, we need $w(\tilde{n})$

$$\hookrightarrow w(\tilde{n}) = \frac{N!}{\tilde{n}!(N-\tilde{n})!} p^{\tilde{n}} q^{N-\tilde{n}} \stackrel{?}{=} ? \text{ For large } N$$

Use Stirling formula

$$n! \approx \sqrt{2\pi n} n^{n-u}$$

for $n \gg 1$

$$\therefore W(\tilde{n}) = \frac{\sqrt{2\pi N} N^{N-N}}{\sqrt{2\pi N_p} (N_p)^{N_p} e^{-N_p} \cdot \sqrt{2\pi (N-N_p)} (N-N_p)^{N-N_p} e^{-(N-N_p)}} \cdot p^{N_p} q^{N_p}$$

$$\rightarrow W(\tilde{n}) = \frac{1}{\sqrt{2\pi N_p q}} \xrightarrow{\text{max of a Gaussian of } \sigma^2 = N_p q}$$

New

$$W(n) = W(\tilde{n}) \exp \left[\frac{1}{2} (n - \tilde{n})^2 \frac{d^2 \ln W}{dn^2} \Big|_{\tilde{n}} \right]$$

$$W(n) = \frac{1}{\sqrt{2\pi N_p q}} e^{-\frac{(n-N_p)^2}{2N_p q}} \xrightarrow{\text{Gaussian Normal}}$$

$$\Rightarrow W(n) = \frac{1}{\sqrt{2\pi \sigma^2}} e^{-\frac{(n-E(n))^2}{2\sigma^2}} \xrightarrow{\text{Random walk for large } N}$$

Example large N . A penny is tossed 400 times
Find the probability of exactly 215 heads

$$p = 1/2 \\ N = 400 \\ n = 215$$

$$W(215) = \frac{1}{\sqrt{2\pi 100}} \cdot \exp \left[-\frac{1}{2} \frac{(215-200)^2}{100} \right]$$

$$N_p = 200$$

$$= 1.3\% \rightarrow \text{very unlikely? ...}$$

More generally,

$$f(x)dx = \frac{1}{\sqrt{2\pi}\sigma} e^{-\frac{(x-\mu)^2}{2\sigma^2}} dx$$

→ probability density function - PDF

$$\int_a^b f(x)dx = P(a < x < b)$$

If probability dist. that depends on more than 1 var

$$P(u_i, v_i) = f(u_i) f(v_i) \rightarrow \text{a log or } u, v \text{ independent}$$

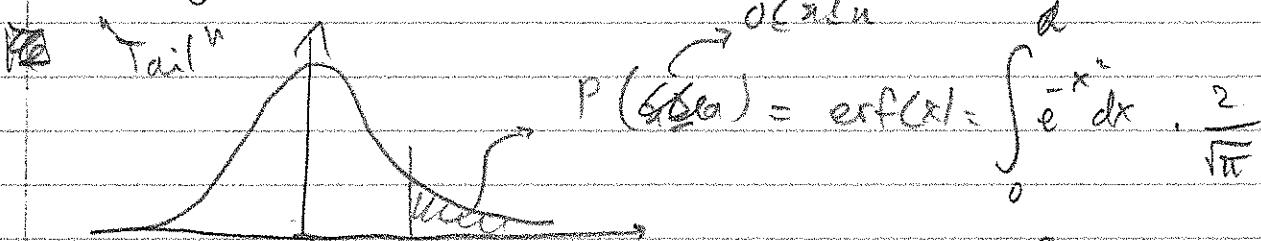
Gaussian integrals are difficult to evaluate
analytically

But there 2 cases when we can have precise answers

$$\int_{-\infty}^{\infty} e^{-x^2} dx = \sqrt{\pi}$$

But since it's symmetrical about $x=0$

$$\int_0^{\infty} e^{-x^2} dx = \int_{-\infty}^0 e^{-x^2} dx = \frac{\sqrt{\pi}}{2}$$



$$P(\text{tail}) = \text{erf}(x) = \int_0^x e^{-t^2} dt \cdot \frac{2}{\sqrt{\pi}}$$

$$\Phi(x \geq a) = \text{erf}(a) \cdot 1 - \Phi(a) = 1 - \int_a^{\infty} \phi(u) du$$

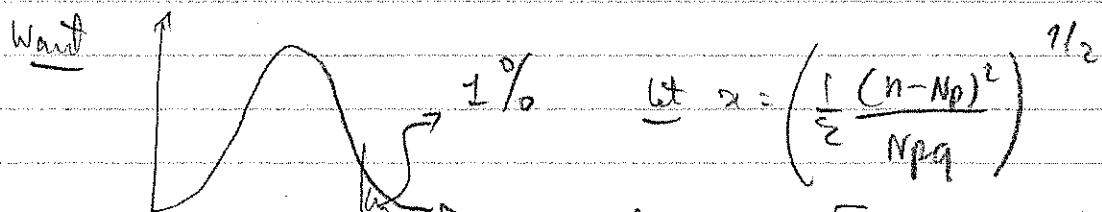
Ex Town A has 2000 customers and they want to talk to town B. What is the minimum # lines needed such that at most 1% of town A's customers fail to have access to a line during the busiest hour of the day?

↳ assume each caller is on the line for 2 mins in that hr randomly list.

$$N = 2000 \quad p = P(\text{line in use}) = \frac{2}{60} = \frac{1}{30}$$

$$n = ? \quad q = \frac{29}{30}$$

$$W(n) = \frac{1}{\sqrt{2\pi Npq}} \exp\left[-\frac{1}{2} \frac{(n-Np)^2}{Npq}\right]$$



$$\frac{dx}{dn} = \frac{d}{dn} \left[\frac{1}{\sqrt{2\pi Npq}} \frac{n-Np}{\sqrt{Npq}} \right]$$

Feb 22
2019

Back to Schroeder, Chap 2.

Terminology \rightarrow microstate \rightarrow any individual outcome

↳ state of each individual particle in the system (order matters). $S = 1$

Macrostate \rightarrow more general description of the system \uparrow
has some multiplicity. Some microstates are indistinguishable

→ multiplicity Ω → the number of microstates in a macrostate

Example

4 dice rolled → outcome 1 3 2 5

microstates

macrostate could be system where we roll two 1's in 4 dice

$$\text{multiplicity} \rightarrow \Omega = \binom{4}{2} = 6$$

Note that small multiplicity implies highly ordered system.

v.v large multiplicity implies disorder

Second Law of Thermodynamics

↳ Systems tend towards more disorder
because multiplicity is higher

Because these macrostates are more likely - (?)

Ω is related to entropy

Two physical systems where we can count individual microstate

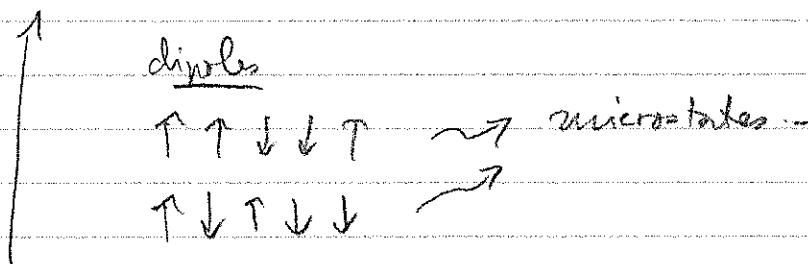
ex (1) Two-state paramagnet → material in a B field

Individual dipoles line up in 1 or 2 states: aligned or anti-aligned

microstate → specified by stating direction of all individual dipoles.

macrostate \rightarrow total # of dipoles that point up, N_p

$$\vec{B} \quad N = N_p + N_s$$



macrostate $S_d + S_p$

$\mu \rightarrow$ magnetic moment of individual dipole

only 2 allowed energy levels: $E_{\uparrow} - E_{\downarrow}$

Total magnetic dipole moment

$$\mu_B^{\uparrow} - \mu_B^{\downarrow} = \mu_B^{\uparrow} - \mu_B^{\downarrow} - \mu_B^{\uparrow} - \mu_B^{\downarrow} - \mu_B^{\uparrow} - \mu_B^{\downarrow}$$

$$\hookrightarrow \vec{m} = \vec{\mu}_i (N_p - N_s)$$

$$\text{or } \boxed{\vec{m} = \vec{\mu}_i (N_p - N_s + N_p) = \vec{\mu}_i (2N_p - N)}$$

energy of 1 dipole $= -\vec{\mu}_i \cdot \vec{B} = \epsilon_i \approx \pm \mu B$ for $\mu \parallel B$

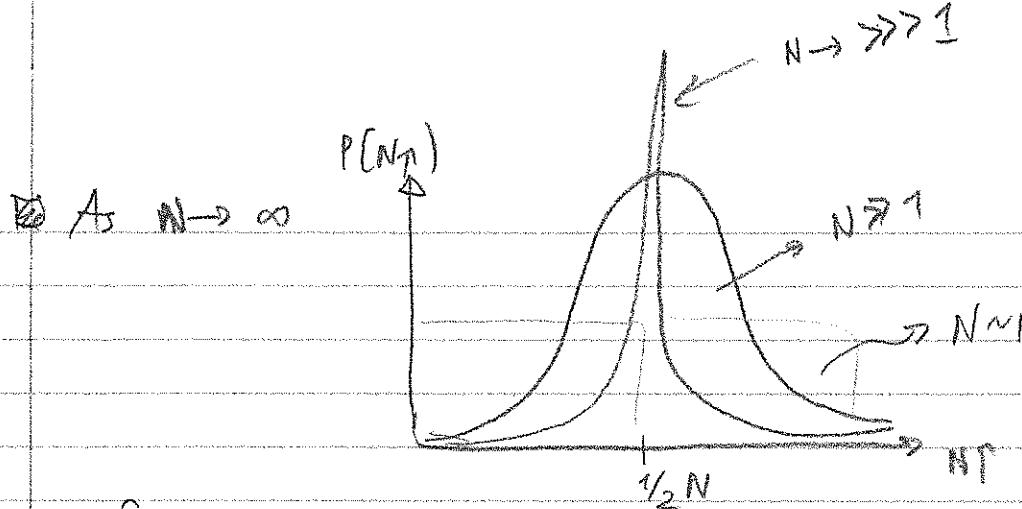
So energy of paramagnet \rightarrow

$$\boxed{U = -N \cdot \vec{\mu}_i \cdot \vec{B} = \mu B (N - N_p)}$$

$$\text{or } \boxed{U = \mu B (N - 2N_p)}$$

Calculate most probable energy $\rho = q = \frac{1}{2}$

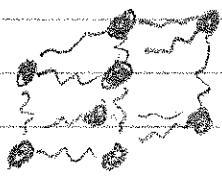
$$\boxed{P(N_p) = \binom{N}{N_p} p^{N_p} q^{N-N_p} = \frac{S(N)}{2^n}}$$



So, random orientation of dipoles is not possible
 \rightarrow 2nd law of thermodynamics.

thus $P \propto e^{-\frac{E}{kT}}$

(2) Einstein's model of solid / bed spring model



N atoms which have $3N$ independent harmonic oscillators, which provides 6 degrees of freedom each. (per atom)
 $(1KE + 1PE)$ per spring

Classical spring

$$U = \frac{1}{2}mv_x^2 + \frac{1}{2}mv_y^2 = KE + PE$$

$$= \frac{1}{2}m(x^2 + y^2 + z^2) + \frac{1}{2}k(x^2 + y^2 + z^2)$$

↳ here we have "unlimited energy spectrum", but as quantum oscillator \rightarrow discrete energies that are allowed

$$\epsilon_i = q_i \cdot hf = q_i \cdot \hbar \omega = q_i \cdot \hbar \nu$$

For $N = 3$ oscillators, the multiplicity of different energy levels

Osc	# 1	# 2	# 3	Σ	Ω
0	0	0	0	0	1
0	0	1	0	$h\nu$	3
1	0	0	0	$h\nu$	3
0	0	0	1	$h\nu$	3

# 1	# 2	# 3	Σv	
2	0	0	2	
0	2	0	2	6
0	0	2		
1	1	0		
1	0	1		
0	i	1		
			3hv	10
			Koker	

↳ General expression for multiplicity:

$S \neq \binom{N}{2}$ Instead

$$S(N, q) = \binom{q+N-1}{q} = \frac{(q+N-1)!}{q!(N-1)!}$$

units of
oscillators energy

Feb 25, 2019

Heat flow & Irreversible processes

Consider 2 Einstein worlds that can interact

Solid A

Solid B

single atom {

N_A = 3

No. 3

$$U = q(h)$$

$$\left\{ \begin{array}{l} q = \text{total \# of energy quanta} = 6 = q_A + q_B \\ 0 \leq q_A \leq 6, \quad 0 \leq q_B \leq 6 \end{array} \right.$$

Multiplicity

$$\Omega = \binom{q+N-1}{q}$$

$$\text{For A } \Omega_A = \binom{q_A + N_A - 1}{q_A}$$

Since A ~ B independent

$$\Omega_{tot} = \Omega_A \cdot \Omega_B$$

for B

$$\Omega_B = \binom{q_B + N_B - 1}{q_B}$$

B

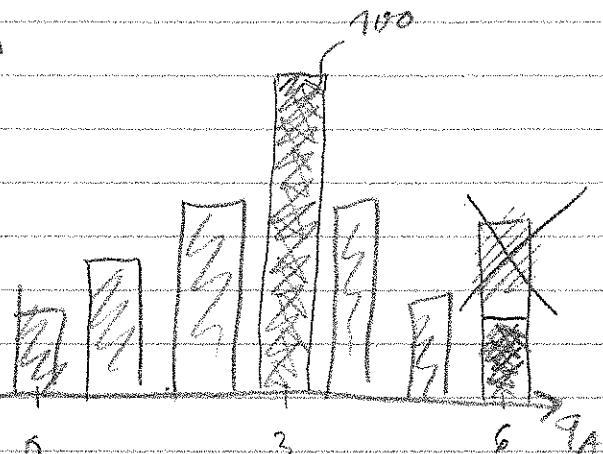
$$\Omega_{tot} = \Omega_A \cdot \Omega_B$$

$$\Omega_{tot}$$

Ex

$$\Omega_A(q_A=3) = \binom{3+3-1}{3} = 10$$

$$\Omega_B(q_B=3) = 10$$



$$\Omega_{tot} = \Omega_A \cdot \Omega_B = 100$$

$$(q_A=q_B=3)$$

B Ex $\Omega_A(q_A=6) = \binom{6+3-1}{6} = 28$

$$\Omega_B(q_B=0) = \binom{0+3-1}{0} = 1$$

$$\therefore \Omega_A \cdot \Omega_B = \Omega_{tot} = 28 \cdot 1 = 28$$

Fundamental assumption \rightarrow in stat mech

\hookrightarrow Any given microstate is equally probable. But some macrostates will be more probable than others because of higher multiplicity Ω

\blacksquare If you start out with a system near most likely macrostate

very unlikely that it will move far away from this distribution.

Ex $N_A = 50, N_B = 50, N_{tot} = 100$

$$\frac{\text{Case 1}}{\text{Case 2}} \quad q_A = 50, q_B = 0 \rightarrow S_{tot} = \binom{100-1}{50} / \binom{100-1}{50+50-1}$$

$$q_A = q_B = 25$$

$$\hookrightarrow S_{tot} = \binom{25+50-1}{25}^2 = 1 \times 10^{39} = \binom{99}{50} \binom{49}{0} \approx 5 \times 10^{22}$$

So $q_A = 25 = 1/3 \leftarrow$ macrostate 20 billion times more probable than $q_A = 50, q_B = 0,$

{Irreversible process}

↳ Energy flows from system A to system B, increasing the total S of the interacting systems.

Rustube 2nd Law of Thermos

↳ {systems in thermal equilibrium will be arranged with the highest amount of disorder}

(or)

↳ {spontaneous flow of energy stops when a system is at or very near its most likely microstate greatest S }

irreversible

III
not spontaneous

Large System

(s) \rightarrow Small # $\rightarrow (n < 100)$

(l) \rightarrow Large # \rightarrow Small # that we expectable 10^{-3}

(L) \rightarrow Very large # \rightarrow Large # that are expected or large # in factual ...

Ex $10^{10^{23}}$

Note some properties

$$(\text{Add}) \cdot 10^{23} + 23 \approx 10^{23}$$

$$(\text{mult.}) \cdot 10^{10^{23}} \times 10^{23} = 10^{10^{23} + 23} \approx 10^{10^{23}}$$

$$(\text{Divn}) \cdot \frac{10^{10^{23}} \times 10^{23}}{10^{10^{23}}} = 10^{23}$$

Manipulating large numbers

$$e^{10} \rightarrow \ln[e^{10^{23}}] = 10^{23}$$

$$\rightarrow e^{10} \approx 10^{4.34 \times 10^{22}}$$

$$e^{10^{23}} \text{ as } 10^x \rightarrow 10^{23} = x \ln 10 \rightarrow x = \frac{10^{23}}{\ln(10)} \approx 4.34 \times 10^{22}$$

Multiplicity of Einstein solid (large)

at high $T \Rightarrow q \gg N \approx N$ large

$$\Omega = \binom{q+N-1}{q} = \frac{(q+N-1)!}{q!(N-1)!} \approx \frac{(q+N)!}{q! N!}$$

Take the log

$$\ln \Omega = \ln \left[\frac{(q+N)!}{q! N!} \right] = \ln(q+N)! - \ln q! - \ln N!$$

The Stirling's formula: $N! \sim N^N e^{-N} \sqrt{2\pi N}$

$$\Rightarrow \ln(N!) \approx N \ln N - N$$

$$\text{So } \ln \Omega = (q+N) \ln(q+N) - (q+N) - [q \ln q - q] - [N \ln N - N]$$

→ next page

$$\underline{\text{So}} \quad \ln S = (q+N) \ln (N+q) - N \ln N - q \ln q$$

$$\underline{\text{Rewrite}} \quad \ln (q+N) = \ln \left(q \left(1 + \frac{N}{q} \right) \right) \rightarrow \ll$$

$$= \ln q + \ln \left(1 + \frac{N}{q} \right)$$

$$\approx \ln q + \frac{N}{q}$$

$$\underline{\text{So}} \quad \ln S \approx (q+N) \left[\ln q + \frac{N}{q} \right] - N \ln N - q \ln q \quad (q \gg N)$$

$$= N \ln q + \frac{N^2}{q} - N \ln N + N \quad \hookrightarrow \frac{N^2}{q} \approx 0$$

So

$$S = \exp [N \ln q - N \ln N + N]$$

$$= \frac{e^{N \ln q} e^N}{e^{N \ln N}} = \frac{e^{N \cdot q^N}}{N^N} = \left(\frac{eq}{N} \right)^N$$

$$\underline{\text{So}} \quad (q \gg N)$$

$$S = \left(\frac{eq}{N} \right)^N$$

or total multiplicity of loose Einstein solid or high temp limit, (like room temp)

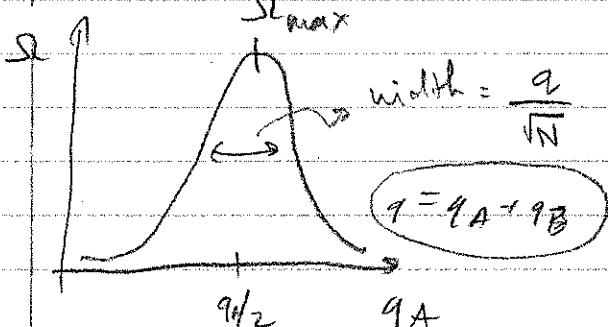
Feb 26, 2019

$$\rightarrow S_{\text{tot}} = S_A S_B$$

For interacting solids \rightarrow

$$S = S_{\max} e^{-N(2\pi/\lambda)^2}$$

or consider



$$\text{width} = \frac{q}{\sqrt{N}}$$

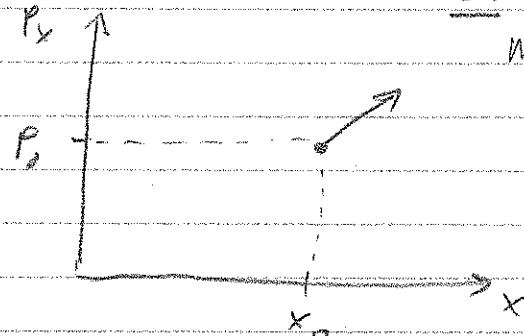
As $N \uparrow$, the fluctuations away from the most likely macrostate become increasingly improbable.
 \rightarrow Thermodynamic limit

Multiplicity of an ideal gas

* Specify the state of a system in classical mechanics using phase space.

If an object's position & momentum is known, we can predict it's position & momentum at any other time.

Ex



$$m\dot{x} = \vec{p} = \vec{v}$$

We can determine $x(t) \rightarrow p(t)$ from initial conditions.

$$m \frac{dx}{dt} = cx \rightarrow \int_{x_0}^{x_0} m dx = \int_{t_0}^t c dt$$

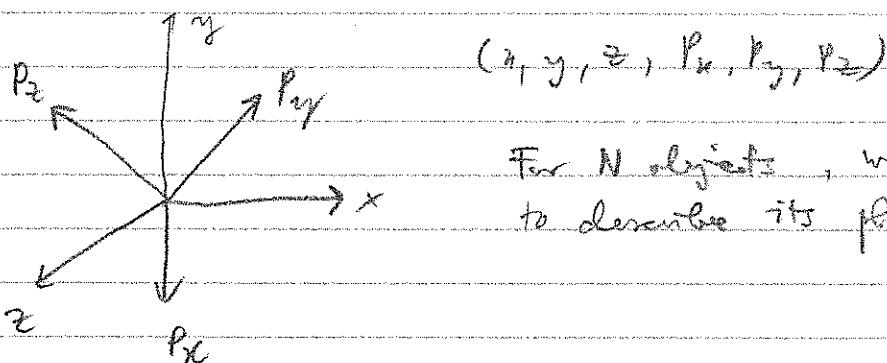
$$\text{So } \ln\left(\frac{x}{x_0}\right) = \frac{c(t-t_0)}{m}$$

$$\text{So } \boxed{x(t) = x_0 e^{\frac{c}{m}(t-t_0)}}$$

To get $p(t)$

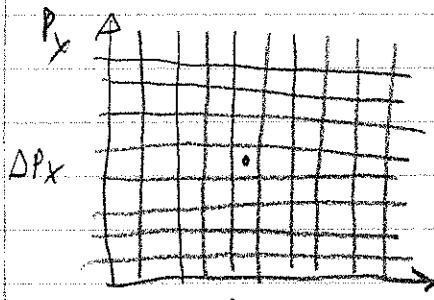
$$\rightarrow p = m\dot{x} = m \frac{c}{m} x_0 e^{\frac{c}{m}(t-t_0)} = c x_0 e^{\frac{c}{m}(t-t_0)}$$

For particle in space



For N objects, we need $6N$ coordinates to describe its phase space.

■ To describe state of system in phase space



Particle located between $x \sim x + \Delta x$
and $p_x \sim p_x + \Delta p_x$

■ Heisenberg Uncertainty principle

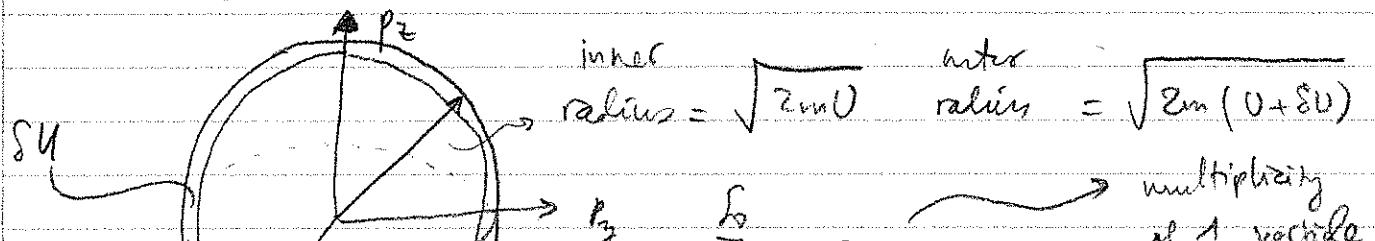
$$\rightarrow \text{let } \Delta x \Delta p = h \quad \Delta p \Delta x \geq \frac{\hbar}{2} (?)$$

■ For a monatomic ideal gas, energy is all kinetic

$$U = \frac{1}{2} m(v_x^2 + v_y^2 + v_z^2) = \frac{1}{2m}(p_x^2 + p_y^2 + p_z^2)$$

$$\therefore p = \sqrt{p_x^2 + p_y^2 + p_z^2} = \sqrt{2mU}$$

■ In 3-D momentum space



• And # states $\propto \frac{V}{\Delta p_x \Delta p_y \Delta p_z}$

$$\therefore S \propto \int_{u}^{u+\Delta u} \int_{p_x}^{p_x+\Delta p_x} \int_{p_y}^{p_y+\Delta p_y} \int_{p_z}^{p_z+\Delta p_z} dp_x dp_y dp_z$$

$$\rightarrow \text{For } N \text{ particles} \quad S \propto \int_{u_1}^{u_N} \int_{p_{x1}}^{p_{xN}} \int_{p_{y1}}^{p_{yN}} \int_{p_{z1}}^{p_{zN}} d^3r_1 \dots d^3r_N d^3p_1 \dots d^3p_N$$

Volume is independent, so

$$S(u) \propto V^N \int_{-u}^{u+\delta u} \cdots \int_{-p_1}^{p_1} d^3 p_1 \cdots d^3 p_N$$

$$\propto V^N \int_{-u}^{\sqrt{2m(V+\delta V)}} p^{3N-1} \cdot dp$$

\downarrow

thickness
"surfaces"

S: $S(u) \propto V^N (\sqrt{2mV})^{3N-1} \left[\sqrt{2m(V+\delta V)} - \sqrt{2mV} \right]$

$\underbrace{\hspace{10em}}$

= $V^N \sqrt{2mV} \left[\sqrt{2mV} \sqrt{1 + \frac{\delta V}{2m}} - \sqrt{2mV} \right]$

thickness

$$S(u) \propto V^N (\sqrt{2mV})^{3N} \left[\sqrt{1 + \frac{\delta V}{2m}} - 1 \right]$$

• Taylor expand $(1+x)^n \sim 1+nx$ ($x \ll 1$)

S: $S(u) \propto V^N (\sqrt{2mV})^{3N} \cdot \left(\frac{\delta V}{2m} \right)$

S: $S(u) \propto V^N u^{3N} \cdot \frac{\delta V}{2m}$

$$S(u) \propto V^N u^{3N/2} \cdot (\delta V) u^{-1}$$

small number

S: $S(u) \propto V^N u^{(3N/2)-1} \delta V$ ignore u^{-1} as well...

S:
$$\boxed{S(u) \propto V^N u^{3N/2}}$$

More careful derivation goes

→ multiplicity of monatomic ideal gas

$$S(u) \approx \frac{\pi}{N! h^{3N} (3N/2)!} V^N (\sqrt{2mV})^{3N}$$

$$S \sim u^{(3/2)N}$$

$\{ \text{For general result} \rightarrow \boxed{\Omega \sim u^{Nf/2}}, f = \# \text{ df for } \}$
 $\underline{\Omega}$ single particle

Feb 27, 1989

Result for monatomic ideal gas

$$\Omega(u, V, N) \approx \frac{\pi^{3N/2}}{N! h^{3N} (3N/2)!} v^N (\sqrt{2\mu u})^{3N}$$

Interacting ideal gas

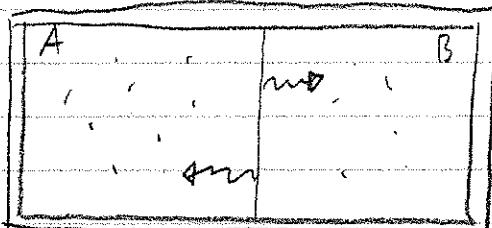
$\{ \text{assuming } \}$ \rightarrow
 $A \neq B$

$$\Omega_{\text{tot}} = \Omega_A \Omega_B$$

$$= [f(N)]^2 (V_A V_B)^N (u_A u_B)^{\frac{3N}{2}}$$

3 ways to exchange multiplicity

① Exchange energy



$$(\Omega \sim u^{3N/2})$$

Width of peak in the multiplicity function $\Omega_{\text{tot}} = \frac{u_{\text{tot}}^{Nf/2}}{\sqrt{BN/2}}$
and maximum u_{tot} is at
 $u_A = \frac{1}{2} u_{\text{tot}}$

② Exchange volumes via a movable partition

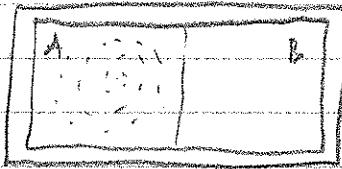
Width of peak in $\Omega = \frac{V_{\text{tot}}}{\sqrt{N}} \quad (\Omega \sim V^N)$

③ Enclose particles in permeable membrane (membrane)



\rightarrow more complicated overall
because of $f(N) \approx u(N)$

Consider specific case



here $V_{tot} \downarrow \times 2 \rightarrow$ this reduces ω_N by 2^n
 \star

ENTROPY

$$S = k \ln \Omega$$

where k is Boltzmann constant $= 1.38 \times 10^{-23}$ J/K
 n is the multiplicity

2nd Law of Thermodynamics: $\Delta S \geq 0$

Note For interacting systems $S_{tot} = S_A + S_B$

$$S_{tot} = k \ln \Omega_{tot} = k \ln (\Omega_A \Omega_B)$$

$$= k \ln \Omega_A + k \ln \Omega_B$$

$$= S_A + S_B$$

$$\boxed{S_{tot} = S_A + S_B}$$

④ Spontaneous processes occur due to a net increase in entropy

Entropy of an ideal gas

$$S = k \ln \Omega$$

$$= k \ln \left[\frac{\pi^{N/2}}{N! h^{3N} (3N/2)!} V^N (2\pi m)^{3N} \right]$$

Stirling's formula: $\ln N! \approx N \ln N - N$

$$\begin{aligned} S &= k \left[\frac{3N}{2} \ln \pi + N \ln V + \frac{3N}{2} \ln (2\pi m) - (N \ln N - N) \right. \\ &\quad \left. - 3N \ln h - \left(\frac{3N}{2} \ln \frac{3N}{2} - \frac{3N}{2} \right) \right] \\ &= Nk \left[\frac{3}{2} \ln \pi + \ln V + \frac{3}{2} \ln (2\pi m) - (\ln N - 1) \right. \\ &\quad \left. - 3 \ln h - \left(\frac{3}{2} \ln \frac{3N}{2} - \frac{3}{2} \right) \right] \end{aligned}$$

$$S = Nk \left\{ \ln \left[\frac{V}{N} \left(\frac{4\pi m V}{3N h^2} \right)^{3/2} \right] + \frac{5}{2} \right\}$$

→ entropy of ideal monatomic gas

↑
Sackur-Tetrode equation

300 K 10^5 Pa
J

Ex. Calc. S of 1 mole of He gas at room temp. 1 atm.

Need V, N, U, m_{He}

$$N \approx 10^{23}$$

$$V \approx \frac{RT}{P} \approx 25 \text{ L}$$

$$m_{He} =$$

$$U = \frac{3}{2} NkT = \frac{3}{2} \times 10^{23} \times 1000 \text{ J} = 3700 \text{ J}$$

Get

$$S_{He} \approx 126 \text{ J/K}$$

If we hold $N = V$ fixed and allow V to change

$$\rightarrow S \sim Nk \ln(V)$$

$$\Delta S = Nk \ln\left(\frac{V_f}{V_i}\right)$$

$$\delta \Delta S = Nk \frac{V_f}{V_i}$$

$\left. \begin{array}{l} \text{quasi-static iso-thermal} \\ \text{expansion/collapse} \end{array} \right\}$

Note if $\delta V > 0$, then $\Delta S > 0$

Mar 1, 2019

free entropy is related to the heat input to system \Rightarrow ?

Heat in = work done by system

= work done on system

$$\Delta U = 0 \quad (\text{isothermal}) \quad Q_{\text{add}} = W_{\text{sys}} = -W_{\text{ext}}$$

$$Q_{\text{add}} = -W_{\text{ext}} = \int_{V_i}^{V_f} P(V) dV$$

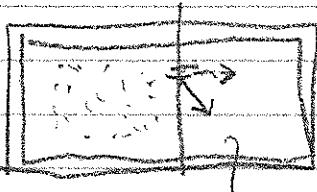
$$= \int_{V_i}^{V_f} \frac{NkT}{V} dV = NkT \ln\left(\frac{V_f}{V_i}\right) = T\Delta S$$

$$\delta \Delta S = \frac{\delta Q_{\text{add}}}{T} \Rightarrow \text{quasistatic isothermal}$$

more precisely

$$\delta S = \frac{\delta Q}{T}$$

Free expansion = no quasistatic



T, V, I constant $\rightarrow \delta V = 0 \Rightarrow \delta Q_{\text{add}} + W_{\text{ext}}$

$\delta Q_{\text{add}} = 0$ because no heat enters or leaves system. So $W = 0$.

But there's an increase in entropy. Neff can't use

$\Delta S = \partial T$ because the eq describes quasistatic isothermal

Entropy of mixing

Consider

He	Ar
1 1 1 1	0 0 0
1 1 1 1	0 0
1 1	0 0

$$\text{know } S_{\text{tot}} = S_A + S_B$$

He Ar

Now, remove partition & let gases mix. How does S change?

$$\text{Rearranging } S-T \text{ eqn: } S = Nk \left[\ln \left(\frac{V}{N} \left(\frac{4\pi m u}{3Nk^2} \right)^{3/2} \right) + \frac{5}{2} \right]$$

For He: N const, u const, $V' = 2V$

For Ar: same thing.

$$\Delta S = Nk \ln(2) \Big|_u + Nk \ln(2) \Big|_A$$

$$\boxed{\Delta S = 2Nk \ln(2)} \quad \text{or entropy of mixing (different gases)}$$

Consider (same gas)



Add $1/2$ to cylinder with same N , u as He
→ expect ST by a factor of 2

If we add He instead (at same energy) → same temperature

$$S = Nk \left\{ \frac{1}{2} \left(\frac{4\pi m u^{3/2}}{3Nk^2} \right)^{3/2} + \frac{5}{2} \right\}$$

$$V \text{ const } N' = 2N$$

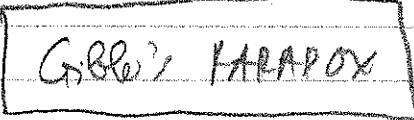
$$U = \frac{3}{2} kNT \rightarrow u = 2u$$

(49)

$$S' = 2S_{He} + 2Nk_B \ln\left(\frac{1}{2}\right)$$

$$= 2S_{He} + \underbrace{(-2Nk_B \ln(2))}_{}$$

$$\boxed{S' = 2S_{He} - \Delta S_{mixing}} \rightarrow \text{don't forget } S' \leq 2S$$

 Gibbs' PARADOX

→ why does distinguishability matter?

Ball

which have $S_N = \frac{1}{N!} \frac{V^N}{h^{3N}} \frac{\pi^{3N/2}}{(3N/2)!} (\sqrt{2\pi N})^{3N}$

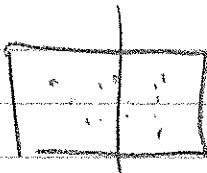
to distinguishable

$$\hookrightarrow \ln S_N \sim \ln\left(\frac{1}{N!}\right) \sim -(N \ln N - N)$$

What if we're able to distinguish particles in gas $\rightarrow N = \frac{1}{N!}$
because particles matter.

$$\boxed{S = Nk_B \ln \left[V \left(\frac{4\pi m}{3Nk_B} \right)^{3/2} + \frac{3}{2} \right]} \rightarrow \text{distinguishable}$$

Consider



container with indistinguishable particles. Add a particle,

$$N_1 \times 1, N_2 \times 2, N_3 \times 2$$

$$\frac{1}{2} S^{\text{new}} = \frac{1}{2} S_{\text{original}} + \frac{1}{2} Nk_B \ln(1/2)$$

$$\frac{1}{2} S^{\text{new}} = \frac{1}{2} S_{\text{original}} - \frac{1}{2} Nk_B \ln(2) \rightarrow \text{decrease in entropy}$$

(↓ set decrease in entropy)

Reversible vs Irreversible process

- A process is irreversible if $\Delta S > 0$ }
 ○ A process is reversible if $\Delta S = 0$ }

→ need to be quasistatic process.

(can be reversible, but don't have to be)

- ☒ All reversible processes are quasistatic - (but not all)
- ☒ quasistatic processes are reversible

[Reversible \subseteq Quasistatic]

☒ Spontaneous heat flow is always irreversible

$sP \neq sP$

☒ "Reversible heat flow"

System in $T_{max} \Rightarrow$ thermal equilibrium

$\overline{\Delta T} \rightarrow$ infinitesimal change in temperature.

$\frac{d}{dt}$

Mar 4, 2019

CHAPTER 3: RELATIONSHIP BETWEEN ENTROPY . TEMPERATURE

☒ Simple interacting system of 2 Einstein solids

$$N_A = 3 \text{ oscillators}$$

$$N_B = 2$$

$$q = 6$$

$$S = k \ln \Omega = \frac{(q+N-1)!}{q!(N-1)!}$$

$$\Omega = \left(\frac{q}{N} \right)^N$$

(J1)

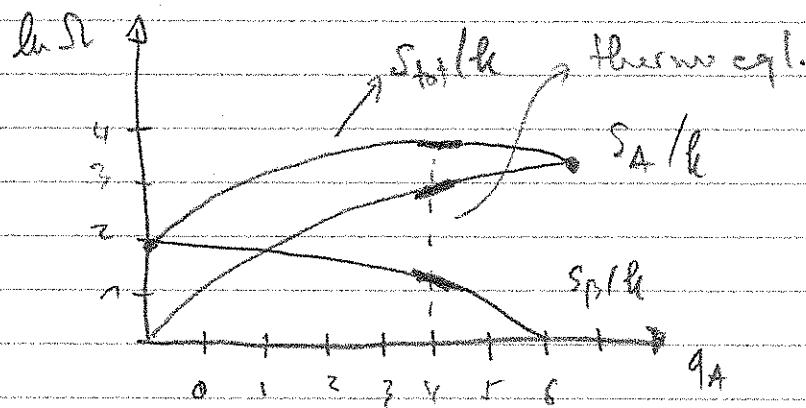
$$\underline{S} = \frac{S}{k} - \ln Z$$

$$N_A = 3$$

$$N_B = 2$$

	η_A	S_A	S_A/k	η_B	S_B	S_B/k	S_{tot}	S_{tot}/k
0	0	1	0	6	4	1.9	7	1.9
1	3	1.1	5	5	6	2.8	7.0	2.9
2	6	1.8	4	4	15	1.6	3.0	3.4
3	10	2.3	3	3	16	1.4	4.0	3.7
4	15	2.7	2	2	17	1.1	4.5	3.9
5	21	3.0	1	1	18	0.7	4.2	3.7
6	28	3.2	0	0	1	0	2.8	3.3

Plot of $\ln Z$ versus ϵ .



$\frac{\partial S_{tot}}{\partial q_A} = 0$, then we set maximum entropy

→ condition for thermodynamic equilibrium

Real $V_A = q_A$ (constant)

$$\underline{\ln} \frac{\partial S_{tot}}{\partial q_A} = 0 \Leftrightarrow \frac{\partial S_{tot}}{\partial q_A} = 0 \text{ at eq.}$$

$$\text{Now, } S_{tot} = S_A + S_B \Rightarrow \frac{\partial S_{tot}}{\partial q_A} = \frac{\partial S_A}{\partial q_A} + \frac{\partial S_B}{\partial q_A}$$

$$\underline{\ln} \frac{\partial S_A}{\partial q_A} = \frac{\partial S_A}{\partial q_A} + \frac{\partial S_B}{\partial q_A} = 0 \Leftrightarrow \left[\frac{\partial S_A}{\partial q_A} = -\frac{\partial S_B}{\partial q_A} \text{ at eq.} \right]$$

Note $U_{tot} = u_A + u_B$ - U_{tot} is conserved

$$\rightarrow \partial U_{tot} = 0 = \partial u_A + \partial u_B \rightarrow \partial u_A = -\partial u_B$$

In next

$$\boxed{\frac{\partial S_A}{\partial u_A} = \frac{\partial S_B}{\partial u_B}}$$

Note when g_A is small $\Rightarrow \frac{\partial S_A}{\partial u_A}$ steep. \rightarrow entropy of system A is increasing faster than $\frac{\partial S_A}{\partial u_A}$. Entropy of B is decreasing.

\rightarrow Spontaneous heat flow.
energy

Energy flows to object with steeper S vs U slope

The steeper the slope, the lower the temperature.

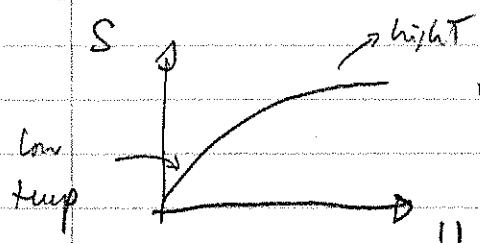
$$\begin{array}{l} \text{Units of } S \rightarrow J/K \\ \text{Units of } U \rightarrow J \end{array} \quad \left. \right\} T = \frac{\partial U}{\partial S} = \frac{\partial U}{\partial S}$$

Definition of temperature

$$\boxed{T = \frac{\partial S}{\partial U}} \rightarrow N, V \text{ constant}$$

-4

Patterns in S vs U graphs.



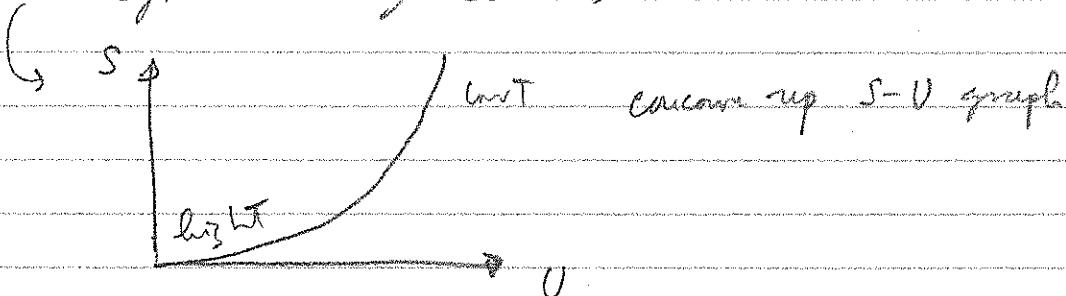
concave down \rightarrow In most systems, as U , T ↑ which means ... slope of $(\frac{\partial S}{\partial U})_{V,N}$ decreases

Result $\Delta U = Q_{\text{add}} + \sqrt{f_{\text{an}}}$ (assume V constant)

$$Q_{\text{add}} = CST$$

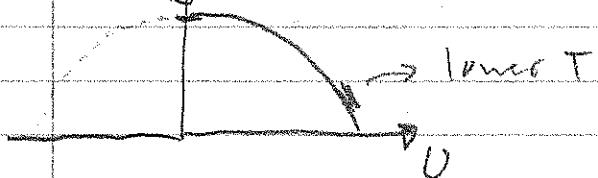
$\therefore \Delta U = CST \rightarrow$ makes sense

- However, there are systems with negative heat capacity (gravitationally bound)



- Ex: Concave down with negative slope ...

$$S \rightarrow 0 \rightarrow T = -\infty$$



Ex: Paramagnet: $U = \mu B (N_f - N_i)$

$$\left(\frac{\partial S}{\partial U}\right)_{N,V} = \text{negative} \rightarrow \boxed{\text{negative temperature}}$$

- Example Relationship between S, U, T

- ① ^{large} Entropy of solid at high temp limit $\rightarrow q \gg N \gg 1$

$$S = \left(\frac{q}{N}\right)^N$$

$\therefore S = k \ln S = Nk \ln \left(\frac{q}{N}\right) = Nk + Nk \ln \left(\frac{q}{N}\right)$

$$\text{def } U = E \cdot g$$

$$\text{So } S = Nk \left[\ln \left(\frac{u}{N\epsilon} \right) + 1 \right]$$

$$= Nk \ln \left(\frac{u}{N\epsilon} \right) + Nk$$

$$= Nk \ln u - Nk \ln (EN) + Nk$$

$$\rightarrow \frac{\perp}{T} = \left(\frac{\partial S}{\partial u} \right)_{N,V} = \frac{Nk}{u} = 0 + 0$$

$$\text{So } T = \frac{u}{Nk}$$

$$\text{Recall } u = \frac{1}{2} NkT$$

or

$$u = NkT$$

\Rightarrow 2 brane SHO has 2 d.o.f.

(2) Ideal gas (monatomic)

$$S = Nk \left(\ln \left[\frac{v}{N} \left(\frac{4\pi m u}{3Nk^2} \right)^{3/2} \right] + \frac{5}{2} \right) \xrightarrow{\text{constant kills by } \ln(\cdot)}$$

$$T = \left(\frac{\partial S}{\partial u} \right)_{N,V}^{-1} = \left[Nk \cdot \frac{v}{N} \left(\frac{4\pi m}{3Nk^2} \right)^{3/2} \cdot \frac{1}{u} \right]^{-1}$$

$$T = \left(\frac{7}{2} Nk \frac{1}{u} \right)^{-1} \rightarrow \boxed{u = \frac{1}{2} NkT}$$

Entropy = that Capacity

Mon 5, 2019

$$\text{Recall: } C_v = \left(\frac{\partial U}{\partial T}\right)_{V,N}$$

$$\begin{aligned} \text{1st law } \Delta U &= Q_{\text{add}} + W_m \\ \text{if } V \text{ constant} \rightarrow W_m &= 0 \end{aligned} \quad \Rightarrow \Delta U = Q_{\text{add}}$$

$$\begin{aligned} \text{Now } T &= \left(\frac{\partial S}{\partial U}\right)^{-1} \Rightarrow dS = \frac{dU}{T} \text{ with constant volume} \\ &= \frac{Q}{T} \quad \boxed{dS = \frac{dQ}{T}} \end{aligned}$$

$$\text{But recall } dQ = C_v dT$$

$$\int dS = \int \frac{C_v dT}{T} \rightarrow \int dS = \int C_v \frac{dT}{T} / \begin{array}{l} \text{if temp range} \\ \rightarrow C_v \end{array} \quad \Rightarrow \boxed{\Delta S = C_v \ln\left(\frac{T_f}{T_i}\right)} \quad \underline{\text{constant}}$$

Examp 6 Heat a cup of H₂O from 20°C to 100°C. Calculate (200g) how much entropy increases? $C_v = 1 \text{ cal/gK} = 4.186 \text{ J/gK}$

$$\Delta S = 4.186 \frac{\text{J}}{\text{gK}} (200\text{g}) \ln\left(\frac{373}{293}\right)$$

$$\approx 200 \text{ J/K}$$

$$\begin{aligned} \text{In terms of } \frac{S_2}{S_1} \rightarrow \Delta S &= k \ln \frac{S_2}{S_1} \rightarrow S_2 = e^{\frac{\Delta S}{k}} S_1 \\ \rightarrow S_2 &= e^{20051 \text{ J}/(1.38 \times 10^{-23} \text{ J/K})} S_1 \end{aligned}$$

$$\boxed{S_2 = e^{1.5 \times 10^{25}} S_1}$$

Q3 Total entropy of the system

$$\Delta S = S_f - S_{(T=0)} = \int_0^T \frac{C_v}{T} dT$$

But we need C_v at $T=0$. Guess that $S(0) \rightarrow 0$

Third Law of Thermodynamics

↳ Planck's Formalism: At $T \rightarrow 0$, entropy goes to its minimum value

↳ Note this is only true for crystalline solids

Another way to state 3rd law [At $T \rightarrow 0$, $C_v \rightarrow 0$]

Ex ideal gas $C_v = \frac{3}{2}Nk \rightarrow 0 \text{ as } T \rightarrow 0$

Q4 Microscopic view of entropy $\Rightarrow dS = \frac{dQ}{T}$

* Example The sun heating the surface of the Earth
 $\sim 1000 \text{ W/m}^2$, $T_0 = 6000 \text{ K}$
 $T_\oplus = 300 \text{ K}$

Estimating energy created in 1 year by the flow of heat to the Earth's surface.

$$\Delta S_\oplus = \frac{Q}{T} = \frac{(-1000 \text{ J/s})(60^2)(24)(365)}{6000 \text{ K}, 1 \text{ m}^2}$$

$$= -1.75 \times 10^6 \text{ J/K}$$

$$\Delta S_\oplus = \frac{Q}{T} = \frac{(-1000 \text{ J/s})(60^2)(124)(765)}{200 \text{ K}, 1 \text{ m}^2}$$

$$= +3.5 \times 10^7 \text{ J/K}$$

(5)

$$\Delta S_{tot} = \Delta S_0 + \Delta S_{\oplus} = 7.3 \times 10^7 \text{ J/Km}^2$$

B Suppose we plant grass on this 1 m^2 area. Does the decrease in entropy violate the 2nd law?

On $1 \text{ m}^2 \rightarrow$ maybe 1 kg of grass. Let's say grass = C
 $n = 12 \text{ g/mol}$
 Say 1200 g of grass

$$\rightarrow N = 1000 N_A \text{ C atoms/m}^2$$

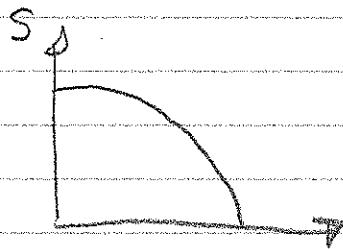
To assemble grass out of smaller molecules.

$$S \sim Nk \sim nk^2 = 1000R = 700, 8.31 \text{ J/molK}$$

$$\rightarrow S \approx 10^4 \text{ J/K} < \Delta S_0$$

* Paramagnetism 1) S 2) S 3) T 4) $U(T)$ 5) C_v

Recall



For paramagnets

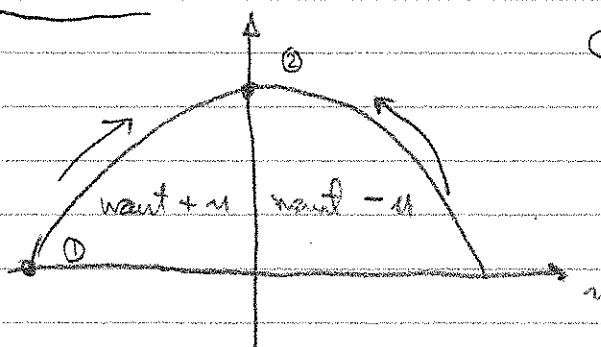
$$U = \mu B(N_f - N_p) \\ = \mu B(2N_f - N)$$

Question how do U, M
depend on temperature

$$M = \mu (N_f - N_p) = \frac{-U}{B}$$

(2)

(1) Get S



- ① all N are $N_f \rightarrow$ low T ,
 $S \propto U \rightarrow$ steep positive
- wants to absorb n

- ③ $U_f = NT = \frac{1}{2} N \cdot \text{Max entropy}$
 $n=0$. If it absorbs n
 $\rightarrow S \propto U$ has (-) slope

Tang of paramagnet ① $u = \text{negative}$ but $\frac{\partial U}{\partial T} = \text{positive}$

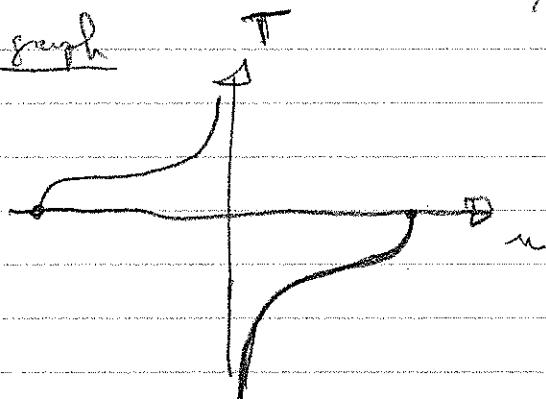
$$T \uparrow \text{as } u \uparrow$$

② $u = \text{positive}$ but $\frac{\partial U}{\partial T} = \text{negative}$

$$T \downarrow \text{as } u \uparrow$$

\rightarrow system wants to give off energy

Tang graph

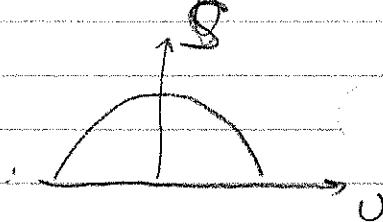


$$\text{Recall } \left(\frac{\partial U}{\partial T}\right)_{N,V} = \frac{1}{T}$$

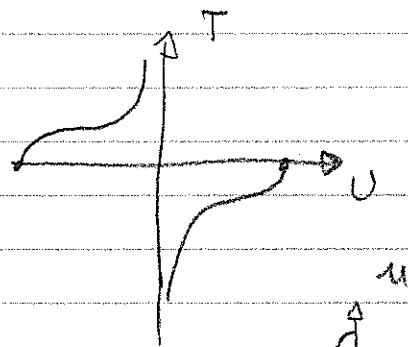
S

Mar 6, 2019

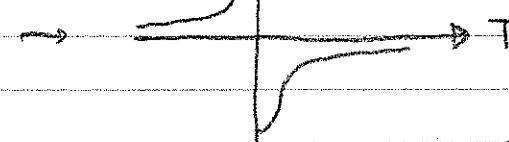
Recall paramagnet has a "normal" S-V graph:



so $T \text{ vs } U$ looks like



Flip the axes



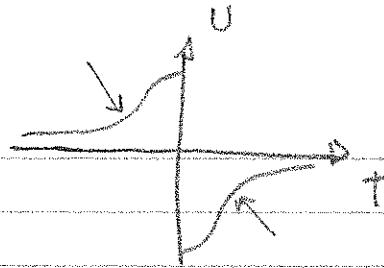
Recall

$$C_V = \left(\frac{\partial U}{\partial T}\right)_{N,V}$$

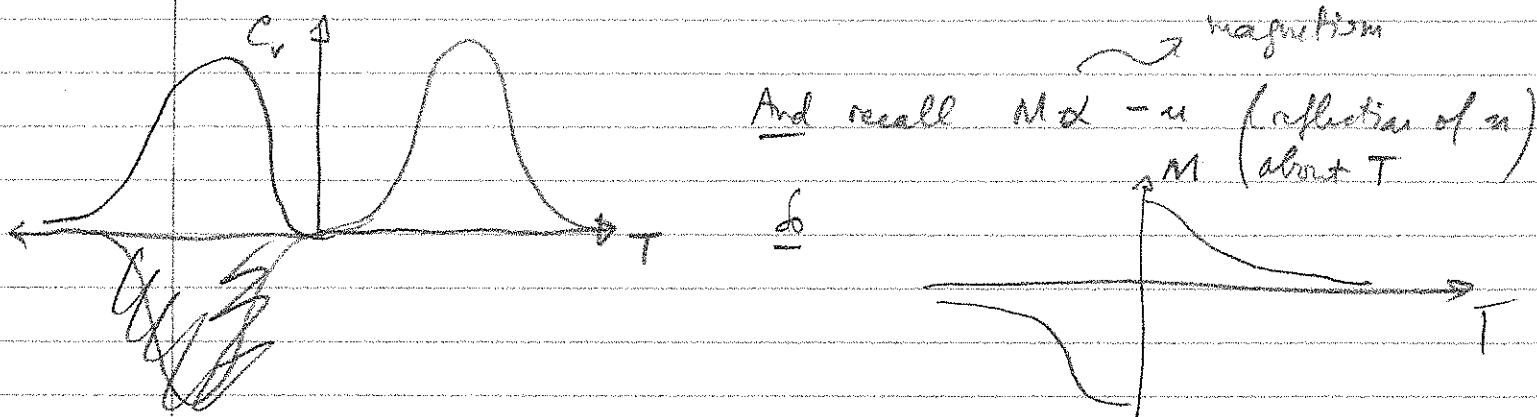
$$\rightarrow \text{or } \left\{ C_V = \left(\frac{\partial U}{\partial T}\right)_{N,V} = 0 \text{ when } T=0 \right.$$

$$\left. C_V = 0 \text{ when } T = \pm \infty \right.$$

Q) There's also an inflection point



• Consider (positive) temperatures only



Analytic solution to paramagnet

$$\text{Recall: } S = \frac{N!}{N^N} \approx \frac{N^N}{N^N N!} = \frac{N!}{N_+! (N-N_+)!} \quad \text{assume } N \gg 1$$

$$S = k \ln \Omega = k \ln (N!) - \ln (N_+!) - \ln (N-N_+!)$$

Stirling's approx $\ln N! \sim N \ln N - N$

$$\begin{aligned} \text{So } \frac{S}{k} &= (N \ln N - N) + (N_+ \ln N_+ - N_+) + (\omega_{N_+}) \ln (N - N_+) \\ &\quad + (\alpha_{N_+} - \alpha_N) \\ &= N \ln N - N_+ \ln N_+ - (\alpha - \alpha_N) \ln (N - N_+) \end{aligned}$$

$$\frac{\partial S}{\partial u} = \frac{(2S)}{\partial u}_{N, B} \quad \text{and } u = \mu B (N - N_+)$$

$$\text{So } \left(\frac{\partial S}{\partial u} \right) = \left(\frac{\partial S}{\partial N_+} \right) \left(\frac{\partial N_+}{\partial u} \right) = (-2\mu B) \left(\frac{\partial S}{\partial N_+} \right) = \frac{-1}{2\mu B} \left(\frac{\partial S}{\partial N_+} \right)$$

$$\left(\frac{\partial S}{\partial N_+} \right) = k \left[-\ln N_+ - 1 + \ln (N - N_+) + \frac{N - N_+}{N - N_+} \right]$$

$$N_p = \frac{1}{2} \left(N - \frac{u}{\mu B} \right)$$

(60)

$$\text{So } \left(\frac{\partial S}{\partial N_p} \right) = k \left[-\ln \left(\frac{1}{2} \left(N - \frac{u}{\mu B} \right) \right) + \ln \left(N - \frac{1}{2} N + \frac{u}{2\mu B} \right) \right]$$

= ...

$$\boxed{\frac{\partial S}{\partial N_p} = k \ln \left(\frac{N + u/\mu B}{N - u/\mu B} \right)}$$

$$\text{So } \left(\frac{\partial S}{\partial u} \right) = \frac{\partial S}{\partial N_p} \frac{\partial N_p}{\partial u} = \left(\frac{k \ln \left(\frac{N + u/\mu B}{N - u/\mu B} \right)}{-2\mu B} \right) = \frac{1}{T}$$

$$\text{So } \boxed{\frac{1}{T} = \frac{k}{2\mu B} \ln \left(\frac{N - u/\mu B}{N + u/\mu B} \right)} \quad T(u)$$

So we can solve for $u(T)$

$$\frac{2\mu B}{kT} = \ln \left(\frac{N - u/\mu B}{N + u/\mu B} \right)$$

$$e^{\frac{2\mu B}{kT}} = \frac{N - u/\mu B}{N + u/\mu B} = \frac{1 - u/N_{\mu B}}{1 + u/N_{\mu B}}$$

$$\text{So } e^{\frac{2\mu B}{kT}} + \frac{u}{N_{\mu B}} e^{\frac{2\mu B}{kT}} = 1 - \frac{u}{N_{\mu B}}$$

$$\text{So } \frac{u}{N_{\mu B}} \left(e^{\frac{2\mu B}{kT}} + 1 \right) = 1 - e^{\frac{2\mu B}{kT}}$$

$$\text{So } u(T) = N_{\mu B} \frac{1 - e^{\frac{2\mu B}{kT}}}{1 + e^{\frac{2\mu B}{kT}}}$$

$$\text{Now, simplify } \rightarrow \underline{\underline{\sinh(x)}} \quad \sinh(x) = \frac{1}{2} (e^x - e^{-x}), \cosh(x) = \frac{1}{2} (e^x + e^{-x})$$

(61)

$$\text{So } \tanh x = \frac{e^x - e^{-x}}{e^x + e^{-x}} = \frac{-(1 - e^{-2x})}{1 + e^{-2x}}$$

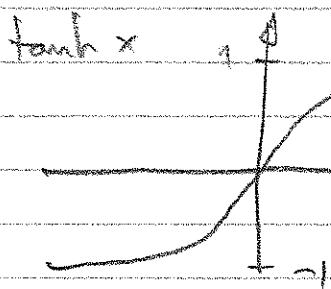
$$\text{So } -\tanh x = \frac{1 - e^{2x}}{1 + e^{-2x}}$$

Let $x = \left(\frac{\mu B}{kT}\right)$, then

$$u(T) = -\mu B N \tanh\left(\frac{\mu B}{kT}\right)$$

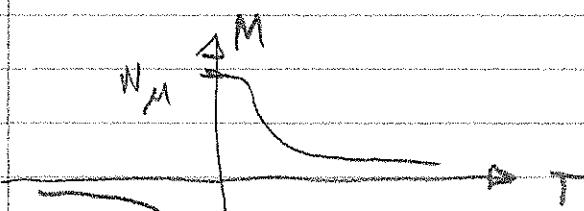
with $M = -\frac{\mu}{B}$

$$M(T) = +N\mu \tanh\left(\frac{\mu B}{kT}\right)$$



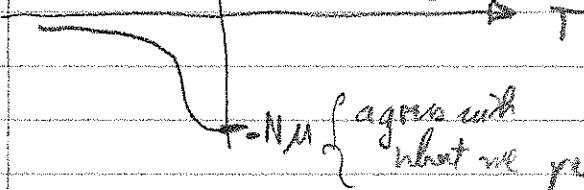
as $x \rightarrow 0$, $\tanh x \rightarrow 0$

$\Rightarrow x = \frac{\mu B}{kT}, T \rightarrow \pm \infty \rightarrow M, u \rightarrow 0$



$\Rightarrow x \rightarrow \infty, \rightarrow T \rightarrow 0$

$\tanh x \approx 1 \rightarrow M = N\mu$



$\Rightarrow x \rightarrow -\infty, T \rightarrow 0$

$\tanh x \approx -1 \rightarrow M = -N\mu$
which we predicted...

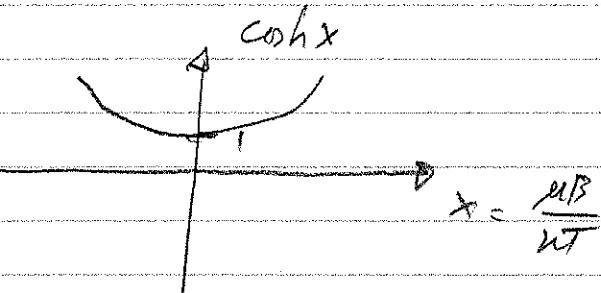
What about heat capacity of paramagnet?

$$C_B = \left(\frac{\partial U}{\partial T}\right)_{N,B} \quad \text{Now, } u = -N\mu B \tanh\left(\frac{\mu B}{kT}\right)$$

$$\text{Recall } \frac{d}{dx} \tanh(x) = \operatorname{sech}^2(x) \cdot \frac{du}{dx} = \frac{1}{\cosh^2(u)} \frac{du}{dx}$$

$$\left(\frac{\partial V}{\partial T}\right)_{N,B} = -N_\text{A}B \tanh^2\left(\frac{\mu B}{kT}\right) \left(\frac{-\mu B}{kT^2}\right) = C_B$$

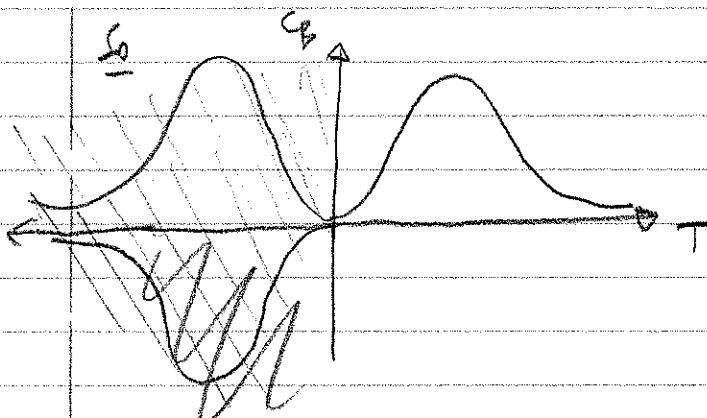
So $C_B = \frac{N_A \left(\frac{\mu B}{kT}\right)^2}{\cosh^2\left(\frac{\mu B}{kT}\right)}$



① as $x \rightarrow 0$, $T \rightarrow \pm \infty$ $\cosh(x) \rightarrow 1$
 $\rightarrow [C_B \rightarrow 0 \text{ as } T \rightarrow \pm \infty]$

② as $x \rightarrow \infty$, $T \rightarrow 0_+$, $\cosh(x) \rightarrow +\infty$ (Faster)

So $C_B \rightarrow 0 \text{ as } T \rightarrow 0$



Ex Consider two-state paramagnet.

$$\text{let } \mu = \mu_B \text{ Bohr magneton } \mu_B = \frac{e\hbar}{4\pi m_e} = \frac{e\hbar}{2m_e}$$

$$\text{Let } B = 1 \text{ T}$$

$$\begin{aligned} &\approx 5.788 \text{ eV/T} \\ &\approx 9.234 \times 10^{-21} \text{ J/T} \end{aligned}$$

then $M = ?$ $\mu B = 5.8 \times 10^{-5} \text{ eV}$
 $kT = \frac{1}{40} \text{ eV}$ $\Rightarrow \frac{\mu B}{kT} \ll 1$

Now $\tanh(x) \approx x$ for small x

∴ $M \approx (N_A) \left(\frac{\mu B}{kT}\right) = \frac{N \mu^2 B}{kT}$ → true in "high-temperature" limit.

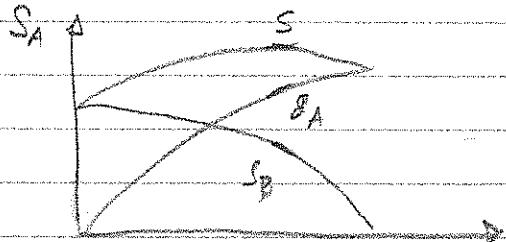
$M \propto \frac{1}{T}$ \rightarrow Curie's Law (Pierre Curie)
 (high temp limit)

$C_B \propto \frac{1}{T^2}$ \rightarrow (high temp limit)

Mar 9, 2019

MECHANICAL EQUILIBRIUM

we're been discussing dU and dS



S_A get

at thermal eq $\frac{\delta S_{tot}}{\delta V} = 0 \rightarrow \boxed{\frac{\delta S_A}{\delta V} = \frac{\delta S_B}{\delta V}}$

constant V

Consider some interacting system that can exchange volume as well as energy



\rightarrow change in V governed by change in P

\rightarrow change in V governed by change in T

or $VT, \sigma T, ST$

$VT, \sigma T, ST$

} Goal develop a relationship between $\frac{\delta S}{\delta V}$ and P

Just like dS_{tot}/dV gives thermal equilibrium

6 $\boxed{\frac{\delta S_{tot}}{\delta V} = 0} \rightarrow$ mechanical equilibrium

$$\text{S} \quad \frac{\partial S_{\text{tot}}}{\partial V_A} = 0 \Rightarrow \boxed{\frac{\partial S_A}{\partial V_A} = \frac{\partial S_B}{\partial V_B}} \quad \left. \begin{array}{l} \\ \downarrow \quad \uparrow \\ \frac{\partial S_A + \partial S_B}{\partial V_A} = 0, \text{ but } \partial V_A = -\partial V_B \end{array} \right\} \text{volume is conserved}$$

med-equl.

What are these held constant?

$$\left(\frac{\partial S_A}{\partial V_A} \right)_{V_B, N_B} = \left(\frac{\partial S_B}{\partial V_B} \right)_{V_A, N_A}$$

Dimensional analysis.

$$[S] \in \frac{J/K}{m^3} = \frac{N \cdot m/K}{m^3} = \frac{N}{m^2 \cdot K} = \frac{[P]}{[T]}$$

Gas

$$\left(\frac{\partial S}{\partial V} \right)_{O, N} = \frac{P}{T}$$

Look at ideal monatomic gas... $n = f(N) V^N u^{3N/2}$

$$S = k \ln \Omega = k \left[\ln f(N) + \ln V^N + \ln u^{3N/2} \right]$$

$$= k \left[\ln f(N) + N \ln V + \frac{3N}{2} \ln u \right]$$

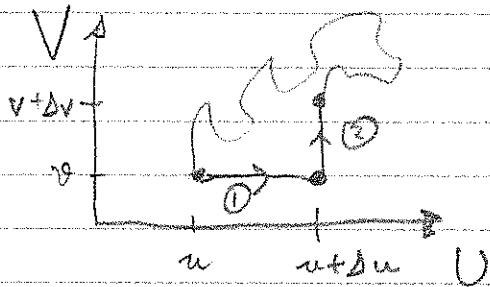
if $P \stackrel{?}{=} T \left(\frac{\partial S}{\partial V} \right)_{O, N}$, then

$$T \stackrel{?}{=} k \cdot N \cdot \frac{1}{V}$$

$$\Rightarrow P \stackrel{?}{=} \frac{NkT}{V} \quad \text{works...}$$

$$\boxed{PV = NkT} \quad \checkmark$$

We'd like to combine both of these relations for thermal and mechanical equilibria.



Entropy is an exact differential

→ path independent

$$\Delta S_{\text{tot}} = \Delta S_1 + \Delta S_2$$

① Isochoric process → volume constant

② Isothermal process → temp. constant or energy

$$\boxed{\Delta S_{\text{tot}} = \left(\frac{\partial S}{\partial u}\right)_{\text{tot}} du + \left(\frac{\partial S}{\partial v}\right)_{\text{tot}} dv}$$

$$\underline{s}(u, v, N) \\ \begin{matrix} T & T & T \\ \text{vol} & \# \text{part.} \end{matrix}$$

$$\Delta S_{\text{tot}} = \left(\frac{\partial S}{\partial u}\right)_{v,N} du + \left(\frac{\partial S}{\partial v}\right)_{u,N} dv$$

$$= \frac{1}{T} du + \frac{P}{T} dv$$

So

$$\boxed{dU = TdS - PdV} \rightarrow \text{thermo dynamic identity}$$

Case by case as N is constant.

Note This is just the first law of thermo.

$$dU = dW_{\text{int}} + dQ$$

For quasi-static processes $\rightarrow W_{\text{int}} = -PdV$

For quasi-static isothermal process $\rightarrow \cancel{dW_{\text{int}}} \Delta S = \frac{\partial Q}{T} \rightarrow dQ = TdS$

d $Q = TdS$ → for any quasi-static process.
Not just iso-thermal

$$dU = TdS - PdV \leftarrow \text{more fundamental}$$

Q Now, if $u = u(s, v)$ and dU exact, then

$$\frac{\partial^2 u}{\partial V \partial S} = \frac{\partial^2 u}{\partial S \partial V} \quad \text{order of diff. doesn't matter.}$$

Then $du = \left(\frac{\partial U}{\partial S}\right) dS + \left(\frac{\partial U}{\partial V}\right) dV$

$$du = TdS - PdV$$

Then $\left(\frac{\partial}{\partial V}\right)_S \left(\frac{\partial u}{\partial S}\right)_V = \left(\frac{\partial}{\partial S}\right)_V \left(\frac{\partial U}{\partial V}\right)_S$

\cancel{T} $\cancel{-P}$

S $\left(\frac{\partial}{\partial V}\right)_S T = -\left(\frac{\partial}{\partial S}\right)_V P \quad \leftarrow \text{maxwell's relation}$

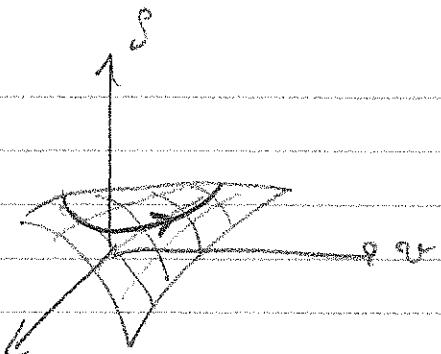
Q Constant entropy process?

If we have quasi-static process & adiabatic process (no heat transfer)
(P equilibrates)

→ no change in Entropy

$$Q = TdS = 0 \quad \leftarrow \text{Isentropic} \quad \left\{ \begin{array}{l} \text{quasi-static} \\ \text{adiabatic} \end{array} \right.$$

(67)



$$dV = TdS - PdV$$

$$TdS = 0 \Rightarrow dV + PdV$$

$$dS_{tot} = 0 \text{ but } \frac{\partial S}{\partial V} \neq 0 \neq \frac{\partial S}{\partial P}$$

\square Recall $C_v = \left(\frac{\partial U}{\partial T}\right)_{V,N}$

$$\delta = C_v dT = TdS$$

$\therefore \delta S = \int \frac{C_v}{T} dT$ But we want to work at constant pressure processes

$$(\delta S)_P = \int \frac{C_p}{T} dT \rightarrow \text{more useful in many cases...}$$

\square Example 1L of air ($N_2 + O_2$) at 1 atm. heat air until it doubles in volume - What is δS ?

Diatomeric gas $C_v = \frac{f}{2} Nk$

$$C_p = C_v + Nk$$

For diatomic gas at room temp. $f=5$

$$\therefore C_p = \frac{7}{2} Nk$$

$$\text{Ideal gas law} \rightarrow PV = NkT \rightarrow Nk = \frac{PV}{T} = \frac{(10^5 \text{ Pa})(1 \times 10^{-3} \text{ m}^3)}{100 \text{ K}} = \frac{1}{3} \text{ J/K}$$

$$N = NkT$$

$$\therefore T^2 = 2T$$

$$\text{So } (\Delta S)_p = \int \frac{C_p}{T} dT = C_p \ln \frac{T_f}{T_i} = C_p \ln(2)$$

$$\text{So } (\Delta S)_p = C_p \ln(2) = \left(\frac{7}{2} Nk\right) \ln(2) = 0.81 \text{ J/K}$$

Another way to do this

$$\rightarrow dU = TdS - PdV$$

$$\sum kN dT = TdS - \frac{Nh}{V} dV$$

~~$\sum kN dT = \int dS - \sum N dh$~~

$$\sum kN \frac{dT}{T} = dS - \frac{Nh}{V} dV$$

So

$$\Delta S = \sum \frac{kN \ln \frac{T_f}{T_i}}{T} + Nh \ln \left(\frac{V_f}{V_i} \right)$$

$$(\Delta S)_p = \frac{7}{2} Nk \ln(2)$$

Nov 21, 2019

Recall $dU = TdS - PdV$ can be used for non-quasi-static processes

① Fast compression

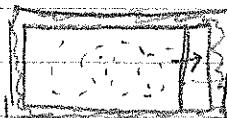
$dV \approx 0$. We have done work but work is greater than $-PdV$



$$dU = TdS - PdV = Q + W$$

$$\text{So } Q < TdS \rightarrow \left| \frac{dS}{T} \right| > \left| \frac{dV}{V} \right| \rightarrow \text{added entropy}$$

② Free-expansion



\rightarrow vacuum \rightarrow allows gas expand into vacuum

$$W = 0, \Delta Q = 0 \xrightarrow{\text{unif. static}} \Delta U = 0$$

But $dU = TdS - PdV = 0 \Rightarrow TdS - PdV \geq 0$ ($W \neq PdV$)

↳ we added entropy

Example Fast compression of air at $P = 1 \text{ atm}$, $T = 300 \text{ K}$
 $= 10^5 \text{ Pa}$



$$F = 2000 \text{ N}$$

$$A = 0.01 \text{ m}^2 \quad V = 1 \text{ L}$$

$$n = \frac{1}{25} \text{ mole}$$

Say piston moves 1 mm before it stops.

If this is quasi-static $W = \int PdV = \int \frac{nRT}{V} dV = nRT \ln \frac{V_f}{V_i}$

$$W = nR \ln \frac{V_f}{V_i}$$

$$V_i = \frac{1.00 \text{ L}}{1000}, \quad V_f = \frac{1.00 - (0.001)(0.01)}{1000}$$

Work actually done

$$W = Fd = (2000 \text{ N}) (0.001 \text{ m}) = 2 \text{ J}$$

$$\geq -PdV$$

Fast compression Adiabatic $\rightarrow \Delta Q = 0$

$$\rightarrow \Delta U = Q + W = 0 + W = 2 \text{ J}$$

How does S change?

$$\Delta S = TdS = \frac{dU + PdV}{T}$$

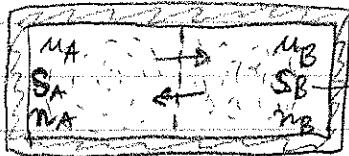
$$\Delta S = \frac{2 \text{ J} + (10^5 \text{ Pa})(-0.01 \text{ m}^2)(0.001 \text{ m})}{300 \text{ K}} \approx \frac{1 \text{ J}}{300 \text{ K}}$$

Diffusion Equilibrium

Thermal equil $\rightarrow T$ same

Mech equil $\rightarrow P$ same

DiBrown equil $\rightarrow N$ same (μ)



\rightarrow assume same gas

Assume V constant. Assume that gases can exchange energy and particles. Assume same gas in both sides - -

$$n_{tot} \approx N_{tot} = \text{fixed}$$

$$S_{tot} = S(\mu_1, N_1)$$

Thermal

$$\text{Before } \cdot \left(\frac{\partial S_{tot}}{\partial \mu_1} \right)_{N,V} = \left(\frac{\partial S_{tot}}{\partial \mu_2} \right)_{N,V} = 0 \text{ at equilibrium.}$$

$$\cdot \left(\frac{\partial S_{tot}}{\partial N_1} \right)_{V,V} = \left(\frac{\partial S_{tot}}{\partial N_2} \right)_{V,V} = 0 \text{ at diffusive eq'l.}$$

$$\cdot \left(\frac{\partial S_A}{\partial N_A} \right)_{V,V} = \left(\frac{\partial S_B}{\partial N_B} \right)_{V,V} = 0 \text{ at equilibrium.}$$

Rather not N , but μ

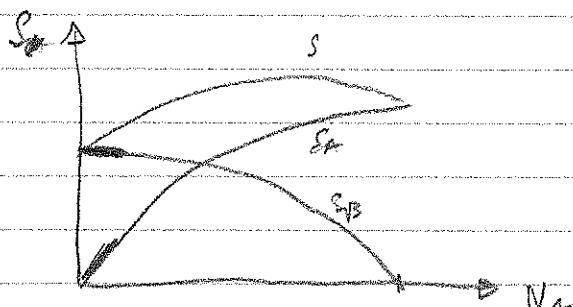
$\rightarrow \mu$: chemical potential (μ) has units of energy [J]

Relating $\frac{\partial S}{\partial N}$ to μ $\frac{\partial S}{\partial N} \left(\frac{\partial \Sigma}{\partial n} \right)$ multiply by temperature + set $n = 1$

$$\frac{J/K}{#}$$

$$\boxed{\mu = -T \left(\frac{\partial S}{\partial N} \right)_{V,V}}$$

At equilibrium, $\mu_A = \mu_B$. Consider S vs. N



→ particles will flow from system with lower $\frac{\partial S}{\partial N}$ to high $\frac{\partial S}{\partial N}$

Since, larger $\left(\frac{\partial S}{\partial N}\right)$ → smaller μ

→ particles flow from system with high to low μ

$\mu \rightarrow$ concentration / density of gas

Generalized Thermodynamic identity

$$\begin{aligned} dS &= \left(\frac{\partial S}{\partial V}\right)_{N,V} dV + \left(\frac{\partial S}{\partial N}\right)_{V,V} dN + \left(\frac{\partial S}{\partial T}\right)_{V,T} dT \\ &\Rightarrow \left(\frac{\partial S}{\partial V}\right)_{N,V} dV + \left(\frac{\partial S}{\partial N}\right)_{V,V} dN + \left(\frac{\partial S}{\partial T}\right)_{V,T} dT \\ &= \frac{1}{T} dT - \mu dN + P dV \end{aligned}$$

$$\delta T dS = dT - \mu dN + P dV$$

$$\delta T \boxed{dV = T dS + \mu dN - P dV}$$

"heat" "diss work" "mech work"

if $q_{uni} \rightarrow$ "heat" "diss work" - static -

When V, V const $\rightarrow \mu = -T \left(\frac{\partial S}{\partial N}\right)$ } sc due to change in N
 When, S, V const $\rightarrow \mu = \left(\frac{\partial V}{\partial N}\right)_{S,V}$

Normally, to keep $\Delta S = 0$, if we TN, need to fix

e.g. Einstein solid w/ $N=3$, $q=3$

$$\Omega = \binom{3+2-1}{3} = 10$$

Then

$$S = k \ln \Omega. \text{ If we TN by 1, } N=4$$

$$\text{Then } \Omega' = \binom{4+3-1}{3} = 20 \quad S' = k \ln 20 > S.$$

To keep S constant \rightarrow need to decrease $q \rightarrow q=2$

$$\Omega'' = \binom{4+2-1}{2} = 10 \text{ so that } S'' = S$$

$$\left\{ \begin{array}{l} \Delta U = q\varepsilon = q;\varepsilon = 2\varepsilon_i - 3\varepsilon_f = -\varepsilon \\ \Delta N = 1 \end{array} \right\} \frac{\partial \mu}{\partial N} = -1$$

$$\underline{\mu} = -\left(\frac{\partial \Omega}{\partial N}\right)_{S,V} = \frac{1}{10}\varepsilon = -\varepsilon$$

Nov 12, 2019 Chemical potential of ideal gas (monatomic)

$$\mu = -T \left(\frac{\partial S}{\partial N} \right)_{V,T} \quad S = Nk \left[\ln \left(\sqrt{\frac{4\pi m V}{3h^2}} \right)^{3/2} \right] - \ln N + \frac{5}{2}$$

$$\begin{aligned} \mu = -T \left\{ k \left[\ln \left(\sqrt{\frac{4\pi m V}{3h^2}} \right)^{3/2} \right] - \ln N^{5/2} + \frac{5}{2} \right. \\ \left. + Nk \left[0 - \frac{5}{2} \frac{1}{N} \right] \right\} \end{aligned}$$

$$\boxed{\mu = -Tk \ln \left[\frac{V}{N} \left(\frac{4\pi m V}{3Nh^2} \right)^{3/2} \right]}$$

$$\text{But } n = \frac{3NkT}{\varepsilon}$$

$$\mu = -T k \ln \left[\frac{v}{N} \left(\frac{2\pi m k T}{h^2} \right)^{3/2} \right]$$

$\frac{\partial \mu}{P}$

Ex for He at room temp = 1 atm. $\Rightarrow \mu = -0.32 \text{ eV}$

higher $\mu \rightarrow$ higher concentration \rightarrow more likely to give off particles

What about for a mixture of gases?

$$\mu_1 = -T \left(\frac{\partial S}{\partial N_1} \right)_{U,V,N_2} \xrightarrow{\text{Total}}$$

$$\mu_2 = -T \left(\frac{\partial S}{\partial N_2} \right)_{U,V,N_1}$$

Thermo identity $\rightarrow dD = TdS - PdV + \sum_i \mu_i dN_i$

In diffusive equilibrium $\rightarrow \mu_A = \mu_{A1}, \mu_{B1} = \mu_{B2}, \dots$
 where $\{ A, B \} \rightarrow$ systems
 $1, 2, \dots \rightarrow$ species of atoms / molecules

Notes Chemist's way $\mu_i = -T \left(\frac{\partial S}{\partial N_i} \right)_{U,V} \rightarrow \# \text{ results}$ $n = N / N_A$

In a mixture of ideal gases, each μ_i behaves as if the other species weren't present. At constant partial pressure

$$P_i = x_i P$$

Define mole $\rightarrow x_i = \frac{N_i}{N_{\text{tot}}}$

$$\text{Now } P_i = x_i P = x_i \frac{N_{\text{tot}} kT}{V} = \frac{x_i N_{\text{tot}} kT}{N_{\text{tot}} V} = \boxed{x_i \frac{kT}{V} = P_i}$$

\square Now, consider 2 gases A + B \rightarrow mixture occupying the same volume V

$$S_{\text{tot}} = S_A + S_B = S(u_A, V, N_A) + S(u_B, V, N_B)$$

If we hold N constant at equilibrium, then this is the same as holding x_A & x_B constant.

$$\boxed{\mu_A = -T \left(\frac{\partial S_{\text{tot}}}{\partial N_A} \right)_{u, V, N_B} = -T \left(\frac{\partial S_A}{\partial N_A} \right)_{u, V}} \quad (\text{since } \partial S_B = 0)$$

\downarrow same as if B not present

Chemical Potential of a Large Extended Solid

$$(a) \Omega = \binom{q+N-1}{q} = \frac{(q+N-1)!}{q!(N-1)!} = \frac{(q+N)!}{(q+N)N!q!}$$

$$\text{Note } (N-1)! = \frac{N!}{N}$$

Fermi's approximation $\rightarrow N! \approx N^N e^{-N} \sqrt{2\pi N}$

$$\Omega \approx \frac{(q+N)^{q+N} e^{-q-N} \sqrt{2\pi(q+N)}}{(q+N)} \cdot \frac{N}{q^q e^{-q} \sqrt{2\pi q} N^N e^{-N} \sqrt{2\pi N}}$$

$$\approx \frac{(q+N)^{q+N}}{q^q N^N} \sqrt{\frac{N}{2\pi q(1+N)}} \approx 1$$

$$\approx \left(\frac{q+N}{q} \right)^q \left(\frac{q+N}{N} \right)^N \sqrt{\dots} \approx \boxed{\left(\frac{q+N}{q} \right)^q \left(\frac{q+N}{N} \right)^N}$$

25

$$\text{So } S = k \ln \Omega = q \ln \ln \left(\frac{q+N}{q} \right) + N k \ln \left(\frac{q+N}{N} \right)$$

$$S = k q \ln \left(1 + \frac{1}{N} \right) + N k \ln \left(\frac{q}{N} + 1 \right)$$

$$\text{So } \frac{\partial S}{\partial N} = \cancel{k q} \frac{1}{1+N} \cdot \frac{1}{q} + k \ln \left(\frac{q}{N} + 1 \right) + N k \frac{1}{1+\frac{q}{N}} \cdot \left(-\frac{q}{N^2} \right)$$

$$\frac{\partial S}{\partial N} = k \ln \left(1 + \frac{1}{N} \right)$$

↳ chemical potential of a gas
Einstein model

Now

$$\mu = -T \left(\frac{\partial S}{\partial N} \right)_{V,T} = -k T \ln \left(1 + \frac{1}{N} \right)$$

-4-

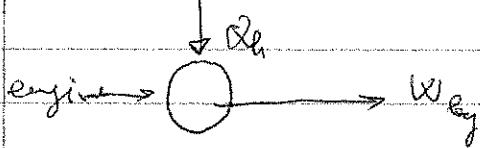
Ch. 4 HEAT ENGINE & REFRIGERATOR

Concept → absorb Q, convert to mechanical W.

Consider



Design considerations



- ① Want to start & end at the same macrostate (energy)
 ↳ cyclic on PV diagram

$$\text{So } \Delta U = 0$$

- ② Must obey 1st law of thermodynamics

$$\Delta U = Q_{\text{absorb}} - W_{\text{exp}}$$

- ③ Must obey 2nd law of thermodynamics $\Delta S \geq 0$

- If turns out that it is impossible to convert 100% of absorbed Q into usable work because we have heat flow.

→ Look at entropy of system.

{ For reversible engine, want $\Delta S_{\text{engine}} = 0$

$$\Delta S_{\text{reservoir}} = -\frac{Q_h}{T_h} \geq 0$$

1st law

$$\Delta U = Q_{\text{abs}} - W_{\text{ex}} \Rightarrow Q_{\text{abs}} = W_{\text{ex}}$$

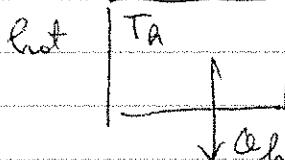
$$\therefore \Delta S_{\text{system}} = \Delta S_{\text{engine}} + \Delta S_{\text{reservoir}} = -\frac{Q_h}{T_h} = -\frac{W_{\text{ex}}}{T_h} \geq 0$$

But then W_{ex} has to be negative.

Result: cannot build an engine with a single reservoir that converts heat into work

To fix this

Assume cyclic engine $\Delta U = 0$

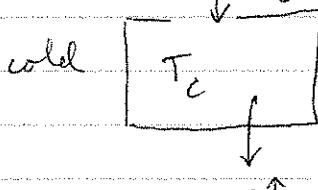


$$\text{Then } \Delta S_h - \Delta S_c = 0$$

$$\therefore Q_h - Q_c - W_{\text{ex}} = 0$$

$$\therefore W_{\text{ex}} = Q_h - Q_c$$

work done by the engine.



$Q_h = Q$ absorbed by the hot engine

$W_{\text{ex}} = W$ done by engine.

$Q_c = Q$ expelled by the engine

Efficiency

$$\epsilon = \frac{W_{\text{out}}}{Q_h} = \frac{W_{\text{out}}}{Q_h}$$

Rth

$$\epsilon = \frac{Q_h - Q_c}{Q_h} = 1 - \frac{Q_c}{Q_h}$$

$$\Delta S_{\text{hot}} = -\frac{Q_h}{T_h}, \quad \Delta S_{\text{cold}} = \frac{Q_c}{T_c}$$

so $\frac{Q_c}{T_c} > -\frac{Q_h}{T_h}$ for $\Delta S \geq 0$

C

$$\epsilon \leq 1 - \frac{T_c}{T_h}$$

Example

$$T_h = 100^\circ C$$

$$Q_h = 150J$$

Assume $J_u = 0$

$$W = 150J - 125J = 25J$$

$$Q_{\text{abs}} = Q_h - Q_c$$

$$Q_c = 125J$$

$$W$$

$$\epsilon = \frac{W}{Q_h} = \frac{25}{150} = \frac{1}{6}$$

$$\begin{array}{|c|} \hline T_c \\ \hline 20^\circ C \\ \hline \end{array}$$

Does this engine reach maximum eff?

$$\text{Max } \epsilon = 1 - \frac{T_c}{T_h} = 1 - \frac{20+273}{100+273} = 21.4\%$$

B

No, doesn't reach maximum efficiency.

Carnot Cycle → towards a more efficient engine.

- To avoid creating excess entropy in our engine.

$$T_{\text{engine}} = T_h \rightarrow \text{not possible.}$$

Instead, we want T_{engine} just slightly below T_h

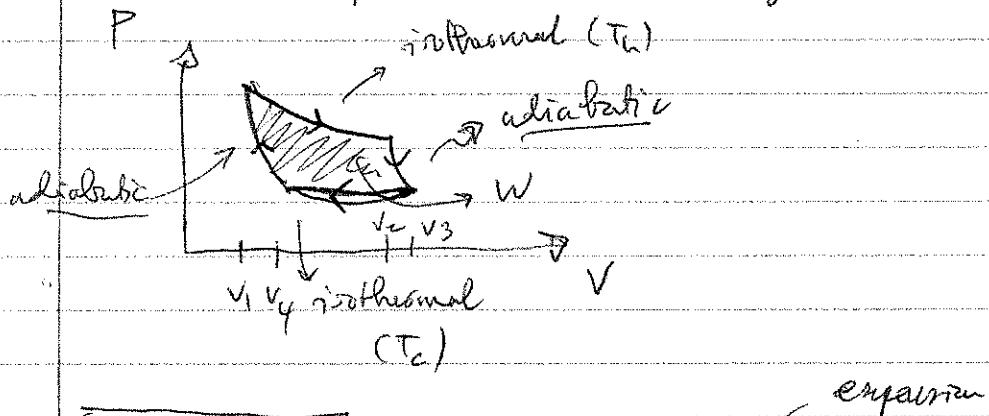
→ Let it expand isothermally to keep $T_{\text{engine}} \approx \text{constant}$

- after isothermal expansion → bring temp of engine down

$$\text{to } T_c \rightarrow (T_{\text{engine}} > T_c \text{ slightly})$$

→ Want [adiabatic expansion] (to avoid additional heat flow)

↳ expel waste heat during an isothermal compression.



Carnot Cycle

(1) Isothermal @ T_h

(2) Adiabatic expansion to get T_c

(3) Isothermal compression @ T_c (waste heat dump)

(4) Adiabatic compression to bring engine back to T_h .

(79)

$$(1) Q_h = W_{cy} = \int_{V_1}^{V_2} P dV = \int_{V_1}^{V_2} \frac{N h T_h}{V} dV = N h T_h \ln \frac{V_2}{V_1}$$

$$(V_3 > V_4) Q_c = - \int_{V_3}^{V_4} P dV = - N h T_c \ln \left(\frac{V_3}{V_4} \right) = N h T_c \ln \left(\frac{V_2}{V_4} \right)$$

$$\eta = 1 - \frac{Q_c}{Q_h} = 1 - \frac{\ln(V_3/V_4)}{\ln(V_2/V_1)} \cdot \frac{T_c}{T_h}$$

Now, for adiabatic processes

$$\rightarrow V T^{\gamma-1} = \text{constant}$$

$$V_3 T_c^{\gamma-1} = V_2 T_h^{\gamma-1} \Rightarrow V_4 T_c^{\gamma-1} = V_1 T_h^{\gamma-1}$$

$$\frac{V_3 T_c^{\gamma-1}}{V_4 T_c^{\gamma-1}} = \frac{V_2 T_h^{\gamma-1}}{V_1 T_h^{\gamma-1}} \Rightarrow \frac{V_3}{V_4} = \frac{V_2}{V_1} \Rightarrow \frac{\ln(V_3/V_4)}{\ln(V_2/V_1)}$$

G

$$e = 1 - \frac{T_c}{T_h}$$

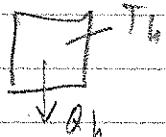
→ assuming adiabatic.

→ Carnot cycle provides near efficiency

eff

Hottest engines

Recall



cyclic process $\rightarrow \Delta u = 0$

$\downarrow Q_c$

$$W_{cy} = Q_{in} - Q_{out}$$

$$\epsilon = \frac{Q_{in} - Q_{out}}{Q_{in}} = \frac{W_{cy}}{Q_{in}} = 1 - \frac{Q_{out}}{Q_{in}}$$

Since $\Delta S \geq 0$, $\therefore \epsilon \leq 1 - \frac{T_c}{T_h}$ equality holds when Carnot engine

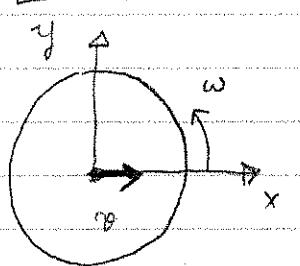
Hurricanes as Heat Engines

Hot reservoir \rightarrow ocean surface

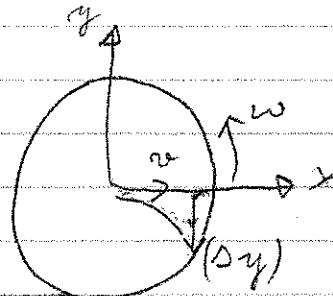
Cold reservoir \rightarrow atmosphere.

② \rightarrow low pressure system with circulation due to Coriolis effect

$$F_c = 2\pi r \times w$$



$$x = vt \Rightarrow$$



if $v \perp w$, then

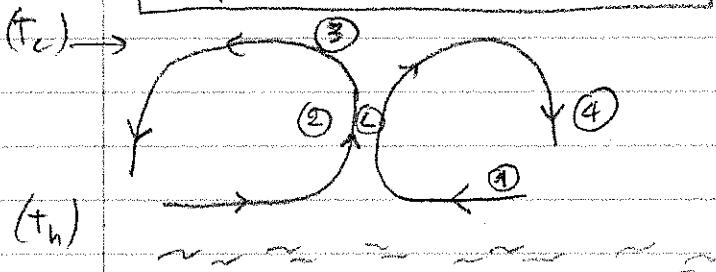
$$\Delta y = (wt)x$$

Coriolis acceleration

$$\text{Put } v = u \quad x = vt \Rightarrow \Delta y = wvt^2 = \frac{1}{2} (2wv)t^2 = \frac{1}{2} a_c t^2$$

Steps of Hurricane engine

\rightarrow same as Carnot's



(1) Isothermal expansion of air over hot ocean ($T \approx 300K$)

(2) Adiabatic expansion

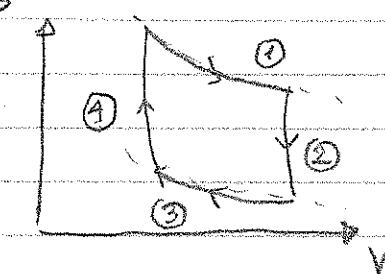
\rightarrow air moves rapidly up

(3) Isothermal compression in tropopause ($T \approx 200K$)

eye wall up to tropopause

(4) Adiabatic compression of dry air

(81)

On PV diagram

Work produced by turbines dissipated by friction

$$\rightarrow d\omega^2 \text{ (turbulent flow)}$$

$$w = F_{drag} \cdot x$$

$$\text{So } \frac{dW}{dt} = (av^2)v \approx av^3$$

heat transfer from the ocean by forced convection $Q_h \propto v$

$$\text{Total : } Q_h = av^3 + bv \rightsquigarrow Q_{ocean}$$

Q due to friction

So

$$e = \frac{Q_h}{Q_{total}} = \frac{av^3 + bv}{av^3 + bv} = 1 - \frac{T_c}{T_h} \rightsquigarrow \text{Carnot engine}$$

⇒ Can solve for v .

$$\frac{av^2}{av^3 + bv} = 1 - \frac{T_c}{T_h} \Rightarrow av^2 = (av^2 + b)(1 - \frac{T_c}{T_h}) = av^2(1 - \frac{T_c}{T_h}) + b(1 - \frac{T_c}{T_h})$$

$$\therefore av^2 \left(\frac{T_c}{T_h} \right) = b \left(1 - \frac{T_c}{T_h} \right)$$

$$v = \sqrt{\frac{b}{a} \left(\frac{T_h}{T_c} - 1 \right)}$$

Refrigerator



Work done on substance to pull heat out cold reservoir

Work \rightarrow except waste heat to heat | now air

$$\text{Now, } \Delta m = 0 \Rightarrow Q_c + W_m = Q_h$$

compression work -

Coefficient of Performance

$$\text{COP} = \frac{Q_c}{W_m}$$

replace $W_m = Q_h - Q_c$

$$\text{So, } \left[\frac{\text{COP}}{\text{COP}} = \frac{Q_c}{Q_h - Q_c} = \frac{1}{\frac{Q_h}{Q_c} - 1} \right] \geq 1$$

\Rightarrow By 2nd law, $\Delta S \geq 0 \Rightarrow \frac{Q_h}{T_h} - \frac{Q_c}{T_c} \geq 0 \quad \therefore \frac{Q_h}{Q_c} \geq \frac{T_h}{T_c}$

$$\text{So, } \left[\frac{\text{COP}}{\text{COP}} = \frac{1}{\frac{Q_h}{Q_c} - 1} \leq \frac{1}{\frac{T_h}{T_c} - 1} \right]$$

\Rightarrow Carnot cycle once again creates the most efficient refrigerator

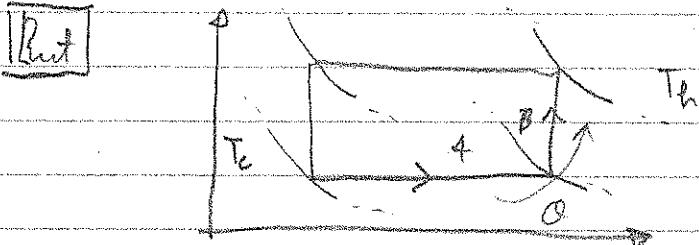
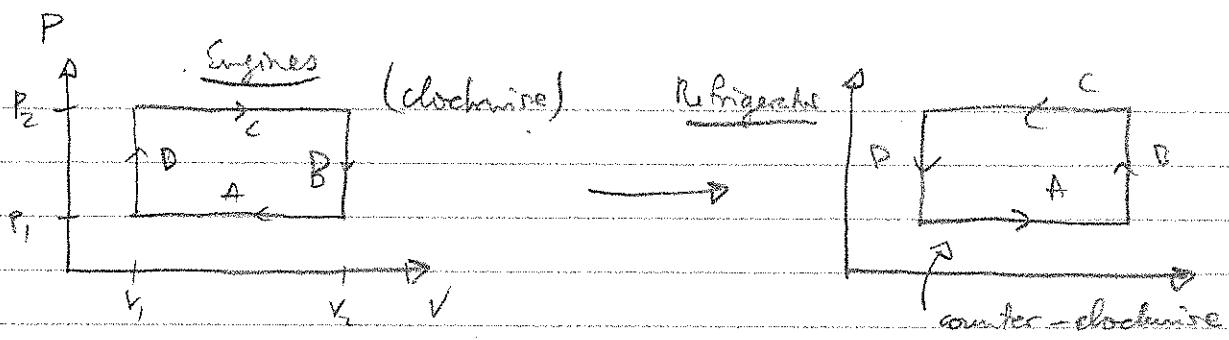
Need $T \geq T_h$ during heat rejection

$T \leq T_c$ during heat absorption

Example What is the max possible COP for a standard AC unit?

$$\text{Let } t_{in} = 22^\circ C \quad \text{Then } \text{COP}_{\max} = \frac{1}{\frac{30+273}{22+273} + 1} \approx 36.9$$

PV diagram



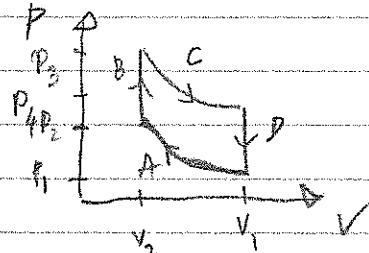
Need $T_c > T_{fr}$ for heat flow A,B
and $T_h < T_c$ for heat flow C,D

→ Need adiabatic processes

Nov 19, 2019

Real Heat Engines

Example Internal Combustion Engine (Otto cycle)



- A: adiabatic compression of air + fuel
- B: spark plug ignites the mixture, increasing T,P, holding V constant
- C: adiabatic expansion in the cylinder due to high pressure
- D: hot exhaust is expelled and replaced by new mixture at lower temperature

Efficiency of this engine?

$$\epsilon = 1 - \frac{Q_c}{Q_h} \quad \text{Steps A \& C are adiabatic} \rightarrow Q = 0$$

$\xrightarrow{\text{B}}$ $\xrightarrow{\text{D}}$

$\rightarrow Q_h$
 $\rightarrow Q_c$

Step B $\Delta U_B = Q + \cancel{W}^0 \Rightarrow Q = \frac{f}{2} N h T = \frac{f}{2} P V = \frac{f}{2} V_2 (P_3 - P_2)$

Step D $\Delta U_D = Q_c + \cancel{W}^0 = -\frac{f}{2} N h T \Rightarrow Q_c = \frac{f}{2} V_2 (P_4 - P_1)$

So,
$$\boxed{\epsilon = 1 - \frac{Q_c}{Q_h} = 1 - \frac{V_1 (P_4 - P_1)}{V_2 (P_3 - P_2)}}$$

But more convenient with temperatures...

Adiabatic $\Rightarrow P_1 V_1^\gamma = P_2 V_2^\gamma \quad \& \quad P_4 V_1^\gamma = P_3 V_2^\gamma$

∴ $(P_4 - P_1) V_1^\gamma = (P_3 - P_2) V_2^\gamma$

∴ $\frac{P_4 - P_1}{P_3 - P_2} = \frac{V_2^\gamma}{V_1^\gamma} = \left(\frac{V_2}{V_1}\right)^\gamma$

∴ $\epsilon = 1 - \frac{V_1 V_2^\gamma}{V_2 V_1^\gamma} = 1 - \left(\frac{V_2}{V_1}\right)^{\gamma-1}$

∴
$$\boxed{\epsilon = 1 - \left(\frac{V_2}{V_1}\right)^{\gamma-1}}$$

Compared to Carnot engine:
$$\boxed{\epsilon = 1 - \frac{T_c}{T_h} = \epsilon = 1 - \frac{T_1}{T_3}}$$

Remember that $T V^{\gamma-1}$ = constant for an adiabat $\Rightarrow \frac{T_1}{T_2} = \left(\frac{V_2}{V_1}\right)^{\gamma-1}$

$\rightarrow \boxed{\epsilon = 1 - \frac{T_1}{T_2}}$

or, another exhibit $\Rightarrow T_3 V_2^{\gamma-1} = T_4 V_1^{\gamma-1}$

$$\therefore \frac{T_4}{T_3} = \left(\frac{V_2}{V_1}\right)^{\gamma-1} \Rightarrow e = 1 - \frac{T_4}{T_3}$$

Note $\frac{T_1}{T_3} < \frac{T_1}{T_2}$ and $\frac{T_1}{T_3} < \frac{T_4}{T_3}$

$\therefore \boxed{e_{Otto} < e_{Carnot}}$

$\therefore \left\{ \begin{array}{l} \text{Otto cycle will always be less efficient than Carnot engine} \\ \text{over the same T} \end{array} \right.$

Revising 3rd Law

\hookrightarrow "Planck's statement" as $T \rightarrow 0$, $S \rightarrow S_{min}$, $S_{max} = 0$
for pure crystalline solids"

Einstein statement

\hookrightarrow "As $T \rightarrow 0$, S remains finite"

$$\therefore S = \int_0^T \frac{C_V}{T} dT \text{ if } C_V \neq 0 \text{ then } S \rightarrow S_{min} = -\infty$$

Nernst unattainability principle

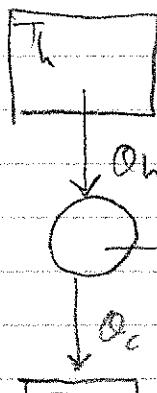
\hookrightarrow "Any thermodynamic process cannot reach absolute zero in a finite number of steps in a finite amount of time"

1st law tells us we can't get work for free

2nd law tells us we can't build a mono-thermal heat engine

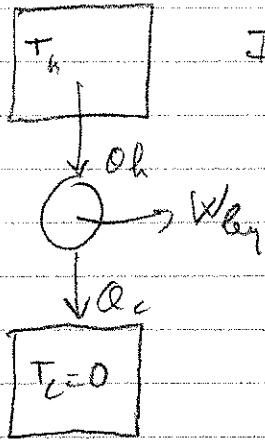
3rd law tells us we can't get 100% utilization of heat to work even if

$$\Delta S = 0$$

Einstein

$Q_h = W_{exp}$ Einstein statement
 $\rightarrow S \text{ finite at } T=0$

$$\begin{cases} T_c = 0 \\ S = -\infty \end{cases}$$

Nernst

If you want $DS=0$, Nernst says can't get engine to $T=0$ in finite time

 $\cancel{\text{t}}$

ch. 5 \rightarrow FREE ENERGY

Enthalpy \rightarrow method at constant P

$$H = U + PV \Rightarrow dH = dU + PdV$$

or
$$\boxed{\Delta H = \Delta U + P\Delta V}$$

\downarrow
 $Q + W_{\text{on}}$

$\rightarrow -P\Delta V + W_{\text{other}}$

Σ
$$\boxed{\Delta H = Q + W_{\text{other}}}$$

Helmholtz free energy (F)

↳ useful for constant T processes.

$$F = U - TS$$

create system
out of nothing

$$Q = T\Delta S, \text{ quasi-static}$$

$$\downarrow \\ S_{\text{final}} = 0$$

Gibbs free energy (G)

↳ useful for constant T = P

$$G = U - TS + PV = H - TS$$

Born-Romuald-Pauli Potential U, H, F, G

Look at changes in these: $F = U - TS \Rightarrow dF = dU - SdT - TdS$

For F, T constant $\Rightarrow \boxed{dF = \Delta U - T\Delta S}$ can minimize

$$\boxed{\Delta F = Q_{in} + W_{on} - T\Delta S} \quad \text{Now } Q_{in} \leq T\Delta S \text{ (in general)}$$

$$\hookrightarrow \boxed{\Delta F \leq W_{on}} \quad (\text{constant T, equality when quasi static})$$

can be expansion/compression work = $\int PdV + \text{other}$

Gibbs free energy $\Rightarrow G = U - TS + PV \Rightarrow dG = dU - TdS - SdT + PdV + VdP$

↳ constant T, P $\Rightarrow dG = dU - TdS + PdV$

$$Q_{in} + W_{on}, Q_{in} \leq TdS, W_{on} = -PdV + W_{\text{other}}$$

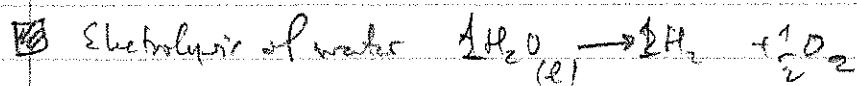
ΔG

$$\boxed{\Delta G \leq W_{\text{other}}}$$

$$\Delta G = \Delta H + PV = Q_{in} + W_{\text{other}} \Rightarrow \boxed{\Delta G = \Delta H - TdS}$$

$$Q_{in} + W_{on}$$

Ex of using ΔG



$$\Delta H_f = -286 \text{ kJ/mol}$$

How much work do we need to apply to get reaction to proceed?

Charge in S: $S_{\text{H}_2\text{O}(l)} = 70 \text{ J/K}$

$$S_{\text{H}_2(g)} = 131 \text{ J/K}$$

$$S_{\frac{1}{2}\text{O}_2(g)} = 205 \text{ J/K}$$

$$\Delta S = (131 \text{ J/K} + \frac{1}{2} \cdot 205 \text{ J/K}) - 70 \text{ J/K} = 163 \text{ J/K}$$

Max amount of heat that can enter system = $T\Delta S = 49 \text{ kJ}$

$$\Delta G = \Delta H - T\Delta S = 286 \text{ kJ} - 49 \text{ kJ} = \boxed{\Delta G = 237 \text{ kJ}}$$

Thermodynamic identities

$$dU = TdS - PdV + \nu dN \Rightarrow u(s, v)$$

$$\text{if } dU = \left(\frac{\partial U}{\partial S}\right)_{V,N} dS + \left(\frac{\partial U}{\partial V}\right)_{S,N} dV$$

$$\text{if } \frac{\frac{\partial^2 u}{\partial S \partial V}}{\frac{\partial^2 u}{\partial S^2}} = \frac{\frac{\partial^2 u}{\partial V^2}}{\frac{\partial^2 u}{\partial S \partial V}} \Rightarrow \frac{\partial}{\partial V} \left[\left(\frac{\partial U}{\partial S} \right)_{V,N} \right]_{S,N} = \frac{\partial}{\partial S} \left[\left(\frac{\partial U}{\partial V} \right)_{S,N} \right]_{V,N}$$

$$\textcircled{1} \quad \boxed{\left(\frac{\partial T}{\partial V} \right)_{S,N} = - \left(\frac{\partial P}{\partial S} \right)_{V,N}} \rightsquigarrow \begin{array}{l} \text{independent variables } s, v \\ \text{Maxwell's relation \#1} \end{array}$$

$$\textcircled{2} \quad dU = TdS - PdV = TdS - \lambda(PV) + VdP \Rightarrow d(V + PV) = TdS + VdP$$

$$\text{if } \boxed{dH = TdS + VdP} \rightsquigarrow \text{how to get } \Delta H \text{ at non-standard P, T ...}$$

$$\text{H} = H(s, p)$$

S
$$dH = \left(\frac{\partial H}{\partial s}\right)_{p,N} ds + \left(\frac{\partial H}{\partial p}\right)_{s,N} dp$$

$\underbrace{\qquad\qquad\qquad}_{T}$ $\underbrace{\qquad\qquad\qquad}_{V}$

S $T = \left(\frac{\partial H}{\partial s}\right)_{p,N} ; V = \left(\frac{\partial H}{\partial p}\right)_{s,N}$

Now $\frac{\partial}{\partial p} \left(\frac{\partial H}{\partial s} \right)_{p,N} + \frac{\partial}{\partial s} \left(\frac{\partial H}{\partial p} \right)_{s,N}$

S
$$\frac{\partial}{\partial s} \left[\left(\frac{\partial T}{\partial p}\right)_{s,N} \right] = \left(\frac{\partial V}{\partial s}\right)_{p,N} \rightarrow \underline{\text{Maxwell's relation 1/2}}$$

(3) Independent variables T, V

$$dU = Tds - Pdv$$

$$= d(Ts) - sdT - Pdv$$

S $d(U - Ts) = - sdT - Pdv$

$$dF = - sdT - Pdv$$

Here $F(T, V)$

S $dF = \left(\frac{\partial F}{\partial T}\right)_{V,N} dT + \left(\frac{\partial F}{\partial V}\right)_{T,N} dV$

$\underbrace{\qquad\qquad\qquad}_{-S}$ $\underbrace{\qquad\qquad\qquad}_{-P}$

L
$$S = - \left(\frac{\partial F}{\partial T}\right)_{V,N}, \quad P = - \left(\frac{\partial F}{\partial V}\right)_{T,N}$$

$$\text{Eq. } \frac{\partial}{\partial V} \left(\frac{\partial F}{\partial T} \right) = \frac{\partial}{\partial T} \left(\frac{\partial F}{\partial V} \right)$$

$$\text{Eq. } - \left(\frac{\partial S}{\partial V} \right)_{T,N} = - \left(\frac{\partial P}{\partial T} \right)_{V,N}$$

$$\text{Eq. } \boxed{\left(\frac{\partial S}{\partial V} \right)_{T,N} = \left(\frac{\partial P}{\partial T} \right)_{V,N}}$$

(4) Independent variables: $T \& P$

$$dU = TdS - PdV = d(TS) - SdT - d(PV) + VdP$$

$$\text{Eq. } d(U - TS + PV) = - SdT + VdP$$

$$\boxed{dG = - SdT + VdP}$$

$$\text{Eq. } V = \left(\frac{\partial G}{\partial P} \right)_{T,N}, \quad S = - \left(\frac{\partial G}{\partial T} \right)_{P,N}$$

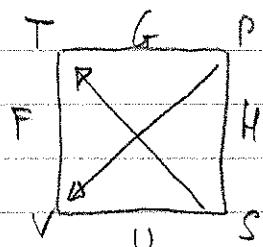
and

$$\boxed{\left(\frac{\partial V}{\partial T} \right)_{P,N} = \left(\frac{\partial S}{\partial P} \right)_{T,N}}$$

Mar 22, 2019

Thermodynamics Potentials $U, H, F, G \rightarrow$ "good physicists have studied under very fine teachers"

Use square



$T \quad G \quad P$

$$dH = VdP + TdS + n dN$$

$$dU = TdS - PdV + n dN$$

Write potentials as fn of vars on front side of square { signs + arrow pt to (\rightarrow) diff, col's diagonal}

Maxwell's Relations

$$L = 1 \rightarrow \left(\frac{\partial T}{\partial V} \right)_S = - \left(\frac{\partial P}{\partial S} \right)_V$$

arrow point to minus sign for the constant variable.

Definitions of potentials from squares

$$H = U + PV$$

○, against arrow $\rightarrow (+)$

$$G = H - TS$$

$$= U + PV - TS$$

Usefulness of Maxwell's Relations

Can derive a relationship between C_P & C_V for any substance

Reminder $C_V = \left(\frac{\partial U}{\partial T} \right)_V$

$$C_P = \left(\frac{\partial H}{\partial T} \right)_P$$

① Start by writing S in terms of T, V

$$dS = \left(\frac{\partial S}{\partial T} \right) dT + \left(\frac{\partial S}{\partial V} \right)_T dV$$

\sim

$$= \left(\frac{C_V}{T} \right) dT + \left(\frac{\partial S}{\partial V} \right)_T dV$$

Express $V = V(T, P)$ ○ consider constant pressure

$$dV = \left(\frac{\partial V}{\partial T} \right)_P dT + \left(\frac{\partial V}{\partial P} \right)_T dP = \left(\frac{\partial V}{\partial T} \right)_P (dT)_P$$

$$\therefore (dS)_P = \left(\frac{C_V}{T} \right) (dT)_P + \left(\frac{\partial S}{\partial V} \right)_T \text{ans } \left(\frac{\partial V}{\partial T} \right)_P (dT)_P$$

[5]

$$\left(\frac{\partial S}{\partial T}\right)_p = C_V + \left(\frac{\partial P}{\partial V}\right)_T \left(\frac{\partial V}{\partial T}\right)_p$$

For C_p , use identity for enthalpy - $dH = TdS + VdP$

$$\text{At constant pressure} \Rightarrow (dH)_p = (TdS)_p$$

$$C_p = \left(\frac{\partial H}{\partial T}\right)_p \stackrel{\text{so}}{=} \left(\frac{\partial H}{\partial T}\right)_p = T \left(\frac{\partial S}{\partial T}\right)_p$$

So

$$T \left(\frac{\partial S}{\partial T}\right)_p = C_V + T \left(\frac{\partial S}{\partial V}\right)_T \left(\frac{\partial V}{\partial T}\right)_p$$

$$\text{So } C_p = C_V + T \left(\frac{\partial S}{\partial V}\right)_T \left(\frac{\partial V}{\partial T}\right)_p$$

$\text{Q Use Maxwell's relation } \left(\frac{\partial S}{\partial V}\right)_T = \left(\frac{\partial P}{\partial T}\right)_V$

So

$$C_p = C_V + T \left(\frac{\partial P}{\partial T}\right)_V \left(\frac{\partial V}{\partial T}\right)_p$$

- Let $\beta = \left(\frac{1}{V}\right) \left(\frac{\partial V}{\partial T}\right)_p$ as "thermal volume coefficient of expansion"

- Let $\kappa = \left(\frac{1}{T}\right) \left(\frac{\partial V}{\partial P}\right)_T$ as "isothermal compressibility"

$\text{Q To write } C_p = C_V \text{ in terms of } \beta \text{ & } \kappa_T, \text{ more partial derivatives manipulation is required.}$

$$z = z(x, y) \text{ then } \left(\frac{\partial z}{\partial y}\right)_x = \frac{-(\partial z / \partial x)x}{(\partial z / \partial x)_y}$$

$$\text{Proof } dz = \left(\frac{\partial z}{\partial y}\right) dy + \left(\frac{\partial z}{\partial x}\right) dx$$

when z constant $\Rightarrow dz = 0$

$$\therefore \left(\frac{\partial z}{\partial x}\right) dx = - \left(\frac{\partial z}{\partial y}\right) dy \quad (dz = 0)$$

$$\therefore \left(\frac{\partial x}{\partial z}\right)_y = - \frac{(\partial z / \partial y)_x}{(\partial z / \partial x)_y}$$

$$\therefore \left(\frac{\partial x}{\partial y}\right)_z = - \frac{(\partial z / \partial y)_x}{(\partial z / \partial x)_y}$$

do back to derive.

$$\left(\frac{\partial P}{\partial T}\right)_V = - \frac{(\partial V / \partial T)_P}{(\partial V / \partial P)_T}$$

$$\downarrow (C_P - C_V) = T \left(\frac{\partial P}{\partial T}\right)_V \left(\frac{\partial V}{\partial T}\right)_P = -T \left(\frac{\partial V}{\partial T}\right)_P \left(\frac{\partial V}{\partial P}\right)_T^{-1} \left(\frac{\partial V}{\partial T}\right)_P$$

$$= -T(V_B)^2 \frac{-1}{k_T V}$$

$$\boxed{C_P - C_V = \frac{T B^2 V}{k_T}} \quad \text{is true for any substance}$$

\forall For ideal gas $\rightarrow C_P - C_V = nR = Nk$

$$B = \frac{1}{V} \left(\frac{\partial V}{\partial T}\right)_P, \quad k_T = \frac{-1}{V} \left(\frac{\partial V}{\partial P}\right)_T$$

$$= \frac{1}{V} \left(\frac{Nk}{P}\right), \quad = \frac{-1}{V} \left(\frac{-NkT}{P^2}\right) = \frac{NkT}{PV^2} = \frac{1}{P}$$

$$B = \frac{1}{T} \quad \therefore \quad \boxed{C_P - C_V = \frac{T(1 - \frac{1}{P})^2 V}{P^2} = \frac{PV}{T} = Nk = nR} \quad \checkmark$$

April 1, 2019

Extensive vs. Intensive parameters

1	2
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Say we have a homogeneous system

- ① if $y_1 + y_2 = y$ then y is an extensive parameter.
- ② if $y_1 = y_2 = y$ then y is an intensive parameter.

③ Extensive { volume, mass, # particles, internal energy, entropy
 (V) (m) (N) (U) (S)
 (enthalpy (H)), (F), (G)}

④ Intensive { Temp, pressure, density, chemical potential
 (T) (P) (ρ) (μ)

Rules of multiphase calculations:

$$\textcircled{1} \quad (\text{Ext}) \cdot (\text{Int}) = (\text{Ext}) \quad \underline{\text{Ex}} \quad V \times p = m$$

$$\textcircled{2} \quad \frac{[\text{Ext}]}{[\text{Ext}]} = [\text{Int}] \quad \underline{\text{Ex}} \quad \frac{m}{V} = p$$

$$\text{or } \frac{c_v}{\text{mass}} = c_v$$

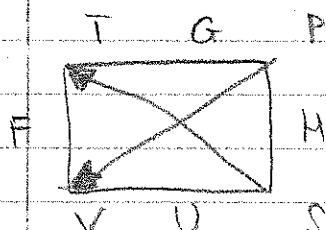
$$\textcircled{3} \quad (\text{Ext}, \text{Ext}) \Rightarrow \text{neither (extensive) nor (intensive)}$$

$$\textcircled{4} \quad [\text{Ext}] + [\text{Ext}] = [\text{Ext}]$$

$$\textcircled{5} \quad \underline{\text{Not allowed }} [\text{Ext}] + [\text{Int}]$$

Ex G has units of J But $G + \mu$ does not make sense
 μ has units of J

Q) Gibbs free energy & chemical potential



$$dG = VdP - SdT + \mu dN$$

$$\left(\frac{\partial G}{\partial P}\right)_{T,N} \propto V, \quad \left(\frac{\partial G}{\partial T}\right)_{P,N} = -S, \quad \left(\frac{\partial G}{\partial N}\right)_{P,T} = \mu$$

Now $\mu = \left(\frac{\partial G}{\partial N}\right)_{P,T}$ ^{ext} intensive
 int ^{ext}

At constant PT $\rightarrow G = \mu N$ or N , G proportional

for a system with only 1 type of particles.

$$\mu = G/N$$

Helmholtz free energy & chemical potential

$$dF = -dE - SdT - PdV + \mu dN$$

$$\mu = \left(\frac{\partial F}{\partial N}\right)_{T,V} \rightarrow F = N\mu(V)$$

^{ext}
int

Derivation of chemical potential of ideal gas

$$\text{But}, \mu = -T \left(\frac{\partial S}{\partial V}\right)_{T,N}$$

Now,

$$G = \mu N \text{ or } \mu = \frac{G}{N}$$

Consider a fixed amount of gas (N) at const (T) and allow P to vary

$$\left(\frac{\partial \mu}{\partial P}\right)_{T,N} = \frac{1}{P} \left(\frac{\partial G}{\partial N}\right)_{T,N} = \frac{1}{N} \left(\frac{\partial G}{\partial P}\right)_{T,N} = \frac{V}{N}$$

$$\text{Ex } \int d\mu = \int \left(\frac{V}{N}\right) dP \Rightarrow d\mu = \int_{P_i}^{P_f} \frac{kT}{P} dP = kT \ln\left(\frac{P_f}{P_i}\right)$$

Ex

$$\boxed{\mu(T, P) - \mu(T, P_i) = kT \ln\left(\frac{P}{P_i}\right)}$$

note $\mu(T, P_i) = \mu^\circ(T) \Rightarrow \boxed{\mu(T, P) = \mu^\circ + kT \ln\left(\frac{P}{P_0}\right)}$

1 atm

typically, 1 atm

• P is the partial pressure

Ex He, H $\mu_{He}(T, P) = \mu_{He}^\circ(G) + \cancel{\mu_H^\circ(G)} + kT \ln\left(\frac{P_{He}}{P_0}\right)$

Ex Test vs μ derived for a monatomic ideal gas

$$\mu = -T \left(\frac{\partial S}{\partial N}\right)_{V,T} \pi$$

$$\mu = -kT \ln \left[\frac{V}{N} \left(\frac{2\pi m k T}{h^2} \right)^{3/2} \right]$$

$$= -kT \ln \left[\frac{P^0 k T}{P^0 P} \left(\frac{2\pi m k T}{h^2} \right)^{3/2} \right]$$

$$= -kT \ln \left[\frac{kT}{P^0} \left(\frac{2\pi m k T}{h^2} \right)^{3/2} \right] + kT \ln\left(\frac{P}{P_0}\right)$$

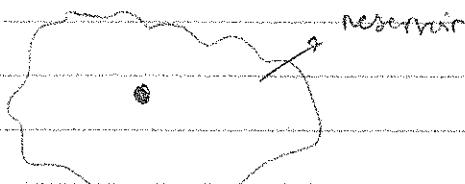
$$\boxed{\mu = -kT \ln \left[\frac{kT}{P^0} \left(\frac{2\pi m k T}{h^2} \right)^{3/2} \right] + kT \ln\left(\frac{P}{P_0}\right)}$$

 $\mu^\circ(T)$

Free Energy as a Force Towards Equilibrium

- For isolated system $\rightarrow S^{\ddagger}$
- For interacting system $\rightarrow S_{\text{tot}}^{\ddagger}$

Assume environment is a reservoir of constant T, V, N



$$S_{\text{tot}} = S_{\text{system}} + S_{\text{reservoir}}$$

$$dS_{\text{tot}} = dS_{\text{sys}} + dS_{\text{res}}$$

 For reservoir, $TdS = dU + PdV - \mu dN$

$$dS = \frac{1}{T}dU + \frac{P}{T}dV - \frac{\mu}{T}dN$$

 if T, N, V constant, then $dS_{\text{res}} = \frac{1}{T_{\text{res}}} dU_{\text{res}}$

$$\therefore dS_{\text{tot}} = dS_{\text{sys}} + \frac{1}{T_{\text{res}}} dU_{\text{res}}$$

$$\text{In eqs } T_{\text{sys}} = T_{\text{res}}, \quad dU_{\text{sys}} = -dU_{\text{res}}$$

$$\therefore dS_{\text{tot}} = dS_{\text{sys}} - \frac{1}{T_{\text{sys}}} dU_{\text{sys}}$$

 $dS_{\text{tot}} = -\frac{1}{T} (dU - TdS) \quad \rightsquigarrow$ dropping sys. subscript

b

$$dS_{\text{tot}} = -\frac{dF}{T}$$

If $dF < 0 \rightarrow$ spontaneous flow towards equilibrium



Now, let V vary, holding $P, T, (\pm N)$ constant

$$dS_{\text{tot}} = dS_{\text{sys}} + \frac{1}{T_{\text{res}}} dU_{\text{res}} + \frac{P_{\text{res}}}{T_{\text{res}}} dV_{\text{res}} - \frac{\mu_{\text{res}}}{T_{\text{res}}} dN_{\text{res}}$$

At equilibrium, $P_{\text{res}} = P_{\text{sys}}$, $T_{\text{res}} = T_{\text{sys}}$, $dV_{\text{res}} = -dV_{\text{sys}}$

1

$$dS_{\text{tot}} = dS - \frac{1}{T} dU = \frac{\mu}{T} dV$$

$$\underline{dS_{tot}} = \frac{-1}{T} (dU - TdS + PdV) \quad dG$$

10

$$dS_{\text{tot}} = -\frac{dG}{T}$$

$$\delta G = \delta G_{\text{ref}}, \quad T = \text{equilibrium } T$$

1

For fixed $P, T, N \Rightarrow G$ tends to decrease

(if $\Delta G < 0 \rightarrow$ spontaneous process)

Example use of free energy to calculate whether a reaction is spontaneous or not

Cryostabilized ammonium nitrate NH_4NO_3



look up $\Delta_f H$, $\Delta_f S$

	$\Delta_f H$	$\Delta_f S$	@ eq, $\Delta G = 0$
$\text{NH}_4\text{NO}_3(s)$	-365.56	151.08	
$\text{NH}_4^+(aq)$	-132.51	113.4	
$\text{NO}_3^-(aq)$	-205.0	146.4	

$$\Delta G = \Delta H - TAS = -4.4 \text{ kJ} < 0 \rightarrow \text{spontaneous}$$

@ Content T

In general, $H = U + PV$ for constant P process, $\Delta H = \Delta U + PV$

$$\Delta H = \Delta U + P\Delta V = Q_{\text{abs}}$$

$\Delta H < 0 \Rightarrow \text{exothermic rxn}$

$\Delta H > 0 \Rightarrow \text{endothermic rxn}$

if $\Delta H < 0, \Delta S > 0 \Rightarrow \Delta G < 0$ spontaneous

$\Delta H > 0, \Delta S < 0 \Rightarrow \Delta G > 0$ not spontaneous rxn.

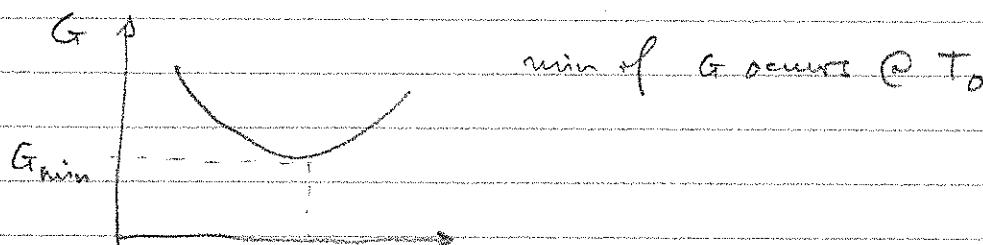
<input checked="" type="checkbox"/> Summary	<u>Reservoir</u>	<u>System</u>
• At const	U, V	$S \uparrow$
• At const	T, V	$F \downarrow$
• At const	T, P	$G \downarrow$

Stability against Temperature Fluctuations

Consider a system. Let T, V be independent params that describe system

1st, hold V fixed & allow T to vary

Interacting with respect to constant T, P, N



• expand G around eq. value

$$\Delta G = G - G_{\text{min}} = \left(\frac{\partial G}{\partial T}\right)_V \Delta T + \frac{1}{2} \left(\frac{\partial^2 G}{\partial T^2}\right)_V (\Delta T)^2$$

where $\Delta T = T - T_0$

Evaluate terms at $T = T_0$

$$\left(\frac{\partial G}{\partial T} \right)_V = 0, \quad \left(\frac{\partial^2 G}{\partial T^2} \right)_V > 0$$

T_0 ≈ 0

• $G = U - TS + PV \quad G_0 @ T_0, P_0$

• $G_0 = U_0 - T_0 S + P_0 V$

$\left(\frac{\partial G_0}{\partial T} \right)_V = \left(\frac{\partial U}{\partial T} \right)_V - T_0 \left(\frac{\partial S}{\partial T} \right)_V = 0 \quad @ T = T_0$

$$dU = TdS - PdV \quad \therefore \left(\frac{\partial U}{\partial T} \right)_V = T \left(\frac{\partial S}{\partial T} \right)_V$$

$$\left(\frac{\partial G}{\partial T} \right)_V = \left(\frac{\partial U}{\partial T} \right)_V - T_0 \left[\frac{1}{T} \left(\frac{\partial U}{\partial T} \right)_V \right]$$

$$\boxed{\left(\frac{\partial G_0}{\partial T} \right)_V = \left(\frac{\partial U}{\partial T} \right)_V \left[1 - \frac{T_0}{T} \right]}$$

• Evaluate $\left(\frac{\partial^2 G_0}{\partial T^2} \right)_V = \left(\frac{\partial}{\partial T} \right) \left(\frac{\partial G_0}{\partial T} \right)_V = \frac{T_0}{T^2} \left(\frac{\partial U}{\partial T} \right)_V + \left(1 - \frac{T_0}{T} \right) \left(\frac{\partial^2 U}{\partial T^2} \right)_V > 0$

at $T = T_0$

$\frac{T_0}{T^2} \left(\frac{\partial U}{\partial T} \right)_V > 0$

$\left(\frac{\partial U}{\partial T} \right)_V > 0$

$c_v > 0$

if heat cap > 0 , then
stable around ΔT

Le Chatelier's Principle

April 3, 2019

If a system in eq. is disturbed, it will respond in a (stable) way to restore itself back to equilibrium.

Result for V changes

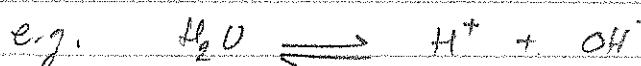
$$\begin{array}{c} G_A \\ \downarrow \\ G_{\min} + \curvearrowright \\ \uparrow v_0 \quad \rightarrow v \end{array} \quad \left(\frac{\partial^2 G}{\partial v^2} \right)_{T=T_0} = - \left(\frac{\partial P}{\partial v} \right)_T > 0$$

$$K_T = \frac{-1}{v} \left(\frac{\partial v}{\partial P} \right)_T$$

$$\frac{1}{K_T} > 0 \text{ or simply } K_T > 0$$

Chemical Equilibrium

Can we Gibbs to determine equilibrium condition...

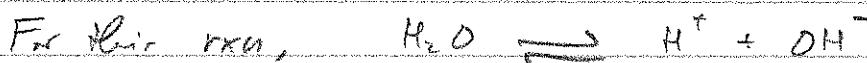


Mixture of $H_2O + \text{ions}$ is most stable state (lower G)

$$G = U - TS$$

e.g. $\Delta G = 0$. Ions have a higher entropy. But additional entropy of mixing makes the mixture more stable.

e.g., $dG = \delta H - TdS = \mu H - \sum_i \mu_i dN_i = \sum_i \mu_i dN_i$



$$dN_{H_2O} = -1, \quad dN_H^+ = +1, \quad dN_{OH^-} = +1 \quad \text{In e.g., } dG = 0 = \sum_i \mu_i dN_i$$

$$\text{Eq 1} \quad -\mu_{H_2O}^{\circ} \cdot \mu_{OH^-} + \mu_H^{\circ} = 0$$

$$\text{Eq 2} \quad \boxed{\mu_{OH^-} + \mu_H^{\circ} = \mu_{H_2O}^{\circ}}$$

More generally, $\gamma_1 X_1 + \gamma_2 X_2 + \dots \rightleftharpoons \gamma_3 X_3 + \gamma_4 X_4 + \dots$

$\gamma_i \rightarrow$ stoichiometric coefficient of species i

$$\text{In eq, } \boxed{\gamma_1 \mu_1 + \gamma_2 \mu_2 + \dots = \gamma_3 \mu_3 + \gamma_4 \mu_4 + \dots}$$

The rxn $H_2O \rightleftharpoons H^+ + OH^-$ produces a solution, which is a mixture of a solvent (primary component) + solute (secondary comp.)

Q3 Dilute solution { # of solute molecules \ll # of solvent molecules
 { const solute molecules don't interact
 with each other
 \rightarrow can treat them as an ideal gas!

Q4 Need to calculate μ for solvent & solute in order to predict eq.

Hypo we have pure water... 100% H_2O ... solvent, A $\xrightarrow{\text{"pure"}}$

$$G = N_A \mu_A = N_A \mu_A^{\circ}(T, P) \quad \mu_A^{\circ}: \text{chem. pot. of pure solvent}$$

Add a single B molecule (solute), holding T, P fixed

$$dG = \underbrace{dU}_{\downarrow \text{index of } N_B} + \underbrace{PdV}_{\text{only dep in } N_B} - \underbrace{TdS}_{\text{dep in } N_A} \quad \rightarrow \text{dep in } N_A \quad (S \propto N_A)$$

$dS = k \ln N_A - \text{additional terms index of } N_A$

$$\text{Eq 6} \quad \boxed{dG = -kT \ln N_A + f(T, P)} \quad \begin{matrix} \text{for adding 1 mole} \\ \text{index of } N_A \end{matrix}$$

Adding 2 B molecules ...

$$\text{Gross} \rightarrow dG' = 2dG = 2 \left[f(T, P) - kT \ln N_A \right] \quad (\times)$$

But B molecules indistinguishable.

↳ needs to be divided by $2!$ \rightarrow indistinguishable
b...

$$\begin{aligned} dG' &= 2f(T, P) - T \left[2k \ln N_A - k \ln 2 \right] \\ &= 2f(T, P) - 2k \ln N_A + k \ln 2 \end{aligned}$$

Generalizing (for N_B molecules) $kT N_A \ln N_B - kT N_B$

$$dG = N_B f(T, P) - N_B kT \ln N_A + kT \ln(N_B!)$$

Free Solvent

$$G = N_A \mu^\circ(T, P)$$

Dilute Solution $G + dG$

Solution

$$\begin{aligned} G &= N_A \mu^\circ(T, P) + N_B f(T, P) - N_B kT \ln N_A \\ &\quad + N_B kT \ln N_B - N_B kT \end{aligned}$$

valid if $N_B \ll N_A$ (dilute solution.)

Since, $\mu = \left(\frac{\partial G}{\partial N} \right)_{T, P}$ we can write for $\mu_A \neq \mu_B$

$$\mu_A = \left(\frac{\partial G}{\partial N_A} \right)_{T, P, N_B} = \mu^\circ(T, P) - N_B kT / N_A \quad \begin{array}{l} \rightarrow \text{chem. pt.} \\ \text{of solvent} \end{array}$$

$$\mu_B = \left(\frac{\partial G}{\partial N_B} \right)_{T, P, N_A} = f(T, P) - kT \ln N_A - kT + kT + kT \cdot \ln \frac{N_B}{N_A} \quad \begin{array}{l} \rightarrow \text{chem. pt.} \\ \text{of solute} \end{array}$$

April 5, 2019

Recall ① Started with G for pure solvent (A)

$$G = \mu^\circ(T, P) N_A$$

② Add solute particles (B) to this

$$dG = \underbrace{dV + PdV - TdS}_{\text{some terms dep. on } N_A}$$

time \rightarrow dep. of N_A

$f(T, P)$ independent of N_A

$$\underline{\Delta} S = \frac{N_A!}{N_B!(N_A-N_B)!}, \text{ and since } N_A > N_B \Rightarrow \underline{\Delta} S \approx \frac{N_A^{N_B}}{N_B!}$$

$$\begin{aligned} \underline{\Delta} S &= k \ln \underline{\Delta} S = k \ln \left[\frac{N_A^{N_B}}{N_B!} \right] = k \ln (N_A^{N_B}) - k \ln (N_B!) \\ &\approx N_B k \ln (N_A) - N_B k \ln N_B + N_B k \end{aligned}$$

Now, $G = G_A + dG$

$$\underline{\Delta} G = N_B f(T, P) - N_B k T \ln N_A + k T \ln N_B - N_B k T$$

$$\underline{\Delta} \boxed{G = \mu^\circ(T, P) N_A + N_B f(T, P) + N_B k T \ln \left(\frac{N_B}{N_A} \right) - N_B k T}$$

Now,

$$\begin{aligned} \mu &= \left(\frac{\partial G}{\partial N} \right)_{T, P} \Rightarrow \left\{ \begin{aligned} \mu_A &= \left(\frac{\partial G}{\partial N_A} \right)_{T, P} = \mu^\circ(T, P) - \frac{N_B k T}{N_A} \\ &\quad (\text{solvant}) \end{aligned} \right. \\ \mu_B &= \left(\frac{\partial G}{\partial N_B} \right)_{T, P} = f(T, P) + k T \ln \frac{N_B}{N_A} \quad (\text{solute}) \end{aligned}$$

Definition

"Molarity" \rightarrow # moles of solute per kg of solvent.

$$m = \frac{\text{moles solute}}{\text{kg solvent}} \propto \frac{N_B}{N_A}$$

Re-writing μ_B in terms of m : \rightarrow absorbed - extra term ...

$$\star \mu_B = f(T, P) + RT \ln(m_B) \quad (1)$$

$\star \mu_B^\circ(T, P) \rightsquigarrow$ standard condition for molality $\approx 1 = m_B$

So when $m_B = 1 \rightarrow \boxed{\mu_B = \mu_B^\circ(T, P) + RT \ln(m_B)}$

Example Dissociation of water



Treat as dilute solution + solvent H_2O

$$\star \mu_{H_2O} = \mu_{H_2O}^\circ(T, P) - N_A \frac{kT}{N_A} \left(\frac{N_H^+ kT}{N_A} + \frac{N_{OH^-} kT}{N_A} \right)$$

$$\star \mu_{H^+} = \mu_{H^+}^\circ(T, P) + RT \ln(m_{H^+})$$

$$\star \mu_{OH^-} = \mu_{OH^-}^\circ(T, P) + RT \ln(m_{OH^-})$$

at room temp, $kT \approx 4 \times 10^{-21} J$

$$\star \mu_{H_2O} = \mu_{H^+} + \mu_{OH^-} \Rightarrow \mu_{H_2O} - \mu_{H^+} - \mu_{OH^-} = 0$$

$$\Rightarrow \mu_{H_2O}^\circ = \mu_{H^+}^\circ + \mu_{OH^-}^\circ = RT \ln(m_{H^+}) + RT \ln(m_{OH^-}) \\ = RT \ln(m_{H^+} \cdot m_{OH^-})$$

$$\text{So } -N_A \left[\mu_{H^+}^\circ + \mu_{OH^-}^\circ - \mu_{H_2O}^\circ \right] = RT \ln(m_{H^+} \cdot m_{OH^-})$$

$$\boxed{-\Delta G^\circ = RT \ln(m_{H^+} \cdot m_{OH^-})}$$

Ex ΔG° dissociation of water = 29.9 kJ/mol

Now

$$\Rightarrow m_{H^+} \cdot m_{OH^-} = e^{-\Delta G^\circ / RT}$$

K equilibrium constant

For room temp & standard P,

$$K_{H_2O} = 10^{-14}$$

$$\text{So } m_{H^+} \cdot m_{OH^-} = 10^{-14} = (m_{OH^-})^2 = (m_{H^+})^2$$

$$\text{So } m_{H^+} = m_{OH^-} = 10^{-7} \text{ mol/kg H}_2\text{O}$$

$$\text{pH} = -\log_{10}(m_{H^+}) \Rightarrow \text{pH} = 7 \text{ for "pure" H}_2\text{O}$$

{ if fewer H⁺ conc. then basic, pH ↑ }
 { if more H⁺ conc. then acidic, pH ↓ }

partial pressure



$$\text{Treat as ideal gas: } \mu(T, P) = \mu^\circ(T) + \cancel{RT \ln(P/P_0)}$$

std. atm. pressure

$$(\mu_p^\circ + \mu_e^- - \mu_H^\circ) = RT \ln\left(\frac{P_H}{P_0}\right) - RT \ln\left(\frac{P_e^-}{P_0}\right) - RT \ln\left(\frac{P_e^+}{P_0}\right)$$

⇒

$$-\Delta G^\circ = N_A RT \ln \left[\frac{P_H P_0}{P_e^+ P_e^-} \right] \Rightarrow \frac{RT}{P_0}$$

$$\text{So recall, for ideal gas } \mu^\circ = -RT \ln \left[\frac{1}{N} \left(\frac{2\pi mkT}{h^2} \right)^{3/2} \right]$$

But μ for H should be less than -13.6 eV when at rest ($kE=0$)

$$\therefore \mu_H^0 = -kT \ln \left[\frac{kT}{P_0} \left(\frac{2\pi m_e kT}{h^2} \right)^{3/2} \right] = -13.6\text{ eV}$$

At 0K Rest p^+ , e^- unbound \rightarrow

$$\therefore \mu_{p^+}^0 = -kT \ln \left[\frac{kT}{P_0} \left(\frac{2\pi m_p kT}{h^2} \right)^{3/2} \right]$$

$$\mu_{e^-}^0 = -kT \ln \left[\frac{kT}{P_0} \left(\frac{2\pi m_e kT}{h^2} \right)^{3/2} \right]$$

Now, $m_H \approx m_e$

$$\therefore \mu_{p^+}^0 + \mu_{e^-}^0 - \mu_{H^0}^0 = -kT \ln \left(\frac{kT}{P_0} \left(\frac{2\pi m_e kT}{h^2} \right)^{3/2} \right) + 13.6\text{ eV}$$

Therefore,

$$-\ln \left(\frac{P_H P^0}{P_p + P_e^-} \right) = \ln \left(\frac{kT}{P_0} \left(\frac{2\pi m_e kT}{h^2} \right)^{3/2} \right) - \frac{13.6\text{ eV}}{kT}$$

$$\therefore \left(\frac{P_H P^0}{P_p + P_e^-} \right)^{-1} = \frac{kT}{P_0} \left(\frac{2\pi m_e kT}{h^2} \right)^{3/2} \cdot e^{-13.6\text{ eV}/kT}$$

$$\therefore \frac{P_H + P_e^-}{P_H} = \frac{kT}{P_0} \left(\frac{2\pi m_e kT}{h^2} \right)^{3/2} \cdot e^{-13.6\text{ eV}/kT}$$

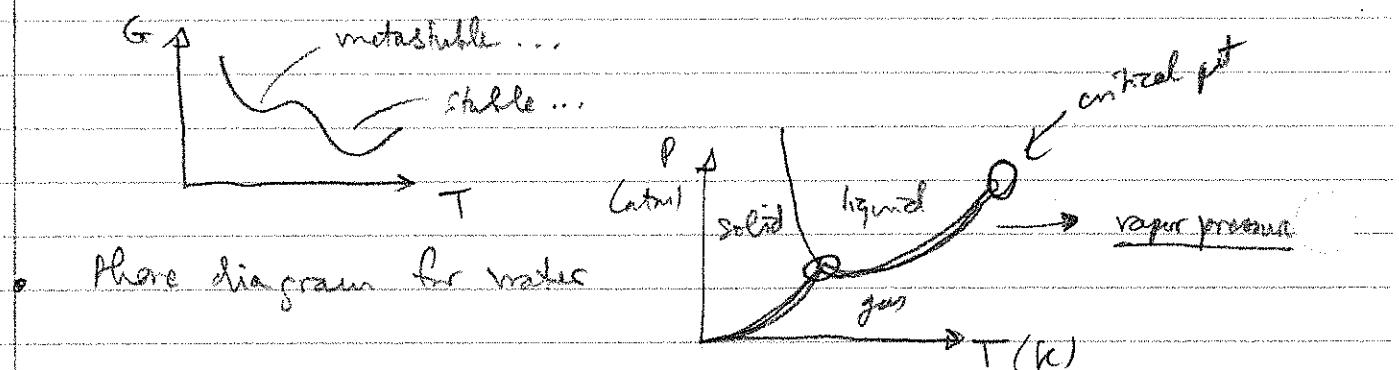
$$\therefore \frac{P_H^+}{P_H} = \frac{kT}{P_0} \left(\frac{2\pi m_e kT}{h^2} \right)^{3/2} \cdot e^{-13.6\text{ eV}/kT} \quad \text{Saha Eqn}$$

$$\frac{Np^+}{NH}$$

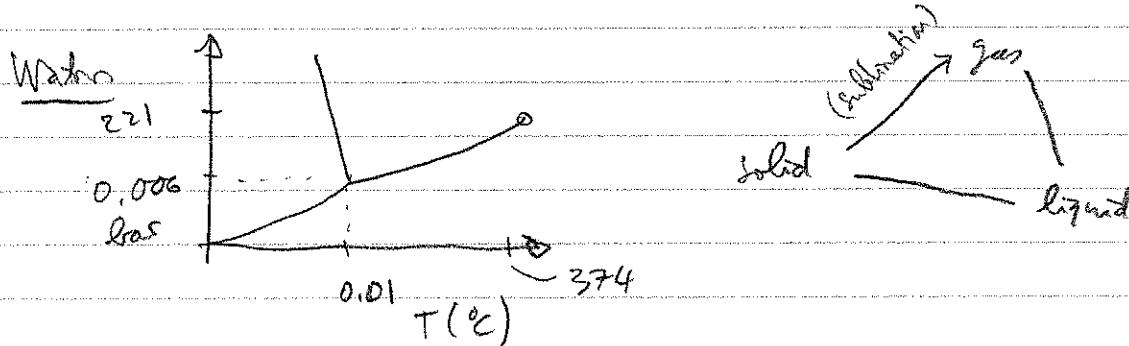
PHASE TRANSFORMATION

- def { A continuous change in property of matter as its environment changes infinitesimally.
- Phases { different states of matter - or unique structural arrangement of atoms within matter.
- Can depend on many variables : eg: P, T, B, ...

↳ Gibbs free energy is key to understanding these...

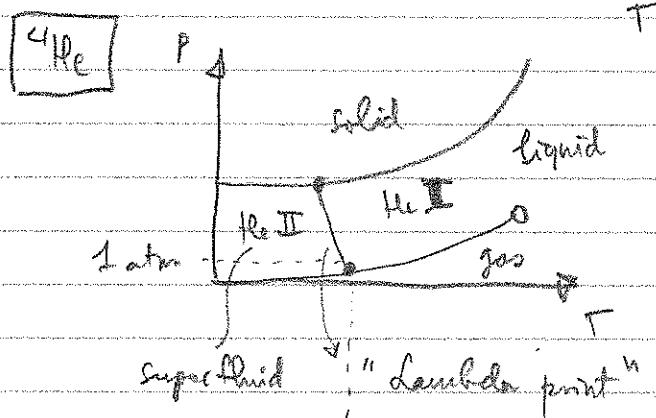
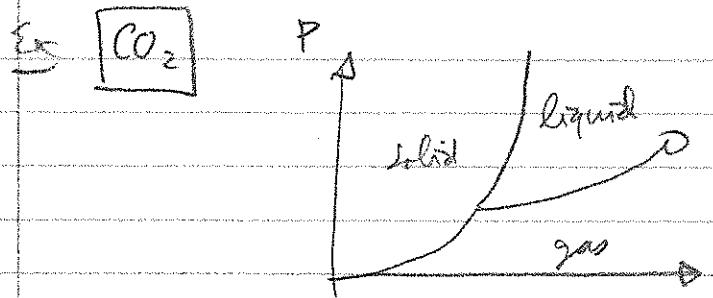


- Vapor pressure \rightarrow pressure at which liquid or solid phase can coexist with gas
- Triple point \rightarrow precise T, P at which all 3 phases (liquid, gas, solid) can coexist + -



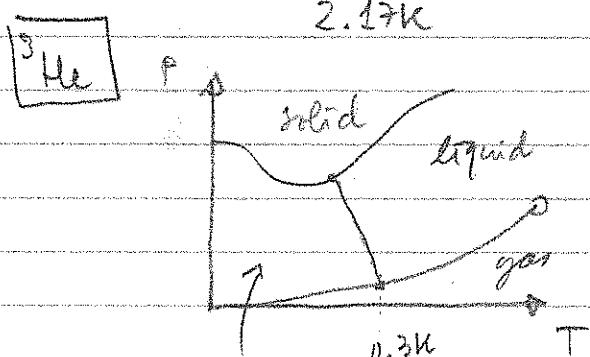
- Critical point As P or T increases, we reach a point where liquid & gaseous phases are indistinguishable.

Ex plasma --



${}^4\text{He}$ is a superfluid below the Lambda point (at 2.17K)

Superfluid \rightarrow zero viscosity
zero entropy
high conductivity



2 superfluid phases:

Other variable that can change phase diagram:

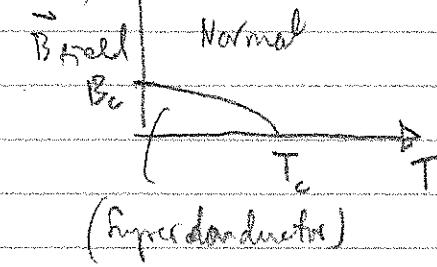
- chemical composition:

- external magnetic field strength \rightarrow (Type I superconductor)
(0 resistance)

(Type I superconductor)

Typical $B_c \sim 0.01 - 0.1 \text{ T}$

$T_c \sim 20 \text{ K}$



Axide Type II - Superconductor

B_{C2} > B_{C1}

B_{C2}

B_{C1}

Normal

mix

B_{C2}

B_{C1}

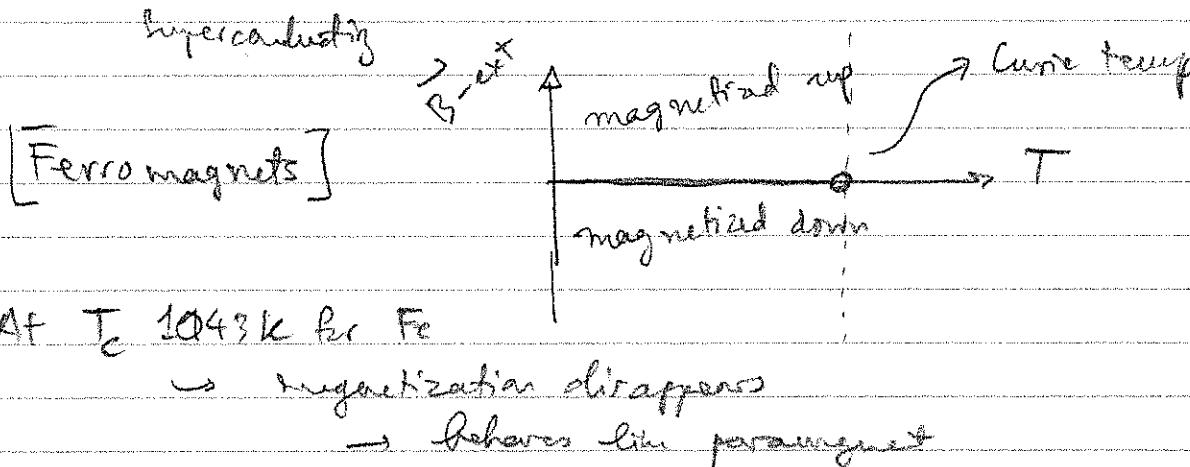
T_c

$B_{C2} \gg B_{C1}$

1

25T

$T_c \sim 10K \sim 90K$



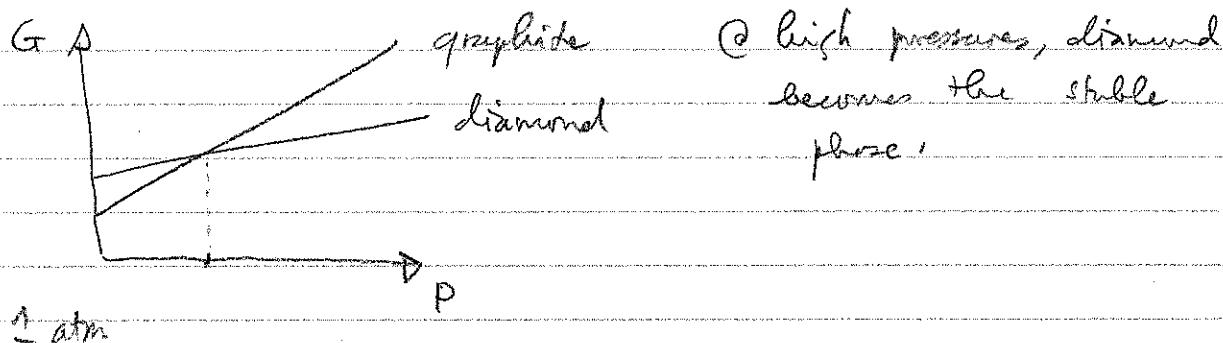
Q Using Gibbs free energy to evaluate stable phase for substances

$$\delta G = -SdT + VdP + \mu dN$$

$$S \left(\frac{\partial G}{\partial T} \right)_{P,N} = -S \quad ; \quad \left(\frac{\partial G}{\partial P} \right)_{T,N} = V$$

E Diamond vs Graphite, dash up $\Delta_f G$ for both from $T = 1$ atm

$\Delta_f G_{graphite}$ is 2900 J less than $\Delta_f G_{diamond}$ @ 218 K, 1 atm

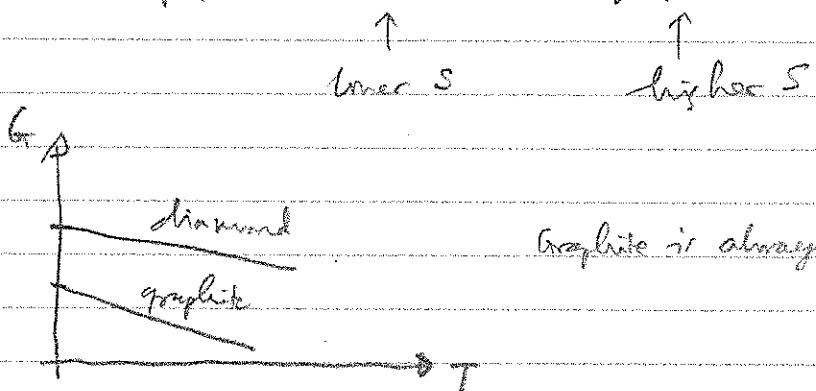


(III)

New look at T dependence

$$\left(\frac{\partial G}{\partial T}\right) = -S \text{ as } T \uparrow, G \downarrow$$

Entropy of diamond vs graphite



298K



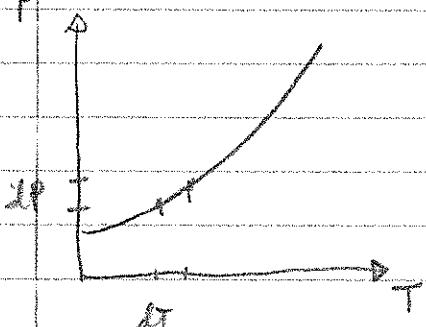
Clausius - Clapeyron relation

Since $\left(\frac{\partial G}{\partial T}\right)_{P,N} = -S$, $\left(\frac{\partial G}{\partial P}\right)_{T,N} = +V$ then slope of the phase boundary line on P.v.T diagram is related to $S \propto V$ of the two phases...

→ assume 1 mole of substance

On the boundary $\Delta G_1 = \Delta G_2$

P



increase P & T at 2 phases remain in eq.

$$\Delta G = -SdT + VdP + \mu dN$$

$$\therefore SdT = VdP \dots$$

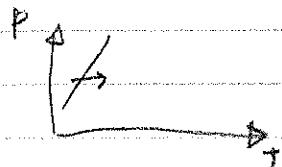
$$\Delta G_1 = -S_1dT + V_1dP$$

$$\Delta G_2 = -S_2dT + V_2dP \quad \text{I equal}$$

$$\text{So } (V_g - V_e) dP = (S_g - S_e) dT$$

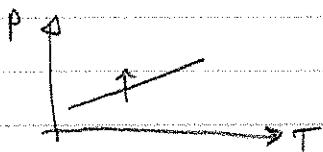
$$\frac{dP}{dT} = \frac{S_g - S_e}{V_g - V_e}$$

- if we have a large entropy difference between phases
→ steep slope...



$\frac{dP}{dT}$ steep: Small T changes will change the phase...

- if large volume difference



$\frac{dP}{dT}$ shallow: Small P change will change phase.

Reminder $\Delta G = \frac{\partial Q}{T} = \frac{L}{T}$

$$\frac{dP}{dT} = \frac{L}{T\Delta V}$$

L: total latent heat of vaporization
 $\Delta V = V_g - V_e$

Clausius - Clapeyron Eqn.

$L = \text{f.m.} \rightarrow \text{extensive}$ } \Rightarrow ratio $\frac{L}{\Delta V} = \text{intensive}$,
 $\Delta V = \text{extensive}$

Example Use Clausius - Clapeyron to explain why H₂O has negative $\frac{dP}{dT}$ between solid - liquid phases.

$$\frac{dP}{dT} = \frac{L}{T\Delta V} = \frac{\Delta S}{\Delta V}$$

$$\rho_{\text{ice}} = 917 \text{ kg/m}^3, \rho_{\text{liquid}} = 1000 \text{ kg/m}^3 \rightarrow \text{one mol of H}_2\text{O}$$

$$V_e = m/p = \frac{1000\text{kg}}{1000\text{kg/m}^3} = 1\text{m}^3 \quad V_{l,e} = \frac{1000\text{kg}}{917\text{kg/m}^3} = 1.09\text{m}^3$$

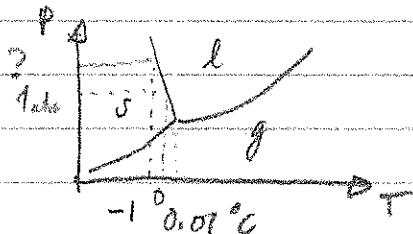
$$(V_e - V_s) = -0.09\text{m}^3$$

As we go from ice to water, $V \downarrow, ST$

$\therefore \frac{dT}{dP}$ is negative

Assume L is constant with P, T : $\frac{dP}{dT} = \frac{3335\text{J/g} \times 10^6\text{g}}{(273\text{K})(-0.09\text{m}^3)} = -1.35 \times 10^9 \text{ Pa/K}$

How much pressure is required to melt ice at -1°C ?

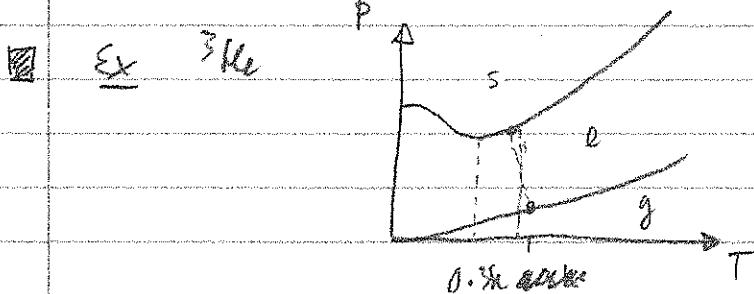


$$\frac{dP}{dT} = -1.35 \times 10^9 \text{ Pa/K}$$

$$dP = (-1.35 \times 10^9 \text{ Pa/K})(-1\text{K})$$

$$dP = 1.35 \times 10^9 \text{ Pa} \approx 135 \text{ atm}$$

$$\approx 135 \text{ bar}$$



- At $T < 0.3\text{K}$, slope between solid - liquid is negative

- Which phase is more dense? Recall that $\left(\frac{\partial G}{\partial T}\right)_{P,N} = V$

Solid ^3He is stable phase at high P , so it must have smaller V . Smaller dV/dP
 \rightarrow Solid is more dense.

Q: Which phase has more entropy?

$$\frac{dP}{dT} = \frac{\Delta S}{\Delta V} < 0 \text{ @ } T < 0.3k$$

if $V \downarrow$ as we go $l \rightarrow s$, $S \uparrow$ as we go from $l \rightarrow s$

so solid ^3He has more entropy.

Q: What is the slope of the phase boundary at $T=0$?

3rd law: As $T \rightarrow 0\text{K}$, $S \rightarrow$ minimum value.

$\therefore \Delta S = 0$ between the phases @ $T=0$

$$\frac{dP}{dT} = \frac{\Delta S}{\Delta V} \rightarrow \frac{dP}{dT} = 0 \rightarrow \text{slope of phase boundary goes away.}$$

April 10, 2019

The van der Waals model

Ideal gas: $PV = nRT = NkT \rightarrow$ want to correct for finite volume of molecules & attractive forces between particles

$$\left(P - \frac{\alpha N^2}{V^2} \right) (V - Nb) = NkT \quad \text{van der Waals equation.}$$

Two modifications:

- ① $V \rightarrow V - V_0 \rightarrow$ can't compress gas to $V=0$
 "b" represents volume per particle
 min volume = Nb @ $P=\infty$

② $P \rightarrow P + \frac{\alpha N^2}{V^2}$ accounts for short range attractive forces between molecules

$$P = \frac{NkT}{V - Nb} - \frac{\alpha N^2}{V^2}$$

Imagine being at $T=0$, frozen thermal motion. \Rightarrow no KE, but still has potential energy.

$$PE \text{ of molecule} \propto N/V \Rightarrow PE_{\text{g}} \propto \frac{N}{V} \cdot N$$

$$\Rightarrow PE_{\text{eff}} = -\frac{aN^2}{V}, \text{ negative since it works against KE}$$

• "a" constant depending on type of molecule \rightarrow $a > 0$

$$\bullet \text{To calculate } P, dU = TdS - PdV \Rightarrow P = -\left(\frac{\partial U}{\partial V}\right)_{T,N}$$

• Contribution to P from PE

$$\hookrightarrow P = -\left(\frac{\partial}{\partial V}\left(-\frac{aN^2}{V}\right)\right)_{T,N} \Rightarrow \boxed{P = \frac{NkT}{V-Nb} - \frac{aN^2}{V^2}}$$

$$\text{Ex Molecular Interaction } H_2O : b \approx 6 \times 10^{-24} \text{ m}^3 \sim (4 \text{ \AA})^3$$

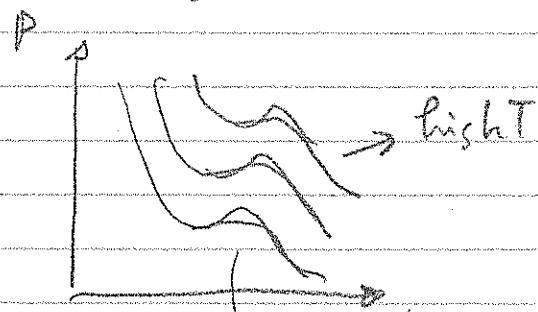
N_2 similar

$$a \text{ varies between molecules... } N_2 : a \approx 2.5 \text{ eV A}^3$$

$$H_2O \approx a_{N_2} \text{ due to dipole interaction}$$

$H_2 : a_{K_2} < a_{N_2}$ (cancellation)

Consequences of vdW model



For a given T , plot P vs. V .

\Rightarrow Multiple possible V 's for a given P, T

Use G to find which volume is stable

$$\delta G = -SdT + VdP + \mu dN, \text{ for } T, N \Rightarrow \left(\frac{\partial G}{\partial V}\right)_{T,N} = V \left(\frac{\partial P}{\partial V}\right)_{T,N}$$

$$P = \frac{NkT}{V-Nb} - \frac{aN^2}{V^2} \quad \text{so,}$$

$$V \left(\frac{\partial P}{\partial V} \right)_{T,N} = V \frac{\partial}{\partial V} \left[\frac{NkT}{V-Nb} - \frac{aN^2}{V^2} \right]$$

$$= V \left[\frac{-NkT}{(V-Nb)^2} + \frac{2aN^2}{V^3} \right]$$

$$\Rightarrow \left(\frac{\partial G}{\partial V} \right)_{T,N} = -\frac{NkTV}{(V-Nb)^2} + \frac{2aN^2}{V^2}$$

$$\therefore \int dG = \int [] dV$$

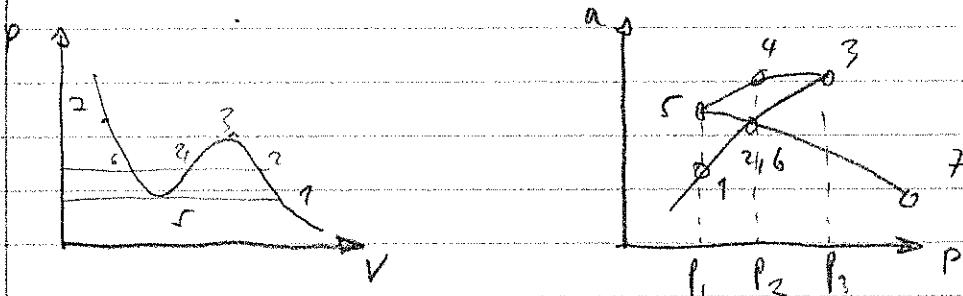
$$= \int \frac{-NkT(V-Nl+Nb)}{(V-Nl)^2} + \frac{2aN^2}{V^2} dV$$

$$= \int \frac{-NkT(V-Nl)}{(V-Nl)^2} - \frac{NkT}{(V-Nl)^2} + \frac{2aN^2}{V^2} dV$$

constant
 \int of int

$$\rightarrow G = -NkT \ln(V-Nl) + \frac{NkT(Nb)}{(V-Nl)} - \frac{2aN^2}{V} + c(T)$$

Want to know G vs. P



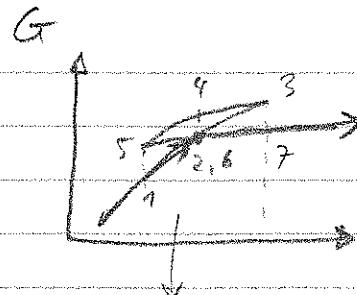
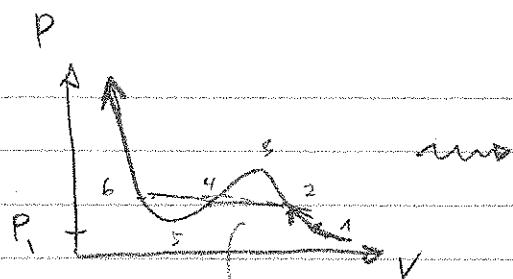
- J₂ & J₅ are inadmissible.
- Substance will go directly from vol ② → vol ⑥ as it's compressed
- Discontinuity = phase change

$$\Delta G \text{ around loop} = 0 \quad \int_{\text{loop}} dG = 0, \quad \left(\frac{\partial G}{\partial P} \right)_T = V \Rightarrow \int \left(\frac{\partial G}{\partial P} \right)_T dP = 0$$

So $0 = \int_{\text{loop}} V dP$

Recall, νdW

April 12, 2019



discontinuity

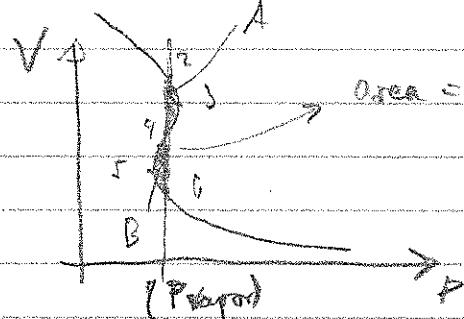
continuity

→ phase transition :-

$$\int_{\text{loop } 2-6} dG = 0 = \int_{\text{loop } 2-6} dG_2 - 0 \quad \text{where } dG_2 = -SdT + PVdV$$

$$\hookrightarrow \left(\frac{\partial G}{\partial P}\right)_{T,N} = V$$

$$\Leftrightarrow \int_{\text{loop } 2-6} VdP_T = 0$$

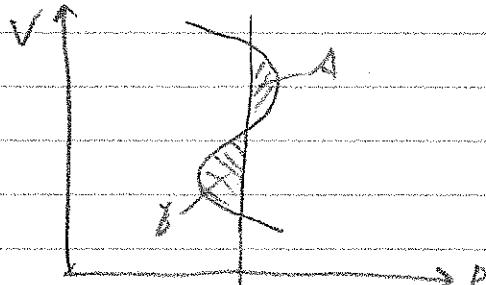


flip areas :-

→ area (A) = area (B) for $\int VdP_T = 0$

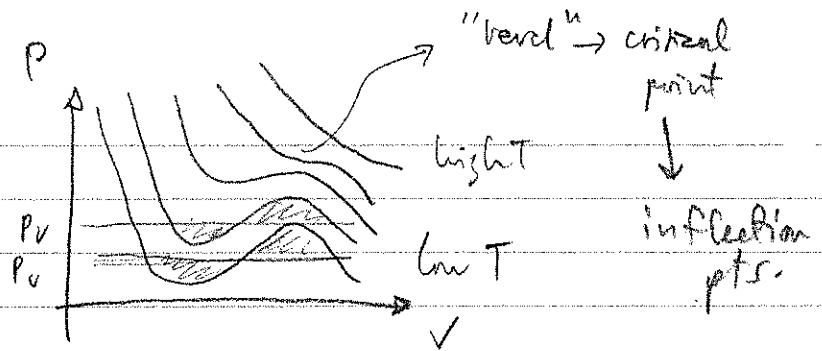
\hookrightarrow [Maxwell's construction]

⇒ P of phase transition occurs where vertical P divides the area in equal halves



P_{max}

Isotherms @ different T

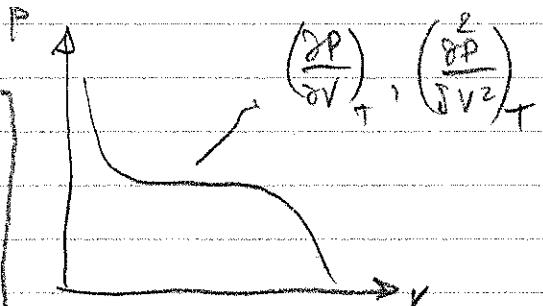


↳ by finding P_{cav} based on Isotherms... --

↳ ↑ liquid & gas on critical point.

$$(\text{Critical point}) \rightarrow \left\{ \begin{array}{l} \left(\frac{\partial P}{\partial V} \right)_T = 0 \\ \left(\frac{\partial^2 P}{\partial V^2} \right)_T = 0 \end{array} \right\}$$

$$\left(\frac{\partial^2 P}{\partial V^2} \right)_T = 0$$



$\left\{ T_c = \text{critical temp} \right. \left. \Rightarrow \text{where 1st \& 2nd desire of } \frac{\partial P}{\partial V} \text{ wrt } V \text{ are zero.} \right\}$

PHASE TRANSFORMATION
OF MIXTURES

(§ 5.4)

Start with G $G = U - TS + PV$

Consider a mixture of 2 substances A : B

A	B
---	---

in thermal + mech. equilibrium

$$\rightarrow T_A = T_B \quad \rightarrow \quad P_A = P_B$$

$$\text{Then } G_{\text{tot}} = G_A + G_B \quad \text{Let } x = \frac{\# B}{\Sigma} \rightarrow 1-x = \frac{\# A}{\Sigma}$$

Can write $G_A^\circ = \text{Gibbs free energy of pure A}$ ($x=0$)
 $G_B^\circ = \text{Gibbs free energy of pure B}$ ($x=1$)

Remove partition & let A + B mix in V, T

$$G = U - TS + PV, \text{ Assume these changes are small}$$

$$\Delta G = \Delta U - T\Delta S + PV$$

Initially, $G_{\text{tot}}^{\circ} = (1-x)G_A^{\circ} + xG_B^{\circ}$

Recall, $\Delta S_{\text{mixing}} = -Nk \left[x \ln x + (1-x) \ln (1-x) \right]$

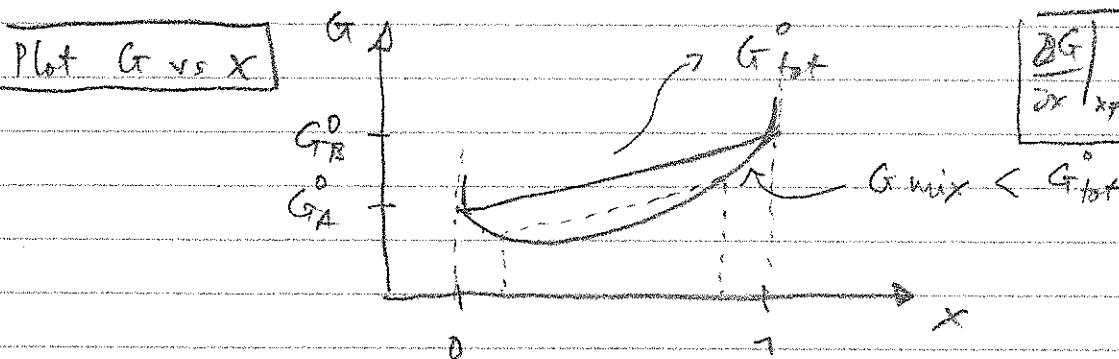
So assuming $\Delta U = 0, \Delta V = 0$, then,

$$G_{\text{mixed}} = G_{\text{tot}}^{\circ} + T\Delta S$$

$$= G_{\text{tot}}^{\circ} + NkT \left[x \ln x + (1-x) \ln (1-x) \right]$$

$$G_{\text{mixed}} = (1-x)G_A^{\circ} + xG_B^{\circ} + NkT \left[x \ln x + (1-x) \ln (1-x) \right] \quad \downarrow < 0$$

→ we call this an ideal mixture → derived from ideal gas...



$$\left. \frac{\partial G}{\partial x} \right|_{x \neq 0, 1} = \infty$$

- slope of G vs x @ $x=0, 1$ is ∞

- mixture (mixed) is always more stable bc of entropy of mixing.

Phase changes of mixtures

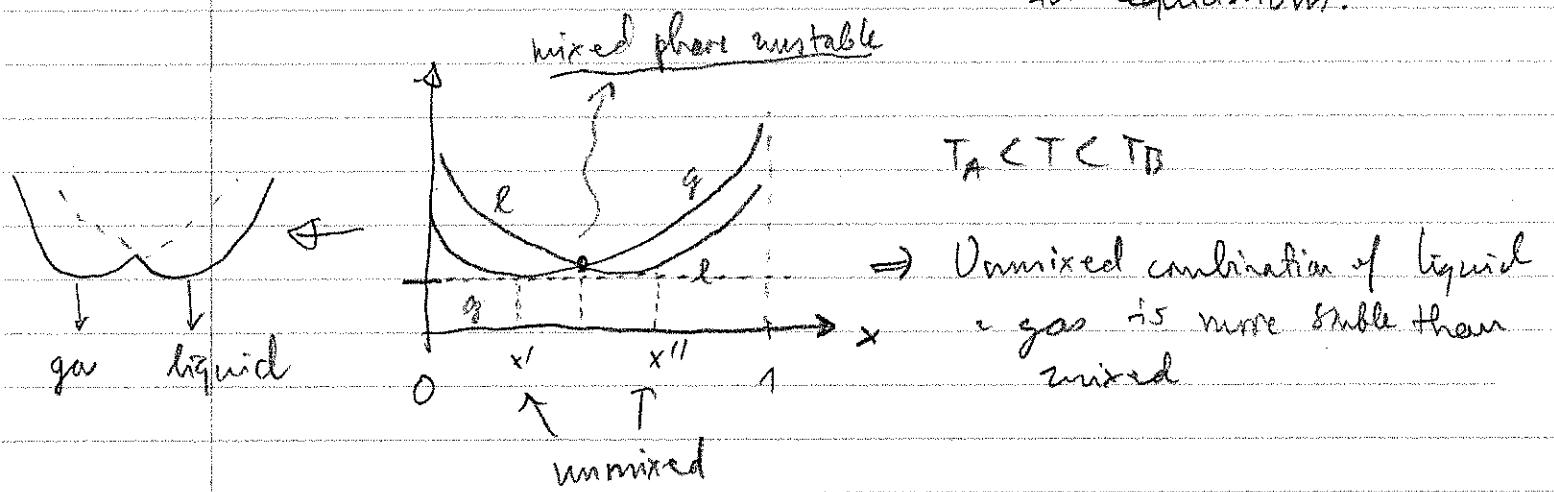
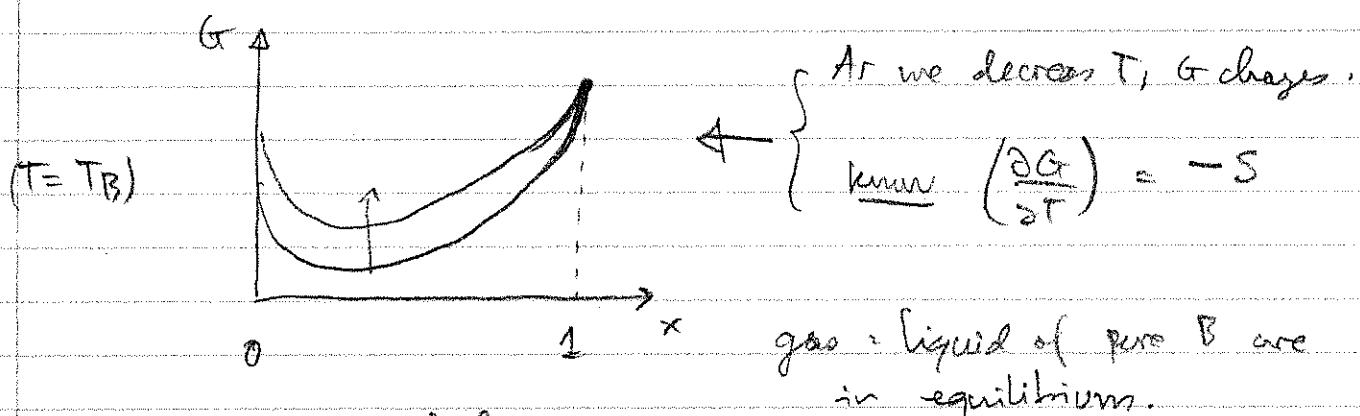
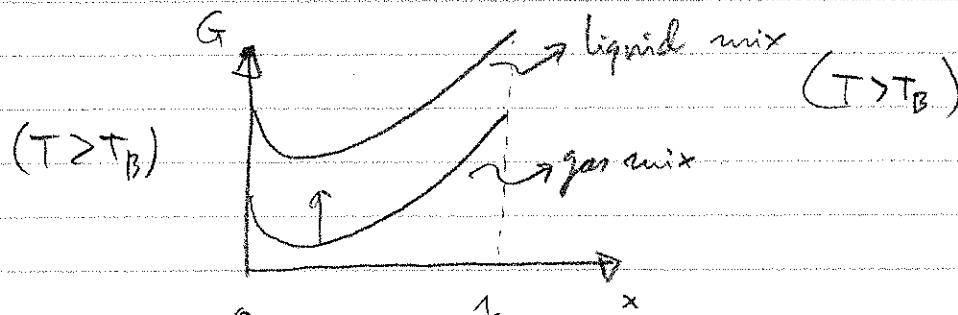
e.g. $N_2 + O_2$

Let T_A = boiling point of pure substance A

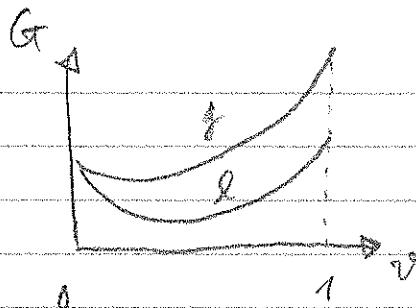
T_B = boiling point of pure substance B

Let $T_B > T_A$. Then at high temp. $T > T_B > T_A$

→ stable phase is a gas regardless of composition.



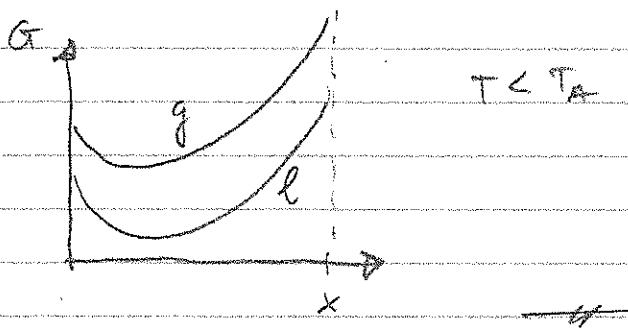
Decrease T further...



(crossed)

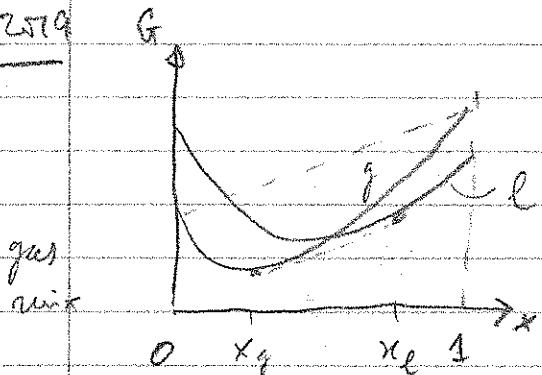
$T < T_A \Rightarrow$ liquid stable

for pure A

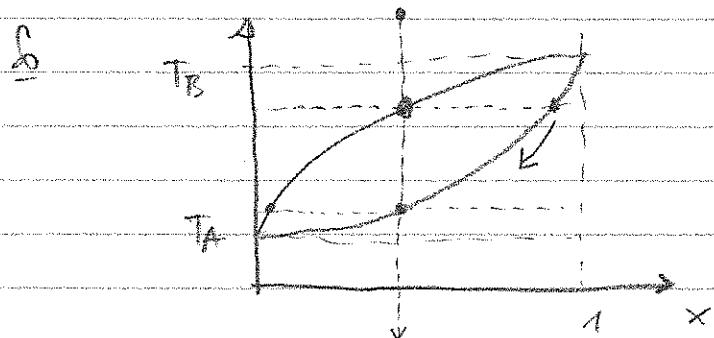
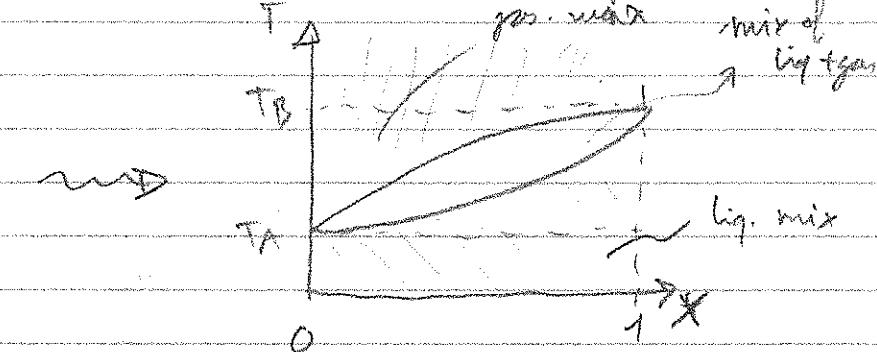


$T < T_A$ no liquid mixed is stable

Jul 15, 2019

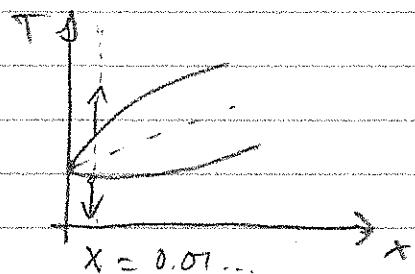


gas mix



as we go down
in temp

For dilute solutions, x is small. Thus solvent does not evaporate as gas is pure solvent



~ only need equilibrium condition for solvent.

A = solvent, B = solute

$\mu_{A, \text{liq}}(T, P) = \mu_{A, \text{gas}}(T, P) \rightarrow A \text{ in equil.}$

Solvent, $\mu_{A, \text{liq}}(T, P) = \mu_0(T, P) - \frac{N_B kT}{N_A}$

Also,

$$\mu_0(T, P) - \frac{N_B kT}{N_A} = \mu_{A, \text{gas}}(T, P)$$

Let T_0 be boiling point of pure solvent (A). Hold pressure steady, vary temperature around T_0 to see how μ changes.

$$\mu_0(T_0, P) + (T-T_0) \left(\frac{\partial \mu_0}{\partial T} \right) - \frac{N_B kT}{N_A} = \mu_{\text{gas}}(T_0, P) + (T-T_0) \left(\frac{\partial \mu_{\text{gas}}}{\partial T} \right)$$

at $T = T_0$, by assumption $\mu_{A, \text{gas}}(T_0, P) = \mu_{\text{gas}}(T_0, P)$ (e.g.,
(assuming gas is pure solvent))

Eq

$$(T-T_0) \left(\frac{\partial \mu_0}{\partial T} \right) - \frac{N_B kT}{N_A} = (T-T_0) \left(\frac{\partial \mu_{\text{gas}}}{\partial T} \right)$$

Also,

$$\mu = \frac{G}{N} \Rightarrow \frac{\partial \mu}{\partial T} = \frac{1}{N} \left(\frac{\partial G}{\partial T} \right)_{V, N} = -\frac{S}{N}$$

Eq

$$(T-T_0) \left(-\frac{S_{\text{liq}}}{N_A} \right) - \frac{N_B kT}{N_A} = (T-T_0) \left(-\frac{S_{\text{gas}}}{N_A} \right)$$

Eq

$$(T-T_0) \left[\frac{S_{\text{gas}}}{N_A} - \frac{S_{\text{liq}}}{N_A} \right] = \frac{N_B kT}{N_A}$$

Eq

$$(T-T_0) = \frac{N_B kT}{S_{\text{gas}} - S_{\text{liq}}} = \frac{N_B kT}{\Delta S} = \frac{N_B kT}{Q/T_0} = \frac{N_B kT T_0}{L}$$

$Q = L = \text{Latent heat}$

Assuming $T_0 \approx T$

$$\rightarrow T - T_0 = \frac{N_B kT_0^2}{L}$$

Eq

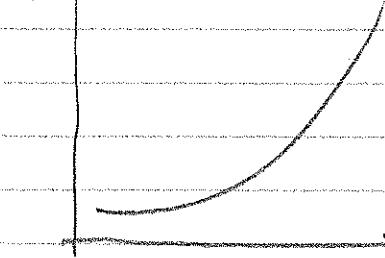
$$T - T_0 = \frac{N_B kT_0^2}{L}$$

shift in boiling
point of solvent
due to m. solute.

Shift in vapor pressure

... (derivation in book)

P ↑



Raoult's law

$$\frac{P}{P_0} = 1 - \frac{N_B}{N_A}$$

only for dilute solutions ...

Ch 6
nm

Boltzmann Statistics

\rightarrow

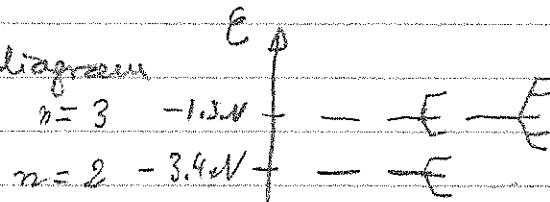
Goal: Get multiplicity for more complicated systems

Class "system" of a single atom is a reservoir of other atoms at some temperature T

- Macrostate = energy level. These energy levels are degenerate
 \rightarrow multiple microstates.

Ex hydrogen atom: n, l, m_l, m_s

- Energy level diagram



principal quantum number, $n \geq 1$

$l=0, l=1$

n is $\# \geq 1$

l : orbital angular momentum. l is $0, 1, \dots (n-1)$

m_l : z-component of orbital angular momentum

$$-l \leq m_l \leq l$$

m_s : z-component of spin angular momentum

$$m_s = \pm \frac{1}{2}$$

In general, for H, degeneracy is $[2n^2]$ for H

- Single atom exchanges energy with reservoir at temp T.
- Assumption \rightarrow all microstates within a given macrostate are equally probable.
- Macrostate of the atom + reservoir system with highest multiplicity should be most probable.

Remember : $P(A) = \frac{\# A}{\# S_A} \rightarrow \Sigma$

- Use ratios instead to avoid $\# S$. Take 2 possible states of atom s_1, s_2

$E(s_i)$ = Energy of atom in s_i

$E(s_2)$ = Energy of atom in s_2

$P(s_1)$ = prob. in s_1

$P(s_2)$ = prob. in s_2

Want state with highest multiplicity in combined atom + reservoir system \rightarrow most probable.

$S_R(s_i)$ \rightarrow multiplicity of reservoir when atom is in state s_i

$$P_R(s_i) \propto S_R(s_i) \Rightarrow \frac{P(s_2)}{P(s_1)} = \frac{S_R(s_2)}{S_R(s_1)} \quad S = k \ln S_R$$

$$S = k \ln R \rightarrow \boxed{\frac{P(s_2)}{P(s_1)} = \frac{e^{S_R(s_2)/k}}{e^{S_R(s_1)/k}} = e^{\underbrace{(S_R(s_2) - S_R(s_1))}_{\text{infinitesimal}}/k}}$$

$$\frac{dS}{T} = \frac{1}{R} [dW + PdV - n dN_R]$$

↑ ↑ ↓

equal & opposite
to the atoms ...

change in entropy of reservoir

$$\rightarrow PdV_K \sim (1\text{ A})^3 \text{ at 1 atm} \rightarrow (10^5 \text{ Pa})(10^{-10})^3 \approx 10^{-25} \text{ J}$$

$$dV_K \sim \text{few eV} \approx 10^{-19} \text{ J}$$

$\therefore PdV_K \ll dV_K \rightarrow \text{ignore.} \rightarrow dV_K \approx 0$

Also, $dN_K \approx 0$

reservoir

$$\therefore [S_p(s_2) - S_p(s_1)] = \frac{1}{k} [U_p(s_2) - U_p(s_1)]$$

atom ...

$$[S_p(s_2) - S_p(s_1)] = -\frac{1}{T_p} [E(s_2) - E(s_1)]$$

Now,

$$\frac{P(s_2)}{P(s_1)} = e^{-[E(s_2) - E(s_1)]/kT}$$

$$\frac{P(s_2)}{P(s_1)} = \frac{e^{-E(s_2)/kT}}{e^{-E(s_1)/kT}}$$

\Rightarrow Boltzmann factor...

$$e^{-E(s)/kT}$$

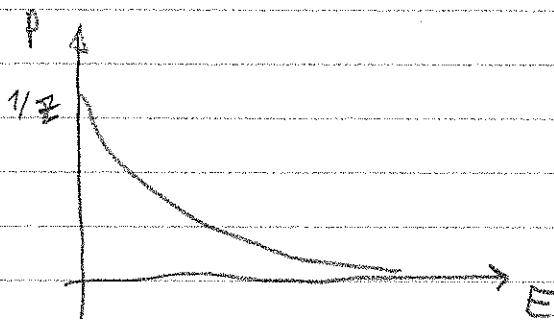
$$\therefore \frac{P(s_2)}{P(s_1)} e^{\frac{E(s_2)/kT}{T}} = \frac{P(s_1)}{P(s_2)} e^{\frac{E(s_1)/kT}{T}} \Rightarrow \text{must be constant.}$$

indep. of s_1 , indep. of s_2

$$\therefore \frac{P(s_2)}{e^{-E(s_2)/kT}} = \frac{P(s_1)}{e^{-E(s_1)/kT}} \Rightarrow \text{constant} = \frac{1}{2}$$

$$P(s) = \frac{1}{Z} e^{-E(s)/kT} \quad \text{and} \quad \text{Boltzmann distribution}$$

(canonical distribution)



Z: The Partition Function

Total probability of finding an atom in some state or another = 1

$$1 = \sum_s P(s) = \sum_s \frac{1}{Z} e^{-E(s)/kT} = \frac{1}{Z} \sum_s e^{-E(s)/kT}$$

So $Z = \sum_s e^{-E(s)/kT}$ ~ partition function...

constant

April 17 2019

$Z \rightarrow$ normalization factor that converts Boltzmann factor into a prob

Temp. dependence of Z

① Low T, @ norm T, $kT \approx 0.0257 \text{ eV}$

ground state energy = 0 eV

→ dominates partition function.

Ex Excited state

$$e^{-10.2 \text{ eV}/kT} \quad \text{while } e^{-0} = 1$$

tiny...

→ @ low T, $\boxed{Z=1}$ ↑ possible states available...

② At high T $E \ll kT$

$$Z = e^{-0/kT} + e^{-E_1/kT} + \dots$$

$$= 1 + (\text{order of unity}) + \dots$$

So $Z \gg 1$

★ At high temp., there are many states available...

Applications of Boltzmann factors

(a) Thermal excitations of atoms in stellar atmospheres.

Consider H atom in atm of sun ($T \approx 5800\text{K}$).

What is the prob. of finding e^- in one of the first excited states compared to probability of finding e^- in ground state?

$$\frac{P(S_2)}{P(S_1)} = \frac{e^{-E_2/kT}}{e^{-E_1/kT}} = e^{-(E_2 - E_1)/kT}$$

$$\text{For H, } E_2 - E_1 = \Delta E = -3.4\text{eV} - (-13.6\text{eV}) = 10.2\text{eV}$$

$$\text{And } kT = (8.62 \times 10^{-5} \text{eV/K})(5800\text{K}) = 0.50\text{eV}$$

$$\frac{P(S_2)}{P(S_1)} = e^{-10.2\text{eV}/0.50\text{eV}} = 1.4 \times 10^{-9}$$

But we need to add "statistical weights" to account for degeneracy of energy levels ...

$$\begin{aligned} g_2 &= 8 \quad (2n^2) \quad \& P(\varepsilon_2)/P(\varepsilon_1) &= \frac{g_2}{g_1} e^{-\Delta E/kT} \\ g_1 &= 2 \\ &= 4 [1.4 \times 10^{-9}] \\ &= 5.6 \times 10^{-9} \end{aligned}$$

Caveat

At some temp T , we start ionizing atoms.

→ No more e^- for upwards transitions.

→ Boltzmann dist is only part of the story ...



Excitation → need to add Salpeter equation to account for

ionization. Salts eqn:

$$\frac{P_{\text{H}^+(\text{ionized})}}{P_{\text{H}_2(\text{neutral})}} = \frac{1}{ne} \left(\frac{2\pi m_e kT}{h^2} \right)^{3/2} e^{-E_I/kT}$$

— 4 —

Average values

§ 5.2.

$$P(s) = \frac{1}{Z} e^{-E(s)/kT} = \frac{1}{Z} e^{-\beta E(s)}$$

where $\beta = 1/kT$

$$\text{And so } Z = \sum_s e^{-E(s)/kT} = \sum_s e^{-\beta E(s)}$$

Imagine we have an atom with 3 discrete energy levels...

0eV, 4eV, 7eV

Say we have 5 real atoms, 2 in ground, 2 in 1st state,
1, in 2nd state.

Average energy of all 5 atoms is:

$$\bar{E} = \frac{0 \cdot \text{eV} \cdot 2 + 4 \text{eV} \cdot 2 + 7 \text{eV} \cdot 1}{5} = \frac{15 \text{eV}}{5} = 3 \text{eV} \dots$$

or

$$E = \left(\frac{2}{5} \cdot 0 \text{eV} \right) + \left(\frac{2}{5} \cdot 4 \text{eV} \right) + \left(\frac{1}{5} \cdot 7 \text{eV} \right)$$

$$= P(0s) \cdot 0 \text{eV} + P(1s) \cdot \dots$$

Generalise

$$E = \frac{\sum_s E(s) N(s)}{N} = \sum_s E(s) \frac{N(s)}{N} = \sum_s E(s) P(s)$$

$$\therefore \bar{E} = \frac{1}{N} \sum_s E(s) e^{-\beta E(s)}$$

Can do this for avg value of any property

$$\bar{X} = \sum_{s=1}^z X(s) P(s) = \frac{1}{z} \sum_{s=1}^z X(s) e^{-\beta E(s)}$$

Also note that average values are additive -

if \bar{E} is avg value of single atom, so in general,

$$\langle u \rangle = N \bar{E} \rightarrow \text{avg energy of ensemble of } N \text{ particles -}$$

* Calculate deviation about the mean

For our 5 atoms @ 3 energy level $\bar{E} = 3eV$... then the difference from the mean

$$2 \text{ atoms } @ \text{ O } : \Delta E = E_1 - \bar{E} = 0 - 3eV = -3eV$$

$$2 \text{ atoms } @ \text{ C } : \Delta E = E_2 - \bar{E} = 4eV - 3eV = 1eV$$

$(\Delta E)^2 \rightarrow$ change of the square deviation.

$$\sigma^2 = \frac{(-3)^2 \cdot 2 + (1)^2 \cdot 2 + 4^2}{7.2} = 7.2 \text{ eV}^2$$

Then, $\sqrt{(\Delta E)^2} = \text{rms} / \text{stdev} \dots = \sigma_E = \sqrt{7.2 \text{ eV}^2} = 2.7 \text{ eV}$

But we observed that

$$\sigma_E^2 = \bar{E}^2 - \bar{E}^2$$

For any system in thermal equilibrium with reservoir at temp T, average value of the energy, \bar{E} :

$$\boxed{\bar{E} = -\frac{1}{Z} \frac{\partial Z}{\partial \beta} \quad \text{where } \beta = \frac{1}{kT}}$$

or equivalently

$$\boxed{\bar{E} = -\frac{\partial \ln(Z)}{\partial \beta}}$$

Proof

$$\frac{\partial Z}{\partial \beta} = \frac{\partial}{\partial \beta} \left[\sum_s e^{-\beta E(s)} \right] = \sum_s \frac{\partial}{\partial \beta} e^{-\beta E(s)} = \sum_s -E(s) e^{-\beta E(s)}$$

So

$$-\frac{1}{Z} \frac{\partial Z}{\partial \beta} = +\frac{1}{Z} \sum_s +E(s) e^{-\beta E(s)} = \sum_s \left(\frac{1}{Z} E(s) e^{-\beta E(s)} \right) = \sum_s E(s) \cdot p(s)$$

$$\boxed{\frac{1}{Z} \frac{\partial Z}{\partial \beta} = \bar{E}}$$

Can also show that

$$\boxed{\bar{E}^2 = \frac{1}{Z} \frac{\partial^2 Z}{\partial \beta^2}}$$

How is work related to Z ?

→ suppose we have a system characterized by a single param, x .

→ Quasi-static change in x , $x \rightarrow x + dx$

• Energy of state (s) changes by some small amount

$$\Delta E_s = \frac{\partial E_s}{\partial x} dx$$

• Work done on the system $\Rightarrow W = \int F \cdot dx \propto \sum F \cdot dx$
where $F \rightarrow$ is change in Energy wrt x .

$$F = \frac{\partial E_s}{\partial x} = \sum_s \frac{\partial E_s / \partial x}{e^{-\beta E(s)}} dx$$

• Work done on system $W = \frac{\sum_s \frac{\partial E_s / \partial x}{e^{-\beta E(s)}} dx}{\sum_s e^{-\beta E(s)}}$

Re-write numerator

$$\sum_s e^{-\beta E(s)} \frac{\partial E(s)}{\partial x} = -\frac{1}{\beta} \frac{\partial}{\partial x} \left(\sum_s e^{-\beta E(s)} \right)$$

So

$$\begin{aligned} \cancel{\sum_s e^{-\beta E(s)} \frac{\partial E(s)}{\partial x}} &= -\frac{1}{\beta} \frac{\partial}{\partial x} \left(\sum_s e^{-\beta E(s)} \right) \\ &= -\frac{1}{\beta} \frac{\partial z}{\partial x} \end{aligned}$$

So,

$$W = -\frac{1}{\beta} \frac{\partial z}{\partial x} / z$$

b

$$W = -\frac{1}{\beta} \frac{\partial z}{z} = -\frac{1}{\beta z} \frac{\partial z}{\partial x} = -\frac{1}{\beta} \frac{\partial \ln z}{\partial x}$$

So

$$W_{on} = -\frac{1}{\beta} \frac{\partial \ln z}{\partial x}$$

For example, $x = V$ (volume)

$$W_{on} = -\bar{F} dV = -\frac{1}{\beta} \frac{\partial \ln z}{\partial V} dV$$

So

$$\boxed{\bar{F} = \frac{1}{\beta} \frac{\partial \ln z}{\partial V}}$$

How is z related to s ? $z = z(\beta, s)$. For small changes in z ,

$$d\ln z = \underbrace{\frac{\partial \ln z}{\partial x}}_{\text{d}x} + \underbrace{\frac{\partial \ln z}{\partial \beta}}_{\text{d}\beta} d\beta$$

$$\begin{aligned} \text{So } \boxed{d\ln(z) = -\frac{1}{\beta} W_{on} + -\bar{E} d\beta} \\ \uparrow \\ dW_{on} \end{aligned}$$

Re-writing $d \ln Z = -\beta dW - d(\bar{E}_B) + \beta d\bar{E}$

So $d(\ln Z + \bar{E}_B) = \beta (\underbrace{d\bar{E} - dW_m}_{dQ \text{ (First law)}}) = \beta dQ = \frac{dQ}{kT} = \frac{1}{k} dS$

So $d(\ln Z + \bar{E}_B) = \frac{dS}{k}$

So $\boxed{S = k(\ln Z + \beta \bar{E})}$

Now, $S = k \ln Z$

So $\ln Z + \beta \bar{E} = \ln Z$

So $\boxed{\ln Z = \ln Z - \beta \bar{E}}$

Example of paramagnetism

↳ Before: ① $Z(N_f) = \binom{N}{N_f} = \frac{N!}{N_f! N_{f'}!}$

② $S = k \ln Z$ (use Stirling approximation)

③ $\frac{1}{T} = \left(\frac{\partial S}{\partial T} \right)$

④ $U = 0(+)$ $\rightarrow u = -N_B \beta \text{B} \text{anh} \left(\frac{\mu B}{kT} \right)$

⑤ $M = -\frac{u}{B}$

⑥ $C_B = \left(\frac{\partial U}{\partial T} \right)_B$

Now, we'll redo this with Boltzmann statistics. Two possible energy states..

"up" $u = -\mu B$ "down" $u' = +\mu B$ $\{ \text{Then } Z = \sum_i e^{-\beta E_i} = e^{-\beta(-\mu B)} + e^{-\beta(\mu B)}$
 $= e^{\mu B} + e^{-\mu B}$

So $\boxed{Z = 2 \cosh(\mu B)}$

Q Probability of finding in up/down direction.

$$P_U = \frac{e^{\beta \mu B}}{2 \cosh(\beta \mu B)}, \quad P_D = \frac{e^{-\beta \mu B}}{2 \cosh(\beta \mu B)}, \quad P_U + P_D = 1$$

Average energy of a dipole

$$\begin{aligned} \bar{E} &= \sum E(G) P(G) = (-\mu B) \frac{e^{\beta \mu B}}{2 \cosh(\beta \mu B)} + (\mu B) \frac{e^{-\beta \mu B}}{2 \cosh(\beta \mu B)} \\ &= (-\mu B) \frac{2 \sinh(\beta \mu B)}{2 \cosh(\beta \mu B)} \\ &= -\mu B \tanh(\beta \mu B) \end{aligned}$$

So $\bar{E} = -\mu B \tanh(\beta \mu B)$

S $E_{ext} = -N \mu B \tanh(\beta \mu B) = -N \mu B \tanh\left(\frac{\mu B}{kT}\right)$

Alternate approach

$$\begin{aligned} \bar{E} &= \frac{-1}{\varepsilon} \frac{\partial \Omega}{\partial \beta} \\ &= \frac{-1}{\varepsilon} \frac{\partial}{\partial \beta} \left[2 \cosh(\beta \mu B) \right] \\ &= \frac{-1}{\varepsilon} \cdot 2 \left(\mu B \sinh(\beta \mu B) \right) \\ &= (2 \mu B) \frac{-1}{2 \cosh(\beta \mu B)} \sinh(\beta \mu B) \\ &= -\mu B \tanh(\beta \mu B) \end{aligned}$$

S $\bar{E}_{ext} = -N \mu B \tanh(\beta \mu B)$

Magnetization $\Rightarrow M = N \mu_0, \mu_z = \sum \mu_s P(z) \dots$

$$= \mu_0 P_U + (-\mu) P_D$$

April 22, 2019

The Equipartition Theorem

↳ applies to systems with quadratic degrees of freedom.

$$\rightarrow E = \frac{1}{2}mv^2$$

$$E = \frac{1}{2}mv^2 \text{ where } q = \text{position or momentum coordinate}$$

- $Z = \sum_q e^{-\beta cq^2}$, and assuming that the spacing Δq is constant and small ...

$$\therefore Z = \frac{1}{\Delta q} \sum_q e^{-\beta cq^2} \Delta q$$

$$= \frac{1}{\Delta q} \int_{-\infty}^{\infty} e^{-\beta cq^2} dq$$

Change of variable: let $x = \sqrt{\beta c} \cdot q \rightarrow x^2 = \beta cq^2$

$$dq = \frac{dx}{\sqrt{\beta c}}$$

$$\therefore Z = \frac{1}{\Delta q} \int_{-\infty}^{\infty} e^{-x^2} dx \cdot \frac{1}{\sqrt{\beta c}} = \frac{1}{\Delta q} \frac{1}{\sqrt{\beta c}} \int_{-\infty}^{\infty} e^{-x^2} dx$$

assumption \nearrow

$$Z = \frac{\sqrt{\pi}}{\Delta q \sqrt{\beta c}}$$

(*) As long as $\Delta q \ll kT$, then
equipartition holds (high temp.)

$$\boxed{Z = \frac{1}{\Delta q} \sqrt{\frac{\pi}{\beta c}}}$$

or equivalently, $Z = C \beta^{-1/2}$ $\rightarrow C$ is some constant

$$\therefore E = \frac{1}{2} \frac{\partial Z}{\partial \beta} = \frac{-1}{C \beta^{3/2}} \left(-\frac{1}{2} C \beta^{-3/2} \right) \Rightarrow E = \frac{1}{2} \beta^{-1}$$

$$\therefore \boxed{E = \frac{1}{2} kT}$$

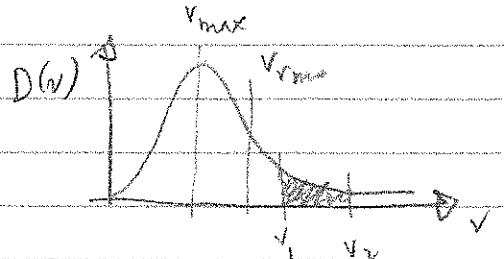
→ eq. partition theorem for 1/2 d.f.

Note Conditions

Equipartition doesn't hold for quantum mechanical systems,
→ it requires a continuum of ΔE .

Equipartition holds if $\Delta E \ll kT$ (high temp)

The Maxwell-Boltzmann Distribution



From equipartition, can imagine:

$$\frac{1}{2}mv^2 = \frac{3}{2}kT, \text{ then } v_{rms} = \sqrt{\frac{3kT}{m}}$$

$$P(v_1 < v < v_2) = \int_{v_1}^{v_2} D(v) dv, \text{ where } D(v) \text{ is the dist. function} \rightarrow \text{pdf}$$

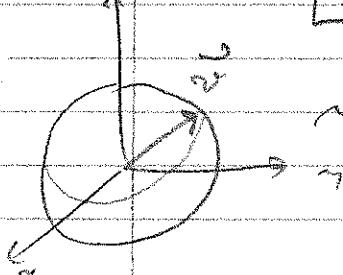
What is $D(v)$? $\rightarrow D(v) \propto$ prob that a molecule will have
velocity \vec{v} - \propto # of states, \propto
consequently to speed v .

$$D(v) \propto (\text{prob. of molecule}) \times (\# \text{ of states}) \underbrace{\propto (\text{comp. to speed } v)}$$

know, $\boxed{?} \propto \text{Boltzmann factor} \dots E = \frac{1}{2}mv^2 \rightarrow = \boxed{e^{-mv^2/2kT}}$

$$\boxed{?} \propto 4\pi r^2$$

→ larger r , more surface area, higher \propto for $\boxed{?}$



$$\underline{D(v) = C (4\pi v^2) e^{-mv^2/2kT}}$$

$$1 = \int_0^\infty D(v) dv = 4\pi C \int_0^\infty v^2 e^{-mv^2/2kT} dv$$

Change of vars. $x = v \sqrt{\frac{m}{2kT}}$, then -

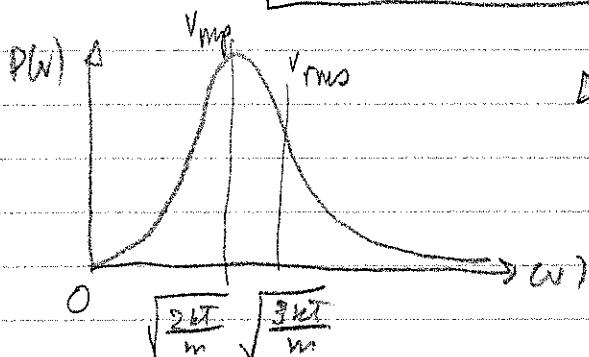
$$1 = 4\pi C \int_0^\infty x^2 e^{-x^2} dx \cdot \left(\sqrt{\frac{2kT}{m}}\right)^3$$

$$= 4\pi C \cdot \left(\frac{2kT}{m}\right)^{3/2} \int_0^\infty x^2 e^{-x^2} dx$$

$$\therefore C = \left(\frac{m}{2kT}\right)^{3/2}$$

Maxwell's speed distribution -

Thus, $D(v) = 4\pi v^2 \left(\frac{m}{2kT}\right)^{3/2} e^{-\frac{mv^2}{2kT}}$



$$D(v) = 0 @ v=0 - v \rightarrow \infty$$

E Calculate v_{mp} (most probable)

$$0 = \frac{d}{dv} D(v) = 0 \rightarrow 0 = \frac{d}{dv} \left[v^2 e^{-mv^2/2kT} \right]$$

$$\therefore 0 = 2v e^{-mv^2/2kT} + v^2 \cdot \left(\frac{-mv}{kT}\right) e^{-mv^2/2kT}$$

$$= 2v + \frac{-mv^2}{kT} \Rightarrow 0 = 2 - \frac{mv^2}{kT} \Rightarrow$$

$$v_{mp} = \sqrt{\frac{2kT}{m}}$$

Calculate \bar{v}

$$\bar{v} = \overline{E(v)} = \int_0^\infty v D(v) dv = \int_0^\infty 4\pi v^3 \left(\frac{m}{2\pi kT}\right)^{3/2} e^{-\frac{mv^2}{2kT}} dv$$

$$\Rightarrow 4\pi \left(\frac{m}{2\pi kT}\right)^{3/2} \int_0^\infty v^3 e^{-\frac{mv^2}{2kT}} dv$$

$$\bar{v} = \left(\frac{m}{2\pi kT}\right)^{3/2} (4\pi) \cdot \frac{1}{2} \left(\frac{2kT}{m}\right)^2$$

$$\therefore \bar{v} = \left(\frac{2kT}{m}\right)^{1/2} \cdot \frac{2}{\sqrt{\pi}}$$

$$\boxed{\bar{v} = \left(\frac{8kT}{m\pi}\right)^{1/2}}$$

$$M = m N_A$$

Ex N₂ in air @ room temp ... T = 298K, m_{N₂} = 14 g/mol
m_{N₂} = 28 g/mol

$$v_{mp} = \sqrt{\frac{2kT}{m}} = \sqrt{\frac{2(1.38 \times 10^{-23})(298K)}{28 \times 10^{-3} \text{ kg/mol}}} \approx 420.5 \text{ m/s}$$

Partition Function & FREE ENERGY

$S(T) \propto \text{const } u \Rightarrow S \text{ tends to } T, S = k \ln \Omega$

$Z(T) \rightarrow F @ \text{constant } T$

$$\text{Recall } F = U - TS \rightarrow \frac{F-U}{T} = -S$$

$$dF = -PdV - SdT + \mu dN \rightarrow \left(\frac{\partial F}{\partial T}\right)_{V,N} = -S$$

$$\therefore \left(\frac{\partial F}{\partial T}\right)_{V,N} = \frac{F-U}{T} \quad (1)$$

$$\text{Given } \tilde{F} = -kT \ln Z \Rightarrow Z = e^{-\tilde{F}/kT}$$

$$\text{Check deriv w.r.t } T: \frac{\partial \tilde{F}}{\partial T} = \frac{\partial}{\partial T} (-kT \ln Z)$$

$$= -k \ln Z - kT \frac{\partial}{\partial T} \ln Z$$

$$= -k \ln Z - kT \underbrace{\frac{\partial \beta}{\partial T} \frac{\partial}{\partial \beta} \ln Z}_{-1 \cdot \frac{1}{kT^2} \frac{\partial Z}{\partial \beta}}$$

$$\Rightarrow \frac{\partial \tilde{F}}{\partial T} = -k \ln Z - \frac{U}{T}$$

$$\frac{\partial \tilde{F}}{\partial T} = \frac{\tilde{F} - U}{T} = \frac{F - U}{T}, \text{ same as (1), so } -U$$

\gg we know given

were correct, except there might be a constant

Check initial condition (to determine constant)

$$F = U - TS \quad \text{Let's use } T=0 \rightarrow \text{then } F(T=0) = U_0.$$

$$Z(0) = Z_0 \sum e^{-E_i/kT}$$

T
lowest possible
energy.

$$= e^{-U_0/kT} + \text{high order terms, negligible because } U \gg kT$$

$$\text{So } \tilde{F}(T=0) = -kT \ln Z = -kT(U_0/kT) = -U_0$$

$$\text{So } \tilde{F}(T=0) = U_0 \text{ is constant!}$$

∴

$$\boxed{F = -kT \ln Z}$$

$$dF = -PdV - SdT + \mu dN$$

$$\left(\frac{\partial F}{\partial V}\right)_{T,N} = -P, \quad \left(\frac{\partial F}{\partial T}\right)_{V,N} = -S, \quad \left(\frac{\partial F}{\partial N}\right)_{V,T} = \mu$$

Example

$$\left(\frac{\partial F}{\partial T}\right)_{V,N} = -S \quad F = -kT \ln Z, \quad S = \frac{\partial}{\partial T} (-kT \ln Z)$$

$$S = \frac{\partial}{\partial T} (-k \ln Z) = -k \ln Z + \frac{\partial P}{\partial T} \frac{\partial}{\partial P} \ln Z$$

$$= -k \ln Z + \frac{kE}{T}$$

$\therefore S = k(\ln Z + \beta E)$ ✓ same as before

$$\text{or } \ln Z = \frac{S}{k} - \beta E$$

Partition Function for Composite System

Goal: write an expression for Z for an ideal gas

1st: determine how Z_{tot} depends on Z for each individual particle

Start w/ system of 2 particles. If they do not interact, total energy:

$$E_{\text{tot}} = E_1 + E_2$$

$$Z_{\text{tot}} = \sum_c e^{-\beta [E_1(c) + E_2(c)]} = \sum_c e^{-\beta E_1(c)} e^{-\beta E_2(c)}$$

If we also assume that states of individual particles are independent of each other:

$$Z_{\text{tot}} = \underbrace{\sum_{S_1} e^{-\beta E_1(S_1)}}_{z_1} \underbrace{\sum_{S_2} e^{-\beta [E_2(S_2)]}}_{z_2} \Rightarrow Z_{\text{tot}} = z_1 z_2$$

(non-interacting distinguishable system particles)

If particles are indistinguishable, we have double counted stats.

$$\therefore Z_{\text{tot}} \approx \frac{1}{2} z_1 z_2 \quad \text{or } Z_{\text{tot}} = z_1^N$$

Generalize this to N particles $\rightarrow Z_{\text{tot}} = z_1 z_2 \dots z_N$ distinguishable
For distinguishable, $Z_{\text{tot}} = \frac{1}{N!} z^N$

3/1/26, 2019

Working towards Z for ideal gas.

$$Z_{\text{tot}} = \frac{1}{N!} Z^N$$

$$E_{\text{tot}} = E_{\text{tr}} + \underbrace{E_{\text{int}}}_{\substack{\text{(translation)} \\ \text{(rotational)}}}$$

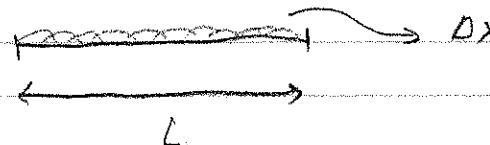
or thermal
energy
[Boltzmann factor] $\rightarrow e^{-E_{\text{tot}}(s)/kT} = e^{-(E_{\text{tr}})/kT} \cdot e^{-E_{\text{int}}(s)/kT}$

or thermal

$$Z_{\text{tot}} = Z_{\text{tr}} Z_{\text{int}}$$

$$Z_{\text{tr}} = \sum_{\text{tr}} e^{-E_{\text{tr}}(s)/kT} \quad Z_{\text{int}} = \sum_{\text{int}} e^{-E_{\text{int}}(s)/kT}$$

(2) When we counted states before:

1D:  $\# \text{Position states} = \frac{L}{dx}$

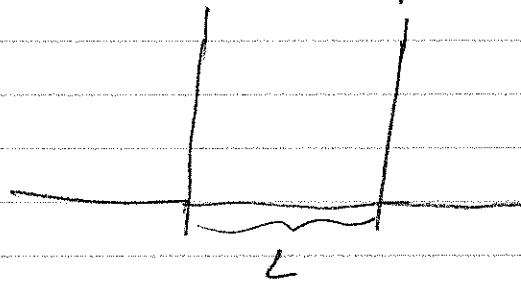
Total # of states

$$\frac{L}{dx} \cdot \frac{dp}{dp} \approx \frac{Lp}{\hbar}$$

Momentum states $= \frac{dp}{Ap}$

(3) More formally,

Count all independent, definite energy states or wavefunction



infinite square well

Potential energy $\begin{cases} 0 & \text{inside box} \\ \infty & \text{outside the box} \end{cases}$

$\Rightarrow U = \begin{cases} \text{something}, \text{inside} \end{cases}$

(141)

$$KE = \frac{1}{2}mv^2 = \frac{p^2}{2m} = \frac{\hbar^2}{2mL^2}$$

\Rightarrow only certain wavelengths are allowed

$$\Rightarrow p = \frac{\hbar}{\lambda} = \frac{\hbar n}{2L} \text{ for allowed momenta}$$

$$\rightarrow \lambda_n = \frac{2L}{n}, n=1, 2, 3, \dots$$

$$E_n = \frac{p^2}{2m} = \left(\frac{\hbar n}{2L}\right)^2 = \frac{\hbar^2 n^2}{8mL^2}$$

for allowed independent energies..

$$\text{So, } Z_{1D} = \sum e^{-E_n/kT}$$

$$= \sum_n N_{1D} \exp\left[-\frac{\hbar^2 n^2}{8mL^2 kT} \cdot \beta\right]$$

$$\text{assume large } T, L \rightarrow \approx \int_0^\infty \exp\left[-\frac{\hbar^2 n^2}{8mL^2 kT}\right] dn$$

$\Delta m = 1$

$$\text{let } x = \frac{\hbar n}{\sqrt{8mL^2 kT}} \rightarrow dx = \frac{\hbar}{\sqrt{8mL^2 kT}} dn$$

$$\text{So, } Z_{1D} = \frac{1}{h} \sqrt{\frac{8mL^2 kT}{\hbar^2}} \int_0^\infty e^{-x^2} dx$$

$$= \sqrt{\frac{8mL^2 kT}{\hbar^2}} \cdot \sqrt{\frac{\pi}{2}}$$

$$Z_{1D} = \frac{\sqrt{2\pi m kT}}{h} L = \frac{L}{\ell_0} \rightarrow \ell_0 = \text{"quantum length"}$$

length

- The quantum length, ℓ_0 is roughly the de Broglie λ of a particle of mass m at energy kT .

$$= \frac{h}{\sqrt{2\pi m kT}} \ell_0 \cdot \sqrt{kT}$$

$$\lambda = \frac{h}{p}, E = \hbar\omega = \frac{p^2}{2m} \rightarrow p = \sqrt{2mkT}, \text{ then } \lambda = \frac{h}{\sqrt{2mkT}}$$

$\lambda \ll r$ roughly the size of a particle... ~~for N₂~~

Q For N₂ @ T = 298 K, $\lambda \approx 1.0 \times 10^{-7}$ m

$\Rightarrow \frac{\lambda}{\ell_a}$ is large

[In three dimensions]

$$E_{fr} = \frac{p_x^2}{2m} + \frac{p_y^2}{2m} + \frac{p_z^2}{2m}$$

$$\text{each } p_{i,n} = \frac{h n_i}{2L}$$

$$S E_{fr} = \sum_s e^{-E(s)/kT} = \sum_{n_x n_y n_z} e^{-\frac{h^2 n_x^2}{8m L_x^2 kT}} e^{-\frac{h^2 n_y^2}{8m L_y^2 kT}} e^{-\frac{h^2 n_z^2}{8m L_z^2 kT}}$$

$$= \frac{L_x}{\lambda_a} \cdot \frac{L_y}{\lambda_a} \cdot \frac{L_z}{\lambda_a} \quad \text{for each atom.}$$

$$S \boxed{Z_f = \frac{V}{\lambda_a^3} = \frac{V}{v_a}} \rightarrow \text{quantum volume}^4$$

$$S \boxed{v_a = \lambda_a^3 = \left(\frac{h}{\sqrt{2\pi m kT}} \right)^3} \rightarrow \text{ignore this}$$

$$S Z_{tot} = \frac{1}{N!} Z^N = \frac{1}{N!} (Z_f \cdot Z_{int})^N$$

$$\boxed{Z_{tot} = \frac{1}{N!} \left(\frac{V}{v_a} \cdot Z_{int} \right)^N}$$

Sometimes, log of Z is more useful...

Stirling's approx

$$\ln Z_{tot} = \frac{N}{V} (\ln V + \ln Z_{int} - \ln v_a) - Nk_B T + N$$

$$\text{So, } \boxed{\ln Z_{tot} = N [\ln V + \ln Z_{int} - \ln v_a - \ln N + 1]}$$

log of partition function for ideal gas.

Now we can predict the thermodynamic properties of ideal gas

Average energy of ideal gas \rightarrow expect $E = \frac{3k_B T}{2}$

$$\hookrightarrow \ln Z_{tot} = N [\ln V + \ln Z_{int} - \ln v_a - \ln N + 1]$$

$$E = \frac{1}{2} \frac{\partial}{\partial P} - \frac{\partial \ln Z}{\partial P}$$

Note: V is independent of T, P

N is also independent of T, P

Int. V_a depend on P .

$$\begin{aligned} \text{So, } \bar{E} &= -N \left[\frac{\partial}{\partial P} (\ln Z_{int}) - \frac{1}{V_a} \frac{\partial v_a}{\partial P} \right] \\ &= -N \left[-\bar{E}_{int} + \frac{1}{V_a} \frac{\partial}{\partial P} \left(\frac{h^2}{2\pi m k T} \right)^{3/2} \right] \\ &= N \bar{E}_{int} + \frac{1}{V_a} \left(\frac{h^2}{2\pi m} \right)^{3/2} \frac{\partial}{\partial P} (\beta^{3/2}) \\ &= N \bar{E}_{int} + \frac{1}{V_a} \left(\frac{h}{\sqrt{2\pi m}} \right)^2 \frac{3}{2} P^{1/2} \end{aligned}$$

$$= \bar{E}_{int} + N \left(\frac{\sqrt{2\pi m k T}}{h} \right)^3 \left(\frac{h}{\sqrt{2\pi m}} \right)^2 \cdot \frac{3}{2} \sqrt{P}$$

$$= N \bar{E}_{int} + \frac{3}{2} N P^{-1} \quad \text{to} \quad \boxed{\bar{E} = N \bar{E}_{int} + \frac{3}{2} N k T}$$

- if assume no internal energy, $E \rightarrow \frac{3}{2}NkT$
 → Ent depends on Eq Partition Func.

Heat Cap $C_V = \left(\frac{\partial U}{\partial T}\right) = \left(\frac{\partial U_{int}}{\partial T}\right) + \frac{3}{2}Nk$

April 29, 2011

Ch 7: QUANTUM STATISTICS

↳ we'll use Gibbs factors instead of Boltzmann factor...

↳ think about system that can exchange energy w/ particles -

↳ look at ratio of probabilities $\frac{P(s_2)}{P(s_1)} = S_R(s_2)/S_R(s_1) = \frac{e^{S_R(s_2)/k}}{e^{S_R(s_1)/k}}$

So, $\frac{P(s_2)}{P(s_1)} = e^{(S_R(s_2) - S_R(s_1))/k}$

$$dS_R \approx \frac{1}{T} [dU_R + PdV_R - \mu dN_R]$$

• Assume that $dV_R = 0$

• keep μdN term & limit func. dU_{sys}

So, $S_R(s_2) - S_R(s_1) = -\frac{1}{T} \left[(E(s_2) - E(s_1)) - (\underbrace{\mu dN(s_2) - \mu dN(s_1)}_{dU_{sys}}) \right]$

\downarrow
 $= -\Delta S_R$

So, $\frac{P(s_2)}{P(s_1)} = \frac{e^{-[(E(s_2) - \mu N(s_2))/kT]}}{e^{-[E(s_1) - \mu N(s_1)]/kT}}$

So, instead of Boltzmann factor, we set this factor \rightarrow Gibbs
 $e^{-(E(s) - \mu dN)/kT}$

④ To get absolute probability \rightarrow need constant at front

$$P(s) = \frac{1}{Z} e^{-(E(s) - \mu N(s))/kT}$$

$Z \Rightarrow$ "grand partition function" or "Gibbs sum"

$$\text{So that } \sum_s P(s) = 1 \Rightarrow Z = \sum_s e^{-(E(s) - \mu N(s))/kT}$$

Sum over all Gibbs factors.

If you have more than 1 type of particles, then sum over all species n_1, n_2, \dots, n_N

$$\text{Ex 2 particles - Gibbs factor: } e^{-(E_1(n_1) - \mu_1 n_1) - (E_2(n_2) - \mu_2 n_2)/kT}$$

BOSONS \Rightarrow FERMIONS

④ Quantum statistics \rightarrow important for high density & low temp systems.

④ In this case, derivation of

$$Z_{\text{tot}} = \frac{1}{N!} z^N \quad \text{breaks down @ high density, low temperature.}$$

$\Rightarrow \frac{1}{N!}$ is not quite correct here.

④ ≤ 2 interacting particles, each with 5 available states \Rightarrow the ground state energy, $E=0$.

$\square \square \square \square \square E = 0$

Boltzmann factor = $e^{-\frac{E}{kT}} = 1 \Rightarrow Z = 5 \text{ so } Z = 5!$

Rule • If distinguishable $\Rightarrow Z = 5 \times 5 = 25 = \boxed{Z}$

• If indistinguishable $\Rightarrow Z = \binom{5}{2} = 10$
 $\text{so } \boxed{Z = 10}$

Previous assumption for indistinguishable particles

$$Z_{\text{indist}} = \frac{1}{N!} Z^N = \frac{25}{2!} = 12.5 \rightarrow \text{does not make sense...}$$

(Fermions) # states for indistinguishable particles $\Rightarrow \boxed{10}$, no particles are occupying the same states.

(Bohrs) \Rightarrow But if we allow them to be in the same state $\Rightarrow \boxed{15}$ for indistinguishable particles that can be in the same state.

\rightarrow boson.

\Rightarrow And so $12.5 \rightarrow$ average between Bohrs + Fermions

$$\boxed{\frac{1}{N!} Z^N}$$

correctly cuts down 20 states for distinguishable particles to 10 for indistinguishable particles. But also cuts down 5 $\rightarrow 7.5$ incorrectly.

Bosons → can share the same (quantum) states (Ex; photons, pions, "le nachi") integer spin: 0, 1, 2, ...

Fermions → cannot occupy the same (q) state ($\vec{p}, \vec{q}^+, n, \nu$)
↳ half-integer spin $\frac{1}{2}, \frac{3}{2}, \dots$

Pauli exclusion principle

⊕ $Z_{\text{tot}} = \frac{1}{N!} \pi^N$ interpolates between exact value for indistinguishable bosons, fermions.

⊕ Bosons → governed by Bose-Einstein statistics.

⊕ Fermions → governed by Fermi-Dirac statistics.



When do we need to use B-E + F-D stats rather than Boltzmann stats?

↳ when # of single particles into \gg # of particles, then it doesn't matter if we have bosons or fermions, use Boltzmann statistics

→ if $Z \gg N$

⊕ Think back to Ideal gas: $Z_i = \frac{V}{V_0} Z_{\text{int}}$, where

$$V_0 = \left(\frac{\hbar}{\sqrt{2\pi m kT}} \right)^{3/2}, \text{ for } Z_i \gg N$$

$\frac{V}{V_0} \gg N$, and so, $\frac{V}{N} \gg V_0 \rightarrow$ average distance between particles is \gg de Broglie wavelengths.

★ When $\frac{V}{N} \approx V_0$, then it matters whether we have Bosons or Fermions. \rightarrow use Quantum Statistics

either B-E or F-D.

At high temperature, $Z \gg N \rightarrow$ Boltzmann Statistics.

Single-particle state of a system

- System \rightarrow particular state of particle
- "Reservoir" \rightarrow all the possible states.

April 10, 2019

DISTRIBUTION FUNCTIONS

- System \Rightarrow single-particle quantum state
- Reservoir \Rightarrow all other possible states

~ IF state is occupied, it has energy E
 IF unoccupied, energy 0

If state can be occupied by N particles \rightarrow Energy $N\epsilon$

- ☒ Probability of being occupied by N particles

$$P(N) = \frac{1}{Z} e^{-(N\epsilon - NV)/kT}$$

$$S P(N) = \frac{1}{Z} e^{-N(\epsilon - \mu)/kT}$$

For Fermions, $n=0 \text{ or } 1$

$$Z_F = e^0 (\dots) / kT + e^{-1(\epsilon - \mu)/kT} = 1 + e^{-(\epsilon - \mu)/kT}$$

S Fermions:

$$Z_F = 1 + e^{-(\epsilon - \mu)/kT}$$

(149)

Determine the average # of particles in a state, or the occupancy of the state

$$\bar{n} = \sum_n n p(n) = 0 \cdot p(0) + 1 \cdot p(\epsilon) \\ = \frac{e^{-(\epsilon - \mu)/kT}}{1 + e^{-(\epsilon - \mu)/kT}}$$

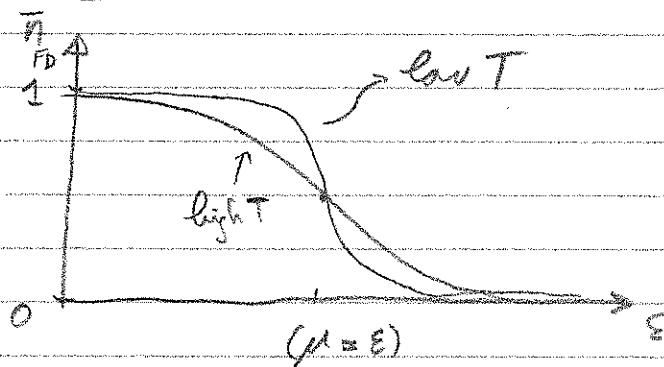
6

$\bar{n}_F =$	$\frac{1}{e^{(\epsilon - \mu)/kT} + 1}$	\rightarrow Fermi-Direc distribution
---------------	---	---

7 If $\epsilon \gg \mu$ $\bar{n} \rightarrow 0$

8 If $\epsilon \ll \mu$ $\bar{n} \rightarrow 1$

9 If $\epsilon = \mu$ $\bar{n} \rightarrow 1/2 \rightarrow 50\% \text{ chance of being occupied}$



Ramsey $\rightarrow n \in \mathbb{N}, 0, 1, 2, \dots$

Then $Z = 1 + e^{-(\epsilon - \mu)/kT} + e^{-2(\epsilon - \mu)/kT} + \dots$

Use $\frac{1}{1-x} = 1 + x + x^2 + x^3 + \dots$ (geometric series)

6

$Z =$	$\frac{1}{1 - e^{-(\epsilon - \mu)/kT}}$
-------	--

Ex. partition functions for bosons,

$$Z_B = \frac{1}{1 - e^{-(\varepsilon_m)/kT}}$$

Average occupancy: $\bar{n} = \sum_n n P(n)$. Let $x = \frac{\varepsilon_m}{kT}$

$$\begin{aligned} \text{Then } \bar{n} &= \sum_n n \frac{e^{-nx}}{Z} = -\frac{1}{Z} \sum_n \frac{d}{dx} e^{-nx} \\ &= -\frac{1}{Z} \frac{d}{dx} \sum_n e^{-nx} \end{aligned}$$

$$\bar{n}_B = -\frac{1}{Z} \frac{dZ}{dx}$$

$$\bar{n}_B = -(1 - e^{-x}) \cdot \frac{d}{dx} (1 - e^{-x})^{-1}$$

$$= \frac{1 - e^{-x}}{(1 - e^{-x})^2} \cdot (e^{-x})$$

$$= \frac{e^{-x}}{1 - e^{-x}}$$

$$\bar{n}_B = \frac{1}{e^x - 1}$$

Bose-Einstein dist.

So

$$\bar{n}_{BE} = \frac{1}{e^{(\varepsilon_m - \mu)/kT} - 1}$$

④ If $\epsilon > \mu \rightarrow \bar{n} \rightarrow 0$

$$\bar{n}_B$$

\rightarrow Cannot have $\epsilon < \mu$

⑤ If $\epsilon < \mu \rightarrow \bar{n} \rightarrow -1$ (X)

\rightarrow since $P(n)$ didn't converge ...

⑥ If $\epsilon = \mu \rightarrow \bar{n} \rightarrow \infty$

$$\mu$$

$$\epsilon$$

⑦ Consider particles obeying Boltzmann statistics

$$P(s) = \frac{1}{Z_1} e^{-E(s)/kT}. \text{ If we have } N \text{ particles, then}$$

$$\bar{n}_p = \frac{N}{Z_1} e^{-E(s)/kT} = \frac{N}{Z_1} e^{-\epsilon/kT}$$

Boltzmann distribution.

$$\mu = \left(\frac{\partial F}{\partial N} \right)_{T,V} \quad \& \quad F = -kT \ln Z$$

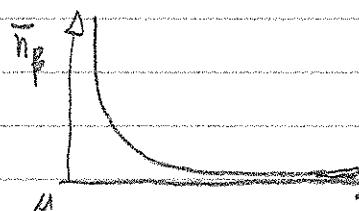
So,

$$\mu = -kT \ln \left(\frac{Z_1}{N} \right)$$

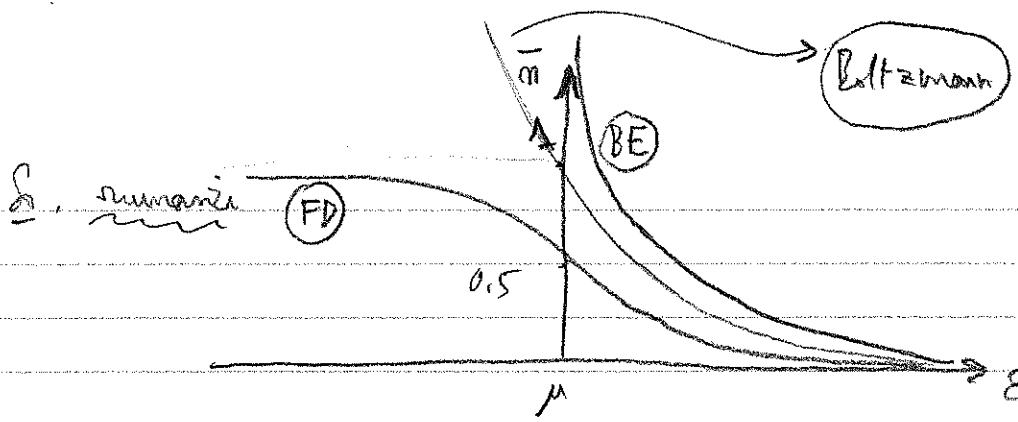
$$\stackrel{D}{=} e^{-\mu/kT} = \frac{Z_1}{N} \quad \stackrel{D}{=} \bar{n}_{\text{Boltz}} = e^{\mu/kT} e^{-\epsilon/kT} = e^{-(\epsilon-\mu)/kT}$$

So

$$\bar{n}_p = \frac{1}{e^{(\epsilon-\mu)/kT}}$$



$$\therefore \bar{n}_F = \frac{1}{e^x + 1}, \quad \bar{n}_B = \frac{1}{e^x - 1}, \quad \bar{n}_p = \frac{1}{e^x}$$



NE
DEGENERATE FERMI GASES

Consider a gas of Fermions at low T, or $\frac{V}{N} \gg V_A$

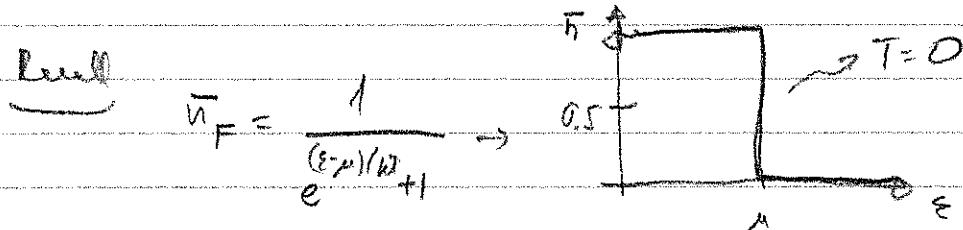
Ex: for an electron at room temp:

$$V_A = \left(\frac{\hbar}{\sqrt{2\pi m k T}} \right)^3 = (4.3 \text{ nm})^3$$

Typical conductor supply 1 free e^- for every atom

$$\rightarrow 1 e^- \text{ per atom} \rightarrow V \sim (\text{size of atom})^3 \sim (0.2 \text{ nm})^3$$

May 1, 2010



At $T=0$ all $\epsilon < \mu$ will be occupied. All $\epsilon > \mu$ unoccupied

\rightarrow "degenerate Fermi gas"

At $T=0$ at $E_F(T=0) = \epsilon_F$ or Fermi Energy

[Goal] Calculate \rightarrow total average energy of Fermions

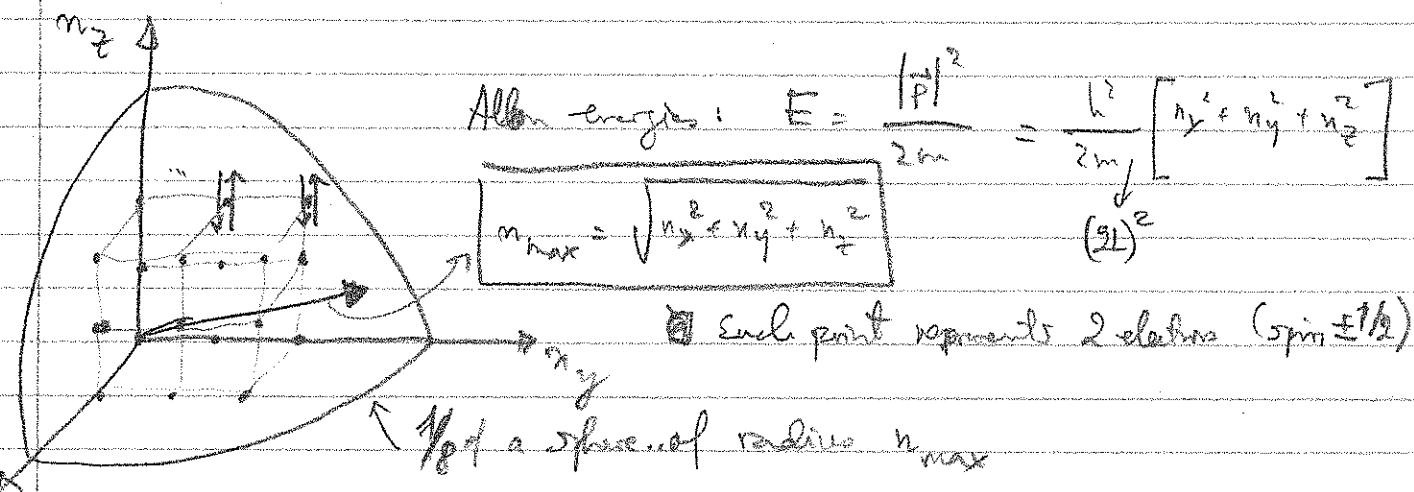
\rightarrow degeneracy pressure. (where there's degenerate Fermi gas in.)

Q Consider packing electrons into some 3D volume (infinite square well)

$$\text{Allowed wavefunctions give } \lambda_n = \frac{2L}{n} \quad \Rightarrow \quad p_n = \frac{\hbar}{\lambda_n} = \frac{\hbar n}{2L}$$

$$p_x = \frac{\hbar n_x}{2L}, \quad p_y = \frac{\hbar n_y}{2L}, \quad p_z = \frac{\hbar n_z}{2L}$$

n_x, n_y, n_z are integers independent of each other



n_x Want to calculate $E_F = \text{max energy}$

$$E_F = \frac{\hbar^2}{2m} \cdot \frac{1}{4L^2} = \frac{\hbar^2 n_{\max}^2}{8m L^2} \quad \left. \begin{array}{l} \text{Total # of electrons} = 2 \cdot \text{Volume of} \\ \text{1/8 sphere} \end{array} \right\}$$

$$N = 2 \cdot \left[\frac{1}{8} \cdot \frac{4}{3} \pi n_{\max}^3 \right] \quad \left. \begin{array}{l} \\ \\ \end{array} \right\}$$

$$N = \frac{1}{3} \pi \left[\sqrt{n_x^2 + n_y^2 + n_z^2} \right]^3$$

Solve for n_{\max}

$$\rightarrow n_{\max} = \left(\frac{3N}{\pi} \right)^{1/3}$$

$$E_F = \frac{\hbar^2}{2m} (n_{\max})^2 \cdot \frac{1}{4L^2}$$

$$\boxed{E_F = \frac{\hbar^2}{8mL^2} \left(\frac{3N}{\pi} \right)^{2/3}} \quad \text{as Fermi energy.}$$

$$\text{Since } V = L^3 \Rightarrow L^2 = V^{2/3}$$

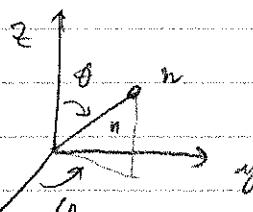
So $E_F = \frac{\hbar^2}{8m} \left(\frac{3N}{\pi V k} \right)^{2/3}$ (for Fermi energy)

number density... intensive property...

Total energy of degenerate Fermi gas

$$U_{\text{tot}} = 2 \iiint_0^\infty \epsilon(n) dx dy dz \rightarrow \text{assuming large \# states...}$$

Convert to spherical coordinates...



with $dV = dx dy dz = r^2 \sin\theta dr d\theta d\phi$

So $U_{\text{tot}} = 2 \iiint_0^{n_{\max}} \epsilon(n) r^2 \sin\theta dr d\theta d\phi dn$

$$= 2 \left(\frac{4\pi}{8} \right) \int_0^{n_{\max}} \epsilon(n) r^2 dn$$

$$= \pi \int_0^{n_{\max}} \epsilon(n) r^2 dn$$

$$= \pi \int_0^{n_{\max}} \frac{\hbar^2 n^2}{8m L^2} r^2 dn$$

$$= \frac{\hbar^2 \pi}{8m L^2} \int_0^{n_{\max}} r^4 dn$$

$$= \frac{\hbar^2 \pi}{8m L^2} \cdot \frac{1}{5} n_{\max}^5 \rightarrow U_{\text{tot}} = \frac{\hbar^2 \pi}{40m L^2} \cdot n_{\max}^5$$

In terms of $E_F = \frac{\hbar^2}{8mL^2} \cdot n_{\max}^2$, $n_{\max} = \left(\frac{3N}{\pi}\right)^{1/3}$

$$U_{\text{tot}} = \frac{\pi E_F}{5} n_{\max}^3$$

2

$$U_{\text{tot}} = \frac{3}{5} N E_F \quad \text{at } T=0$$

temp - isol.

average energy as expected,

a little bit $> \frac{1}{2} E_F$ 

3, average energy per particle ...

$$\bar{U} = U_{\text{tot}}/N = \frac{3}{5} E_F$$

If $E_F \gg kT \sim \text{degenerate gas}$ 

[Fermi Temperature] \rightarrow Temp. at which characteristic thermal energy = Fermi energy

$$kT = E_F \Rightarrow T_F = \frac{E_F}{F} \rightarrow \text{need } T_F \text{ to set degenerate gas over than}$$



[Pressure of degenerate gas] (due to Pauli's exclusion principle)

From

$$dU = TdS - PdV + \mu dN$$

$$\frac{\partial}{\partial V} \left(\frac{dU}{dV} \right)_{S,N} = -P = P_F = -\left(\frac{\partial U}{\partial V} \right)_{S,N}$$

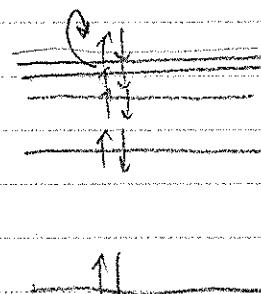
$$\therefore P_F = -\frac{3}{2V} \left[\frac{3}{5} N \frac{\hbar^2}{8m} \left(\frac{3N}{\pi} \right)^{2/3} \cdot V^{-2/3} \right]$$

$$= \frac{3}{5} N \frac{\hbar^2}{8m} \left(\frac{3N}{\pi} \right)^{2/3} \cdot \left(\frac{-2}{2} \right) V^{-5/3} \quad \therefore P_F = \frac{2}{5} N E_F$$

In terms of $U_{\text{tot}} \Rightarrow P = \frac{2}{3} \frac{U_{\text{tot}}}{V} \rightarrow \frac{2}{3}$ of energy density
 \times of degenerate Fermi gas

$P > 0 \rightarrow$ pushing outwards \rightarrow ex white dwarf star prevents collapse due to gravity

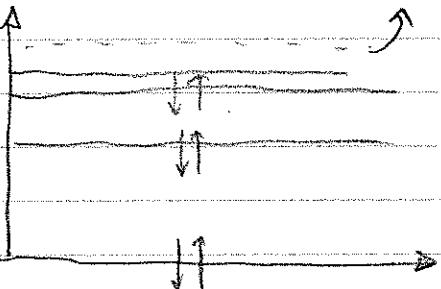
Consider small, non-zero temp

E_F  Total energy gained by degenerate gas
 is proportional to (# of e⁻) \times (E gained per electron)

$$\underline{\text{So}} \quad U_{\text{gained}} \propto N(kT)^2$$

May 6, 2019

(Degenerate Fermi Gas at small non-zero temp)

E_F  $T=0$
 if $\Delta T > 0$, small, $e^- \rightarrow \Delta E = kT$

Energy gained by degenerate $\propto N(kT)^2$
 Fermi-gas

$\times (\# \text{e that can jump}) \times (\text{energy gained})$

$\underline{\text{So}}$ $U_{\text{gained}} \sim N(kT)^2 \rightarrow$ when $\Delta T > 0$, small $\propto (NkT) \propto v(kT)$

So, since $U_{\text{gained}} \propto N(kT)^2$

units of constants = $\left(\frac{1}{\text{energy}}\right)$

$$\text{Gross} \Rightarrow \frac{1}{E_F}$$

Additional constant of proportionality $\Rightarrow \frac{\pi^2}{4}$

$$\text{So } U_{\text{gained}} = \frac{\pi^2}{4 E_F} N(kT)^2$$

∴

$$U_{\text{tot}} = U(T=0) + U(\Delta T)$$

$$U_{\text{tot}} = \frac{3}{5} N E_F + \frac{\pi^2}{4} \frac{N}{E_F} (kT)^2$$

as usage of degeneracy
↑ goes...

this true for any temperature ...

$kT \ll E_F$

Heat capacity

$$\hookrightarrow \text{at constant volume} \Rightarrow C_V = \left(\frac{\partial U}{\partial T} \right)_V$$

$$\text{So } C_V = \frac{2}{3T} \left(\frac{\pi^2}{4} \frac{N}{E_F} (kT)^2 \right)$$

$$\Rightarrow C_V = \frac{\pi^2 N k^2 T}{2 E_F}$$

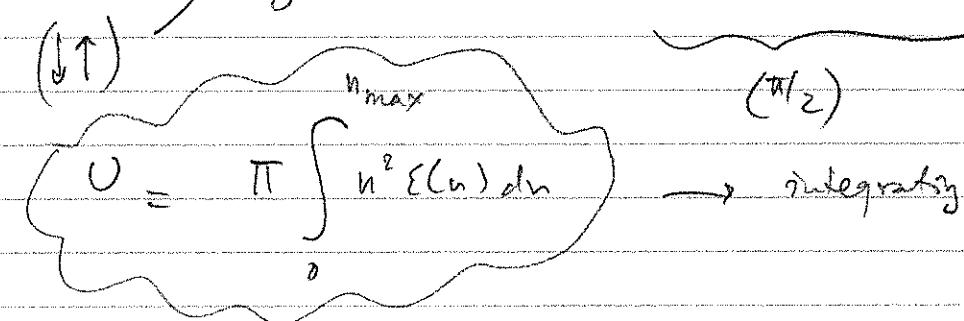
$\hookrightarrow \text{as } T \rightarrow 0, C_V \rightarrow 0$, as expected.

Note

$$C_V \propto T \quad (\text{linearly w.r.t temp})$$

Density of States

$$U = 2 \int_0^{n_{\max}} n^2 \epsilon(n) dn \int_0^{\pi/2} d\phi \int_0^{\pi/2} \sin \theta d\theta$$



What about integrating over all energies...

$$\epsilon = \frac{\hbar^2}{8mL^2} n^2 \rightarrow n = \sqrt{\frac{8mL^2}{\hbar^2}} \sqrt{\epsilon}$$

$$\int_0^{\infty} dn = \sqrt{\frac{8mL^2}{\hbar^2}} \frac{1}{2\sqrt{\epsilon}} d\epsilon \quad (n_{\max} \approx \epsilon_F)$$

~~$$U = \pi \int_0^{\infty} \epsilon \left[\sqrt{\frac{8mL^2}{\hbar^2}} \frac{1}{2\sqrt{\epsilon}} \right] d\epsilon$$~~

$$U_{\text{tot}} = \pi \int_0^{\infty} \epsilon \left[\left(\frac{8mL^2}{\hbar^2} \right)^{1/2} \epsilon \left(\frac{8mL^2}{\hbar^2} \right)^{1/2} \frac{1}{2\sqrt{\epsilon}} \right] d\epsilon$$

Call { Density of states }

$$g(\epsilon) = \pi \left(\frac{8mL^2}{\hbar^2} \right)^{3/2} \cdot \frac{\sqrt{\epsilon}}{2} = \pi (8m)^{3/2} \cdot \frac{\sqrt{\epsilon}}{2\hbar^2}$$

\square $g(\epsilon) \rightarrow$ probability density, or total # of States with energy ϵ

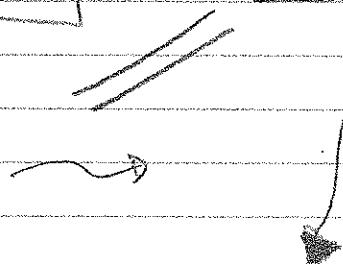
Now,

$$\epsilon_F = \frac{\hbar^2}{8m} \left(\frac{3N}{\pi V} \right)^{2/3}$$

$$g(\epsilon) = \frac{\pi (\epsilon_F)^{3/2}}{2\hbar^3} \sqrt{\epsilon}$$

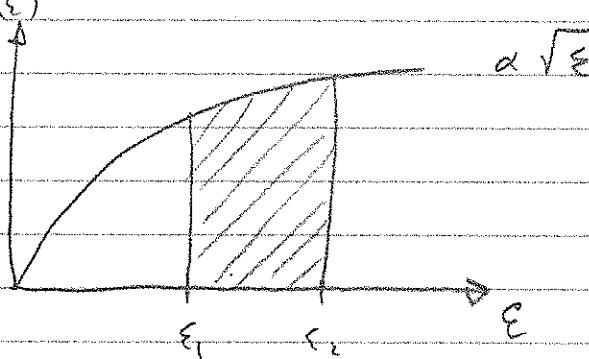
So

$$g(\epsilon) = \frac{3N}{2\epsilon_F^{3/2}} \sqrt{\epsilon}$$



\square Note: $g(\epsilon) \propto V$, independent of N
 $\propto \sqrt{\epsilon}$

Now



\square At $T=0$, then, all ϵ are below ϵ_F , then

$$\left. \begin{array}{l} P(\text{occupied} | \epsilon < \epsilon_F) = 1 \\ P(\text{occupied} | \epsilon > \epsilon_F) = 0 \end{array} \right\}$$

$$\square \quad N(T=0) = \int_0^{\epsilon_F} g(\epsilon) d\epsilon$$

$e^{-E/kT}$ zero
 Σ Fermi

\square For non-zero temperature ...

$$N(T \neq 0) = \int_0^{\infty} g(\epsilon) \cdot P(\epsilon) d\epsilon$$

Prob dist

$$N = \int_0^{\infty} g(\epsilon) P(\epsilon) d\epsilon$$

↓

$$\bar{n}_{FP} = \frac{1}{e^{(\epsilon_F - \mu)/kT} + 1}$$

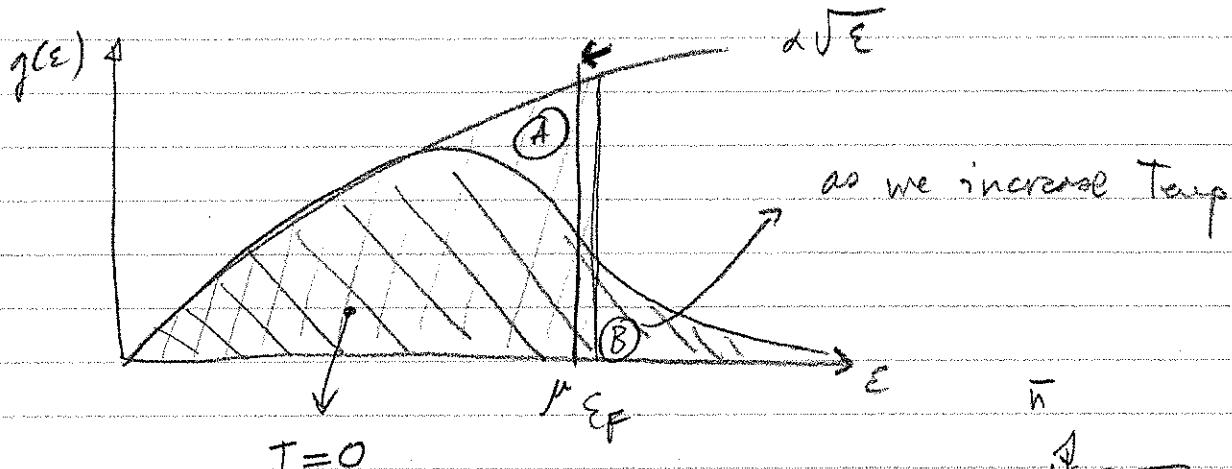
b

$$N = \int_0^{\infty} g(\epsilon) \frac{1}{e^{(\epsilon - \mu)/kT} + 1} d\epsilon$$

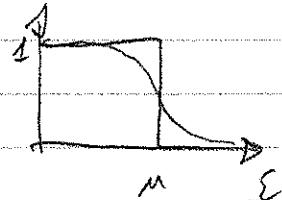
(.stuff)

So, total energy =

$$U_{tot} = \int_0^{\infty} \epsilon g(\epsilon) \frac{1}{e^{(\epsilon - \mu)/kT} + 1} d\epsilon$$



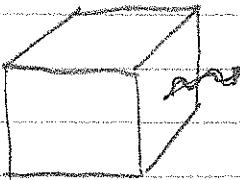
$$\boxed{(Area A) = (Area B)} \quad \text{At } T=0, \epsilon_F = \mu$$



At $T > 0$, n decreases...

(concentration drops)

Black-body radiation



Inside box... definite energy wavefunctions

$$\lambda = \frac{cL}{n}$$

- Each wave has frequency $\nu = \frac{c}{\lambda}$ eq. per hz
- Each wave has 2 df)
- Average thermal energy = $2 \cdot \left(\frac{1}{2}kT\right) = kT$

Ultraviolet Catastrophe \rightarrow too much radiation is predicted at short λ ...

Selective ears from GM \rightarrow energy is quantized.

$$E_n = 0, \hbar\nu, 2\hbar\nu, 3\hbar\nu, \dots$$

$$\text{then } Z = \sum_n e^{-E_n/kT} = 1 + e^{-\hbar\nu/kT} + (e^{-\hbar\nu/kT})^2 + \dots$$

$$= \frac{1}{1 - e^{-\hbar\nu/kT}}$$

$$\underline{\underline{Z}} = \frac{1}{1 - e^{-\hbar\nu/kT}} = \frac{e^{\hbar\nu/kT}}{e^{\hbar\nu/kT} - 1}$$

$$\underline{\underline{E}} = -\frac{1}{z} \frac{\partial z}{\partial \beta} = \frac{kT}{e^{h\nu/kT} - 1}$$

Energy comes in units of $\hbar\nu = \text{two}$,

Then average # of units = $\frac{\text{avg. Energy}}{\hbar\nu}$

$$\frac{\hbar\nu}{\gamma} \overline{n}_{PL} = \frac{\bar{E}}{\hbar\nu} = \frac{1}{e^{\frac{E}{kT}} - 1}$$

Planck's distribution ...

Planck

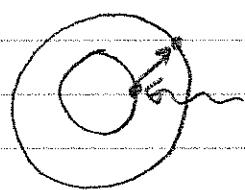
Note NOT the same as Bose-Einstein dist
where

$$\overline{n}_{BE} = \frac{1}{e^{\frac{E_B}{kT}} - 1}$$

So $\mu = 0$ for photons

γ not unoccupied

photons created =
destroyed
all the time



$$\mu_e^- + \mu_\gamma = \mu_e^- \quad \text{so} \quad \mu_\gamma = 0$$

May 7, 2019

→ Blackbody Radiation



→ what is the total energy inside the box

Reminder Planck's distribution gives the average "occupancy" of an energy mode

$$\overline{n}_{PL} = \frac{1}{e^{\frac{E}{kT}} - 1}$$

Allowed wfn $\rightarrow \lambda = \frac{2L}{n}, p = \frac{\hbar n}{2L} \rightarrow$ allowed energies?

Allowed energies $\rightarrow E = pc$, not $P_{\text{kin}}^2 \rightarrow |E| = \frac{hc n}{2L}$

$$\text{In 3D, } E = cp = c/\sqrt{x^2 + p_x^2 + p_y^2 + p_z^2} \\ = \frac{hc}{2L} \sqrt{n_x^2 + n_y^2 + n_z^2}$$

Avg energy per mode, ideal

$$= E \times (\text{occupancy of mode}) =$$

Planck's distribution: \bar{n}_{PC}

So,

$$\text{total energy} \Rightarrow \left[n = 2 \sum n_x \sum n_y \sum n_z \bar{n}_{PC}(E) \right]$$

2 independent
polarization states for photons.

So,

$$U = \sum_{n_x, n_y, n_z} \frac{hc n}{L} \cdot \frac{1}{e^{hc n / 2kT} - 1}$$

Convert this to an integral in spherical coordinates

$$U = \int_0^\infty n^2 \frac{hc n}{L} \frac{1}{e^{hc n / 2kT} - 1} dn \int_0^{\pi/2} d\phi \int_0^{\pi/2} \sin\theta d\theta$$

$$= \left(\frac{\pi}{2}\right) \cdot [\text{change of variable}]$$

$$\varepsilon = \frac{hc n}{2kT} \Rightarrow n^2 = \frac{4\varepsilon^2 L^2}{h^2 c^2}$$

$$d\varepsilon = \frac{hc}{2kT} dn$$

$$= \frac{\pi}{2} \int_0^\infty \frac{4\varepsilon^2 \cdot 2\left(\frac{\varepsilon}{2}\right)}{h^2 c^2} \cdot \frac{1}{e^{\varepsilon / kT} - 1} \left(\frac{2L}{hc}\right) d\varepsilon$$

$$\text{S}, \quad U = \frac{8\pi L^3}{(hc)^3} \int_0^\infty \frac{\epsilon^3}{e^{\epsilon/kT} - 1} d\epsilon \quad \text{Call } L^3 = V$$

then

$$\frac{U}{V} = \int_0^\infty \frac{8\pi}{(hc)^3} \frac{\epsilon^3}{e^{\epsilon/kT} - 1} d\epsilon \quad \rightarrow \text{total energy density (per unit volume)}$$

\downarrow Energy density per unit photon energy.

\hookrightarrow Spectrum of photons \rightarrow called $u(\epsilon)$

Spectrum

$$u(\epsilon) = \frac{8\pi}{(hc)^3} \frac{\epsilon^3}{e^{\epsilon/kT} - 1}$$

PLANCK'S SPECTRUM

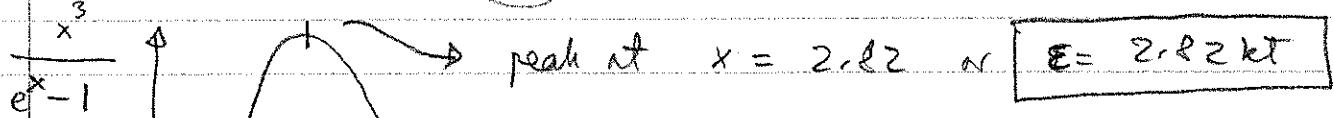
(cancel when convert to λ
fix $d\epsilon \propto d\lambda \dots$)

Next, evaluate the integral..

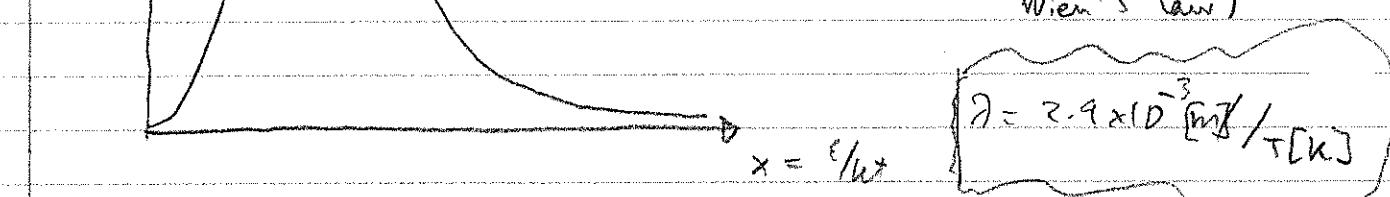
$$x = \epsilon/kT, \quad \text{so} \quad dx = \frac{1}{kT} d\epsilon$$

peak energy of
spectrum of γ

$$\frac{U}{V} = \frac{8\pi}{(hc)^3} \cdot (kT)^4 \int_0^\infty \frac{x^3}{e^x - 1} dx$$



(one version of
Wien's law)



$\int_{-1}^{\infty} \frac{x^3}{e^x - 1} dx = \frac{\pi^4}{15}$ (Appendix B)

$\frac{U}{V} = \frac{8\pi^5 (kT)^4}{15 (hc)^3}$ \rightarrow electromagnetic energy density

Entropy of Photon gas

B First calculate heat capacity, C_V

$$\boxed{C_V = \left(\frac{\partial U}{\partial T}\right)_V \approx 4aT^3 \text{ where } a = \frac{8\pi^5 k^4 \nu}{15 (hc)^3}}$$

Entropy

$$S = \int_0^T \frac{C_V}{T} dT' = \int_0^T 4a \frac{(T')^3}{T'} dT' = \int_0^T (4aT') dT' = \frac{4}{3} a T^3$$

$S = \frac{32\pi^5}{45} V \left(\frac{ht}{hc}\right)^3 \cdot h$ \rightarrow entropy of photon gas..

Pressure of a photon gas...

$$dU = TdS - PdV + \mu dN$$

$$\Rightarrow P = - \left(\frac{\partial U}{\partial V}\right)_{S,N} \rightarrow \text{med } U = U(V,S) \\ \text{if } S \text{ constant, } N = \text{constant} \dots$$

$$\frac{U}{V} = \frac{8\pi^5}{15 (hc)^3} (kT)^4 \approx S \cdot \frac{32\pi^5}{45} \left(\frac{ht}{hc}\right)^3 k \cdot V$$

So want to eliminate temperature ...

Q8 Let $\alpha = \frac{8\pi^5 k^4}{15(hc)^3}$, then $U = \alpha V \cdot T^4$, $S = \frac{4}{3} \alpha V T^{3/2}$

\Rightarrow Solve for temperature ... $T = \left(\frac{3S}{4}\right)^{1/3} \cdot (\alpha V)^{-1/3}$

S $U = (\alpha V) \left(\frac{3S}{4}\right)^{4/3} \cdot (\alpha V)^{-4/3}$

$$\boxed{U = \left(\frac{3S}{4}\right)^{4/3} (\alpha V)^{-1/3}}$$

S, $P = -\left(\frac{\partial U}{\partial V}\right)_{S, N} = -\frac{\partial}{\partial V} \left[\left(\frac{3S}{4}\right)^{4/3} (\alpha V)^{-4/3} \right]_{S, N}$

$$= \left(\frac{3S}{4}\right)^{4/3} \cdot \frac{1}{3} \alpha^{-1/3} V^{-4/3}$$

$$= \frac{1}{3} \left(\frac{3}{4} \left[\frac{4}{3} \alpha V T^3 \right] \right)^{4/3} \alpha^{-1/3} V^{-4/3}$$

S $\boxed{P = \frac{1}{3} \alpha T^4}$

or In terms of U/V ... $\Rightarrow \boxed{P = \frac{1}{3} \frac{U}{V}}$

Compare this pressure of Ideal gas ...

Molar mass

$$PV = NkT \Rightarrow U = \frac{f}{2} NkT = \frac{3}{2} NkT$$

S $PV = \frac{2}{3} U$

S $\boxed{P = \frac{2}{3} \frac{U}{V}}$

Ex

CMB - Cosmic Microwave Background radiation.

$$T = 2.73 \text{ K}, \text{ Peak } \lambda = \frac{2.93 \times 10^{-3}}{2.73} \sim 1 \text{ mm}$$

Total energy density in CMB ...

$$\frac{U}{V} = \frac{8\pi^5 (hc)^4}{45 (hc)^3} = [0.26 \text{ MeV/m}^3]$$

Ordinary matter $1 \text{ proton/m}^3 \rightarrow [1 \text{ GeV/m}^3]$

→ photon density changes pretty low...

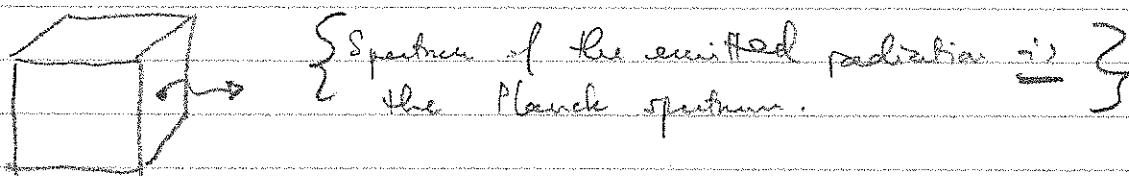
$$\text{Entropy of CMB} \Rightarrow S = \frac{22\pi^5}{45} V \cdot (hc)^3 \cdot k \approx$$

$$\Rightarrow \frac{S}{V} \approx 2.89 \times 10^9 \text{ K} \quad \text{much higher}$$

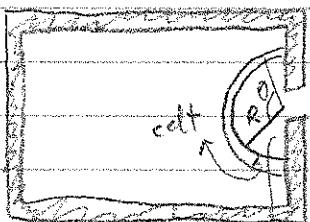
ordinary matter ... $S/V \sim Nk \sim k$.

May 8, 2019

Radiation emitted by a Blackbody



How much energy escapes from hole?



Volume of chunk of radiation that could escape

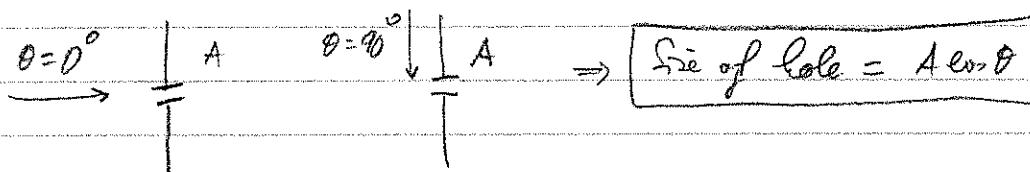
$$= (R d\theta) (R \sin\theta d\phi) (cdt)$$

3D chunk of radiation

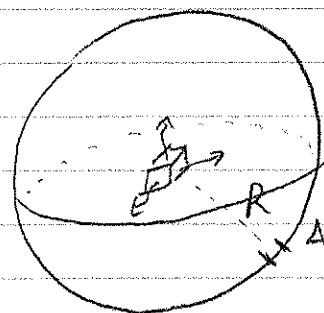
$$\text{Energy density} = \frac{U}{V} = \frac{8\pi^5 (hc)^4}{45 (hc)^3}$$

$$\text{Total energy} = \frac{8\pi^5 (c\tau)^4}{15 (hc)^3} R^2 c \sin \theta d\theta d\phi dt$$

Project hole size depend on angle of photon wrt hole..



Now



probability of photon exiting hole } $\Rightarrow \frac{A \cos \theta}{4\pi R^2}$ = hole size tolerance

Energy that escapes hole

$$U = \frac{U}{V} \times R^2 c \sin \theta d\theta d\phi dt \cdot \frac{A \cos \theta}{4\pi R^2}$$

$$\begin{aligned} U_{\text{tot}} &= \int_0^{2\pi} d\phi \int_0^{\pi/2} d\theta \sin \theta \cos \theta \cdot \left(\frac{A}{4\pi}\right) \cdot c \left(\frac{U}{V}\right) dt \\ &= 2\pi \cdot \frac{A}{4\pi} \frac{U}{V} c dt \underbrace{\int_0^{\pi/2} \cos \theta \sin \theta d\theta}_{1/2} \end{aligned}$$

$$U_{\text{tot}} = \frac{A}{4} \left(\frac{U}{V}\right) c dt$$

Energy per unit time gives power

\Rightarrow "luminosity"

$$P = \frac{U_{\text{tot}}}{dt} \rightarrow \text{Flux} = \frac{\text{Power}}{\text{Area}} = \frac{Uc}{4V}$$

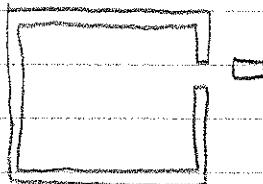
$$\boxed{B} \quad \text{Flux} = \frac{c}{4} \left(\frac{u}{v} \right) = \frac{c}{4} \left(\frac{2\pi^5}{15} \right) \frac{(kT)^4}{(hc)^3} = \frac{2\pi^5}{15} \frac{(kT)^4}{h^3 c^2} = \sigma T^4$$

$$\sigma = \frac{2\pi^5 h^4}{15 k^3 c^2} = 5.67 \times 10^{-8} \text{ W/m}^2 \text{ K}^4$$

Stefan - Boltzmann Constant

{ Stefan - Boltzmann Law }

Why is this blackbody radiation?



What if our object is not black?

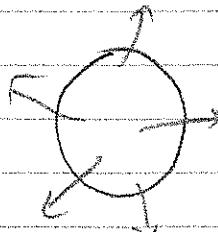
Some λ 's are reflected rather than absorbedDefine Emissivity, ϵ ϵ = amount of radiation absorbedIf $\epsilon = 1 \rightarrow$ blackbodyIf $\epsilon = 0 \rightarrow$ perfect reflectorNote ϵ is λ -dependent.

$$\boxed{b} \quad \frac{\text{Power}}{\text{Area}} \rightarrow \text{Flux} = \epsilon \sigma T^4$$

$$\text{Power} = \epsilon \sigma A T^4 \rightarrow \text{luminosity}$$

Example Sun assume $\epsilon = 1$ Solar luminosity = $\frac{\text{Power}}{4\pi} \Rightarrow$

$$L_0 = 3.8 \times 10^{26} \text{ W}$$



$$A = 4\pi R_0^2, \quad F_{\text{at surface}} = \frac{L}{A} = \frac{L}{4\pi R_0^2} \cdot F_0 = e \sigma T^4$$

$$\text{So } T = \sqrt[4]{\frac{L}{4\pi R_0^2 e \sigma}} = \sqrt[4]{\frac{L}{4\pi R_0^2 \sigma}} \approx 5800 \text{ K}$$

Can do we Wien's law

$$\lambda_{\text{peak}} = \frac{2.9 \times 10^{-3}}{T} \rightarrow \text{set } T \rightarrow \text{set } R \dots$$

Can do the same thing for the Earth...

May 10, 2004

BOSE-EINSTEIN CONDENSATES

Now, dealing with ordinary bosons at 0, $\mu = \mu(T, P)$

Thermism \Rightarrow a gas of bosons will abruptly "condense" into the ground state energy as T goes below critical value.

1st under $T \rightarrow 0$ Every boson in ground state

$$E_0 = \frac{\hbar^2}{8m^2 L^2} (1^2 1^2 1^2) = \frac{3\hbar^2}{8m L^2}$$

Arg # of atoms, in ground state at temp T

$$N_0 = \pi_{DE} = \frac{1}{e^{(E_0 - \mu)/kT} - 1} \quad \text{At low } T, N_0 \rightarrow \text{large}$$

$$\underbrace{e^{(E_0 - \mu)/kT} - 1}_{\text{close to 1}} \rightarrow \text{small } \# \quad \text{since } \frac{E_0 - \mu}{kT} \ll 1$$

Now, $e^x \approx 1+x$

$$\text{So } N_0 \approx \frac{1}{1 + \frac{\epsilon_0 - \mu}{kT}} \approx \frac{kT}{\epsilon_0 - \mu} \rightarrow \text{large } N_0 \text{ at low } T$$

at $T=0$, $\mu = \epsilon_0$

at $T \geq 0$, $\mu < \epsilon_0$ to keep $N_0 \approx \text{constant}$

Q How low does T need to be for N_0 to be large?

$$N_{\text{tot}} = \sum_{\epsilon} \frac{1}{e^{(\epsilon - \mu)/kT} - 1} \quad \text{If } kT \gg \epsilon, \text{ convert sum to integral}$$

$$\Rightarrow N_{\text{tot}} = \int_0^{\infty} g(\epsilon) \frac{1}{e^{(\epsilon - \mu)/kT} - 1} d\epsilon$$

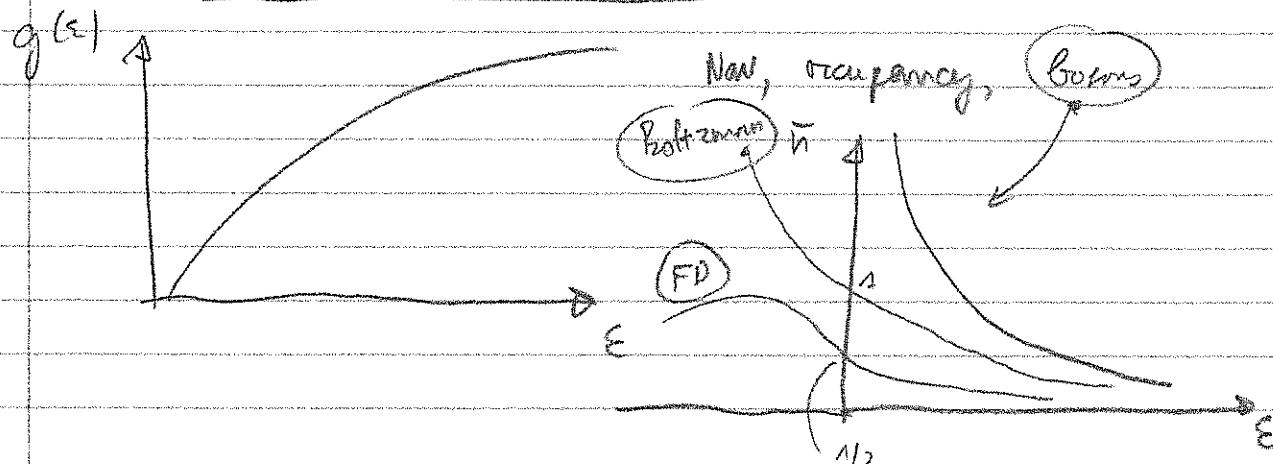
density of states - multiplying

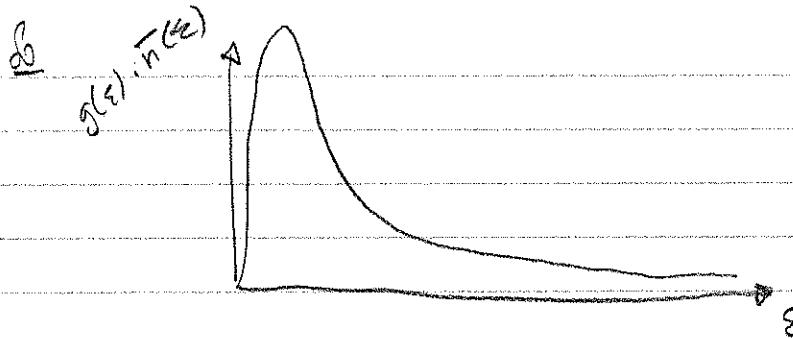
for fermions

$$g(\epsilon) = \frac{\pi (2m)^{3/2}}{2h^3} V \sqrt{\epsilon} \quad (\text{fermions})$$

For bosons, divide by 2 (since there's only one spin)

$$\text{So } g(\epsilon) = \frac{2}{V\epsilon} \left(\frac{2\pi m}{h^2} \right)^{3/2} \cdot V \sqrt{\epsilon} \quad \text{or density of states for bosons}$$





Q Total # of particles ...

$$N_{\text{tot}} = \int_0^{\infty} g(\epsilon) \frac{1}{e^{(\epsilon-\mu)/kT} - 1} d\epsilon$$

Q guess values for μ ... 1st guess $\mu = 0$

$$\begin{aligned} \text{So } N_{\text{tot}} &= \int_0^{\infty} \frac{2}{\sqrt{\pi}} \left(\frac{2\pi m}{h^2} \right)^{3/2} \sqrt{\epsilon} \frac{1}{e^{\epsilon/kT} - 1} d\epsilon \\ &= \frac{2}{\sqrt{\pi}} \left(\frac{2\pi m}{h^2} \right)^{3/2} \sqrt{\int_0^{\infty} \sqrt{\epsilon} \cdot \frac{1}{e^{\epsilon/kT} - 1} d\epsilon} \end{aligned}$$

Change of variable $\Rightarrow x = \frac{\epsilon}{kT}$, $d\epsilon = \frac{1}{kT} dx$

$$N_{\text{tot}} = \frac{2}{\sqrt{\pi}} \left(\frac{2\pi mkT}{h^2} \right)^{3/2} \sqrt{\int_0^{\infty} \frac{\sqrt{x}}{e^x - 1} dx}$$

(2-315)

$$N_{\text{tot}} = (2.612) \left[\frac{2\pi mkT}{h^2} \right]^{3/2} \cdot \sqrt{\quad}$$

But if $T \neq T_c$, $N \neq N_c$ \rightarrow wrong ...

Fact At $T = T_c \rightarrow$ condensation temperature, this is true

$$N_{\text{tot}} = (2.612) \left[\frac{2\pi mkT_c}{h^2} \right]^{3/2} \cdot \sqrt{\quad}$$

S

$$\delta t_c = 0.527 \left(\frac{\hbar^2}{2m\pi} \right) \left(\frac{N}{V} \right)^{2/3} \rightarrow (\text{density})$$

At high temperatures T_c , ($T \gg E$)

expect very few bosons in the ground state --

↳ large $e^{E_0/kT} \rightarrow$ large $\frac{e^{-E_0}}{kT} \rightarrow$ [weak $\mu < 0$]

At low T , ($T \ll T_c$)

$kT \gg E_0$, i.e. $kT \gg E \rightarrow$ can convert the sum to an integral

BB b, just consider excited states where

$kT \gg E_0 \rightarrow$ have integral again.

So, $\#_{\text{excited}} = (2.612) \left(\frac{2\pi m k T}{\hbar^2} \right)^{3/2} \cdot V$

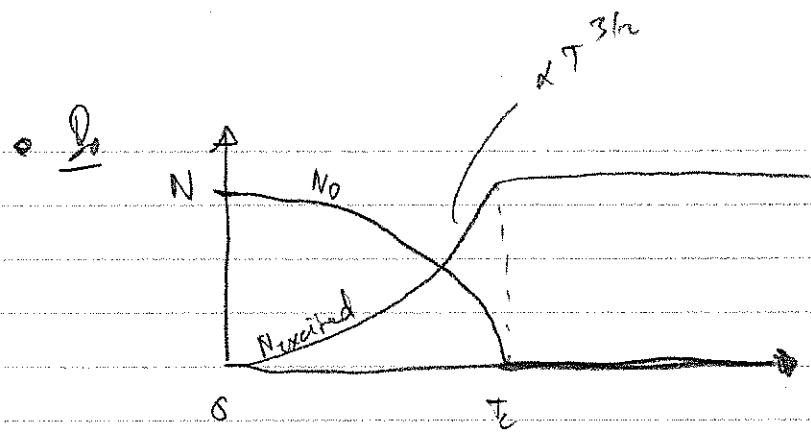
And $N_{\text{tot}} = (2.612) \left(\frac{2\pi m E_0}{\hbar^2} \right)^{3/2} \cdot V$

low temp

And so $N_{\text{excited}} = N_{\text{tot}} \left(\frac{T}{T_c} \right)^{3/2}$ * $T \ll T_c$

→ the rest must be in the ground state... ↗ low temp...

$$N_0 = N_{\text{ground}} = N_{\text{tot}} - N_{\text{excited}} = \left[1 - \left(\frac{T}{T_c} \right)^{3/2} \right] N_{\text{tot}}$$



■ T_c is approximately when $\frac{V}{N} \approx V_0$ $\left(\frac{2\pi mkT_c}{\hbar^2}\right)^{3/2}$

n

THE END)