#### Supplementary Material

This document contains Supplementary Material associated with the paper "LEVEL: A Computer Program for Solving the Radial Schrödinger Equation for Bound and Quasibound Levels", submitted to the *Journal of Quantitative Spectroscopy and Radiative Transfer* in February 2016. It consists of the six Appendices enumerated below. Note that Equation and Reference numbering appearing herein refer to the equation and reference numbering in the Journal Article.

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#### Appendix A. Structure of the Input Data File

All of the READ statements for inputting data to the program, and the associated logical structure, are listed here. Appendix B then provides a detailed description of the nature of and/or options associated with each of the input variables.

```
READ(5,*,END=999) IAN1, IMN1, IAN2, IMN2, CHARGE, NUMPOT
#1
#2
         IF (CHARGE.NE.O) READ(5,*) hCHARGE1, hCHARGE2
#3a
         IF(IAN1.LE.O) READ(5,*) NAME1, MASS1
#3b
         IF(IAN2.LE.O) READ(5,*) NAME2, MASS2
#4
         READ(5,*) TITL
#5
         READ(5,*) RH, RMIN, RMAX, EPS
         DO IPOT= 1, NUMPOT
#6
             READ(5,*) NTP, LPPOT, OMEGA, VLIM
             IF(NTP.GT.O) THEN
                 READ(5,*) NUSE, IR2, ILR, NCN, CNN
#7
                 READ(5,*) RFACT, EFACT, VSHIFT
#8
#9
                 READ(5,*) (XI(I), YI(I), I= 1,NTP)
               ELSE
#10
                  READ(5,*) IPOTL, QPAR, PPAR, Nbeta, APSE, IBOB
                 READ(5,*) DSCM, REQ, Rref
#11
                 IF(IPOTL.GE.4) THEN
#12
                     READ(5,*) NCMM, rhoAB, sVSR2, IDSTT
                     DO i= 1, NCMM
#13
                         READ(5,*) MMLR(i),CMM(i)
                         ENDDO
                     ENDIF
                 IF(NVARB.GT.O) THEN
                     IF((IPOTL.EQ.4).AND.(APSE.GT.0)) THEN
                         DO i= 1, NVARB
```

```
#14a
                             READ(5,*) XPARM(I), PARM(I)
                             ENDDO
                       ELSE
#14b
                         READ(5,*) (PARM(I), I=1,NVARB)
                     ENDIF
                 IF(IBOB.GT.O) THEN
                     READ(5,*) MN1R, MN2R, qAD, pAD, NU1, NU2, qNA, NT1, NT2
#15
#16
                     IF(NU1.GE.O) READ(5,*) (U1(I), I=0,NU1)
#17
                     IF(NU1.GE.O) READ(5,*) U1INF
                     IF(NU2.GE.0) READ(5,*) (U2(I), I=0,NU2)
#18
#19
                     IF(NU2.GE.O) READ(5,*) U2INF
#20
                     IF(NT1.GE.0) READ(5,*) (T1(I), I=0,NT1)
#21
                     IF(NT1.GE.O) READ(5,*) T1INF
#22
                     IF(NT2.GE.O) READ(5,*) (T2(I), I=0,NT2)
#23
                     IF(NT2.GE.O) READ(5,*) T2INF
                     ENDIF
               ENDIF
             ENDDO
         READ(5,*) NLEV1, AUTO1, LCDC, LXPCT, NJM, JDJR, IWR, LPRWF
#24
         NLEV= MAX(1, NLEV1)
         IF(AUTO1.GT.0) READ(5,*) (IV(I), IJ(I), I= 1,NLEV)
#25a
#25b
         IF(AUTO1.LE.O) READ(5,*) (IV(I), IJ(I), GV(I), I= 1,NLEV)
         IF((LXPCT.NE.O).AND.(LXPCT.NE.-1)) THEN
#26
             READ(5,*) MORDR, IRFN, DREF
#27
             IF((IABS(IRFN).LE.9).AND.(MORDR.GE.0)) READ(5,*) (DM(J), J= 0,MORDR)
             IF(IRFN.GE.10) THEN
#28
                 READ(5,*) NRFN, RFLIM
#29
                 READ(5,*) NUSEF, ILRF, NCNF, CNNF
                 READ(5,*) RFACTF, MFACTF
#30
#31
                 READ(5,*) (XIF(I), YIF(I), I= 1,IRFN)
                ENDIF
             ENDIF
         IF(IABS(LXPCT).GE.3) THEN
             READ(5,*) NLEV2, AUTO2, J2DL, J2DU, J2DD
#32
#33a
             IF(AUTO2.GT.0) READ(5,*) (IV2(I), I= 1, NLEV2)
#33b
             IF(AUTO2.LE.0) READ(5,*) (IV2(I),GV(I),I= 1,NLEV2)
           ENDIF
```

## Appendix B. Definitions and Description of Input Data File

Read integers identifying the molecule or system.

- #1. READ(5,\*) IAN1, IMN1, IAN2, IMN2, CHARGE, NUMPOT
  - IAN1 & IAN2: integer atomic numbers of the atoms/particles #1 and 2 forming the molecule. If both are positive and  $\leq 109$ , atomic masses from the tabulation in subroutine MASSES are used to generate the reduced mass of the system. If either is < 0 or > 109 the mass of that non-standard particle will be input via READ #3. Setting IANi = 0 selects masses of proton, deuteron or triteron for mass numbers IMNi = 1 3, respectively.
  - IMN1 & IMN2: integer mass numbers of the atoms/particles #1 and 2 forming the molecule. For a normal stable atomic isotope, its mass is taken from the tabulation in subroutine MASSES; if its value lies outside the range for the normal stable isotopes of that atom, the abundance-averaged atomic mass will be used.
  - **CHARGE:** ± integer for the total charge on the molecule. Normally causes the reduced mass of a molecular ion to be defined as the 'charge-modified' reduced mass of Eq. (2) [5].
  - **NUMPOT:** the number of potentials considered: NUMPOT = 1 for calculations involving only a single potential function; NUMPOT = 2 to input and generate two different potentials and calculate matrix elements coupling their levels.
- #2 If (CHARGE  $\neq 0$ ) READ(5,\*) CHARGE1, CHARGE2
  - CHARGE1 & CHARGE2: the integer number of  $m_e/2$  masses to be added to or subtracted from the normal masses of atoms #1 and #2 prior to calculation of a conventional 2-body reduced mass for each isotopologue [42, 68]. If CHARGE1 = CHARGE2 = 0, use Watson's charged-modified reduced mass for all species. Otherwise, necessarily,  $^{1}/_{2}$  (CHARGE1 + CHARGE2) = CHARGE.

In the special case in which IAN1 and/or IAN2 is either  $\leq 0$  or > 109, read in a two-character alphanumeric name for that particle and its mass (in amu). This facilitates the treatment of model systems or exotic species such as muonium or positronium "molecules".

```
#3.a IF(IAN1.LE.O) READ(5,*) NAME1, MASS1
#3.b IF(IAN2.LE.O) READ(5,*) NAME2, MASS2
```

- **NAME1 & NAME2:** a two-character alphanumeric name for the (1 or 2) particle whose mass is being read, enclosed in single quotes, as in 'mu'.
- MASS1 & MASS2: the masses of particles 1 and 2, in amu.

Read a text title or description for the calculation.

```
^{\#}4. READ(5,510) (TITL(I),I= 1,20)
```

**TITL:** a title or output header for the calculation, consisting of up to 78 characters on a single line, enclosed between single quotes: e.g., 'title of problem'.

Read real numbers defining the mesh and range of the numerical integration (all in Å), and the eigenvalue convergence criterion to be used (in  $cm^{-1}$ ).

#5 READ(5,\*) RH, RMIN, RMAX, EPS

- **RH**: the numerical integration mesh size; see discussion associated with Eq. (3) in § 2.1.
- RMIN & RMAX: the inner and outer limits, respectively, of the range of numerical integration (see § 2.1). Plausible zero<sup>th</sup> order estimates would be  $RMIN \approx 0.6 \times (potential inner wall position)$  and RMAX fairly large (say 40 Å). Internally RMAX is set to the smaller of: this read-in value, or the largest distance allowed by RMIN, RH and the array dimension NDIMR (see § 3).
- **EPS:** the eigenvalue convergence parameter used by SCHRQ (in  $cm^{-1}$ ). To ensure that appropriately accurate expectation values or matrix elements are generated, it should normally be set ca. 2 orders of magnitude smaller than the eigenvalue precision actually required.

Some combination of the next 18 Read statements defines the potential energy function. A particular case always starts with Read  $^{\#}6$ , but then uses either Reads  $^{\#}7-9$  for numerical interpolation over a set of input turning points, or (some of) Reads  $^{\#}10-23$  for the case of an analytic potential function.

- #6. READ(5,\*) NTP, LPPOT, OMEGA, VLIM
  - NTP: an integer that is set  $\leq 0$  to generate an analytic potential using POTGEN, in which case the program skips Reads #7–9 and goes directly to Read #10. If NTP > 0, it is the number of turning points to be input via Read #9.
  - **LPPOT:** controls printing of the potential array (normally set =0 to have no printing). If LPPOT > 0, write the potential and its first 2 derivatives-by-differences to standard output (Channel-6) at every LPPOT<sup>th</sup> mesh point; it is sometimes useful to do this when troubleshooting. Setting LPPOT < 0 writes the resulting potential in condensed format to Channel-8 at every  $|\text{LPPOT}|^{th}$  mesh point; this is useful if one wants to employ this calculated potential as input for a plotting program.
  - **OMEGA:** the (integer) projection of the electronic orbital angular momentum onto the molecular axis for this state. It causes the reduced centrifugal potential to become  $[J(J+1)-{\tt OMEGA}^2]\hbar^2/(2\mu r^2)$ . Setting  ${\tt OMEGA} \geq 99$  will cause the centrifugal potential to have the form  $[J^2-1/4]\hbar^2/(2\mu r^2)$  that is appropriate for rotation constrained to a plane.
  - **VLIM:** the absolute energy (in cm<sup>-1</sup>) of the potential asymptote. This value sets the absolute energy scale for the calculations. For power-series (GPEF- or Dunham-type) potentials (IPOTL = 2), it specifies the energy at the potential function minimum, where  $r=r_e$ .

For a pointwise potential we must specify how the interpolation is to be done, and since RMAX usually lies outside the range of the input turning points, we also must specify how the potential is to be represented in that large-r extrapolation region.

- #7. READ(5,\*) NUSE, IR2, ILR, NCN, CNN
  - **NUSE:** specifies how the interpolation is to be done. If NUSE > 0, use NUSE—point piecewise polynomials; if NUSE  $\le 0$ , perform cubic spline interpolation. For highly precise and smooth input points, such as those generated from an RKR calculation, NUSE = 8, 10 or 12 is often most appropriate; for less precise or less dense points, such as those from ab initio calculations, low-order piecewise polynomials (NUSE = 4) or a spline (NUSE  $\le 0$ ) is normally best.

- IR2: for very steep repulsive potential walls, better interpolation is often attained by interpolating over  $r^2 \times V(r)$ , rather than over V(r) itself; setting integer IR2 > 0 causes this to be done (normally recommended). A comparison between results obtained with this option turned on vs. off provides an indication of the magnitude of 'interpolation noise' uncertainties in the final results.
- **ILR:** specifies how to extrapolate from the outermost read-in turning points to RMAX. For a long extrapolation, one of ILR = -1, 0 or 1 is often most appropriate; however, if the outer turning points extend moderately close to the dissociation limit (at VLIM), one should set ILR  $\geq 2$ , specify the theoretically appropriate value of NCN ( $\geq 1$ ), and if it is available, also input an estimate of CNN (see below).

```
For ILR < 0, fit the last 3 points to: V(r) = VLIM - A \times \exp[-b(r - r_o)^2]
```

For ILR = 0, fit the last 3 points to: 
$$V(r) = VLIM - A \times r^p \times \exp[-br]$$
.

For ILR = 1, fit the last 2 points to: 
$$V(r) = VLIM - A/r^B$$
.

- For ILR = 2 or 3, respectively, fit the outermost 2 or 3 points to a sum of 2 or 3 inverse-power terms, with powers differing by 2:  $V(r) = \text{VLIM} \sum_{m=0}^{\text{ILR}-1} C_{\text{NCN}+2m} / r^{\text{NCN}+2m}$ .
- For ILR  $\geq 4$ , fit outermost ILR turning points to a sum of ILR inverse-power terms, with powers differing by 1:  $V(r) = \text{VLIM} \sum_{m=0}^{\text{ILR}-1} C_{\text{NCN}+m}/r^{\text{NCN}+m}$ .
- NCN: For inverse-power potential extrapolation with ILR  $\geq 2$ , NCN (> 0) specifies the limiting inverse-power behaviour:  $V(r) \propto \text{VLIM} \text{CNN}/r^{\text{NCN}}$ . Otherwise (for ILR  $\leq 1$ ), it is a dummy input variable.
- CNN: For inverse-power potential extrapolation with ILR  $\geq 2$ , setting CNN  $\neq 0$  causes the leading inverse-power coefficient to be fixed at the read-in value CNN =  $C_{\text{NCN}}$  [cm<sup>-1</sup> Å<sup>NCN</sup>] rather than to be determined from a fit to the outermost turning points.

The input turning points may come from *ab initio* or RKR calculations, and their energies may need to be shifted to make them consistent with the value of VLIM input through READ #6, and they may also need also need to have their units converted to those employed in the program (Å and cm<sup>-1</sup>).

- #8. READ(5,\*) RFACT, EFACT, VSHIFT
  - **RFACT & EFACT:** multiplicative factors required to convert units of the NTP input turning point distances XI(i) and energies YI(i) to Å and cm<sup>-1</sup>, respectively. If no conversion is required, set these factors at 1.0D+0.
  - **VSHIFT:** an energy shift (in cm<sup>-1</sup>) to be added to the input potential point energies to make them consistent with the user-specified asymptote energy VLIM. It addresses the fact that the input *ab initio* or RKR turning points may be expressed relative to a different energy zero.

Read in the actual turning points.

```
^{\#}9. READ(5,*) (XI(I), YI(I), I= 1,NTP)
```

XI(i) & YI(i): are the (distance, energy) input turning points defining the potential function.

If the input potential is defined by an analytic function (i.e., when NTP  $\leq 0$ ), use subroutine POTGEN, which reads parameters via some or all of Reads  $^{\#}10-23$ . For a user-supplied POTGEN function, no input parameters are read here, and its calling sequence must match that expected by subroutine PREPOT (see the discussion of § 2.6.9). The variable NVARB, which specifies the number of parameters being read in through Read  $^{\#}14$ , is determined internally, as specified below.

#10. READ(5,\*) IPOTL, QPAR, PPAR, Nbeta, APSE, IBOB

**IPOTL** is an integer specifying the type of analytic function used for the potential.

- IPOTL = 1: generates a Lennard-Jones (m = QPAR, n = PPAR) potential energy function using Eq. (12). In this case APSE and Nbeta are dummy variables, and NVARB = 0.
- IPOTL = 2: uses Eq. (13) to generate a GPEF power series potential of order  $N_{\beta}=$  Nbeta using Seto's [27] form of the Šurkus [26] expansion variable  $z=z(r)=(r^{\text{QPAR}}-r_e^{\text{QPAR}})/(a_S\,r^{\text{QPAR}}+b_S\,r_e^{\text{QPAR}})$ , with  $\beta_0$  defined by the input value of DSCM, PARM $(i)=\beta_i$  for i=1 to Nbeta,  $a_S=\text{PARM}(\text{Nbeta}+1)$  and  $b_S=(\text{Nbeta}+2)$ . Note that the Šurkus case of QPAR <0 is accommodated by Seto's identity [27]:  $z(-\text{QPAR},a_S,b_S)=z(\text{QPAR},-b_S,-a_S)$ . For this case NVARB = Nbeta +2, while QPAR, APSE and NCMM are dummy variables.
  - Dunham expansions are generated by setting QPAR = 1,  $\alpha_S = 0.0$  and  $b_S = 1.0$ .
  - SPF expansions are generated by setting QPAR = 1,  $\alpha_S = 1.0$  and  $b_S = 0.0$ .
  - Ogilvie-Tipping expansions are generated by setting QPAR = 1,  $\alpha_S = b_S = 0.5$ .
  - A harmonic oscillator potential is obtained by setting QPAR = 1, Nbeta = 0,  $a_S = 0.0$  and  $b_S = 1.0$ , and the harmonic force constant is  $k = 2 \, \text{DSCM}/\text{REQ}^2$ .
  - All of these polynomial-type potentials have an undefined (or at best, indirectly-defined) asymptote, so parameter VLIM defines the potential energy minimum.
  - If QPAR = 0, the potential is generated as an order-Nbeta polynomial in r whose constant coefficient is set as  $c_0 = \text{VLIM}$  and NVARB = Nbeta.
- IPOTL = 3: generates the Morse or EMO potential of Eq. (15), in which  $\mathfrak{D}_e = \mathtt{DSCM}$ ,  $r_e = \mathtt{REQ}$ , and the expansion-variable of Eq. (17) is defined by the positive integer  $q = \mathtt{QPAR}$ , while the expansion coefficients are  $\mathtt{PARM}(i) = \beta_{i-1}$  for i = 1 to  $\mathtt{NVARB} = (\mathtt{Nbeta} + 1)$ . In this case PPAR and APSE are dummy variables. Setting  $\mathtt{Nbeta} = 0$  ( $\mathtt{NVARB} = 1$ ) yields the ordinary Morse potential.
  - If  $\operatorname{QPAR} \leq 0$ , generate the 4-parameter Morse-like potential of Hua Wei [36],  $V(r) = \mathfrak{D}_e \left( [1-e^{-b\,(r-r_e)}]/[1-C\,e^{-b\,(r-r_e)}] \right)^2$  in which  $b = \operatorname{PARM}(1)$  and  $C = \operatorname{PARM}(2)$ . In this case NVARB = 2 while QPAR, APSE and Nbeta are dummy variables.
- IPOTL = 4: generates an MLR potential from Eqs. (19–20) [33, 34, 37], in which  $\mathfrak{D}_e \equiv$  DSCM,  $r_e \equiv \text{REQ}$ , and the potential tail  $u_{LR}(r)$  is defined either by Eq. (20) or by one of the coupled-state matrix eigenvalues discussed at the end of § 2.6.4.
  - For APSE  $\leq 0$ , the exponent coefficient in Eq. (19) is represented by the constrained polynomial expansion of Eq. (23), in which positive integers QPAR = q and PPAR = p are the powers defining its two radial variables, and the upper bound on the summation is  $N_{\beta} = \text{Nbeta}$ , while the exponent expansion coefficients are PARM $(i) = \beta_{i-1}$  for i = 1 to NVARB = (Nbeta + 1).

- For APSE > 0, the exponent coefficient in Eq. (19) is represented by the natural cubic spline of Eq. (24) passing through Nbeta points at distances defined by the set of input  $y_q^{\text{ref}}$  values, whose ordinate values  $\beta_i = \text{PARM}(i)$  for i=1 to Nbeta define the potential function shape.
- IPOTL = 5: generates the DELR potential of Eqs. (28–30) [11], in which  $\mathfrak{D}_e \equiv \mathtt{DSCM}$ ,  $r_e \equiv \mathtt{REQ}$ , the power defining the expansion variable  $y_q^{\mathrm{ref}}(r)$  is  $\mathtt{QPAR} = q$ , and the exponent coefficient  $\beta(r)$  is the simple power-series expansion of Eq. (16) in  $y_q^{\mathrm{ref}}(r)$  with expansion coefficients  $\mathtt{PARM}(i) = \beta_{i-1}$  for i=1 to (NVARB = Nbeta + 1). The additive long-range tail function  $u_{\mathrm{LR}}(r)$  is defined either by Eq. (20) or by one of the diagonalizations mentioned at the end of §2.6.4 (see READS #12 and 13), and PPAR is a dummy parameter.
- IPOTL = 6: generates a generalized HFD-type potential from Eq. (31), with  $A_{\rm HFD}$  and  $\beta_1$  defined (internally) by the input values of  $\mathfrak{D}_e \equiv {\tt DSCM}$ ,  $r_e \equiv {\tt REQ}$ , and the attractive inverse-power-sum tail, while the parameters defining the damping function  $D_{\rm HFD}(r)$  are read in as  ${\tt PARM}(i) = \alpha_i$  for i = 1-3, and the other exponent coefficients are  $\beta_2 = {\tt PARM}(4)$  and  $\gamma = {\tt PARM}(5)$ . For this case, the inverse-power long-range coefficients  $C_m$  (in units cm<sup>-1</sup>·Å<sup>m</sup>) are input through READ #13, and Nbeta = NVARB = 5, while PPAR, QPAR and APSE are all dummy parameters.
- IPOTL = 7: generates a generalized Tang-Toennies-type potential from Eq. (33), with the attractive term  $u_{LR}(r)$  defined by READS #12 and 13, and the repulsive term parameters  $\{\beta_i\}$  read in as PARM(i) for i=1 to NVARB = Nbeta = 9. The reported values of the well depth  $\mathfrak{D}_e$  and equilibrium distance  $r_e$  are read in as DSCM and REQ, respectively, and the code compares them with the actual energy and position of the potential minimum as defined by the  $\{\beta_i\}$  and  $\{C_m\}$  input parameters. For this case, PPAR, QPAR, and APSE are dummy parameters.
- IPOTL = 8: generates a 'Hannover Polynomial Potential' (HPP) [58] from Eq. (34), a power series of order Nbeta in the variable  $\xi = (r-r_m)/(r+b\,r_m)$ , with coefficients  $\beta_i = \text{PARM}(i+1)$  for i=0 to Nbeta, in which b=PARM(Nbeta+2). The well depth  $\mathfrak{D}_e$  is read as DSCM, and the reference distance  $r_m$  (which for  $a_1 \neq 0$  is not identical to  $r_e$ ) is read in as REQ. For  $r < r_{\text{inn}} \equiv \text{PARM}(\text{Nbeta}+3)$  the potential is extrapolated inward by smoothly attaching the function  $A\,e^{-\alpha(r-r_{\text{inn}})}$  at distance  $r_{\text{inn}}$ . For  $r > r_{\text{out}} \equiv (\text{Nbeta}+4)$  the potential is extrapolated outward continuously as the sum of NCMM inverse-power terms defined by READs #12 and 13, with the (internal) inclusion of an additional term  $C_{m_{\text{L}}}/r^{m_{\text{L}}}$  with  $m_{\text{L}} = [\text{MMLR}(\text{NCMM})+2]$ , whose coefficient  $C_{m_{\text{L}}}$  is defined (internally) to attach this long-range tail continuously to the polynomial at  $r = r_{\text{out}}$ . For this model, QPAR, PPAR and APSE are dummy parameters, and NVARB = (Nbeta + 4).
- QPAR, PPAR, Nbeta and APSE: integers used to characterize specific potential forms (see above).
- **IBOB**: an integer to specify whether (for IBOB > 0) or not (for IBOB  $\leq$  0) atomic-mass-dependent Born-Oppenheimer breakdown correction terms are to be included in the potential energy function V(r), and/or in the centrifugal  $\{[J(J+1) \Omega^2]\hbar^2/(2\mu r^2)\}$  potential (see § 2.7).

- #11. READ(5,\*) DSCM, REQ, Rref
- #12. IF(IPOTL.GE.4) READ(5,\*) NCMM, rhoAB, sVSR2, IDSTT
- #13. IF(IPOTL.GE.4) READ(5,\*) (MMLR(I), CMM(I), I= 1,NCMM)
  - **DSCM:** normally (except for the IPOTL = 2 case) the potential well depth  $\mathfrak{D}_e$  in cm<sup>-1</sup>.
  - **REQ:** normally (except for the IPOTL = 8 case, in which it defines  $r_m$ ) the equilibrium distance  $r_e$  in Å.
  - **Rref:** the reference distance in the definition of the exponent expansion radial variable of Eqs. (17) and (23). If the input value is  $\leq 0.0$ , the code sets  $r_{\text{ref}} = r_e$ .
  - **NCMM:** the number of inverse-power long-range terms to be incorporated into  $u_{LR}(r)$  via Eq. (20), or to be used to define the elements of the  $2 \times 2$  or  $3 \times 3$  matrices whose eigenvalues define  $u_{LR}(r)$  for nS + nP alkali homo-dimers [33, 49–51, 69].
    - For the  $2 \times 2$  alkali-homodimer  $(X_2)$  cases, set NCMM = 7 with MMLR(1) = 0 or -1 and MMLR(i > 1) = 3, 3, 6, 6, 8, 8, while the input values of CmVAL(i) are  $A_{so}$ ,  $C_3^{\Sigma}$ ,  $C_3^{\Pi}$ ,  $C_6^{\Sigma}$ ,  $C_6^{\Pi}$ ,  $C_8^{\Sigma}$  and  $C_8^{\Pi}$  for i = 1 7, respectively, and
      - For the  $A^{1}\Sigma_{u}^{+}$  state of  $X_{2}$ , set MMLR(1)= 0 to select the lower root of the  $2 \times 2$  determinant.
      - For the  $b^3\Pi_u$  state of  $X_2$ , set MMLR(1)= -1 to select the upper root of the  $2 \times 2$  determinant.
    - For the  $3\times 3$  alkali-homodimer cases, set  $\mathrm{NCMM}=10$  with  $\mathrm{MMLR}(1)=-2$  or -3 or -4, and  $\mathrm{MMLR}(i>1)=3,\ 3,\ 3,\ 6,\ 6,\ 6,\ 8,\ 8,\ 8$ , while  $\mathrm{CmVAL}(i)=A_{\mathrm{so}}$ ,  $C_3^{\Sigma}$ ,  $C_3^{1\Pi}$ ,  $C_3^{3\Pi}$ ,  $C_6^{\Sigma}$ ,  $C_6^{1\Pi}$ ,  $C_6^{2\Pi}$ ,  $C_8^{\Sigma}$ ,  $C_8^{1\Pi}$  and  $C_8^{3\Pi}$ , respectively, and:
      - For the  $1\,^3\Sigma_g^+$  state of  $X_2$ , set MMLR(2)= -2 to select the lowest root of the  $3\times 3$  determinant [49, 50].
      - For the  $B^1\Pi_u$  state of  $X_2$ , set MMLR(2) = -3 to select the middle root of the  $3 \times 3$  determinant.
      - set MMLR(2) = -4 to select the highest root of the  $3 \times 3$  determinant.
  - **rhoAB**: selects whether (rhoAB > 0) or not (rhoAB  $\leq$  0) damping functions are to be used with the inverse-power long-range terms. If rhoAB > 0, it is the value of the system-dependent range-scaling parameter of  $\rho$  of Eqs. (25) and (26).
  - sVSR2: when damping functions are used, integer sVSR2 is twice the value of the very-short-range power parameter 's' of Eqs. (25)-(27), (sVSR2  $\equiv 2s$ ). For the generalized Tang-Toennies functions of Eq. (26), its allowed values are -4 -2, 0, 2, or 4, while for the generalized Douketis-type functions of Eq. (25), its allowed values are -4, -3, -2, -1, or 0.
  - **IDSTT:** an integer specifying the form of the damping function, for rhoAB > 0:
    - IDSTT > 0 invokes use of the Douketis-type damping functions of Eq. (25).
    - IDSTT < 0 specifies use of the Tang-Toennies-type damping functions of Eq. (26).
- #14a. IF((IPOTL.EQ.4).AND.(APSE.GT.0)) READ(5,\*) (XPARM(I), PARM(I), I=1,NVARB)
  - **XPARM**(i) & **PPARM**(i): the NVARB values of the distance coordinate  $y_q^{\text{ref}}(r_i)$  and of the associated exponent coefficient  $\beta(r_i)$  defining the cubic spline used to represent the MLR exponent coefficient function  $\beta(r)$  when APSE > 0. Read them in, one pair per line.

- #14b. IF((NVARB.GE.O).AND.(APSE.LE.O)) READ(5,\*) (PARM(I), I=1,NVARB)
  - **PPARM**(i): are the NVARB parameters characterizing the potential functions described above for all cases other than an MLR with APSE > 0. For example, the  $\beta_i$  parameters of Eqs. (13), (23), (33) or (34), or the coefficients  $\beta_i$  of the exponent polynomials defining the EMO or DELR potentials.

If atomic-mass-dependent Born-Oppenheimer breakdown (BOB) terms are to be incorporated into the potential energy and/or centrifugal potential functions (IBOB > 0), use READS #15 and two or more (as needed) of #16-23. These BOB functions have the forms defined by Eqs. (35) and (36). If a given type of correction function is to be omitted, the associated expansion order (e.g., NU1, NU2, NT1 or NT2) should be set < 0, in which case the associated parameter READ statements (from among #16-23) are omitted, while if no BOB corrections are considered (IBOB  $\leq$  0), omit all of READS #15-23.

- #15. READ(5,\*) MN1R, MN2R, QAD, PAD, NU1, NU2, QNA, NT1, NT2
  - MN1R & MN2R: The integer mass numbers of the *reference* isotopes of atoms 1 and 2, respectively, whose masses  $M_a^{\text{ref}}$  appear in Eqs. (35) and (36) [70].
  - **NU1 & NU2:** For atoms a=1 and 2 (or A and B), these are the orders  $N_{\rm ad}^a$  of the polynomial expansions of Eq. (35). If either of them is set <0, neglect the corresponding pair from among Reads  $^{\#}16-19$ .
  - **NTA & NTB:** For atoms a=1 and 2 (or A and B), these are the orders  $N_{\rm na}^a$  of the polynomial expansions of Eq. (36). If either of them is set <0, neglect the corresponding pair from among Reads #20-23.
  - QAD, PAD & QNA: positive integers  $q_{\rm ad}$ ,  $p_{\rm ad}$ , and  $q_{\rm na}$ , respectively, define the variables  $y_p^{r_e}(r)$  and  $y_q^{r_e}(r)$  in the expressions for the potential energy and centrifugal BOB functions of Eqs. (35) and (36). One should normally set PAD  $\equiv p_{\rm ad} > m_{\rm Last} \equiv \text{MMLR(NCMM)}$ . Note that if PAD = 0 and UaINF = 0, the adiabatic potential correction function is collapsed to a simple power series in  $y_q(r)$ .

For cases in which IBOB > 0,

```
^{\#}16. IF(NU1.GE.0) READ(5,*) (U1(i), i= 0,NU1)
```

- #21. IF(NT1.GE.O) READ(5,\*) T1INF
- #22. IF(NT2.GE.0) READ(5,\*) (T2(i), i= 0,NT2)
- #23. IF(NT2.GE.O) READ(5,\*) T2INF
  - Ua(i) and UaINF: For a=1 or 2, they are, respectively, the REAL\*8 expansion parameters and limiting asymptotic values defining the 'adiabatic' potential correction functions of Eq. (35):  $Ua(i) = u_i^a$  and  $UaINF = u_\infty^a$ , all have units cm<sup>-1</sup>.
  - ${\bf T}a(i)$  and  ${\bf T}a{\bf INF}$ : For a=1 or 2, they are, respectively, the REAL\*8 expansion parameters and limiting asymptotic values defining the 'non-adiabatic' centrifugal potential energy correction functions of Eq. (36). All of  ${\bf T}a(i)=t_i{}^a$  and  ${\bf T}a{\bf INF}=t_\infty^a$  are dimensionless.

<sup>#17.</sup> IF(NU1.GE.O) READ(5,\*) U1INF

 $<sup>^{\#}18</sup>$ . IF(NU2.GE.0) READ(5,\*) (U2(i), i= 0,NU2)

<sup>#19.</sup> IF(NU2.GE.O) READ(5,\*) U2INF

<sup>#20.</sup> IF(NT1.GE.0) READ(5,\*) (T1(i), i= 0,NT1)

For a calculation involving only a single potential energy curve (NUMPOT = 1 in Read  $^{\#}1$ ), the code now proceeds directly to Read  $^{\#}24$ . However, if NUMPOT = 2, it first first repeats Reads  $^{\#}6-23$  to input the second potential function.

Now read the parameters controlling which levels (of Potential-1) are to be calculated, and what expectation values and or matrix elements are to be calculated (if any).

- #24. READ(5,\*) NLEV1, AUTO1, LCDC, LXPCT, NJM, JDJR, IWR, LPRWF
  - **NLEV1:** if > 0, integer NLEV1 is the number of vibrational or vibrotational levels to be calculated. Their quantum number specifications are then input via READ #25.
    - if  $\leq 0$ , the program automatically finds all vibrational levels from  $v=0-|{\tt NLEV1}|$  associated with the rotational quantum number read in as  ${\tt IJ}(1)$  (see below). If the input value of NLEV is very large and negative, the program will (attempt to) find *all* possible vibrational levels associated with the specified  $J={\tt IJ}(1)$ .
  - AUTO1: integer AUTO1 > 0 (normal option) causes the program to (attempt to) generate automatically realistic trial eigenvalues for all desired levels, so that only their quantum number labels need be input via (READ #25a). If this fails, setting AUTO1  $\leq 0$  will allow/require a trial energy GV(i) to be input (via READ #25b) for each specified level using the NLEV1 > 0 option.
  - **LCDC:** If LCDC > 0, calculate the inertial rotational constant  $B_v$  and the first 6 centrifugal distortion constants  $\{-D_v, H_v, L_v, M_v, N_v, \& O_v\}$  for all of the levels specified by NLEV1. These results are also written in a compact format to Channel-9.
  - **LXPCT:** An integer controlling which expectation values/matrix elements are to be calculated. For LXPCT = 0, no expectation values or matrix elements are calculated (in which case READs #26-31 are omitted).
    - Even values of  $|LXPCT| \neq 0$  cause the results to be written in compact form to Channels-7 or 8 (as appropriate, see below), as well as to Channel-6;
    - Odd values of LXPCT yield only Channel-6 output, while negative values of LXPCT cause most of the (relatively wordy) output to Channel-6 to be suppressed.
    - LXPCT = -1 causes the eigenvalues and (if appropriate) quasibound level widths to be written compactly to Channel-7, and no expectation values or matrix elements are calculated (so Reads #26-31 are omitted).
    - LXPCT = 1, 2 or -2 causes calculation of expectation values of the kinetic energy and of positive powers of the distance variable specified by READ #26 plus either #27 or #28 31 (as appropriate, see below). Write results to Channel-6 if LXPCT = 1 or 2; also write them (compactly) to Channel-7 if LXPCT = 2, and write them only (compactly) to Channel-8 if LXPCT = -2.
    - $|\mathtt{LXPCT}| \geq 3$  invokes the calculation of matrix elements coupling levels of Potential-1 to each other (if NUMPOT = 1) or to levels of Potential-2 (if NUMPOT = 2), as specified by Reads #27 and 28. Write results to Channel-6 if  $\mathtt{LXPCT} > 0$  and (compactly) to Channel-8 if  $\mathtt{LXPCT} = \pm 4$ .
    - $|\mathtt{LXPCT}| \geq 5$  also causes the component radial moments comprising the overall matrix elements to be written to Channel-7, while still writing the overall matrix elements for selection-rule allowed transitions to Channel-8. For  $\mathtt{LXPCT} = \pm 6$  write only the radial moment components, and omit the output to Channel-8.

- NJM & JDJR: if (integer) NJM > 0, then for each (vibrational) level generated by the NLEV1 specification, automatically calculate eigenvalues (and if appropriate, expectation values and matrix elements) for all rotational sublevels J ranging from the input-specified (see below) J = IJ(i) to a maximum of J = NJM (or until that vibrational level energy predissociates above the potential barrier), with J increasing in steps of JDJR. e.g., to determine automatically all possible rotational levels, set JDJR = 1, IJ(i) = 0 (or more strictly =  $|\Omega|$ ) and NJM very large (e.g., NJM = 999).
- **IWR:** an integer controlling the printout of diagnostics and calculation details inside subroutine SCHRQ.
  - If  $IWR \neq 0$  print warning and error messages inside SCHRQ, as appropriate. Unless one is troubleshooting, normally set IWR = -1.
  - If  $IWR \geq 1$  also print final eigenvalue and node count for every level determined.
  - If IWR  $\geq 2$  also print end-of-range wave function amplitudes.
  - ullet If IWR  $\geq 3$  also print intermediate trial eigenvalues as the iterative convergence proceeds.
- **LPRWF:** If LPRWF > 0 write to Channel-6 the wavefunction of each specified level at every  $\{\text{LPRWF}\}^{th}$  mesh point.
  - If LPRWF < 0 write wavefunction of each specified level compactly to Channel–10, at every  $|\text{LPRWF}|^{th}$  mesh point.
  - If LPRWF = 0, no wavefunction printout.
- SINNER & INNOD1: parameters to facilitate finding inner vs. outer wells of a double well potential if IAUT01 > 0 fails, or to facilitate treating a precisely symmetric potential. These parameters may be added to READ #24 by making small modifications to Lines #411–423 of the code.

Read quantum numbers specifying which vibration-rotation levels (of Potential-1) are to be determined.

```
^{\#}25\,\mathrm{a.} IF(AUT01.GT.0) READ(5,*) (IV(i),IJ(i),i= 1, max\{1,|\mathrm{NLEV1}|\}) ^{\#}25\,\mathrm{b.} IF(AUT01.LE.0) READ(5,*) (IV(i),IJ(i),GV(i),i= 1, max\{1,|\mathrm{NLEV1}|\})
```

- **IV**(i) & **IJ**(i): For NLEV1 > 0 these are the vibrational [v = IV(i)] and rotational [J = IJ(i)] quantum numbers of the levels to be determined; if NJM > IJ(i) the program also automatically calculates rotational levels for that v = IV(i) with J = IJ(i) to NJM in steps of JDJR.
  - For NLEV1  $\leq 0$ , read one  $\{IV(i), IJ(i)\}$  pair. The value of IV(1) is ignored, but J = IJ(1) is the rotational quantum number for which all vibrational levels up to v = |NLEV1| are to be determined.
- $\mathbf{GV}(i)$ : If  $\mathtt{AUT01} \leq 0$ , Read #25b is used in place of #25a, and  $\mathtt{GV}(i)$  is the trial energy read in for each level  $v = \mathtt{IV}(i)$ ,  $J = \mathtt{IJ}(i)$ . This option presumes  $\mathtt{NLEV1} > 0$ .

If expectation values or matrix elements are to be calculated (i.e., if LXPCT  $\neq 0$  or -1), READS #26-31 specify the desired arguments. However, if LXPCT = 0 or -1, the data input for this case is now finished.

<sup>#26.</sup> READ(5,\*) MORDR, IRFN, DREF

- **MORDR:** an integer specifying the highest power of the chosen radial function or distance coordinate RFN(r) for which expectation values or matrix elements are to be calculated (see Eq. (8)). The current program version is dimensioned for  $MORDR \le 20$ . To calculate only Franck-Condon factors (when  $|LXPCT| \ge 3$ ), set MORDR = -1.
- **IRFN & DREF:** integer and real variables, respectively, specifying the definition of the radial function or distance coordinate RFN(r).
  - If IRFN  $\leq -10$ , RFN is generated by user-supplied code inserted at Lines #565-586 of the main program. In this case DREF is a dummy variable, and READS #27-31 are omitted.
  - If IRFN = -4, then RFN(r) = r and the matrix element operator is a polynomial in r, of order MORDR, and having coefficients DM(i), that pre-multiplies the derivative operator d/dr that acts on the wavefunction for 'Potential-2' (inserted for Bob Field).
  - If IRFN = -3, RFN $(r) = 1/r^3$ .
  - $\bullet \ \text{If} \ \text{IRFN} = -2 \,, \ \text{RFN}(r) = 1/r^2 \,.$
  - If IRFN = -1, use a Dunham-type expansion coordinate RFN(r) = (r DREF)/DREF.
  - If IRFN = 0, the function RFN(r) = r, the distance coordinate itself.
  - If IRFN = 1-9, use the Šurkus-type variable RFN $(r) = y_p^{\text{DREF}}(r) = (r^p \text{DREF}^p)/(r^p + \text{DREF}^p)$ , with p = IRFN.
  - For IRFN = -1 or 1-9, a positive (real) input value of DREF specifies it as the reference distance r= DREF; for these cases, normally set DREF =  $r_e$ . However, if the input value of DREF  $\leq 0.0$ , the program internally (iteratively) determines a value of DREF such that the expectation value of RFN(r) is identically zero for the first vibration-rotation level considered.
  - If  $IRFN \geq 10$ , RFN(r) is a function defined by reading in and interpolating over (and extrapolating beyond) input values of some known radial function (e.g., a dipole or transition moment function). This reading and interpolation/extrapolation is performed by the same subroutine package PREPOT used to treat a numerical input potential (see Reads #6-9). In this case DREF is a dummy variable, Read #27 is omitted, and the code internally sets MORDR = 1, DM(0) = 0.0 and DM(1) = 1.0.
- #27. IF(DABS(IRFN).LE.9) READ(5,\*) (DM(J), J= 0,MORDR)
  - $\mathbf{DM(j)}$ : Coefficients of the power series in  $\mathsf{RFN}(r)$  defining the argument of the overall expectation values or matrix elements:  $M(r) = \sum_{j=0}^{\mathsf{MORDR}} \mathsf{DM}(j) \times \mathsf{RFN}(r)^j$ .

If the expectation value or matrix element radial function argument is to be defined by interpolating over and extrapolating beyond a set of read-in points (IRFN  $\geq$  10), use the same read sequence, options and procedures employed for treating a numerical input potential. Most input parameters here have definitions essentially equivalent to those associated with READ #6–9.

- #28. READ(5,\*) NRFN, RFLIM
- $^{\#}29$ . READ(5,\*) NUSEF, ILRF, NCNF, CNNF
- #30. READ(5,\*) RFACTF, MFACTF
- $^{\#}31$ . READ(5,\*) (XIF(I), YIF(I), I= 1,NRFN)

**NRFN:** Is the number of known function values  $\{XIF(i), YIF(i)\}$  to be read in,

- **RFLIM:** Is the limiting asymptotic value imposed when extrapolating beyond the range of the input values, and
- **NUSEF:** Specifies how the interpolation is to be performed, while **ILRF**, **NCNF** and **CNNF** define the manner in which it extrapolates to large r (see comments for READ #7).
- **RFACTF** & **MFACTF**: Convert units of input distances XIF(i) and ordinates YIF(i), respectively, to Å and whatever units are required for the expectation value/matrix element argument M(r) (debye, for a dipole or transition moment function).

For matrix element calculations ( $|\text{LXPCT}| \geq 3$ ), couple each level of Potential-1, generated as specified by Reads #24 and 25, to all rotation levels of the NLEV2 vibrational levels v = IV2(i) allowed by the rotational selection rules  $\Delta J = \text{J2DL}$  to J2DU in steps of J2DD (e.g., for P and R transitions: J2DL = -1, J2DU = +1 J2DD = +2). If NUMPOT = 2 these are levels of Potential-2 and no constraints are imposed, but if NUMPOT = 1 the matrix elements couple levels of Potential-1 to one another, and to avoid redundancy the program considers only emission from (rotational sublevels of) these NLEV2 vibrational levels into lower(v'', J'') levels generated as per Reads #32 & 33. Integer AUTO2 > 0 causes LEVEL to generate trial eigenvalues automatically for all desired levels (preferred option), so only their vibrational quantum number labels need be input (Read #33a). If this fails, setting AUTO2  $\leq 0$  will require a trial pure vibrational energy GV2(i) to be read in (Read #33b) for each specified level.

```
#32. READ(5,*) NLEV2, AUTO2, J2DL, J2DU, J2DD
```

<sup>#33</sup> a. IF(NLEV2.GT.0) READ(5,\*) (IV2(I), I= 1,NLEV2)

<sup>#33</sup>b. IF(NLEV2.GT.0) READ(5,\*) (IV2(I), GV2(I), I= 1,NLEV2)

#### Appendix C: Illustrative Cases and Sample Input and Output Files

The running time for this program depends entirely upon the complexity of the calculation being performed and the type of computer being used; CPU requirements may range from a fraction of a second to a couple of minutes. This Appendix presents three sets of sample data files and the resulting output for representative cases illustrating some of the types of problems to which the program may be applied. The sets of sample input data files described below are available as a plain ASCII text file in the Supplementary Material associated with this paper. Note that entries after the "%" sign on each line of those input data files are comments identifying the variables, and are ignored by the program.

### Appendix C1: Input/Output for LJ(12,6) PECs and a double minimum potential

The first three cases considered in this subsection are based on use of a simple Lennard-Jones(12,6) potential and serve to provided an introduction to the types of calculations that may be performed, and illustrates the nature of the resulting output. The fourth case is introduced to illustrate the ability of **LEVEL** to locate specified eigenvalues of a double-minimum potential. On a decade-old SGI UNIX workstation, the 4 examples of **Case 1** require 0.125 s of CPU time.

- Case 1: This data file consists of five separate data sets that illustrate a variety of the capabilities of the program, including the fact that it can treat several independent problems in a single run by simply putting the input data for several cases into the same file, one after the other.
  - (a) For a Lennard-Jones(12,6) potential, find all the vibrational levels, and calculate the associated values of the centrifugal distortion constants. This is a model system with fictitious particle masses, so those masses and the chosen particle names 'L1' and 'J2' are input by READ #3.
  - (b) For the same simple model Lennard-Jones(12,6) potential of Case I (a), calculate all possible infrared matrix elements involving levels with  $v \leq 2$  and  $J(upper) \leq 1$ .
  - (c) For the same model Lennard-Jones(12,6) potential of Case 1a (a), locate all (four) vibrational levels of the centrifugally-distorted potential associated with J=18. This demonstrates that the procedure for automatically finding all vibrational levels works for a potential with a barrier (here, centrifugal in origin) protruding above its dissociation limit. This example invokes the highest print level inside SCHRQ (by setting IWR = 3, see Read #24) in order to illustrate the progress of the iterative eigenvalue convergence procedure. In this case convergence details for each level are presented twice (though only one iteration is required the second time) because of a quirk of the internal program logic.
  - (d) To illustrate the ability to determine the eigenvalues of a double-minimum potential, find the eigenvalues for vibrational levels v = 56 80 of an *ab initio* potential for the  ${}^3\Pi_g$  state of  $Cl_2$  [71], and calculate expectation values of various powers of r. The lowest of these levels lies in the region in which all levels belong to the deeper outer well, while the highest lies above the barrier separating the two wells. The output expectation values show that as the energy increases, the region of maximum wave function amplitude hops back and forth between the two wells. This case illustrates the ability of the program, and in particular, its automatic level-finder subroutine ALF, to find arbitrary levels of a double minimum potential automatically.

```
-1 0 -1 0 0 1
                                   % IAN1 IMN1 IAN2 IMN2 CHARGE NUMPOT
 'L1' 30.34373256D0
                                   % NAME1 MASS1
'J2' 30.34373256D0
                                  % NAME2 MASS2
'Case 1.a: For a model L.J.(12,6) get all vib. levels and their CDCs'
0.0020 0.6 20. 1.d-6 % RH RMIN RMAX EPS
0 0 0 0.D0
                                  % NTP LPPOT IOMEG VLIM
                                % IPOTL PPAR QPAR APSE Nbeta IBOB
% DSCM REQ Rref
1 12 6 0 0 0
 1000.d0 1.d0 1.d0
                              % NLEV1 AUTO1 LCDC LXPCT NJM JDJR IWR
-999 1 1 -1 0 1 -1 0
LPRWF
 0 0
                                   % IV(1) IJ(1)
-1 30 -1 30 0 1
                                  % IAN1 IMN1 IAN2 IMN2 CHARGE NUMPOT
 'L1' 30.34373256D0
                                   % NAME1 MASS1
'J2' 30.34373256D0
                                  % NAME2 MASS2
'Case 1.b: For same model L.J.(12,6) get radial matrix elements for v < 3'
0.0020 0.6 20. 1.d-6
                                  % RH RMIN RMAX EPS
0 0 0 0.D0
                                  % NTP LPPOT IOMEG VLIM
1 12 6 0 0 0
                                  % IPOTL PPAR QPAR APSE Nbeta IBOB
 1000.d0 1.d0 1.d0
                                  % DSCM REQ Rref
-2 1 0 5 1 1 -1 0
                                  % NLEV1 AUTO1 LCDC LXPCT NJM JDJR IWR
LPRWF
 0 0
                                   % IV(1) IJ(1)
4 -1 1.D0
                                   % MORDR IRFN RREF
1.d0 -0.2d0 0.03d0 -0.004d0 0.0005d0 % {DM(j)}
3 1 -1 +1 2
                                   % NLEV2 AUTO2 J2DL J2DU J2DD
 0 1 2
                                   % IV2(1) IV2(2) IV2(3)
 -1 0 -1 0 0 1
                                   % IAN1 IMN1 IAN2 IMN2 CHARGE NUMPOT
 'L1' 30.34373256D0
                                   % NAME1 MASS1
'J2' 30.34373256D0
                                  % NAME2 MASS2
'Case 1.c: For the same L.J.(12,6), find levels of potential with a barrier'
0.0020 0.6 20. 1.d-6
                                  % RH RMIN RMAX EPS
0 0 0 0.D0
                                  % NTP LPPOT IOMEG VLIM
                                 % IPOTL PPAR QPAR APSE Nbeta IBOB
1 12 6 0 0 0
 1000.d0 1.d0 1.d0
                                 % DSCM REQ Rref
                               % NLEV1 AUTO1 LCDC LXPCT NJM JDJR IWR
-999 1 0 -1 0 1 3 0
LPRWF
 0 18
                                   % IV(1) IJ(1)
17 35 17 35 0 1
                                  % IAN1 IMN1 IAN2 IMN2 CHARGE NUMPOT
'Case 1.d: Levels of a pointwise double-minimum potential for 3(PI)g Cl2'
0.001 1.6 10. 1.d-06 % RH RMIN RMAX EPS
29 0 0 95440.D0
                                   % NTP LPPOT IOMEG VLIM
0 0 2 1 0.D5
                                  % NUSE IR2 ILR NCN CNN
0.5291772108D0 8065.5444D0 0.d0 % RFACT EFACT VSHIFT
 3.34 10.608 3.40 9.683 3.43 9.221 3.49 8.758
 3.57 8.295 3.66 8.132 3.76 8.051 3.86 8.132 3.94 8.268
 4.03 8.350 4.17 8.595 4.26 8.704 4.31 8.758 4.46 8.432
 4.56 8.134 4.66 7.887 4.80 7.615 4.91 7.425 5.00 7.343
 5.17 7.125 5.37 6.962 5.51 6.908 5.66 6.880 5.80 6.908
 5.94 6.989 6.00 7.044 6.20 7.125 6.40 7.261 6.60 7.425
22 1 0 1 0 1 -1 0
                                   % NLEV1 AUTO1 LCDC LXPCT NJM JDJR IWR
LPRWF
 56 0 57 0 58 0 59 0 60 0 61 0 62 0 63 0 64 0 65 0 66 0 67 0
 68 \ 0 \quad 69 \ 0 \quad 70 \ 0 \quad 72 \ 0 \quad 72 \ 0 \quad 73 \ 0 \quad 74 \ 0 \quad 75 \ 0 \quad 76 \ 0 \quad 77 \ 0 \quad 78 \ 0 \quad 80 \ 0
3 0 0.D0
                                  % MORDR IRFN RREF
 1.d0 -2.d-1 3.d-2 -4.d-3
                                   % {DM(j)}
```

# Standard Channel-6 output for Introductory Illustrative Cases 1(a) - 1(d)

Case 1.a: For a model L.J.(12,6) get all vib. levels and their CDCs

```
ZMU= 15.17186628000(u)
                                             &
                                                  BZ= 8.999999997D-01((1/cm-1)(1/Ang**2))
 from atomic masses: 30.34373256000 & 30.34373256000(u) Integrate from RMIN= 0.600 to RMAX= 20.00 with mesh RH= 0.002000(Angst)
 Potential #1 for L1( 0)-J2( 0)
 State has OMEGA= 0
                           and energy asymptote: Y(lim)=
                                                                         0.00000(cm-1)
 Lennard-Jones(12, 6) potential with De= 1000.000(cm-1)
                                                                           Re = 1.000000(A)
 Calculate properties of the single potential described above
 Potential-1 uses inner boundary condition of zero value
 Eigenvalue convergence criterion is
                                               EPS = 1.0D - 06(cm - 1)
Airy function at 3-rd turning point is quasibound outer boundary condition Since state-1 has (projected) electronic angular momentum OMEGA= 0
eigenvalue calculations use centrifugal potential [J*(J+1) For J= 0, seek the first 400 levels of Potential-1 with VLIM= ALF finds the highest calculated level is E(v=6)=-7.7249284D-01
                                   Bv= 1.0540426 -Dv= -4.1381D-05

Mv= -7.2230D-16 Nv= -3.1926D-19

Bv= 0.9332450 -Dv= -6.0794D-05

Mv= -3.7208D-15 Nv= -2.4359D-18

Bv= 0.8013476 -Dv= -9.2177D-05

Mv= -2.0879D-14 Nv= -2.1041D-17
 E(v= 0, J= 0)=
                       -811.519
                                                                                Hv = -6.5120D - 09
Lv= -1.9007D-12
E(v= 1, J= 0)= -507.17
                                                                                Hv= -1.4820D-08

0v= -1.7523D-21

Hv= -3.5187D-08

0v= -2.3384D-20
                  )= -507.170
-6.5533D-12
)= -287.838
             Lv=
               v= 0

0)= -287.00

v= -2.3947D-11

-141.50
 E(v=
        2, J=
             Lv=
                                   Bv= 0.6566553
Mv= -1.5291D-13
Bv= 0.4974391
My= -1.9135D-12
                                                         -Dv= -1.4627D-04
Nv= -2.6179D-16
-Dv= -2.4978D-04
E(v= 3, J=
Lv=
                   )= -141.503
-1.0432D-10
                                                                                 Hv= -9.2303D-08
Ov= -4.9802D-19
               0)= -54.890
v= -6.5212D-10
0)= -13.337
v= -9.1824D-09
                                                                                Hv= -2.9569D-07

Ov= -2.5885D-17

Hv= -1.4933D-06

Ov= -8.8619D-15
 E(v= 4, J= 0)=
             Lv=
                                                          Nv= -6.6507D-15
                                                         -Dv= -4.9470D-04
Nv= -7.8195D-13
 E(v=5, J=
                                   Bv= 0.3221808
Mv= -7.7465D-11
             Lv=
       6, J= 0)=-.772493
Lv= -2.0424D-06
                                   Bv= 0.1290036
Mv= -1.4479D-07
                                                          -Dv= -1.6478D-03
Nv= -1.1986D-08
                                                                                Hv = -3.8715D-05

0v = -1.0942D-09
 E(v=
         7 Potential-1 vibrational levels with
 Find
             Ĕ(v)
                                   E(v)
                                                          E(v)
                                                                                 E(v)
                                                                         V
      0
           -811.5192
-507.1696
                              -287.8379
-141.5034
                                                         -54.8902
-13.3368
                                                                         6
                                                                                 -0.7725
             N-D theory extrapolation from
                                                    v=
                                                          5 &
                                                                     implies
                                                                                  vD =
                                                                                         6.439
Case 1.b: For same model L.J.(12,6) get radial matrix elements for {\rm v}\,<\,3
                                            & BZ= 8.99999997D-01((1/cm-1)(1/Ang**2))
             ZMU= 15.17186628000(u)
                                     30.34373256000 & 30.34373256000(u)
to RMAX= 20.00 with mesh RH= 0.002000(Angst)
 Potential #1 for L1( 30)-J2( 30)
 State has OMEGA= 0 and energy asymptote: Y(lim)=
 Lennard-Jones(12, 6) potential with De= 1000.000(cm-1)
                                                                           Re = 1.000000(A)
 Calculate properties of the single potential described above
 Potential-1 uses inner boundary condition of
                                                          zero value
 Eigenvalue convergence criterion is EPS= 1.0D-06(cm-1)
 Airy function at 3-rd turning point is quasibound outer boundary condition
 Since state-1 has (projected) electronic angular momentum OMEGA= 0
   eigenvalue calculations use centrifugal potential [J*(J+1) - 0 or J= 0, seek the first 3 levels of Potential-1 with VLIM= and automatically increment J in steps of 1 to a maximum value of
                                                                          [J*(J+1) - 0]/r**2
 Matrix element argument expansion variable is:
                                                              X = (r - DREF)/DREF
      where reference length is held fixed at DREF = 1.0000000000(Angstroms)
 Coefficients of expansion for radial matrix element/expectation value argument:
        1.000000D+00 -2.000000D-01 3.000000D-02 -4.000000D-03 5.000000D-04
 Using the rotational selection rule: delta(J) = -1 to 1 with increment 2
   calculate matrix elements for coupling to the 3 vibrational levels of
 to E(v= 0, J= 0)=
                                                                     <X** 1>= 0.0315663983
<X** 4>= 0.0000681864
                                                                     <X** 4>= 0.0000681864
A(Einst)= 9.6706D-07 s-
 For vibrational level v = 0
                                        of Potential-1
J E
        -811.519
                           -809.411
<X** 4>= 0.0002051809
A(Einst)= 9.0586D-04 s-1
 Coupling E(v= 1, J= 1)= -505.3034 to E(v= 0, J= 0)= -811.5192
 Coupling E(v= 1, J= 1)=
Moment matrix elements:
                                      <X** 0>= -0.0007036644
<X** 3>= 0.0011650604

                                                                     <X** 1>=
<X** 4>=
                                                                                  0.0554599642
 >= 0.0011650604
d(E)= -306.22
                                                                                  0.0002048749
                                                                     A(Einst)=
   Coupling E(v= 1, J= 1)= -505.3034 to E(v= 0, J= 2)=
```

```
<X** 1>= 0.0556429498
<X** 4>= 0.0002064159
A(Einst)= 5.1293D-04 s-1
                                   J= 0)=
                                                                            -507,1696
 Coupling
            E(v= 1, J= 1)=
 <X** 1>=
                                                                           0.1072309514
                                                               <X** 4>=
A(Einst)=
                                                                           0.0010331538
6.5155D-07 s-1
 For vibrational level v = 1
                                     of Potential-1
                                                                     E
  0 -507.170 1 -505.303
                                              to E(v=
                                                                            -809.4112
 Coupling E(v= 2, J= 0)=
                                   -287.8379
                                                             0, J= 1)=
                                   <X** 0>= -0.0001445686
<X** 3>= 0.0006270858
D-03 d(E)= -521.57
     Moment matrix elements: <X**

<X** 2>= 0.0021494006 <X**

= 2.0900D-08 <M>= 2.85487D-03
                                                                <X** 1>=
                                                                           -0.0146868141
                                                                           0.0002038462
3.6268D-04 s-1
                                                                <X** 4>=
 FCF= 2.0900D-08
                                                               A(Einst)=
                                                             1, J= 1)=
                   2, J= 0)=
                                   -287.8379
                                                      E(v=
                                                                            -505.3034
           E(v=
 Coupling
                                                to
     Moment matrix elements: <X** 

<X** 2>= 0.0215270661 <X** 

= 1.5288D-06 <M>=-1.49150D-02
                                   <X** 0>= 0.0012364336
<X** 3>= 0.0065378301
D-02 d(E)= -217.47
                                                               <X** 1>=
<X** 4>=
                                                                           0.083860202
                                                                           0.0019424342
 FCF= 1.5288D-06
                                                               A(Einst)=
                                                                           7.1749D-04 s-1
 0, J= 0)=
                                                                            -811.5192
                                   <X** 0>= 0.0001452962
<X** 3>= 0.0006226650
BD-03 d(E)= -525.28
     Moment matrix elements:

<X** 2>= 0.0021295981
                                                               <X** 1>=
<X** 4>=
                                                                          -0.0147714152
                                                                           0.0002028174
 FCF= 2.1111D-08
                     <M>= 3.16108D-03
                                                                           1.5140D-04 s-1
                                                               A(Einst)=
 0, J= 2)=
                                                                            -805.1964
                                   <X** 0>= -0.0002889435
<X** 3>= 0.0006307829
     Moment matrix elements:
                                                                           0.0146592358
 <X** 2>= 0.0021551720 <X**
FCF= 8.3488D-08 <M>= 2.70514D-03
                                           >= 0.0006307829
d(E)= -518.96
                                                                <X** 4>=
                                                                           0.0002051064
2.1384D-04 s-1
                                                                A(Einst)=
  1, J= 0)=
 Coupling E(v=2, J=1)=
                                   -286.2356
                                               to E(v=
                                                                            -507.1696
                                   <X** 0>= -0.0012355622
<X** 3>= 0.0065170119
D-02 d(E)= -220.93
     Moment matrix elements: 
<X** 2>= 0.0214393061
                                                               <X** 1>=
<X** 4>=
                                                                           0.0834456954 0.0019370216
 FCF= 1.5266D-06
                     <M>=-1.73066D-02
                                                               A(Einst)=
    ++++++++++
1, J= 2)=
                                                             1, J=
 Coupling
     Moment matrix elements: 
<X** 2>= 0.0216303217
                                   <X** 0>= 0.0024778195

<X** 3>= 0.0065743346

D-02 d(E)= -215.34
                                                               <X** 1>=
<X** 4>=
                                                                           0.0841137737
 0.0019558701
                                                                           3.9306D-04 s-1
                                                                A(Einst)=
 Coupling E(v= 2, J= 1)=
                                   -286.2356
                                                             2, J= 0)=
                                               to
     Moment matrix elements: 
<X** 2>= 0.0661950523
                                   <X** 0>= 0.9999970447
<X** 3>= 0.0214010286
                                                               <X** 1>=
<X** 4>=
                                                                           0.2089561346
0.0074711130
 FCF= 9.9999D-01
                                           d(E)=
                     <M>= 9.60110D-01
For vibrational level v = 2
J \quad E
                                     of Potential-1 J \quad E
                  1 -286.236
        3 Potential-1 vibrational levels with J=
 Find
                                               2 -287.8379
v= 1 & ^
          -811.5192
     0
                         1 -507.1696
                                              2
                                                                           vD =
                                                                                   5.757
    n=12 N-D theory extrapolation from
                                                               implies
Case 1.c: For the same L.J.(12,6), find levels of potential with a barrier
             ZMU= 15.17186628000(u) & BZ= 8.999999997D-01((1/cm-1)(1/Ang**2))
                                   30.34373256000
                                                          30.34373256000(u)
 from atomic masses: 30. Integrate from RMIN= 0.600 to
                                                     &
                                       RMAX=
                                               20.00 with mesh RH= 0.002000(Angst)
 Potential #1 for L1( 0)-J2(
                                  0)
 State has OMEGA= 0 and energy asymptote:
                                                   Y(lim) =
                                                                   0.00000(cm-1)
 Lennard-Jones (12, 6) potential with De= 1000.000(cm-1)
                                                                     Re = 1.000000(A)
 Calculate properties of the single potential described above
 Potential-1 uses inner boundary condition of zero value at
 Eigenvalue convergence criterion is EPS= 1.0D-06(cm-1)
 Airy function at 3-rd turning point is quasibound outer boundary condition
 Since state-1 has (projected) electronic angular momentum \, OMEGA= \,0
          eigenvalue calculations use centrifugal potential [J*(J+1)]
                                                                              - 0]/r**2
     J= 18, seek the first 400 levels of Potential-1
                                                               with
                                                                       VLIM=
                                                                                   0.000
 Solve for v= 0 ITER ETRIAL
                    J= 18
D(E)
                               ETRIAL= -4.6535526D+02
M R(M) /WF(M)
                                                          INNER= 0
                                                                       WF(1st) WF(NEND)
R(NEND) NBEG ITP1
                                                             /WF(M)
                                                                          2.54
2.54
2.54
                                                             2.5D-13
3.6D-13
3.5D-13
    -4.6535526D+02 9.86D+00
                                    258
                                            1.11
                                                   8.3D-27
                                                                                      178
                     -6.65D-01
-4.08D-03
                                    260
260
                                                   1.0D-26
9.9D-27
    -4.5616720D+02 -1.53D-07
                                    260
                                                   9.9D-27
                                                                                      177
                                         R(M) = 1.12 WF(NBEG=
INNER= 0 WF(NEND=
0) = -456.17 v(SC)=
E(v = 0, J = 18) = -456.1672
                                 4 Iter
                                                                     52)/WF(M) = 9.9D-27
                                                                   799)/WF(M)= 3.5D-13
0.002 dGdv= 308.355
Single well ICOR= 0: E(v=
                                 0,J= 18)=
                                                                   E(next) = -1.9930D+02
                                            (vD-v)=
                                                         4.0487
                              ETRIAL= -1.9929905D+02 INNER= 0
                                                                       WF(1st) WF(NEND)
 Solve for v=1
                      J= 18
```

| ITER                     | ETRIAL   | D(E)  | M                               | R(M)                                 | /WF(M)   | /WF(M)  | R(NEND)  | NBEG                              | ITP1                                   |
|--------------------------|--|---|---------------------------------|--------------------------------------|--|---|--|-----------------------------------|--|
| 2 -1<br>3 -1             | .9929905D+02<br>.9565349D+02<br>.9581525D+02<br>.9581563D+02   | -1.62D-01<br>-3.75D-04  | 331<br>331                      | 1.26<br>1.26                         | -1.9D-26<br>-2.1D-26<br>-2.1D-26<br>-2.1D-26                                     | 3.6D-13<br>4.5D-13<br>4.5D-13<br>4.5D-13                                  | 3.23<br>3.23<br>3.23<br>3.23                         | 1<br>1<br>1<br>1                  | 164<br>164<br>164<br>164               |
|                          | 1,J= 18)= -  |   |                                 | INNER= (                             | ) WF(  | NEND= 106   | 1)/WF(M)=<br>6)/WF(M)=                               | = 4.5I                            | 0-13                                   |
| Ü                        | well ICOR=   |   | ·                               | (vD-7                                | •  | 9262 E(n  | 03 dGdv=<br>ext)= -3                                 |                                   |  |
| Solve<br>ITER            | for v= 2<br>ETRIAL   | J= 18<br>D(E)   | ETRIAL=<br>M                    | -3.12324<br>R(M)                     | 180D+01 ]<br>/WF(M)  | INNER= 0<br>/WF(M)  | WF(1st)<br>R(NEND)                                   | WF(NE<br>NBEG                     | END)<br>ITP1                           |
| 2 -2<br>3 -2             | .1232480D+01<br>.6003756D+01<br>.6442466D+01<br>.6447160D+01   | -4.39D-01   | 423<br>422                      | 1.43<br>1.44<br>1.44<br>1.44         |  | 7.1D-13<br>6.8D-13<br>6.1D-13<br>6.1D-13                                  | 5.09<br>5.30<br>5.30<br>5.30                         | 1<br>1<br>1<br>1                  | 158<br>158<br>158<br>158               |
|                          | 2,J= 18)=  |   |                                 | INNER= (                             | ) WF(  | VEND= 178   | <pre>0)/WF(M)=</pre>                                 | = 6.1I                            | ) <del>-</del> 13                      |
| J                        | well ICOR=   |   |                                 | (vD-7                                | <i>i</i> )= 1.7  | 7121 E(n  |  | . 29971                           | 0+01                                   |
| ITER                     | for v= 3<br>ETRIAL   | J= 18<br>D(E)   | ETRIAL=<br>M                    | R(M)                                 | 575D+01 ]<br>/WF(M)  |   | WF(1st)<br>R(NEND)                                   |                                   |  |
| 2 5<br>3 5<br>5 5<br>6 5 | .2996575D+01<br>.9253832D+01<br>.8543620D+01<br>.8496786D+01<br>.8495398D+01<br>.8495352D+01<br>.8495350D+01 | -7.10D-01<br>-4.68D-02<br>-1.39D-03<br>-4.63D-05<br>-1.54D-06 | 600<br>594<br>594<br>594<br>594 | 1.80<br>1.79<br>1.79<br>1.79<br>1.79 | -1.6D-26<br>-2.5D-26<br>-2.3D-26<br>-2.3D-26<br>-2.3D-26<br>-2.3D-26<br>-2.3D-26 | 1.6D-01<br>4.1D-01<br>3.8D-01<br>3.7D-01<br>3.7D-01<br>3.7D-01<br>3.7D-01 | 2.49<br>2.27<br>2.29<br>2.30<br>2.30<br>2.30<br>2.30 | 1                                 | 156<br>156<br>156<br>156<br>156<br>156 |
| E(v= :                   | 3,J= 18)=  | 58.4954   | 7 Iter                          | R(M)=<br>INNER= (                    | 1.79 WF(   | (NBEG= 5<br>VEND= 84  | 1)/WF(M)=<br>9)/WF(M)=                               | =-2.3D<br>= 3.7D                  | )-26<br>)-01                           |
| Life<br>Single           | etime= 5.035<br>well ICOR=   | D-12(s)<br>0: E(v=  | Width= 1<br>3,J= 18             | .054D+00<br>3)= {                    | ) dG/dv=<br>58.50 v(S  | = 41.60<br>SC)= 2.9   | V(max)=<br>83 dGdv=                                  | = 44.                             | 1.01<br>.289                           |
| ALF f                    | Find high  | hest level<br>hest calcu                                      |                                 | potenti                              | ial is I   | E(v=3)=   | 5.849535   | . 3932I<br>50075I                 |  |
| Solve<br>ITER            | for v= 0<br>ETRIAL   | J= 18<br>D(E)   |                                 |                                      | 720D+02 ]<br>/WF(M)  | INNER= 0<br>/WF(M)  | WF(1st)<br>R(NEND)                                   |                                   |  |
| 1 -4                     | .5616720D+02   | -1.53D-07   | 260                             | 1.12                                 | 9.9D-27  | 3.5D-13   | 2.54   | 1                                 | 177                                    |
| E(v=                     | 0,J= 18)= -  | 456.1672  | 1 Iter                          | R(M)=<br>INNER= (                    | 1.12 WF()  | (NBEG= 5<br>NEND= 79  | 2)/WF(M)=<br>9)/WF(M)=                               | = 9.9I<br>= 3.5I                  | 0-27<br>0-13                           |
| ITER                     | for v= 1<br>ETRIAL   | D(E)  | M                               | -1.95818<br>R(M)                     | 563D+02 1<br>/WF(M)  | INNER= 0<br>/WF(M)  | WF(1st)<br>R(NEND)                                   | WF (NE<br>NBEG                    | ITP1                                   |
|                          | .9581563D+02<br><br>1,J= 18)= -  |   |                                 |                                      |  | 4.5D-13<br><br>(NBEG= 5   | 3.23<br><br>1)/WF(M)=                                | 1<br><br>=-2.1□                   |  |
|                          | for v= 2<br>ETRIAL   | J= 18   |                                 | INNER= 0<br>-2.64471                 | ) WF(1   | NEND= 106<br>INNER= 0<br>/WF(M)   | R(NEND)  | WF(NE                             | END)                                   |
| 1 -2                     | .6447160D+01   | -5.09D-07   | 422                             | 1.44                                 | 2.8D-26  | 7.2D-13   | 5.27   | 1                                 | 158                                    |
| E(v= :                   | 2,J= 18)=  for v= 3  ETRIAL  | J= 18<br>D(E)   | 1 Iter ETRIAL= M                | R(M)=<br>INNER= 0<br>5.84953<br>R(M) | 1.44 WF(<br>WF(N<br>350D+01 ]<br>/WF(M)  | (NBEG= 5<br>VEND= 178<br>INNER= 0<br>/WF(M)                               | 0)/WF(M)=<br>0)/WF(M)=<br>WF(1st)<br>R(NEND)         | = 2.8I<br>= 7.2I<br>WF(NE<br>NBEG | 0-26<br>0-13<br>END)<br>ITP1           |
| 1 5                      | .04903000+01   | -5.120-06   |                                 | 1.79                                 | -2.30-20   | 3.70-01   | 2.30   |                                   | 150                                    |
| E(v= :                   | 3,J= 18)=<br>etime= 5.035  | 58.4954<br>D-12(s)  | 1 Iter<br>Width= 1              | R(M)=<br>INNER= (<br>.054D+0(        | 1.79 WF()<br>WF()<br>dG/dv=  | (NBEG= 5<br>NEND= 84<br>= 41.60   | 1)/WF(M)=<br>9)/WF(M)=<br>V(max)=                    | =-2.3E<br>= 3.7E<br>64            | 0-26<br>0-01<br>1.01                   |
|                          | 4 Potentia<br>E(v)   |   |                                 |                                      |  |   |  |                                   |  |
| 0                        | -456.1672  | 1 -   | 195.8156                        | 2                                    | -26.447  | 72 3  | 58.49  |                                   |  |
| ====:                    | .d: Levels   | =======   | ======                          | ======                               |  |   | ======   |                                   |  |
| Genera                   | ate ZMU= 1<br>from atom<br>rate from R   | 7.48442634  | 000(u)                          | & BZ=                                | = 1.037181   | L808D+00((  | 1/cm-1)(1  | l/Ang∗                            | (2)                                    |
|                          | tial #1 for  |   |                                 |                                      |  |   |  |                                   |  |
| State<br>Perfo           | has OMEGA=<br>rm cubic spl   | 0 and e   | nergy as                        | ymptote:                             | Y(lim)<br>29 int   | = 95440.0<br>out points   | 0000(cm-1  | L)                                |  |
| To mal                   | ke input point   | nts Y(i) c  | onsisten                        | t with                               | Y(lim),  | add Y(sh  | ift)=  | 0.0                               | 0000                                   |
|                          | to ge  | t required  | interna                         | l units                              | [Angstro   | oms & cm-1  | for pote   | ential                            |  |
|                          | 340000 10.6  | Y(i)<br>0800000   | 4.17000                         | 0 8.59                               | 9500000  | 5.370000  | 6.9620   | 00000                             |  |
| 3.4<br>3.4<br>3.4        | 340000 10.6<br>400000 9.6<br>430000 9.2<br>490000 8.7  | 830000<br>210000<br>580000                                    | 4.26000<br>4.31000<br>4.46000   | 00 8.70<br>00 8.75<br>00 8.43        | 0400000<br>5800000<br>3200000  | 5.510000<br>5.660000<br>5.800000  | 6.9080<br>6.8800<br>6.9080                           | 00000                             |  |

```
3.570000
                                                        8.1340000
7.8870000
7.6150000
7.4250000
7.3430000
                                                                                            6.98900000
7.04400000
7.12500000
7.26100000
7.42500000
                                                                            5.940000
6.000000
6.200000
6.400000
                    8.29500000
8.13200000
8.05100000
                                        4.560000
4.660000
4.800000
     3.760000
                    8.13200000
8.26800000
                                        4.910000
5.000000
       860000
     3.940000
                                                                             6,600000
     4.030000
                    8.35000000
                                        5.170000
Extrapolate to
                       X .le. 1.7992 with
   Y = -5091495.587 + 5.609801D + 06 * exp(-4.542065D - 02*X)
Extrapolate to X .GE. 3.3867 using
   Y= 95440.0000 - [ 1.128770D+05/X**1 +1.377826D+05/X**3]
Calculate properties of the single potential described above
Potential-1 uses inner boundary condition of zero value at RMIN
Eigenvalue convergence criterion is EPS= 1.0D-06 (cm-1) Airy function at 3-rd turning point is quasibound outer boundary condition
Since state-1 has (projected) electronic angular momentum OMEGA= 0
            eigenvalue calculations use centrifugal potential [J*(J+1) - 0]/r**2
Solve for the 22 vibration-rotation levels of Potential-1:

(v,J) = (56, 0) (57, 0) (58, 0) (59, 0) (60, 0) (61, 0)

(62, 0) (63, 0) (64, 0) (65, 0) (66, 0) (67, 0)

(68, 0) (69, 0) (70, 0) (72, 0) (72, 0) (73, 0)

(74, 0) (75, 0) (76, 0) (77, 0)

Matrix element arguments are powers of the distance r (in Angstroms)

Coefficients of expansion for radial matrix element/expectation value argum
<KE>= 4617.063
<X** 3>= 53.71727533
<KE>= 1651.393
E(v= 58, J= 0)= 68476.426 <M(r)>= 0.6824612177 
 <X** 1>= 2.04384519 <X** 2>= 4.1884
                                                                                    <KE>= 1651.393
<X** 3>= 8.60585634
<KE>= 4652.829

<X** 3>= 54.54340917
E(v= 60, J= 0)= 68729.539 <M(r)>= 0.4643045290 
<X** 1>= 3.68083020 <X** 2>= 14.06617696
                                                                                    <KE>= 4686.656
<X** 3>= 55.37868492
                                                                                    <KE>= 4718.810
<X** 3>= 56.21723207
<KE>= 4718.810
<KE>= 4749.186
<X** 3>= 57.05354180
                                                                                    <KE>= 1985.878

<X** 3>= 9.33364510

<KE>= 4751.128

<X** 3>= 57.39807961
E(v= 65, J= 0)= 69390.488 <M(r)>= 0.4540380379

<X** 1>= 3.74528392 <X** 2>= 14.60094615

E(v= 66, J= 0)= 69551.030 <M(r)>= 0.4516314964

<X** 1>= 3.75994565 <X** 2>= 14.72704336
                                                                                    <KE>= 4803.188

<X** 3>= 58.73339038

<KE>= 4825.287

<X** 3>= 59.54766857
E(v= 67, J= 0)= 69709.530 <M(r)>= 0.4496202586 
<X** 1>= 3.77158473 <X** 2>= 14.8346
                                                                                              4837.877
                                                                                    <KE>= 4831.87/
<X** 3>= 60.27548393
<KE>= 4633.896
<X** 3>= 57.46061741
E(v= 68, J= 0)= 69864.123 <M(r)>= 0.4631813287 
<X** 1>= 3.66813651 <X** 2>= 14.22170337
E(v= 69, J= 0)= 69900.180 <M(r)>= 0.6579325788
<X** 1>= 2.22764740 <X** 2>= 5.25807538
                                                                                    <KE>= 2352.457
<X** 3>= 13.57005061
E(v= 70, J= 0)= 70022.038 <M(r)>= 0.4464976859 
<X** 1>= 3.78784876 <X** 2>= 15.00980661
                                                                                    <KE>= 4867.346
<X** 3>= 61.55668989
E(v= 72, J= 0)= 70321.487 <M(r)>= 0.4485338715
<X** 1>= 3.76631221 <X** 2>= 14.93793365
                                                                                    <KE>= 4776.940
<X** 3>= 61.58542409
                                                                                    <KE>= 4776.940
<X** 3>= 61.58542409
E(v= 72, J= 0)= 70321.487 <M(r)>= 0.4485338715
<X** 1>= 3.76631221 <X** 2>= 14.93793365
E(v= 73, J= 0)= 70453.823 <M(r)>= 0.5032628690 
<X** 1>= 3.36247828 <X** 2>= 12.39895889
                                                                                    <KE>= 4057.676
<X** 3>= 49.05256070
<KE>= 3567.119
                                                                                    <X** 3>= 35.10248406
                                                                                    <KE>= 4812.997
<X** 3>= 60.55568119
<KE>= 4880.577
                                                                                    <X** 3>= 63.24854142
E(v= 77, J= 0)= 70905.689 <M(r)>= 0.4521314033 
<X** 1>= 3.72580681 <X** 2>= 14.82855323
```

### Appendix C2: Input/Output files for Several Families of Analytic Potentials

- Case 2. Illustrative input data files are presented for eigenvalue calculations using a number of the analytic potential energy functions supported by the code, as described in § 2.6. Performing this set of seven calculations required 1.60 s of CPU on a decade-old Silicon Graphics UNIX server.
  - (a) To illustrate an application to an **Extended Morse Oscillator (EMO)** potential and the inclusion of BOB correction terms, this case presents a calculation of the eigenvalues of <sup>109</sup>AgD from the 'EMO<sub>3</sub>(7)' potential determined in Ref. [72] from a combined-isotopologue analysis that treated <sup>107</sup>AgH as the 'reference isotopologue'.
  - (b) To illustrate use of a standard Polynomial-Exponent Morse/Long-Range (PE-MLR) potential form, and incorporation of Born-Oppenheimer breakdown (BOB) contributions to the radial and centrifugal potentials, this case is a calculation of properties of levels of the ground state of <sup>24</sup>MgD using the analytic PE-MLR potential and BOB correction functions determined from a combined isotopologue analysis of data for the MgH system in which <sup>24</sup>MgH was the "reference isotopologue" (see Ref. [73]). Note that in such cases, calculation of the rotational constants is based on a centrifugal potential that includes the BOB correction function of Eq. (36).
  - (c) To illustrate use of a Spline-Exponent Morse/Long-Range (SE-MLR) potential form, this case calculates the band constants for all levels of the ground  $X^{1}\Sigma^{+}$  state of NaH using parameter values generated from the example of Appendix C.3 of Ref. [44].
  - (d) This is an example of a calculation performed using the **D**ouble-Exponential **L**ong-Range (**DELR**) potential form that was introduced in Ref. [11]. This is not precisely the same **DELR** functional form reported there, since our current model for this function no longer allows the exponent polynomial to have different orders for  $r \leq r_e$  and  $r > r_e$ . However, it provides an equally good representation of the data for emission into the  $B^1\Pi_u$  state of Li<sub>2</sub>.
  - (e) This calculation is performed using the "X-expansion or HPP" polynomial potential for the  $X^{1}\Sigma_{g}^{+}$  state of Ca<sub>2</sub> reported by Allard *et al.* [74]. Note that the fact that the 18-digit polynomial expansion coefficients reported in Ref. [74] are rounded to (approximately) 13 digits by our program appears to have no significant effect on the results.
  - (f) This calculation for the ground  $X^{1}\Sigma^{+}$  state of  $^{20}\mathrm{Xe^{84}Kr}$  is performed using the **generalized HFD function** reported by Aziz *et al.* [75].
  - (g) This calculation for the ground  $X^{1}\Sigma^{+}$  state of  $^{40}\mathrm{Ar_{2}}$  using the **generalized Tang-Toennies type function** reported by Jaeger *et al.* [76].

```
% IAN1 IMN1 IAN2 IMN2 CHARGE NUMPOT
47 109 1 2
'Case 2.a: EMO potential for {109}AgD w. BOB corrn [JCP 123, 204304(2005)]'
0.0010 0.8 30.0 1.d-6
                                    % RH RMIN RMAX EPS
           19250.d0
                      0.d0
   0 0
                                    % NTP LPPOT OMEGA VLM
3 3 3 7 0 1
                                    % IPOTL QPAR PPAR Nbeta APSE IBOB
19250.d0 1.6179162d0 0.d0
                                    % DSCM REQ Rref
 1.54358095D+00 3.73860D-02 1.66424D-01 9.8030D-02 1.7089D-01 6.0200D-02
 1.4000D-01 2.2400D-01
                                   % MN1R MN2R qAD pAD NU1 NU2 qNA NT1 NT2
107 1 3 3 -1 3 3 -1 2
0.0D+0 1.175D+01 1.756D+01 -1.270D+01 % UA2(0) UA2(1) ...
```

```
0.0D+0
                                       % U2INF
                                    % TA2(0) TA2(1) ...
 0.0D+0 1.5D-04 9.3D-04
 0.0D+0
                                    % T2INF
-99 1 2 -1 0 1 -1 0
                                    % NLEV1 AUTO1 LCDC LXPCT NJM JDJR IWR LPRWF
 0 0
                                    % IV(1) IJ(1)
12 24 1 2 0 1
                                    % IAN1 IMN1 IAN2 IMN2 CHARGE NUMPOT
'Case 2.b: PE-MLR fx for MgD w. BOB corrn: from JPCA 117, 13373 (2013)'
 0.0005d0 0.50 99.d0 1.d-05
                                   % RH RMIN RMAX EPS
 0 0 0 0.0d0
                                    % NTP LPPOT IOMEG VLIM
 4 4 5 12 -1 1
                                    % IPOTL QPAR PPAR Nbeta APSE IBOB
 11104.25d0 1.7296854D0 2.74d0
                                    % DSCM REQ Rref
                                    % NCMM rhoAB IVSR IDSTT
 3 0.81 -2 1
 6 2.77550D+05
 8 3.45490D+06
10 4.61400D+07
                                    % MMLR CMM
 1.170475460D+00 1.08015790D+00 2.67329710D+00 2.483590D+00
 7.40130000D-01 1.91470000D-01 6.03830000D-01 -2.48730D+00
 -7.665300000D+00 -5.7310000D+00 2.83900000D+00 6.05400D+00
 2.40000000D+00
                                    % PARM(i=0,13)
 24 1 4 6 3 13 4 -1 7
                                    % MN1R MN2R qAD pAD NU1 NU2 qNA NT1 NT2
 1.310D+00 4.180D+00 2.670D+00 4.0D+00 % U1i(i)
                                    % U2INF
 -1.5183D+01 3.7524D+01 -1.1607D+01 3.2200D+01 6.0570D+01 2.2950D+02
 -1.5610D+03 -2.0130D+03 1.2530D+04 5.3600D+03 -4.9740D+04 1.0500D+04
 7.110D+04 -4.70D+04
                                    % U2i(i)
                                    % U2INF
 0.0D+00 7.266D-04 2.70D-04 9.110D-04 2.970D-03 -1.90D-03 -7.20D-03
 2.30D-02
                                    % T2i(i)
                                    % T2INF
 0.0D + 0
-99 1 1 -1 0 1 1 0
                                    % NLEV1 AUTO1 LCDC LXPCT NJM JDJR IWR LPRWF
 0 0
                                    % IV(1) IJ(1)
                                    % IAN1 IMN1 IAN2 IMN2 CHARGE NUMPOT
11 23 1 1 0 1
'Case 2.c: SE-MLR potential for NaH X^1Sigma^+: see betaFIT paper in JQSRT'
0.001d0 0.4d0 50.d0 5.d-08
                                    % RH RMIN RMAX EPS
                                    % NTP LPPOT IOMEG VLIM
0 -0 0 0.d0
4 3 6 16 16 0
                                    % IPOTL PPAR QPAR APSE Nbeta IBOB
15793.4d0 1.88681084d0 3.6d0
                                    % DSCM REQ Rref
 30.69 - 21
                                    % NCMM rhoAB IVSR IDSTT
6 3.57502D+05
8 5.41796D+06
10 1.12920D+8
                                    % (MMLR(I) CMM(I) I= 1,NCMM)
  -1.0000000
              -1.4436321033D-03
  -0.9300000
                5.5253175808D-02
  -0.8700000
                5.2283859294D-02
                4.4152720636D-02
  -0.8100000
  -0.7900000
                4.1302296514D-02
  -0.6300000
                3.2224967101D-02
  -0.4800000
                3.7117729038D-02
  -0.3200000
                6.2549013369D-02
  -0.1600000
                1.2724804641D-01
  0.000000
                2.5944401578D-01
  0.1500000
                4.6902225016D-01
   0.3100000
                7.9765582107D-01
   0.4700000
                1.2594053426D+00
   0.6300000
                1.9422405193D+00
  0.7900000
                2.7670029551D+00
   1.0000000
               3.0169976694D+00
-99 1 1 -1 0 1 1 0 0
                                    % NLEV1 AUTO1 LCDC LXPCT NJM JDJR IWR LPRWF
```

```
0 0
                                   % IV(1) IJ(1)
3 7 3 7 0 1
                                   % IAN1 IMN1 IAN2 IMN2 CHARGE NUMPOT
'Case 2.d: DELR(8) for Li2(B) [see JCP 119, 7398 (2003)]'
0.005 1.5 60.
                                  % RH RMIN RMAX EPS
                 1.d-8
-1 0 1 0.d0
                                   % NTP LPPOT IOMEG VLIM
5 3 3 8 -1 1
                                   % IPOTL PPAR QPAR APSE Nbeta IBOB
2986.600d0 2.935961d0 3.6d0
                                   % DSCM REQ Rref
4 0.54d0 -0 1
                                   % NCMM rhoAB IVSR IDSTT
3 -1.788d5
                                   % MMCM(1) CMM(1)
6 6.97586d6
                                   % MMCM(2) CMM(2)
                                   % MMCM(3) CMM(3)
 8 1.378d8
10 3.445d9
                                   % MMCM(4) CMM(4)
1.0585149D+00 3.70878D-01 2.77660D-01 1.1109D-01 -1.3076D-01 -2.805D-01
-8.69D-02
            3.29D-01 1.61D-01
 7 7 3 3 2 2 3 -1 -1
                                   % MN1R MN2R pAD qAD NU1 NU2 QNA NT1 NT2
 2.52D-01 -3.29D+00 1.40D+00
                                   % U1(0) U1(1)
 1.05578d0
                                   % U1INF
                                   % U2(0) U2(1)
 2.52D-01 -3.29D+00 1.40D+00
 1.05578d0
                                   % U2INF
 -99 1 2 0 0 1 -1 0
                                   % NLEV1 AUTO1 LCDC LXPCT NJM JDJR IWR LPRWF
 0 0
                                   % IV(i) IJ(i)
20 40 20 40 0
                                   % IAN1 IMN1 IAN2 IMN2 CHARGE NUMPOT
'Case 2.e: "Tiemann-type" potential for Ca2(X) [Phys.Rev. A66, 042503(2002)'
0.0005 3.0 80. 1.d-08 % RH RMIN RMAX EPS
-1 0 0 1102.096077d0
                                  % NTP LPPOT IOMEG VLIM
8 1 1 20 -1 0
                                   % IPOTL PPAR QPAR APSE Nbeta IBOB
 1102.096077d0 4.277277d0 0.d0
                                   % DSCM REQ Rref
 2 0.d0 -2 1
                                   % NCMM rhoAB IVSR IDSTT
 6 -1.074d7
                                   % MMLR(1) CMM(1)
 8 -2.4505d8
                                   % MMLR(2) CMM(2)
 0.00042747d0
 -0.254083092764773077d01 \\ \phantom{-}0.379611002601149221d04 \\ \phantom{-}0.382070302022495241d03
 -0.274390396954679318d04 -0.322736334190800926d04 0.363113805693018548d03
 0.634370542189755270d04 - 0.740151835960846893d04 - 0.190738913003729067d05
 -0.836628381353236182d05 \\ \phantom{-}0.213831067083156871d06 \\ \phantom{-}0.155922449222826835d06
 -0.156260872999483137d06 \ -0.146711120959219668d06 \ \ 0.277542999772230869d05
 0.712908015579339117d05 -0.126115550408998979d04
                                   % b R{inn} R{out}
 -0.5929d0
               3.66d0 10.d0
 -99 1 2 0 0 1 -1 0
                                   % NLEV1 AUTO1 LCDC LXPCT NJM JDJR IWR LPRWF
 0 0
                                   % IV(i) IJ(i)
10 20 36 84 0 1
                                   % IAN1 IMN1 IAN2 IMN2 CHARGE NUMPOT
'Case 2.f: Barrow-Aziz HFD-B(6,8,10,12) for {20}Ne{84}Xe [JCP 91, 6348 (1989)]'
0.001 1.5 29. 1.d-08
                                  % RH RMIN RMAX EPS
                                   % NTP LPPOT IOMEG VLIM
-1 00 0
             0.d0 49.75d0
                                   % IPOTL PPAR QPAR APSE Nbeta IBOB
6 0 0 5 0 0
                                   % DSCM REQ Rref
51.5750d0 3.861d0 0.d0
4 0.d0 -2 1
                                   % NCMM rhoAB IVSR IDSTT
 6 1.892088392d5
                                   % MMLR(1) CMM(1)
                                   % MMLR(2) CMM(2)
 8 1.032416239d6
                                   % MMLR(3) CMM(3)
10 9.939199461d6
 12 1.693237609d8
                                   % MMLR(4) CMM(4)
 1.d0 3.872583d0 2.d0 0.1324d0 0.d0 % alpha_i (i=1-3),beta2,gamma
 -99 1 2 0 0 1 -1 0
                                  % NLEV1 AUTO1 LCDC LXPCT NJM JDJR IWR LPRW
0 0
                                   % IV(i) IJ(i)
10 20 36 84 0 1
                                   % IAN1 IMN1 IAN2 IMN2 CHARGE NUMPOT
```

```
'Case 2.g: Generalized Tang-Toennies PEC for Ar2 [Jaeger Mol.Phys. 107, 2181]'
 0.001 1.5
                         29.
                                   1.d-08
                                                                  % RH RMIN RMAX EPS
  -1 00 0
                         0.d0 49.75d0
                                                                  % NTP LPPOT IOMEG VLIM
  7 0 0 9 0 0
                                                                  % IPOTL PPAR QPAR Nbeta APSE IBOB
  99.4734d0
                       3.762d0 0.d0
                                                                  % DSCM REQ Rref
  6 4.02517211d0 +2 0
                                                                  % NCMM rhoAB IVSR IDSTT
   6 3.077697440d+05
                                                                  % MMLR(1) CMM(1)
   8 2.270731967d+06
                                                                  % MMLR(2) CMM(2)
  10 1.707398322d+07
                                                                  % MMLR(3) CMM(3)
                                                                  % MMLR(4) CMM(4)
  12 1.308376851d+08
  14 1.021785836d+09
                                                                  % MMLR(5) CMM(5)
  16 8.132347553d+09
                                                                  % MMLR(6) CMM(6)
     2.98337630d0
     0.097120881d0
   -2.75206827d-1
     1.01489050d0
  -99 1 2 0 0 1 -1 0
                                                                   % NLEV1 AUTO1 LCDC LXPCT NJM JDJR IWR LPRW
                                                                   % IV(i) IJ(i)
     Standard Channel-6 output for Introductory Illustrative Cases 2(a) - 2(g)
Case 2.a: EMO potential for {109}AgD w. BOB corrn [JCP 123, 204304(2005)]
                 ZMU= 1.97752904306(u) & BZ= 1.173076605D-01((1/cm-1)(1/Ang**2))
 from atomic masses: 108.90475530000 & 2.01410177812(u) Integrate from RMIN= 0.800 to RMAX= 30.00 with mesh RH= 0.001000(Angst)
 Potential #1 for Ag(109)- D( 2)
 State has OMEGA= 0 and energy asymptote: Y(lim)= 19250.00000(cm-1)
 BOB adiabatic potential correction for atom-2 of mass
    consists of mass factor [1- MASS( 1 H)/MASS( 2 H)] multiplying all of:
       u1INF= 0.000000 times y3= [(r**3 - Re**3)/(r**3 + Re**3)] plus
       [1 - y3] times an order 3 polynomial in y3=[(r**3 - Re**3)/(r**3 + Re**3)] with the 4 coefficients: 0.000000000D+00 1.175000000D+01 1.756000000D+01 -1.27000000D+01
 BOB centrifugal correction for atom-2 of mass 2.01410177812 consists of mass factor [MASS( 1 H)/MASS( 2 H)] multiplying all of:
   q2INF= 0.00000000D+00 times y3= [(r**3 - Re**3)/(r**3 + Re**3)]
plus [1 - y3] times an order 2 polynomial in y3(r) with the 3 coefficients:
0.00000000D+00 1.50000000D-04 9.30000000D-04
 EMO_3 Potential with De= 19250.0000 Re= 1.61791620 Rref= 1.61791620 Exponent coeft: order- 7 power series in y=(r**3 - Rref**3)/(r**3 + Rref**3) with 8 coefficients: 1.543580950D+00 3.738600000D-02 1.664240000D-01 9.80300000D-02 1.708900000D-01 6.02000000D-02 1.40000000D-01
             2.24000000D-01
 Calculate properties of the single potential described above
 Potential-1 uses inner boundary condition of zero value
 Eigenvalue convergence criterion is EPS= 1.0D-06(cm-1)
 Airy function at 3-rd turning point is quasibound outer boundary condition
 Since state-1 has (projected) electronic angular momentum OMEGA= 0
             eigenvalue calculations use centrifugal potential [J*(J+1) - 0]/r**2
        J= 0, seek the first 100 levels of Potential-1 with
                                                                                           VLIM= 19250.000
 ALF finds the highest calculated level is E(v=25)=1.9244508D+04
                                         Bv= 3.205459
Mv= 2.8933D-19
Bv= 3.1483027
Mv= 8.9664D-20
Bv= 3.0762265
Mv= -1.2066D-19
Bv= 3.0042163
Mv= -3.8002D-19
Bv= 2.9321578
Mv= -7.2433D-19
Bv= 2.8599186
Mv= -1.1935D-18
Bv= 2.7873437
Mv= -1.8395D-18
Bv= 2.7376D-18
Bv= 2.6404234
Mv= -4.0023D-18
Bv= 2.5656104
Mv= -5.8127D-18
 E(v= 0, J= 0)= 621.52
Lv= -3.8730D-14
                                                                                               Hv= 1.3523D-09
Ov= -1.2833D-27
                             621.527
                                                                  -Dv= -8.7936D-05
                                                                    Nv = -2.8833D - 23
         1, J= 0)= 1837.802
Lv= -3.9617D-14
                                                                                              Hv= 1.2955D-09

Ov= -1.4750D-27

Hv= 1.2322D-09

Ov= -2.2640D-27
                                                                   -Dv= -8.7227D-05
Nv= -3.7762D-23
                                                                   NV- -3.7762D-25
-Dv= -8.6598D-05
Nv= -5.3964D-23
-Dv= -8.6064D-05
Nv= -7.8139D-23
                  0)= 3019.707

y= -4.1154D-14

0)= 4167.280
                  0)=
         2, J=
 E(v= 3, J= 0
                 v= 4167.280
v= -4.3541D-14
0)= 5280.497
v= -4.7039D-14
0)= 6359.267
                                                                                               Hv= 1.1614D-09
Ov= -3.7304D-27
                                                                                               Hv= 1.0814D-09
Ov= -6.1362D-27
 E(v=4, J=
                                                                   -Dv= -8.5642D-05
Nv= -1.1204D-22
               Lv=
        5, J=
                                                                   -Dv= -8.5352D-05
 \begin{array}{llll} E(v=&5,\ J=&0)=&6359.26/\\ Lv=&-5.1964D-14\\ E(v=&6,\ J=&0)=&7403.421\\ Lv=&-5.8715D-14\\ E(v=&7,\ J=&0)=&8412.700\\ Lv=&-6.7817D-14\\ E(v=&8,\ J=&0)=&9386.744\\ Lv=&-7.9999D-14\\ E(v=&9,\ J=&0)=&10325.075\\ Lv=&-9.6308D-14\\ \end{array} 
                                                                   Nv= -1.5921D-22
-Dv= -8.5219D-05
Nv= -2.2594D-22
-Dv= -8.5273D-05
Nv= -3.2294D-22
                                                                                               Ov= -9.9956D-27
Hv= 8.8331D-10
                                                                                               0v= -1.6211D-26
Hv= 7.5763D-10
0v= -2.6337D-26
                                                                   -Nv- -3.2244D-22

-Dv- -8.5549D-05

Nv- -4.6800D-22

-Dv- -8.6092D-05

Nv- -6.9092D-22
                                                                                              Hv= 6.0753D-10

0v= -4.3071D-26

Hv= 4.2622D-10

0v= -7.1230D-26
```

Lv= -9.6308D-14

Mv = -5.8127D - 18

```
Bv= 2.4895158
Mv= -8.4541D-18
Bv= 2.4117931
Mv= -1.2391D-17
Bv= 2.3320360
                                                                                                                                                                             Hv= 2.0474D-10
0v= -1.1967D-25
                                                                                                                          -Dv= -8.6955D-05
Nv= -1.0426D-21
-Dv= -8.8203D-05
                                                                                                                                                                             Hv= -6.9065D-11
                                                                                                                          Nv= -1.6122D-21
-Dv= -8.9920D-05
                                                                                                                                                                             Ov= -2.0531D-25
Hv= -4.1216D-10
 Mv= -1.8402D-17
Bv= 2.2497650
                                                                                                                          Nv= -2.5624D-21
-Dv= -9.2210D-05
                                                                                                                                                                             Ov= -3.6175D-25
Hv= -8.4892D-10
                                                                            Mv= -2.7830D-17
Bv= 2.1644091
                                                                                                                                                                            HV= -8.4892D-10

Ov= -6.5890D-25

HV= -1.4153D-09

Ov= -1.2503D-24

HV= -2.1663D-09

Ov= -2.4951D-24

HV= -3.1883D-09

Ov= -5.2999D-24

HV= -4.6243D-09

Ov= -1.2176D-22
                                                                                                                          Nv= -4.2008D-21

-Dv= -9.5214D-05

Nv= -7.1385D-21

-Dv= -9.9120D-05
                                                                            Mv= -4.3090D-17
Bv= 2.0752796
Mv= -6.8730D-17
                             Lv=
                                                                           Lv= -4.053/U-13

E(v= 16, J= 0)= 15820.880

Lv= -6.6291D-13

E(v= 17, J= 0)= 16436.280

Lv= -9.8634D-13

E(v= 18, J= 0)= 17003.044

Lv= -1.5397D-12

E(v= 19, J= 0)= 17518.114

Lv= -2.5552D-12

E(v= 20, J= 0)= 17977.832
                                                                                                                          NV- -1.2038D-20

-Dv= -1.0419D-04

Nv= -2.3634D-20

-Dv= -1.1081D-04

Nv= -4.7051D-20

-Dv= -1.1955D-04
                                                                                                                                                                            Hy= -4.6243D-09

Ov= -1.2176D-23

Hy= -6.7223D-09

Ov= -3.0940D-23

Hv= -9.9432D-09

Ov= -8.9823D-23

Hy= -1.5222D-08

Ov= -3.1333D-22

Hv= -2.4701D-08

Ov= -1.4293D-21

Hy= -4.4238D-08
                                                                                                                        -Dv= -1.1955D-04

Nv= -1.0165D-19

-Dv= -1.3130D-04

Nv= -2.4462D-19

-Dv= -1.4758D-04

Nv= -6.8287D-19

-Dv= -1.7116D-04

Nv= -2.3671D-18

-Dv= -2.0777D-04

Nv= -2.1578D-17

-Dv= -2.7179D-04

Nv= -1.0641D-16
Bv= 1.2302153

Mv= -1.4927D-14

Bv= 1.0378809

Mv= -8.2964D-14

Bv= 0.7945156
                                                                                                                                                                             Hv= -4.4238D-08
0v= -9.9942D-21
                                                                                                                                                                             Hv = -9.5322D - 08
                                                                                                                         -Dv= -2.7179D-04

Nv= -1.0641D-16

-Dv= -4.1659D-04

Nv= -4.4539D-15

-Dv= -1.4775D-03
                                                                                                                                                                            0v= -1.5297D-19
Hv= -3.2127D-07
0v= -1.5359D-17
Hv= -1.4620D-05
                                                                            Mv= -1.4623D-12
Bv= 0.4195501
                                                                             Mv = -1.1158D - 08
                                                                                                                            Nv= -4.1855D-10
                             Lv= -3.4825D-07
                                                                                                                                                                             Ov= -1.7371D-11
 Find 26 Potential-1 vibrational levels with J= 0 _{V} _{E(v)} _{v} _{E(v)}
                                                                                                                                                                             E(v)
                        621.5267
1837.8022
                                                                       8412.7004
9386.7439
                                                                                                                  14454.0900
15159.4225
                                                                                                                                                          21
22
23
                                                                                                                                                                     18377.7702
18712.4681
             0
                                                                  10325.0747
11227.0834
                                                                                                          16
17
18
                        3019.7070
4167.2795
                                                                                                                  15820.8804
16436.2800
                                                                                                                                                                     18975.0358
                                                                                                                                                           24
                                                          10
                                                                                                                                                                     19156.4822
                        5280.4968
6359.2672
                                                                     12092.0119
12918.9344
                                                                                                                    17003.0435
17518.1136
                                                                                                                                                                     19244.5078
  An n=99 N-D theory extrapolation from v= 24 & 25 implies vD = 25.332
Case 2.b: PE-MLR fx for MgD w. BOB corrn: from JPCA 117, 13373 (2013)
  Generate ZMU= 1.85807333140(u) & BZ= 1.102215091D-01((1/cm-1)(1/Ang**2))
  from atomic masses: 23.98504169800 & 2.01410177812(u)
Integrate from RMIN= 0.500 to RMAX= 99.00 with mesh RH= 0.000500(Angst)
  Potential #1 for Mg( 24)- D( 2)
  State has OMEGA= 0 and energy asymptote: Y(lim)=
  BOB adiabatic potential correction for atom-1 of mass 23.98504169800 consists of mass factor [1- MASS( 24Mg)/MASS( 24Mg)] multiplying all of:
            u1INF= 0.000000 times y6= [(r**6 - Re**6)/(r**6 + Re**6)] plus
             [1 - y6] times an order 3 polynomial in y4=[(r**4 - Re**4)/(r**4 + Re**4)] with the 4 coefficients: 1.310000000D+00 4.18000000D+00 2.670000000D+00 4.00000000D+00
        B adiabatic potential correction for atom-2 of mass 2.01410177812 consists of mass factor [1- MASS( 1 H)/MASS( 2 H)] multiplying all of:
  BOB adiabatic potential correction for atom-2 of mass
                                  0.000000 times y6= [(r**6 - Re**6)/(r**6 + Re**6)] plus
                   [1 - y6] times an order 13 polynomial in
                  y4=[(r**4 - Re**4)/(r**4 + Re**4)] with the 14 coefficients:
            -1.518300000D+01 3.752400000D+01 -1.160700000D+01 3.22000000D+01 6.05700000D+01 2.29500000D+02 -1.56100000D+03 -2.01300000D+03 1.25300000D+04 5.3600000D+03 -4.97400000D+04 1.05000000D+04 7.11000000D+04 -4.7000000D+04
 BOB centrifugal correction for atom-2 of mass 2.01410177812 consists of mass factor [MASS( 1 H)/MASS( 2 H)] multiplying all of: q2INF= 0.00000000000+00 times y4= [(r**4 - Re**4)/(r**4 + Re**4)]
       plus [1 - y4] times an order 7 polynomial in y4(r) with the 8 coefficients: 0.000000000D+00 7.26600000D-04 2.70000000D-04 9.11000000D-04 2.97000000D-03 -1.90000000D-03 -7.20000000D-03 2.30000000D-02
  uLR inverse-power terms incorporate DS-type damping with
                                                                                                                                                             rhoAB= 0.810000
                     defined to give very short-range Dm(r)*Cm/r^m behaviour r^{-2/2}
                     Dm(r) = [1 - exp(-3.30(rhoAB*r)/m - 0.423(rhoAB*r)^2/sqrt{m})]^{m -2/2}
                                                                                                         C6 = 2.77550000D+05
C8 = 3.45490000D+06
C10= 4.61400000D+07
  uLR(r) has 3 inverse-power terms:
 exponent power series of order 12 in a variable in which Rref= 2.74000 with 13 coefficients: 1.170475460D+00 1.080157900D+00 2.673297100D+00 2.48359000D+00 7.40130000D-01 1.91470000D-01 6.038330000D-01 -2.48730000D+00 -7.66530000D+00 -5.73100000D+00 2.83900000D+00 6.05400000D+00 2.4000000D+00 -7.66530000D+00 2.83900000D+00 -7.66530000D+00 2.83900000D+00 -7.66530000D+00 -7.6653000D+00 -7.6653000D+00 -7.6653000D+00 -7.6653000D+00 -7.665300D+00 -7.6
                                       betaINF= 2.046201180015 from uLR(Re)= 2.8698906226D+03
```

```
Calculate properties of the single potential described above
 Potential-1 uses inner boundary condition of zero value at RMIN
                                                          EPS = 1.0D - 05(cm - 1)
  Eigenvalue convergence criterion is
 Airy function at 3-rd turning point is quasibound outer boundary condition
 Since state-1 has (projected) electronic angular momentum OMEGA= 0
              eigenvalue calculations use centrifugal potential [J*(J+1) - 0]/r**2
 For J= 0, seek the first 100 levels of Potential-1 with VLIM=
                                                                                                                0.000
E(v=0,J=
                  0) = -10576.9713
         1,J=
                  0) = -9531.1273
E(v=
E(v=
         2,J=
                  0)= -8517.5782
                  0)= -7537.4551
E(v=
         3,J=
         4,J=
E(v=
                   0) = -6592.2479
E(v=
         5,J=
                  0) = -5683.9300
E(v=
         6,J=
                  0) = -4815.1134
                  0) = -3989.2702
E(v=
         7,J=
                  0) = -3211.0590
E(v=
        8,J=
                  0) = -2486.8045
E(v=9,J=
E(v= 10,J=
                  0) = -1825.1989
                  0) = -1238.3300
E(v=11,J=
E(v= 12, J=
                   0) = -743.1449
                  0) = -363.0851
E(v= 13.J=
E(v= 14, J=
                  0) = -126.0360
E(v=15,J=
                 0)=
                          -30.5770
E(v= 16, J=
                  0)=
                            -2.7309
              Find highest level of this potential is E(v=16)=-2.7309323395D+00
 ALF finds the highest calculated level is E(v=16)=-2.7309323D+00
E(v= 0, J= 0)=-10576.9713
E(v= 0, J= 0)=-10576.971

Lv= -1.0297D-13

E(v= 1,J= 0)= -9531.1273
                                                                       -Dv= -9.6194D-05
Nv= -2.8462D-22
                                                                                                    Hv= 2.0891D-09
Ov= -3.9837D-27
                                              By= 3.0009468
                                            Mv= 1.8787D-18
Bv= 2.9333876
Mv= 6.7506D-19
                                                                       -Dv= -9.6337D-05
Nv= -4.0035D-22
                                                                                                    Hv= 1.9600D-09
0v= -1.8539D-26
                                                                       -Dv= -9.6828D-05
                                              By= 2.8643763
                                                                                                    H_{V} = 1.7810D - 09
                                            Mv = -1.4522D - 18
                                                                        Nv = -7.1077D - 22
                                                                                                    Ov= -4.9236D-26
                                              Bv= 2.7933659
                                                                       -Dv= -9.7786D-05
                                                                                                    Hv= 1.5280D-09
                                            Mv = -5.2122D - 18
                                                                        Nv= -1.2423D-21
                                                                                                    Ov = -1.3838D - 25
E(v= 4, J= 0) = -6592.248

Lv= -2.1360D-13

E(v= 5,J= 0) = -5683.9300
                                                                                                    Hv= 1.1631D-09
                                            Bv= 2.7196297
Mv= -1.2452D-17
                                                                       -Dv= -9.9396D-05
                                                                                                    Ov = -3.4728D - 25
                                                                        Nv = -2.3423D - 21
\begin{array}{lll} E(v=&5,J=&0)=-5863.930\\ E(v=&5,J=&0)=-5683.930\\ Lv=&-2.9701D-13\\ E(v=&6,J=&0)=-4815.1134\\ E(v=&6,J=&0)=-4815.113\\ Lv=&-4.4425D-13\\ E(v=&7,J=&0)=-3989.2702\\ \end{array}
                                                      2.6421849
                                                                        -Dv= -1.0193D-04
                                            Mv = -2.6867D-17
                                                                        Nv= -4.8363D-21
                                                                                                    0v = -8.5123D - 25
                                                                                                    Hv= -2.0991D-10
Ov= -2.1867D-24
                                                                        -Dv= -1.0579D-04
                                            Mv = -5.6382D - 17
                                                                        Nv = -1.0793D-20
 \begin{array}{lll} E(v=&7,J=&0)=-3989.2702\\ E(v=&7,J=&0)=-3989.270\\ Lv=&-7.1777D-13\\ E(v=&8,J=&0)=-3211.0590\\ E(v=&8,J=&0)=-3211.059\\ Lv=&-1.2572D-12\\ E(v=&9,J=&0)=-2486.804\\ E(v=&9,J=&0)=-2486.804\\ Lv=&-2.4088D-12\\ E(v=&10,J=&0)=-1825.1989\\ E(v=&10,J=&0)=-1825.1989\\ E(v=&10,J=&0)=-1825.1989 \end{array} 
                                            Bv= 2.4701994
Mv= -1.1988D-16
                                                                        -Dv= -1.1164D-04
Nv= -2.6016D-20
                                                                                                    Hv= -1.5383D-09
Ov= -6.1356D-24
                                            Bv= 2.3709745
Mv= -2.6769D-16
                                                                       -Dv = -1.2055D-04
                                                                                                    Hv = -3.7550D - 09
                                                                        Nv= -6.8839D-20
                                                                                                    Ov= -1.9375D-23
                                                                                                    Hv= -7.6602D-09
Ov= -7.1509D-23
                                                                       -Dv= -1.3439D-04
                                            Mv = -6.5150D-16
                                                                        Nv= -2.0617D-19
E(v= 10, J= 0)= -1825.199

Lv= -5.1513D-12

E(v= 11,J= 0)= -1238.3300
                                                                       -Dv= -1.5657D-04
Nv= -7.3449D-19
                                                                                                    Hv= -1.5062D-08
Ov= -3.2785D-22
                                              By= 2.1245297
                                            Mv = -1.8077D - 15
E(v= 11, J= 0)= -1238.330

E(v= 11, J= 0)= -1238.330

Lv= -1.2783D-11

E(v= 12, J= 0)= -743.1445

E(v= 12, J= 0)= -743.145

Lv= -3.9679D-11
                                                                       -Dv= -1.9391D-04
Nv= -3.3875D-18
                                                                                                    Hv= -3.0630D-08
0v= -2.0746D-21
                                                     1.9607791
                                            Mv = -6.1094D - 15
-, - 0)= -743

Lv = -3.9679D

E(v = 13, J = 0) = -363.08

E(v = 12)
                                                     1.7495212
                                                                       -Dv= -2.6164D-04
Nv= -2.3600D-17
                                                                                                    Hv = -6.8835D - 08
                                                                                                    Ov= -2.1938D-20
                                            Mv = -2.8259D-14
 E(v= 13, J= 0) = -363.0851

E(v= 13, J= 0) = -363.085

Lv= -1.7762D-10
                                                     1.4609104
                                                                       -Dv = -3.9887D - 04
                                                                                                    Hv = -1.8763D - 07
                                              Bv=
E(V=13, J=0) = -363.085

LV=-1.7762D-10

E(V=14, J=0) = -126.0360

E(V=14, J=0) = -126.036

LV=-1.1429D-09

E(V=15, J=0) = -30.5770

E(V=15, J=0) = -30.5770
                                            Mv = -2.2062D - 13
                                                                        Nv= -3.2568D-16
                                                                                                    Ov= -5.3844D-19
                                            Bv= 1.0524948
Mv= -2.8624D-12
                                                                       -Dv= -6.9579D-04
Nv= -8.7147D-15
                                                                                                    Hv= -6.2944D-07
0v= -3.0196D-17
E(v= 15, J= 0)= -30.5770

E(v= 15, J= 0)= -30.577

Lv= -7.8253D-09

E(v= 16, J= 0)= -2.7309

E(v= 16, J= 0)= -2.731

Lv= -9.2968D-07
                                                                                                    Hv= -1.4581D-06
0v= -4.2484D-15
                               -30.577
                                              Bv=
                                            Mv = -5.6840D - 11
                                                                        Nv = -4.6701D - 13
                                                                                                    Hv= -2.9685D-05
Ov= -1.1090D-10
                Lv= -9.2968D-07
                                                                        Nv = -1.9920D - 09
                                            Mv = -3.9645D - 08
 Find 17 Potential-1 vibrational levels with
                                                                                                    E(v)
                                            E(v)
        0 -10576.9713
                                        -5683.9300
                                                             10 -1825.1989
                                                                                         15
                                                                                                  -30.5770
            -9531.1273
-8517.5782
                                      -4815.1134
-3989.2702
                                                             11 -1238.3300
12 -743.1449
                                      -3211.0590
-2486.8045
                                                                     -363.0851
            -6592.2479
                                                                     -126.0360
                                                             14
  An n=6 N-D theory extrapolation from v=15 & 16 implies
                                                                                                     vD = 16.808
```

Case 2.c: SE-MLR potential for NaH X^1Sigma^+: see betaFIT paper in JQSRT

```
ZMU= 0.96549948567(u)
                                                                                 BZ= 5.727374080D-02((1/cm-1)(1/Ang**2))
  Generate
                                                                           &r.
  from atomic masses: 22.98976928200 & 1.00782503223(u)
Integrate from RMIN= 0.400 to RMAX= 50.00 with mesh RH= 0.001000(Angst)
  Potential #1 for Na(23)-H(1)
  State has OMEGA= 0 and energy asymptote:
                                                                                             Y(lim) =
  uLR inverse-power terms incorporate DS-type damping with
                                                                                                                        rhoAB= 0.690000
                defined to give very short-range Dm(r)*Cm/r^m behaviour
                                                                                                                                         r^{-2/2}
                Dm(r)= [1 - exp(- 3.30(rhoAB*r)/m - 0.423(rhoAB*r)^2/sqrt{m})]^{m -2/2}
                                                                                 C6 = 3.57502000D+05
  uLR(r) has 3 inverse-power terms:
                                                                                 C8 = 5.41796000D+06
  MLR(q=3, p=6) Potential with:
                                                                   De=15793.4000[cm-1]
                                                                                                                 Re= 1.88681084[A]
      with SE-MLR exponent coefft
                                                                  beta(r)=
                                            y6^{eq} *{Spline through the 16 function values} beta_i = 
|D-02 0.55253176D-01 0.52283859D-01 0.44152721D-01 
| D-01 0.32224967D-01 0.37117729D-01 0.62549013D-01 
| D-00 0.25944402D+00 0.46902225D+00 0.79765582D+00 |
                        -0.14436321D-02
0.41302297D-01
0.12724805D+00
          0.12594053D+01 0.19422405D+01 0.27670030D+01 0.30169977D+01 at distances defined by y_3(r; RREF) = 0.3600000D+01 -0.1000000D+00 -0.8100000D+00 -0.7900000D+00 -0.6300000D+00 -0.4800000D+00 -0.3200000D+00 -0.1600000D+00 -0.3200000D+00 -0.1600000D+00 0.000000D+00 0.1500000D+00 0.3200000D+00 0.4700000D+00 0.3200000D+00 0.4700000D+00 0.3200000D+00 0.4700000D+00 0.3200000D+00 0.4700000D+00 0.3200000D+00 0.7700000D+00 0.3200000D+00 0.7700000D+00 0.3200000D+00 0.470000D+00 0.3200000D+00 0.7700000D+00 0.3200000D+00 0.3200000D+00 0.3200000D+00 0.3200000D+00 0.3200000D+00 0.3200000D+00 0.3200000D+00 0.320000D+00 0.320000D+00 0.320000D+00 0.3200000D+00 0.320000D+00 0.32000D+00 0.320000D+00 0.320000D+00 0.320000D+00 0.320000D+00 0.32000D+00 0.32000D+00 0.320000D+00 0.320000D+00 0.32000D+00 0.320000D+
                        0.3100000D+00
                                                      0.4700000D+00
                                                                                         0.6300000D+00
                                                                                                                          0.7900000D+00
                        0.3100000000F00 0.1.551
0.10000000D+01 from uLR(Re)= 1.5839598324D+03
betaINF= 2.992811377060 from uLR(Re)= 1.5839598324D+03
        Generate
  Calculate properties of the single potential described above Potential-1 uses inner boundary condition of zero value at RMIN
  Eigenvalue convergence criterion is EPS=5.0D-08(cm-1) Airy function at 3-rd turning point is quasibound outer boundary condition
  Since state-1 has (projected) electronic angular momentum OMEGA= 0
                  eigenvalue calculations use centrifugal potential [J*(J+1) - 0]/r**2
  For J= 0, seek the first 100 levels of Potential-1
E(v=
           0,J=
                        0) = -15205.1139
                        0)=-14059.9108
E(v=
           1,J=
E(v=
           2,J=
                        0) = -12954.1908
            3,J=
                        0)=-11887.6945
E(v=
E(v=
            4,J=
                        0) = -10859.4081
E(v=
            5,J=
                        0) = -9868.5071
                        0) = -8914.4586
F(v=
            6,J=
            7,J=
                        0) = -7997.0494
E(v=
                        0)= -7116.3661
E(v=
           8,J=
                        0) = -6272.7065
E(v=
           9,J=
                        0)= -5466.5854
E(v=10,J=
E(v= 11,J=
                        0) = -4698.9715
E(v= 12, J=
                        0) = -3971.4345
E(v= 13, J=
                        0) = -3286.1933
E(v= 14, J=
                        0) = -2646.3120
E(v= 15, J=
                        0) = -2055.9614
E(v= 16, J=
                        0) = -1520.8021
E(v= 17, J=
                        0) = -1048.1654
                        0)= -647.3388
0)= -330.1624
E(v= 18, J=
E(v= 19, J=
E(v= 20, J=
                        0)=
                                -111.1142
E(v= 21,J=
                        0)=
                                      -7.5824
                    Find highest level of this potential is E(v=21)=-7.5824289234D+00
  ALF finds the highest calculated level is E(v=21)=-7.5824289D+00
E(v= 0, J= 0)=-15205.1139
E(v= 0, J= 0)=-15205.114

Lv= -1.6555D-12

E(v= 1,J= 0)=-14059.9108
                                                          Bv= 4.8331668
Mv= 2.2203D-16
                                                                                             -Dv= -3.3310D-04
Nv= -3.9992D-20
                                                                                                                                              1.9277D-08
2.4754D-24
                                                                                                                                    0v =
E(v= 1, J= 0)=-14059.911

Lv= -2.1257D-12

E(v= 2,J= 0)=-12954.1908
                                                                                              -Dv= -3.2844D-04
Nv= 2.6476D-20
                                                                                                                                             2.0000D-08
-7.9004D-24
                                                            Bv=
                                                                       4.6941582
                                                                   2.1432D-16
                                                                                                                                    0v =
E(v= 2, J= 0)=-12954.191

Lv= -1.7867D-12

E(v= 3,J= 0)=-11887.6945
                                                                   4.5586852
5.5906D-17
                                                                                              -Dv= -3.2535D-04
Nv= -3.3163D-20
                                                                                                                                              2.0353D-08
3.7621D-23
                                                             Bv=
E(v= 3, J= 0)=-11887.695

Lv= -1.7212D-12

E(v= 4,J= 0)=-10859.4081
                                                            Bv= 4.4257375

dv= 2.0411D-16
                                                                                               -Dv= -3.2148D-04
Nv= -1.6028D-19
                                                                                                                                              1.9969D-08
6.3876D-23
E(v= 4, J= 0)=-10859.408

Lv= -2.1157D-12

E(v= 5,J= 0)= -9868.5071
                                                                       4.2945424
                                                                                              -Dv= -3.1731D-04
Nv= -2.2889D-19
                                                                                                                                              1.9479D-08
                                                            Bv=
                                                           Mv= 6.0713D-16
                                                                                                                                    0v = -1.4273D - 23
  E(v= 5, J= 0) = -9868.507
                                                                       4.1645485
                                                                                              -Dv= -3.1354D-04
                                                                                                                                              1.9600D-08
                                                            Bv=
                                                                                                                                    Hv=
Lv= -2.9019D-12
E(v= 6,J= 0)= -8914.4586
                                                           Mv= 7.0236D-16
                                                                                               Nv= -1.0183D-19
                                                                                                                                    0v = -1.4209D - 23
 E(v= 6, J= 0) = -8914.459
                                                                       4.0355776
                                                                                              -Dv= -3.1085D-04
                                                                                                                                              1.9839D-08
                                                             Bv=
E(v= 7, J= 0)= -7997.049
E(v= 7, J= 0)= -7997.049
                                                           Mv= 7.0500D-16
                                                                                               Nv= -1.0195D-19
                                                                                                                                              4.0625D-23
                                                             Bv=
                                                                       3.9071118
                                                                                              -Dv= -3.0945D-04
                                                                                                                                              1.9995D-08
Lv= -3.9581D-12
E(v= 8,J= 0)= -7116.3661
                                                           Mv= 8.2102D-16
                                                                                               Nv = -1.4751D-19
                                                                                                                                    0v = -9.2558D - 24
E(v= 8, J= 0)= -7116.366

Lv= -4.4146D-12

E(v= 9, J= 0)= -6272.7065
                                                             Bv=
                                                                       3.7784456
                                                                                               -Dv= -3.0925D-04
                                                                                                                                              2.0222D-08
                                                           Mv= 7.4436D-16
                                                                                               Nv = -1.8574D - 19
                                                                                                                                    0v = -5.6741D - 23
           9, J= 0)= -6272.707
Lv= -5.2227D-12
 E(v=
                                                           Bv= 3.6489419
Mv= 5.8585D-16
                                                                                                       -3.1027D-04
2.6970D-20
                                                                                                                                    Hv= 2.0001D-08
Ov= -1.3817D-22
                                                                                               -Dv= -
Nv=
```

```
E(v=10,J=0)=-5466.5854
E(v= 10, J= 0)= -5466.585

Lv= -5.9354D-12

E(v= 11, J= 0)= -4698.9715
                                                Bv= 3.5175361
Mv= 3.9491D-16
                                                                             -Dv = -3.1331D - 04
                                                                                                             Hv = 1.8882D - 08
                                                                                                             Ov= -1.0225D-22
                                                                              Nv= 2.8319D-19
E(v= 11, J= 0)= -4698.971
Lv= -6.2479D-12
E(v= 12,J= 0)= -3971.4345
                                                Bv= 3.3824634
Mv= -1.7939D-16
                                                                             -Dv= -3.1910D-04
Nv= -8.7693D-20
                                                                                                                    1.7026D-08
2.1916D-22
E(v= 12, J= 0)= -3971.434

Lv= -7.1829D-12

E(v= 13,J= 0)= -3286.1933
                                                Bv= 3.2416371
Mv= -5.2298D-16
                                                                             -Dv= -3.2807D-04
Nv= -2.1715D-19
                                                                                                                     1.3791D-08
                                                                                                                    2.1104D-22
E(v= 13, J= 0)= -3286.193

Lv= -8.6163D-12

E(v= 14,J= 0)= -2646.3120
                                                Bv= 3.0923821
Mv= -1.2237D-15
                                                                             -Dv= -3.4152D-04
Nv= -1.1067D-18
                                                                                                                     8.6767D-09
                                                                                                                     2.0155D-22
E(v= 14, J= 0)= -2646.312

Lv= -1.2034D-11

E(v= 15,J= 0)= -2055.9614
                                                Bv= 2.9311694
Mv= -2.1016D-15
                                                                             -Dv= -3.6133D-04
Nv= -1.2972D-18
                                                                                                            Hv= 2.8620D-10
Ov= -3.4999D-22
E(v= 15, J= 0)= -2055.961

Lv= -1.7209D-11

E(v= 16, J= 0)= -1520.8021
                                                Bv= 2.7530085
Mv= -4.1249D-15
                                                                             -Dv= -3.9095D-04
Nv= -2.7177D-18
                                                                                                            Hv= -1.2843D-08
Ov= -1.2986D-21
E(v= 16, J= 0)= -1520.802

Lv= -2.7298D-11

E(v= 17,J= 0)= -1048.1654
                                                Bv= 2.5512339
Mv= -1.1300D-14
                                                                             -Dv= -4.3431D-04
Nv= -8.9361D-18
                                                                                                            Hv= -3.2942D-08
Ov= -5.2467D-21
E(v= 17, J= 0)= -1048.165

E(v= 17, J= 0)= -1048.165

Lv= -5.3828D-11

E(v= 18, J= 0)= -647.3388

E(v= 18, J= 0)= -647.339

Lv= -1.2066D-10
                                                Bv= 2.3174627
Mv= -3.1131D-14
                                                                              -Dv= -4.9839D-04
Nv= -2.3355D-17
                                                                                                             Hv= -6.9505D-08
Ov= -2.1422D-20
                                                  By= 2.0391708
                                                                             -Dv= -5.9924D-04
Nv= -1.1615D-16
                                                                                                             H_{V} = -1.4274D - 07
Lv= -1.2066D-10

E(v= 19, J= 0)= -330.1624

E(v= 19, J= 0)= -330.162
                                                Mv = -1.0524D-13
                                                                                                             Ov= -1.4195D-19
                                                  Bv= 1.6970822
                                                                             -Dv = -7.6935D-04
                                                                                                            Hv= -3.2068D-07
Ov= -2.2057D-18
E(v= 20, J= 0)= -330.162

E(v= 20, J= 0)= -111.1142

E(v= 20, J= 0)= -111.114
                                                Mv= -5.9131D-13
                                                                              Nv= -1.0961D-15
                                                  Bv= 1.2568292
                                                                             -Dv= -1.1313D-03
                                                                                                            Hv= -1.0898D-06
Ov= -2.0574D-16
E(v= 21, J= 0)= -7.5824
                                                Mv = -9.8299D - 12
                                                                              Nv= -4.2384D-14
 E(v= 21, J= 0)= -7.5824

E(v= 21, J= 0)= -7.582

Lv= -7.0675D-07
                                                Bv= 0.6000757
Mv= -2.2843D-08
                                                                             -Dv= -3.2026D-03
Nv= -8.6687D-10
                                                                                                            Hv= -2.9845D-05
Ov= -3.6386D-11
  Find 22 Potential-1 vibrational levels with v E(v) v E(v) v
                                                                                                             E(v)
                                      6 -8914.4586
7 -7997.0494
8 -7116.3661
9 -6272.7065
10 -5466.5854
        0 -15205.1139
                                                                   12 -3971.4345
                                                                                                         -647.3388
                                                                   13
14
                                                                        -3286.1933
-2646.3120
           -14059.9108
                                                                                                         -330.1624
        1 -14059.9108
2 -12954.1908
3 -11887.6945
4 -10859.4081
                                                                                                 20
                                                                                                         -111.1142
-7.5824
                                                                         -2055.9614
-1520.8021
                                     9
10
  An n= 6 N-D theory extrapolation from v= 20 & 21 implies vD = 21.691
from atomic masses: 7.01600343700 & 7.01600343700(u)
Integrate from RMIN= 1.500 to RMAX= 60.00 with mesh RH= 0.005000(Angst)
  Potential #1 for Li( 7)-Li( 7)
  State has OMEGA=1 and energy asymptote: Y(lim)=
                                                                                                  0.00000(cm-1)
 BOB adiabatic potential correction for atom-1 of mass 7.01600343700 consists of mass factor [1- MASS( 7Li)/MASS( 7Li)] multiplying all of:
                       1.055780 times y3= [(r**3 - Re**3)/(r**3 + Re**3)] plus
        u1INF=
            [1 - y3] times an order 2 polynomial in y3=[(r**3 - Re**3)/(r**3 + Re**3)] with the
         2.520000000D-01 -3.29000000D+00 1.40000000D+00
 BOB adiabatic potential correction for atom-2 of mass 7.01600343700 consists of mass factor [1- MASS( 7Li)/MASS( 7Li)] multiplying all of:
                      1.055780 times y3= [(r**3 - Re**3)/(r**3 + Re**3)] plus
            [1 - y3] times an order 2 polynomial in y3=[(r**3 - Re**3)/(r**3 + Re**3)] with the
                                                                                          3 coefficients:
         2.520000000D-01 -3.29000000D+00 1.40000000D+00
 uLR inverse-power terms incorporate DS-type damping with $\rm rho\,AB=~0.540000$ defined to give very short-range Dm(r)*Cm/r^m behaviour $\rm r^{0/2}$
             Dm(r) = [1 - exp(-3.95(rhoAB*r)/m - 0.390(rhoAB*r)^2/sqrt{m})]^{m + 0/2}
                                                                  C3 = -1.7880000D+05

C6 = 6.97586000D+06

C 8= 1.37800000D+08

C10= 3.44500000D+09
  uLR(r) has 4 inverse-power terms:
  \label{eq:delta} DELR(q=~3)~Potential~with~~De=~~2986.6000[cm-1]
                                                                                     Re= 2.93596100[A]
     exponent coefft. has power series order 8
          with polynomial coefficients
                                                                           1.05851490D+00
                                                                                                      3.70878000D-01
    with polynomial coefficients 1.058514900+00 3.70878000D-01 2.7766000D-01 1.1109000D-01 -1.3076000D-01 -2.8050000D-01 -8.6900000D-02 3.2900000D-01 1.6100000D-01 where the radial variable y_3= (r**3 - Rref**3)/(r**3 + Rref**3) is defined w.r.t. Rref= 3.60000000 Generate A(DELR)= 3.595299321D+03 B(DELR)= 8.493929499D+03 from uLR defined by 4 inverse-power terms
  Calculate properties of the single potential described above Potential-1 uses inner boundary condition of \, zero value \, at \, RMIN \,
  Eigenvalue convergence criterion is EPS= 1.0D-08(cm-1)
```

```
Appendix C.2: Input/Output files for Several Families of Analytic Potentials
                                                                                                                                                                                                                                        28
  Airy function at 3-rd turning point is quasibound outer boundary condition
 Since state-1 has (projected) electronic angular momentum OMEGA= 1
                  eigenvalue calculations use centrifugal potential [J*(J+1) - 1]/r**2
 For J= 0, seek the first 100 levels of Potential-1 with VLIM=
  Case 2.d: DELR(8) for Li2(B) [see JCP 119, 7398 (2003)]
                                                                                                                                                                for Li( 7)-Li( 7)
                                                                                                            _____
  Although OMEGA= 1, these band constants obtained for [J(J+1) - OMEGA^2] = 0
  ALF finds the highest calculated level is E(v= 17)= 4.7570998D+02
                                                        Bv= 0.5532317

Mv= 7.3145D-20

Bv= 0.5445462

Mv= 6.7107D-20

Bv= 0.5355791

Mv= 5.1407D-20

Bv= 0.5262880

Mv= 2.1592D-20

Bv= 0.5166217

Mv= -3.0040D-20

Bv= 0.5065187

Mv= -1.1683D-19

Bv= 0.4959047

Mv= -2.6233D-19

Bv= 0.4846894

Mv= -5.0959D-19
 E(v= 0, J= 0) = -2852.038
                                                                                          -Dv= -9.4985D-06
 E(v= 1, J= 0
                                                                                                                                 0v= 8.8161D-29
Hv= 1.1744D-10
0v= 4.7341D-29
Hv= 1.1133D-10
                         v= -4.4026D-15
0)= -2587.420
                                                                                            Nv= -5.4567D-24
-Dv= -9.6053D-06
 \begin{array}{llll} E(v=&1,\;J=&0)=-2587.420\\ &Lv=-4.8761D-15\\ E(v=&2,\;J=&0)=-2329.158\\ &Lv=-5.4803D-15\\ E(v=&3,\;J=&0)=-2077.485\\ &Lv=-6.2617D-15\\ E(v=&4,\;J=&0)=-1832.661\\ &Lv=-7.2904D-15\\ E(v=&5,\;J=&0)=-1594.986\\ &Lv=-8.6766D-15\\ E(v=&6,\;J=&0)=-1364.801\\ &Lv=-1.0597D-14\\ E(v=&7,\;J=&0)=-1142.500\\ &Lv=-1.3345D-14 \end{array} 
                                                                                            Nv= -7.2329D-24
-Dv= -9.7359D-06
                                                                                             Nv= -9.6568D-24
                                                                                                                                  0v = -4.6601D - 29
                                                                                                                                 Hv= 1.0327D-10

Ov= -2.4070D-28

Hv= 9.2527D-11
                                                                                            -Dv= -9.8948D-06
                                                                                          -Dv= -9.8948D-06
Nv= -1.3222D-23
-Dv= -1.0088D-05
Nv= -1.8801D-23
-Dv= -1.0323D-05
Nv= -2.7998D-23
-Dv= -1.0610D-05
Nv= -4.3886D-23
-Dv= -1.0963D-05
Nv= -7.2654D-23
-Dv= -1.1399D-05
Nv= -1.2748D-22
                                                                                                                                 Ov= -6.2656D-28
Hv= 7.8113D-11
                                                                                                                                 Ov= -1.3898D-27
Hv= 5.8653D-11
Ov= -2.9237D-27
Hv= 3.2132D-11
 Lv= -1.3345D-14
E(v= 8, J= 0)= -928.539
                                                         Mv= -5.0959D-19
Bv= 0.4727617
                                                                                                                                 Ov= -6.1073D-27
Hv= -4.5249D-12
                                                        Bv= 0.4727617

Mv= -9.4086D-19

Bv= 0.4599828

Mv= -1.7227D-18

Bv= 0.4461745

Mv= -3.2179D-18

Bv= 0.4311013

Mv= -6.2925D-18

Bv= 0.4144372

Mv= -1.3284D-17

Bv= 0.3957050

Mv= -3.1668D-17
                              )= -920.000
-1.7424D-14
))= -723.447
                                                                                           -Dv= -1.1399D-05

Nv= -1.2748D-22

-Dv= -1.1945D-05

Nv= -2.3841D-22

-Dv= -1.2638D-05

Nv= -4.8005D-22

-Dv= -1.3538D-05
                                                                                                                                 0v= -1.3033D-26

Hv= -5.6223D-11

0v= -2.9080D-26

Hv= -1.3120D-10
                     Lv=
 E(v = 9, J = 0) =
 Lv= -2.3747D-14
E(v= 10, J= 0)= -527.85
 E(v= 10, J= 0)= -527.850

Lv= -3.4054D-14

E(v= 11, J= 0)= -342.490
                                                                                                                                 0v= -6.9492D-26
Hv= -2.4417D-10
0v= -1.8317D-25
Hv= -4.2372D-10
 E(v=11, Lv=-5.11]
E(v=12, J=0)=-168.266
Lv=-8.5655D-14
-6.299
                                                                                          -DV= -1.3538D-U5
NV= -1.0587D-21
-DV= -1.4741D-05
NV= -2.6332D-21
-DV= -1.6421D-05
NV= -7.7763D-21
-DV= -1.8929D-05
                              -5.1946D-14
0)= -168.266
                                                                                                                                 0v= -5.5532D-25
Hv= -7.3179D-10
0v= -2.0724D-24
Hv= -1.3267D-09
 Ov= -1.0817D-23
Hv= -2.7377D-09
Ov= -1.0754D-22
                                                                                                                               2.5D-05 8.4D-05
                                                                                                                               Hv= -8.1442D-09
Ov= -1.7009D-20
2.8D-03 4.5D-03
 E(v= 17, J= 0)= 475.710 Bv= 0.2568926
Lv= -8.5881D-11 Mv= 9.5157D-14
                                                                                           -Dv= -8.5613D-05
Nv= 6.8551D-16
                                                                                                                                 Hv= -9.0170D-08
Ov= 1.5784D-18
 Find 18 Potential-1 vibrational levels with J=
                    E(v)
                                           v E(v)
                                                                                             E(v)
                                                                                                                                 E(v)
                                             5 -1594.9861
6 -1364.8012
7 -1142.5003
             -2852.0385
-2587.4196
                                                                               10
11
                                                                                         -527.8503
-342.4898
                                                                                                                   15
16
                                                                                                                               274.4971
388.1516
         0
              -2329.1579
                                                                               12
13
                                                                                          -168.2661
-6.2994
                                                                                                                               475.7100
             -2077.4845
-1832.6611
                                                 -928.5388
-723.4475
                                                                                            141.9588
Case 2.e: "Tiemann-type" potential for Ca2(X) [Phys.Rev. A66, 042503(2002)
                     ZMU= 19.98129543200(u) & BZ= 1.185296888D+00((1/cm-1)(1/Ang**2))
  Generate
 from atomic masses: 39.96259086400 & 39.96259086400(u)
Integrate from RMIN= 3.000 to RMAX= 103.00 with mesh RH= 0.000500(Angst)
  Potential #1 for Ca(40)-Ca(40)
  State has OMEGA= 0 and energy asymptote: Y(lim)= 1102.09608(cm-1)
 uLR(r) inverse-power terms inlude NO individual-term damping
 uLR(r) has 2 inverse-power terms: C6 = -1.07400000D+07
C8 = -2.45050000D+08
Tiemann-type potential with De= 1102.0961 Rm= 4.277277
                                                                                                                             is a power series
   in (r - Re)/(r -0.59290*Re) of order 20 with the 21 coefficients: 0.42747000D-03 -0.25408309D+01 0.37961100D+04 0.38207030D+03 -0.27439040D+04 -0.32273633D+04 0.36311381D+03 0.63437054D+04 -0.74015184D+04 -0.19073891D+05 0.54234739D+05 0.44039230D+05 -0.15538794D+06 -0.38662838D+05 0.21383107D+06 0.15592245D+06 -0.15626087D+06 -0.14671112D+06 0.27754300D+05 0.71290802D+05 0.21261455ED+06 -0.15626087D+06 -0.14671112D+06 0.27754300D+05 0.71290802D+05
```

```
Calculate properties of the single potential described above
Potential-1 uses inner boundary condition of zero value at RMIN
Eigenvalue convergence criterion is EPS= 1.0D-08(cm-1)
Airy function at 3-rd turning point is quasibound outer boundary condition
Since state-1 has (projected) electronic angular momentum OMEGA= 0
       eigenvalue calculations use centrifugal potential [J*(J+1) - 0]/r**2
For J= 0, seek the first 100 levels of Potential-1 with VLIM= 1102.096
```

-1.169444D+10/r\*\*10

-0.126115550+04
where for r < Rinn= 3.6600 V= +950.7477 +4.305315D+00/R\*\*12
and for r > Rout= 10.000 V= VLIM -1.074000D+07/r\*\* 6
-2.450500D+08/r\*\* 8

-0.12611555D+04

For J= 0 ETRY=

0.0032 > VMAX=

```
** CAUTION ** For J= 0 E= 1.102096D+03 WF(NEND)/WF(Max)= 5.7D-01 > 1.0D-09 & initialization quality test 1.2D-01 > 1.D-3 so RMAX may be too small
 ALF finds the highest calculated level is E(v=40)=1.1020959D+03
                                                  Bv= 0.0457401
Mv= -4.0622D-23
Bv= 0.0450062
Mv= -5.0319D-23
 E(v = 0, J = 0) =
                                    32.204
                                                                                -Dv = -9.4654D - 08
                                                                                 Nv= -5.6827D-28
-Dv= -9.8341D-08
Nv= -7.5985D-28
                           -3.3246D-18
                                                                                                                  0v = -8.5755D - 33
                  J= 0)= 95.054
Lv= -3.9526D-18
                                                                                                                 Hv= -3.7684D-13
Ov= -1.2498D-32
 E(v= 1, J=
                     = 0)= 155.798
v= -4.7010D-18
0)= 214.445
v= -5.5623D-18
0)= 271
 E(v= 2, J= 0)=
                                                  Bv= 0.0442590
Mv= -6.3142D-23
                                                                                -Dv = -1.0221D-07
                                                                                                                  Hv= -4.2344D-13
                                                                                Nv= -9.9740D-28
-Dv= -1.0630D-07
Nv= -1.3062D-27
                                                                                                                  0v= -1.7691D-32
Hv= -4.7409D-13
0v= -2.4535D-32
                   Lv=
                                                  Bv= 0.0434991
Mv= -7.9639D-23
 E(v=3, J=
                  Lv=
                                                  Bv= 0.0427269

Mv= -1.0030D-22

Bv= 0.0419425

Mv= -1.2566D-22
                           )= 271.006
-6.5442D-18
                                                                                 -Dv= -1.1060D-07
Nv= -1.7194D-27
                                                                                                                  Hv= -5.3001D-13
Ov= -3.3662D-32
 E(v=4, J=
                   Lv=
                                                                                -Dv= -1.1515D-07
Nv= -2.2786D-27
                                                                                                                 Hv= -5.9239D-13
Ov= -4.6134D-32
 E(v= 5, J= 0)= 325.494
Lv= -7.6705D-18
 E(v= 6, J= 0)= 377.924
Lv= -8.9811D-18
                                                  Bv= 0.0411461
Mv= -1.5651D-22
                                                                                -Dv= -1.1994D-07
Nv= -3.0327D-27
                                                                                                                  Hv= -6.6232D-13
Ov= -6.3729D-32
                                                  Bv= 0.0403376
Mv= -1.9417D-22
Bv= 0.0395169
Mv= -2.4081D-22
 E(v= 7, J= 0)= 428.311
Lv= -1.0532D-17
                                                                                -Dv= -1.2499D-07
Nv= -4.0386D-27
                                                                                                                 Hv= -7.4089D-13
Ov= -8.9291D-32
 E(v= 8, J= 0)=
                  J= 0)= 476.674
Lv= -1.2392D-17
                                                                               -Dv= -1.3032D-07
Nv= -5.3626D-27
                                                                                                                 Hv= -8.2923D-13
Ov= -1.2710D-31
  ..... omit 44 lines .....
 Bv= 0.0154215
                                                                                 -Dv= -6.7120D-07
                                                  Mv= -1.6245D-18

Bv= 0.0139305

Mv= -3.7909D-18

Bv= 0.0123769
                                                                                Nv= -3.8921D-22
-Dv= -7.7955D-07
Nv= -1.1253D-21
-Dv= -9.2059D-07
                                                                                                                 Ov= -1.0265D-25
Hv= -7.5399D-11
                                                                                                                 Ov= -3.6457D-25
Hv= -1.1401D-10
 Lv= -2.8196D-14
E(v= 34, J= 0)= 1095.127
                                                  Mv= -9.2413D-18
Bv= 0.0107672
                                                                                Nv= -3.6481D-21
-Dv= -1.1012D-06
                                                                                                                  Ov= -1.6459D-24
Hv= -1.7891D-10
                                                                                -Dv= -1.1012D-06
Nv= -1.5615D-20
-Dv= -1.3486D-06
Nv= -8.1857D-20
-Dv= -1.7140D-06
Nv= -6.2338D-19
-Dv= -2.3165D-06
                          -6.1402D-14
)= 1097.986
                                                  Mv= -2.8932D-17
Bv= 0.0091176
                                                                                                                 0v= -9.1350D-24
Hv= -3.1207D-10
0v= -7.1549D-23
Hv= -6.1272D-10
                   Lv=
 E(v=35, J=0)=
                                                  Bv= 0.0091176

Bv= -1.0323D-16

Bv= 0.0074345

Mv= -5.0339D-16

Bv= 0.0057239
 Lv= -4.7939D-13

E(v= 37, J= 0)= 1097.390

Lv= -4.7939D-13

E(v= 37, J= 0)= 1101.14
                                                                                                                 Nv - -0.1272D-10

Ov = -8.5943D-22

Hv = -1.4545D-09

Ov = -2.0996D-20

Hv = -4.8270D-09
 E(v= 37, J= 0)= 1101.14 By= 0.0057239 -Dv= -2.3165D-06 Hy= -1.4545D-0

Lv= -2.0275D-12 Mv= -3.8107D-15 Nv= -8.4656D-18 Ov= -2.0996D-20

E(v= 38, J= 0)= 1101.79 By= 0.0039883 -Dv= -3.5003D-06 Hy= -4.8270D-0

Lv= -1.4991D-11 Mv= -6.3394D-14 Nv= -3.1918D-16 Ov= -1.8021D-18

E(v= 39, J= 0)= 1102.05 By= 0.0022213 -Dv= -6.8558D-06 Hy= -3.4745D-0

Lv= -4.0813D-10 My= -6.6059D-12 Nv= -1.2744D-13 Ov= -2.7477D-0

** CAUTION ** For J= 0 E= 1.102096D+03 WF(NEND)/WF(Max)= 5.7D-01 > 1.0D-09

& initialization quality test 1.2D-01 > 1.D-3 so RMAX may be too small

** CAUTION ** CDJOEL orthogonality tests 0V01,0V02 & 0V03: 4.4D+01 -2.9D+00 A SCAUTION ** COMPARISON tests for Hy Ly & My give A 8D-01 1 5D+00 2.5D+00
                                                                                                                 0v= -1.8021D-18
Hv= -3.4745D-08
 ** CAUTION ** Comparison tests for Hv, Lv & Mv give: 4.8D-01 1.5D+00 2.5D+00
 E(v= 40, J= 0)= 1102.10
Lv= 1.4042D-07
                                                 Bv= 0.0003267 -Dv= -1.9045D-05 Hv= 3.3129D-07
Mv= -1.1500D-08 Nv= -1.7039D-09 Ov= 1.7270D-10
 Find 41 Potential-1 vibrational levels with J=
                   Ĕ(v)
                                                  E(v)
                                                                                  Ĕ(v)
                   32.2039
95.0542
                                                609.8189
650.2901
                                                                                                              1091.2007
1095.1269
        Ō
                                      11
12
                                                                     22
23
                                                                                953.1705
973.7409
                 155.7982
                                                 688.8432
                                                                     24
25
                                                                                992.6240
                                                                                                              1097.9858
                                                                              1009.8399
1025.4107
1039.3608
                                                 725.5009
760.2858
793.2205
                 214.4453
                                      14
                                                                                                      36
                                                                                                              1099.9340
                                                                     26
27
                                                                                                     37
38
                                                                                                              1101.1416
1101.7856
                 325.4942
377.9236
                                      16
                                                                     28
29
30
                                                                               1051.7191
                 428.3109
476.6741
                                      18
19
                                                 853.6268
881.1410
                                                                               1062,5203
                                                                                                              1102.0959
                                                                               1071.8076
                                                                      31
                 523.0327
                                      20
                                                 906.8899
                                                                               1079.6353
       10
                 567,4071
                                                 930.8932
                                                                              1086.0717
       n= 6 N-D theory extrapolation from v= 39 & 40
                                                                                                 implies
Case 2.f: Barrow-Aziz HFD-B(6,8,10,12) for {20}Ne{84}Xe [JCP 91, 6348 (1989)]
                    ZMU= 16.14564021596(u) & BZ= 9.577645835D-01((1/cm-1)(1/Ang**2))
 from atomic masses: 19.99244017620 & 83.91149772800(u)
Integrate from RMIN= 1.500 to RMAX= 29.00 with mesh RH= 0.001000(Angst)
 Potential #1 for Ne( 20)-Kr( 84)
 State has OMEGA= 0
                                                                               Y(lim)=
                                      and energy asymptote:
                                                                                                      0.00000(cm-1)
 \verb"uLR"(r)" inverse-power terms in lude NO individual-term damping"
                                                                     C6 = 1.89208839D+05
 uLR(r) has
                      4 inverse-power terms:
                                                                     C8 = 1.03241624D+06
C10= 9.93919946D+06
                                                                      C12 =
                                                                               1.69323761D+08
                          and overall damping function:
 \label{eq:decomposition} D(r) = \exp[-1.000000*(3.87258300/r -1.0)** 2.00] Potential is Generalized HFD-ABC with radial power gamma= 0.000000
                                                                               with exponential-term factors:
               51.5750[cm-1]
                                          Re= 3.861000[Ang.],
                                                                                                                                                 beta1= 2.85717137 beta= 0.13240000
                                                                                                                                                                                                                     and A(pre-
 Calculate properties of the single potential described above Potential-1 uses inner boundary condition of \, zero value \, at \, RMIN \,
                                                                   EPS = 1.0D - 08(cm - 1)
 Eigenvalue convergence criterion is
 Airy function at 3-rd turning point is quasibound outer boundary condition
 Since state-1 has (projected) electronic angular momentum OMEGA= 0
               eigenvalue calculations use centrifugal potential [J*(J+1) - 0]/r**2
 For J= 0, seek the first 100 levels of Potential-1 with
                                                                                                             VLIM=
```

-0.0003 find onee turn point: R= 3.46

```
*** CAUTION for v=999 J= 0 SCHRQ doesn't converge by ITER=30 DE=-6.40D-05
 *** SCHRQ FAILS in ALF when searching for v= 5 J= 0 with Check range and/or contact R.J. Le Roy [leroy@uwaterloo.ca]
                                                           act R.J. Le Roy [Leroywuwaterioo.cc
Bv= 0.0662725 -Dv= -2.7537D-06
Mv= -7.9564D-17 Nv= -4.2802D-20
Bv= 0.0578380 -Dv= -4.6900D-06
Mv= -8.0955D-16 Nv= -7.5504D-19
Bv= 0.0475245 -Dv= -8.9746D-06
Mv= -1.1521D-14 Nv= -2.1084D-17
Bv= 0.0348686 -Dv= -1.9514D-05
Mv= -3.5340D-13 Nv= -1.6458D-15
Bv= 0.0198498 -Dv= -5.4842D-05
Mv= -7.8830D-11 Nv= -1.6610D-12
              0, J= 0)= -39.839

Lv= -1.7301D-13

1, J= 0)= -21.463

Lv= -1.0039D-12
              0, J = 0) =
                                                                                                                                        H_{V} = -4.9208D - 10
                                                                                                                                        0v= -2.5532D-23
Hv= -1.5922D-09
0v= -7.7801D-22
 Hv = -6.0767D - 09
                                                                                                                                        Ov= -4.2986D-20
Hv= -3.0794D-08
                                                                                                                                        Ov= -8.6004D-18
                                                           Bv= 0.0198498
Mv= -7.8830D-11
                                                                                                 -Dv= -5.4842D-05
Nv= -1.6610D-12
                                                                                                                                          Hv = -3.4307D - 07
                                                                                                                                        0v = -3.9046D - 14
 Find
              5 Potential-1 vibrational levels with
                                                                                                 Ĕ(v)
                                                                                                                                        E(v)
                                                            E(v)
                     -39.8395
                                                            -9.4449
                                                                                                  -0.4266
          0
                     -21.4627
                                                                                                 3 & 4 implies
  An n= 6 N-D theory extrapolation from v=
                                                                                                                                          vD =
Case 2.g: Generalized Tang-Toennies PEC for Ar2 [Jaeger Mol.Phys. 107, 2181]
                        ZMU= 16.14564021596(u) & BZ= 9.577645835D-01((1/cm-1)(1/Ang**2))
 from atomic masses: 19.99244017620 & 83.91149772800(u)
Integrate from RMIN= 1.500 to RMAX= 29.00 with mesh RH= 0.001000(Angst)
  Potential #1 for Ne( 20)-Kr( 84)
 State has OMEGA= 0 and energy asymptote: Y(lim)=
                                                                                                                           0.00000(cm-1)
  uLR inverse-power terms incorporate TT-type damping with \, rhoAB= 4.0251721100
                defined to give very short-range Dm(r)*Cm/r^m behaviour Dm(r)=[1 - exp(-bTT*r)*SUM\{(bTT*r)^k/k!\}] where bTT=:
                                                                                                            where bTT= rhoAB
  uLR(r) has 6 inverse-power terms:
                                                                                   C6 = 3.07769744D+05
                                                                                              2.27073197D+06
1.70739832D+07
                                                                                   C8 = C10=
                                                                                              1.30837685D+08
1.02178584D+09
                                                                                    C14 =
                                                                                               8.13234755D+09
                                                                                    C16=
  Generalized Tang-Tonnies Potential function with exponent function
 DSCM=
                                                        99.4734
                     Input
                                                                             REQ= 3.762000
                                                                             REQ= 3.761825
                                       DSCM=
                                                        99.4756
                     Actual
  Calculate properties of the single potential described above
  Potential-1 uses inner boundary condition of zero value at RMIN
  Eigenvalue convergence criterion is EPS= 1.0D-08(cm-1)
  Airy function at 3-rd turning point is quasibound outer boundary condition
  Since state-1 has (projected) electronic angular momentum OMEGA= 0
                   eigenvalue calculations use centrifugal potential [J*(J+1) - 0]/r**2
 For J= 0, seek the first 100 levels of Potential-1
                                                                                                                                   VT.TM=
 ** CAUTION ** For J= 0 E=-1.531965D-03 WF(NEND)/WF(Max)= 7.8D-01 > 1.0D-09 & initialization quality test 1.7D+00 > 1.D-3 so RMAX may be too small ALF finds the highest calculated level is E(v=7)=-1.5319646D-03
E(v= 0, J= 0)= -83.056 Bv= 0.0709971 -Dv= -1.5817D-06 Hv= -1.3654D-10 Lv= -2.3775D-14 Mv= -5.4168D-18 Nv= -1.4376D-21 Ov= -4.2174D-25 E(v= 1, J= 0)= -55.113 Bv= 0.0649167 -Dv= -2.2323D-06 Hv= -3.0495D-10 Lv= -8.0158D-14 Mv= -2.7074D-17 Nv= -1.0537D-20 Ov= -4.5027D-24 E(v= 2, J= 0)= -33.559 Bv= 0.0579472 -Dv= -3.3313D-06 Hv= -7.2758D-10 Lv= -2.9172D-13 Mv= -1.4903D-16 Nv= -8.7685D-20 Ov= -5.6762D-23 E(v= 3, J= 0)= -18.081 Bv= 0.0498513 -Dv= -5.3022D-06 Hv= -1.9203D-09 Lv= -1.2440D-12 Mv= -1.0337D-15 Nv= -9.9732D-19 Ov= -1.0659D-21 E(v= 4, J= 0)= -8.097 Bv= 0.0404110 -Dv= -9.0846D-06 Hv= -5.9100D-09 Lv= -6.9579D-12 Mv= -1.0733D-14 Nv= -1.9480D-17 Ov= -3.9467D-20 E(v= 5, J= 0)= -2.654 Bv= 0.0295445 -Dv= -1.7235D-05 Hv= -2.4255D-08 Lv= -6.5523D-11 Mv= -2.3848D-13 Nv= -1.0333D-15 Ov= -5.0240D-18 E(v= 6, J= 0)= -4.42120 Bv= 0.0172872 -Dv= -4.1499D-05 Hv= -2.0780D-07 Lv= -2.1990D-09 Mv= -3.1958D-11 Nv= -5.5340D-13 Ov= -1.0713D-14 ** CAUTION ** For J= 0 E=-1.531965D-03 WF(NEND)/WF(Max)= 7.8D-01 > 1.0D-09 & initialization quality test 1.7D+00 > 1.D-3 so RMAX may be too small ** CAUTION ** CDJOEL orthogonality tests 0V01,0V02 & 0V03: 1.6D+01 -2.3D+00 -1. E(v= 7, J= 0)= -.153196ED-02 Bv= 0.0031793 -Dv= -7.2632D-05 Hv= 7.7691D-07 Lv= 4.6342D-07 Mv= -5.2140D-08 Nv= -1.6843D-09 Ov= 6.1002D-10 Find the standard of the s
                                                              Bv= 0.0709971
 E(v = 0, J = 0) =
                                          -83.056
                                                                                              -Dv= -1.5817D-06
                                                                                                                                       Hv = -1.3654D - 10
                                                                                                                              1.6D+01 -2.3D+00 -1.4D-01
 Find 8 Potential-1 vibrational levels with
                      Ĕ(v)
                                                                                                                                        E(v)
                                                            E(v)
                     -83.0560
                                                                                                  -8.0969
                                                                                                                                        -0.4421
                     -55.1130
                                                          -18.0807
                                                                                                  -2.6540
                                                                                                                                        -0.0015
  An n= 6 N-D theory extrapolation from v= 6 & 7 implies
                                                                                                                                       vD =
```

### Appendix C3: Input/Output files for for Illustrative linelist "production run"

Case 3. This is a data set for an illustrative line-list "production run" for the case of two pointwise potentials (NUMPOT = 2 in Read #1 and NTP > 0 in Read #6) which generates the predicted transition energies and Einstein emission coefficients for some 267555 lines in the  $B(^3\Pi^+_{0u})$  –  $X(^1\Sigma^+_g)$  spectrum of Br<sub>2</sub>. This case again exploits the capability of the NLEV1 < 0 option for locating automatically the first |NLEV1| + 1 levels of a given potential. It also illustrates a use of the NJM > 0 option to find many (or all) rotational sublevels for each v, and of the application of rotational selection rules to calculate transitions between two different electronic states. The input data file is listed in below, followed by parts of the main Channel–6 output and a portion of the associated Channel–8 output file. This calculation of 267555 matrix elements coupling levels of the two electronic states consumed 23.64 s of CPU time on our decade-old SGI UNIX server.

```
35 79 35 79 0
                             % IAN1 IMN1 IAN2 IMN2 CHARGE NUMPOT
'Case 3: Predict emission for B-X Br2 based on Gerstenkorn (1987) constants'
0.0015 1.85 15.0 1.d-4 % RH RMIN RMAX EPS
123 0 0 19742.072d0
                            % NTP LPPOT IOMEG VLIM
10 0 4 5 1.8D+05 % NUSE IR2 ILR NCN CNN
1.D0 1.D0 15902.4802d0 % RFACT EFACT VSHIFT & B-state turn. pnts.
  2.32483352887883 3834.348717 2.32492725139916 3831.646866
  2.32505070817846 3828.090070 2.32520875281731
                                            3823.540508
  2.32540641247184 3817.856430 2.32564885907544 3810.893306
 ..... skip 56 lines listing 112 more turning points ......
 6.87678817820732 \quad 3817.856430 \quad 7.25492791418183 \quad 3823.540508
  7.69918940093639 3828.090070 8.22965127226713
                                           3831.646866
  8.87579778305112 3834.348717
                             % NTP2 LPPOT2 IOMEG2 VLIM2
47 0 0 16056.926D0
10 0 0 6 0.D0
                             % NUSE2 IR22 ILR2 NCN2 CNN2
                             % RFACT EFACT VSHIFT2
1.D0 1.D0 0.d0
  2.05649830399176 4483.356304 2.06283295581950 4189.629584
  2.06951602200031 3893.539190 2.07659093472317
 ..... skip 20 lines listing 36 more turning points ......
 2.60140908192717 3893.539190 2.61738272682198 4189.629584
  2.63310768612594 4483.356304
-40 1 0 -4 999 1 -1 0
                             % NLEV1 AUTO1 LCDC LXPCT NJM JDJR IWR LPRWF
 0 0
                             % IV(1) IJ(1)
1 0
      1.D0
                             % MORDR IRFN RREF
-0.219 0.265
                             % DM(0) DM(1)
15 1 -1 +1 2
                             % NLEV2 AUTO2 J2DL J2DU J2DD
0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 % {IV2(i)}
```

# Standard Channel-6 output for Illustrative linelist "production run"

The largest piece of output for this case consists of a listing of the transition frequencies and Einstein  $\mathcal{A}$ -coefficients for some 267 555 transitions (yielding a line-list of that length) written to Channel–8. A small segment of this output file is presente at the end of this Appendix. Since the associated "standard" output to Channel–6 is also moderately lengthy (some 3221

lines), the listing of it presented below is also considerably truncated. However, this output illustrates some of the (normally not serious) warning messages that may be generated by the program. In particular, for v' = 34, J' = 100 - 103 of the truncated listing below, warnings occur for quasibound levels for which RMAX is smaller than the outermost turning point at which the program was attempting to apply the Airy function boundary condition (see Section II.B). This warning is printed once each iteration as SCHRQ converges on the associated eigenvalue; as it indicates, in this case the Airy function boundary condition is replaced by use of the WKB wave function initialization of Eq. (4). The second type of warning ("... so tunneling calculation uses...") is printed following convergence on the eigenvalue for such a level, as a reminder that the width calculation for this case uses an approximation estimate of the portion of the exponent integral from the end of the range to the actual outermost turning point. However, when this situation arises, the associated tunneling level widths are usually extremely small, and although the resulting predicted width may be slightly in error, the calculated eigenvalue is normally quite accurate.

A different type of problem gives rise to the lines beginning with "CAUTION for ..." "SCHRQ doesn't converge by ...', seen here for v=34, J=127. This is the highest quasibound level for this v; it lies very close to the centrifugal barrier maximum, and after 30 iterations from each of two separate starting points, the Airy function boundary condition was unable to achieve full convergence to EPS for this particular level. In spite of this problem, however, the last eigenvalue change of "DE= 1.75D-03" cm<sup>-1</sup> is considerably smaller than the width (FWHM = 0.90 cm<sup>-1</sup>) of this tunneling predissociation level, so the lack of full convergence has negligible effect on the true accuracy of the resulting eigenvalue.

Another type of warning message is that seen for v = 40 when J = 93 ("... "find onee turn point: ..."). This message appears when the automatic search for ever higher rotational sublevels goes past the top of the (centrifugal) barrier maximum. In this case the code makes additional tries to place a level marginally below the barrier maximum, an effort that sometimes succeeds, but always eventually fails (as it did for this case).

```
Case 3: Predict emission for B-X Br2 based on Gerstenkorn (1987) constants
           ZMU= 39.45916880000(u) & BZ= 2.340730616D+00((1/cm-1)(1/Ang**2))
from atomic masses: 78.91833760000 & 78.91833760000(u)
Integrate from RMIN= 1.850 to RMAX= 15.00 with mesh RH= 0.001500(Angst)
Potential #1 for Br( 79)-Br( 79)
State has OMEGA= 0 and energy asymptote: Y(lim)= 19742.07200(cm-1)
Perform 10-point piecewise polynomial interpolation over 123 input points Beyond read-in points extrapolate to limiting asymptotic behaviour:
to get required internal units [Angstroms & cm-1 for potentials]
      r(i)
                    Y(i)
                                               Y(i)
                                                            r(i)
                                 r(i)
                                                                          Y(i)
                              2.42191370
2.43001839
                                            1696.7527
   2.32483353
                 3834.3487
                                                         3.22507343
                                                                       1821.0440
   2.32492725
                 3831.6469
                                            1568.5519
                                                         3.26089292
                      .... skip 37 lines of this listing
                 1941.3789
1821.0440
                                            1568.5519
1696.7527
                              3.15509529
3.18985642
                                                         8.22965127
8.87579778
   2.40751394
2.41443578
Extrapolate to
                   X .le. 2.3249 with
         14763.263 +3.552602D+09 * exp(-5.797858D+00*X)
 Function for X .GE. 8.230 generated by 4-point inverse-power interpolation
   with leading term 1/r**5 relative to dissociation limit
                                                                    YLIM= 19742.072
   and (dimensionless) leading coefficient fixed as
                                                          C5= 180000.00
 Get matrix elements between levels of Potential-1 (above) & Potential-2 (below)
For Potential #2:
```

```
State has OMEGA= 0
                          and energy asymptote:
                                                        Y(lim) = 16056.92600(cm-1)
Perform 10-point piecewise polynomial interpolation over 47 input points
To make input points Y(i) consistent with Y(lim), add Y(shift)= 0.0000
Scale input points: (distance)* 1.000000000D+00 & (energy)* 1.000000000D+00
               to get required internal units [Angstroms & cm-1 for potentials]
                                                                  r(i)
                      Y(i)
                                     r(i)
                                                     Y(i)
   2.05649830
2.06283296
                   4483.3563
4189.6296
                                  2.18626063
2.19810575
                                                   646.2909
485.5309
                                                                  2.42013527
2.43259119
                                  2.21248391
2.22316187
                                                                 2.44438269 2.45563605
   2.06951602
                   3893.5392
                                                   324.2269
                                                                                  1283.8592
                                                   227.1840
162.3804
97.4903
   2.07659093
                   3595, 1043
                                                                                  1441.8751
  2.08411094
2.09214251
                   3294.3433
2991.2740
                                  2.23177061
2.24253421
                                                                 2.46644318
2.47687343
                                                                                  1599.3372
1756.2436
  2.10077036
2.11010533
                   2685.9133
2378.2776
                                  2.25851483
2.28102606
                                                     32.5137
                                                                 2.49680783
2.51575473
                                                                                  2068.3827
2378.2776
                                  2.30436129
2.32199230
   2.12029713
                   2068.3827
                                                     32.5137
                                                                 2.53392724
                                                                                  2685.9133
                                                   97.4903
162.3804
227.1840
   2.13155647
                   1756.2436
                                                                 2.55147764
                                                                                  2991.2740
  2.13767849
2.14419655
                                  2.33440900
2.34467357
                                                                 2.56851941
2.58514009
                                                                                  3294.3433
3595.1043
                   1599.3372
                   1441.8751
                   1283.8592
                                  2.35784040
                                                                 2.60140908
                                                                                  3893.5392
  2.15871971
2.16694249
                   1125.2912
966.1727
                                  2.37638051
2.39240504
                                                   485.5309
646.2909
                                                                 2.63310769
  2.17602973
                    806.5054
                                  2.40683303
                                                   806.5054
Extrapolate to
                    X .le. 2.0628 with
        -2292.367 +1.200354D+10 * exp(-6.996051D+00*X)
Function for X .GE. 2.6174 generated as
  Y= 16056.9260 - (1.657906D+06) * r** 22.046446 * exp{-(9.991684*r)}
Potential-1 uses inner boundary condition of zero value at RMIN
Eigenvalue convergence criterion is EPS= 1.0D-04(cm-1)
Airy function at 3-rd turning point is quasibound outer boundary condition
Since state-1 has (projected) electronic angular momentum OMEGA= 0
          eigenvalue calculations use centrifugal potential [J*(J+1) - 0]/r**2
For J= 0, seek the first 41 levels of Potential-1
                                                                              VLIM= 19742.072
                                                                   with
   and automatically increment J in steps of 1 to a maximum value of 999
Matrix element arguments are powers of the distance r (in Angstroms)
Coefficients of expansion for radial matrix element/expectation value argument:
                        2.650000D-01
      -2.190000D-01
Potential-2 uses inner boundary condition of zero value at RMIN
Using the rotational selection rule: delta(J) = -1 to 1 with increment 2
  results the rotational selection rule. Getta(3)- 1 to 1 with increment 2 calculate matrix elements for coupling to the 15 vibrational levels of Potential-2: v = 0 1 2 3 4 5 6 7 8 9 10 11 12 13
Since state-2 has (projected) electronic angular momentum OMEGA= 0
          eigenvalue calculations use centrifugal potential [J*(J+1) - 0]/r**2
..... skip 2724 lines summarizing results for v= 1-33 .....
*** For J=100 E= 19743.24 R(3-rd) > RMAX & E < V(N) so try WKB B.C. @ RMAX *** For J=100 E= 19743.22 R(3-rd) > RMAX & E < V(N) so try WKB B.C. @ RMAX
*** For J=100 E= 19743.22 R(3-rd) beyond range so tunneling calculation uses
pure centrifugal potential with J(app)= 99.17 for R > R(max)= 15.00 *** For J=101 E= 19748.69 R(3-rd) > RMAX & E < V(N) so try WKB B.C. @ RMAX
*** For J=101 E= 19748.67 R(3-rd) > RMAX & E < V(N) so try WKB B.C. @ RMAX
*** For J=101 E= 19748.67 R(3-rd) beyond range so tunneling calculation uses
pure centrifugal potential with J(app) = 100.17 for R > R(max) = 15.00 *** For J=102 E= 19754.16 R(3-rd) > RMAX & E < V(N) so try WKB B.C. @ RMAX *** For J=102 E= 19754.15 R(3-rd) > RMAX & E < V(N) so try WKB B.C. @ RMAX
*** For J=102 E= 19754.15 R(3-rd) beyond range so tunneling calculation uses
        pure centrifugal potential with J(app)=101.18 for R > R(max)=15.00
*** For J=103 E= 19759.66 R(3-rd) > RMAX & E < V(N) so try WKB B.C. @ RMAX *** For J=103 E= 19759.65 R(3-rd) > RMAX & E < V(N) so try WKB B.C. @ RMAX
*** For J=103 E= 19759.65 R(3-rd) beyond range so tunneling calculation uses
pure centrifugal potential with J(app)=102.19 for R > R(max)= 15.00 For J=127 ETRY= 19891.7867 > VMAX= 19891.7746 find onee turn point: R= 2.37
              E= 1.99D+04 SCHRQ has cgce prob at IT= 7, so halve DE= -3.22D-03 E= 1.99D+04 SCHRQ has cgce prob at IT= 8, so halve DE= 1.80D-03
** @ J=127
** @ J=127
** @ J=127
               E= 1.99D+04 SCHRQ has cgce prob at
                                                            IT= 10, so halve
                                                                                   DE = -3.51D - 03
               E= 1.99D+04 SCHRQ has cgce prob at E= 1.99D+04 SCHRQ has cgce prob at
** @ J=127
                                                            IT= 12, so halve
                                                                                   DE = -3.40D - 03
** 0 J=127
                                                            IT= 14, so halve
                                                                                   DE= -3.39D-03
** @ J=127
               E= 1.99D+04 SCHRQ has cgce prob at
                                                            IT= 16, so halve
                                                                                   DE= -3.39D-03
               E= 1.99D+04 SCHRQ has cgce prob at
                                                            IT= 18, so halve
** @ J=127
                                                                                   DE= -3.39D-03
               E= 1.99D+04 SCHRQ has cgce prob at
                                                            IT= 20, so halve
IT= 22, so halve
** @ J=127
                                                                                   DE= -3.39D-03
               E= 1.99D+04 SCHRQ has cgce prob at
** @ J=127
                                                                                   DE= -3.39D-03
** @ J=127
               E= 1.99D+04 SCHRQ has cgce prob at
                                                            IT= 24, so halve
                                                            IT= 26, so halve
** @ J=127
               E= 1.99D+04 SCHRQ has cgce prob at
                                                                                   DE= -3.39D-03
** @ J=127
               E= 1.99D+04 SCHRQ has cgce prob at
                                                            IT= 28, so halve
                                                                                   DE= -3.39D-03
              E= 1.99D+04 SCHRQ has cgce prob at IT= 29, so halve for v= 34 J=127 SCHRQ doesn't converge by ITER=30
                                                                                   DE= 1.70D-03
DE= 1.01D-03
** @ J=127
*** CAUTION for
               E= 1.99D+04 SCHRQ has cgce prob at
                                                           IT= 6, so halve
IT= 7, so halve
                                                                                   DE= -3.22D-03
** 0 .I=127
               E= 1.99D+04 SCHRQ has cgce prob at
                                                                                   DE= 1.80D-03
** @ J=127
               E= 1.99D+04 SCHRQ has cgce prob at
** @ J=127
                                                            IT= 9, so halve
                                                                                   DE= -3.51D-03
               E= 1.99D+04 SCHRQ has cgce prob at
                                                           IT= 11, so halve
** @ J=127
                                                                                   DE= -3.40D-03
** @ J=127
               E= 1.99D+04 SCHRQ has cgce prob at
                                                            IT= 13, so halve
```

E= 1.99D+04 SCHRQ has cgce prob at IT= 15, so halve DE= -3.39D-03

```
E= 1.99D+04 SCHRQ has cgce prob at
                                                                                                                                                  DE= -3.39D-03
** @ J=127
                                                                                                        IT= 17, so halve
                           E= 1.99D+04 SCHRQ has cgce prob at
                                                                                                         IT= 19, so halve
** @ J=127
                                                                                                                                                  DE= -3.39D-03
                           E= 1.99D+04 SCHRQ
                                                                                                          IT= 21, so halve
                                                                                                                                                  DE= -3.39D-03
 ** @ J=127
                                                                  has cgce prob at
 ** @ J=127
                           E= 1.99D+04 SCHRQ has cgce prob at
                                                                                                          IT= 23, so halve
                                                                                                                                                  DE= -3.39D-03
          J=127
                           E= 1.99D+04 SCHRQ
                                                                                                          IT= 25, so halve
                                                                                                                                                  DE= -3.39D-03
                                                                  has cgce prob at
                          E= 1.99D+04 SCHRQ has cgce prob at
                                                                                                         IT= 27, so halve
                                                                                                                                                  DE= -3.39D-03
** @ J=127
** @ J=127 E= 1.99D+04 SCHRQ has cgce prob at IT= 28, so halve DE= 1.70D-03
** @ J=127 E= 1.99D+04 SCHRQ has cgce prob at IT= 30, so halve DE= -3.52D-03
*** CAUTION for v= -1 J=127 SCHRQ doesn't converge by ITER=30 DE=-1.76D-03
For vibrational level v = 34
J
E
J
E
                                                                       of Potential-1
J E
                                                                                 19529.969
19533.224
19536.537
                                            19466.021
19467.723
19469.486
                                                                                                                     19632.179
19636.793
                                                                                                                                                        19765.173
19770.719
           19443.803
19443.867
                                                                         53
                                                                                                                                              105
                                                                                                                      19641.452
                                              19471.312
19473.198
                                                                         55
56
57
                                                                                  19539.905
19543.330
                                                                                                                                                         19781.868
19787.469
                                                                                                                      19646, 158
                                              19475.147
19477.157
19479.228
19481.360
            19444.756
                                      31
                                                                                  19546.811
                                                                                                            83
                                                                                                                     19655.702
                                                                                                                                              109
                                                                                                                                                         19793.083
            19445.138
                                                                                  19550.347
                                                                                                                      19660.539
                                                                                                                                                         19798.709
                                                                                                                                              110
           19445.582
19446.090
                                                                                  19553.939
19557.585
                                                                                                            85
86
                                                                                                                     19665.420
19670.343
                                                                                                                                             111
112
                                                                                                                                                         19804.345
19809.988
            19446.662
19447.297
                                               19483.553
19485.806
                                                                                  19561.286
19565.042
                                                                                                                      19675.307
19680.311
                                                                                                                                                         19815.634
19821.282
                                                                                 19568.851
19572.714
19576.629
19580.598
           19447.995
19448.756
                                              19488.120
19490.495
                                                                         63
64
                                                                                                            89
                                                                                                                     19685.356
19690.440
                                                                                                                                              115
                                                                                                                                                         19826.927
                                                                                                                                              116
                                                                                                                                                         19832.565
            19449.581
19450.468
                                              19492.930
19495.425
                                                                                                                     19695.561
19700.721
                                                                                                                                                         19838.191
19843.802
                                                                                                            91
92
93
94
95
96
97
                                                                                                                     19700.721
19705.916
19711.148
19716.413
19721.713
19727.044
19732.407
19737.800
19743.222
19748.672
           19451.419
19452.433
19453.510
19454.650
                                              19497.979
19500.594
19503.267
19506.000
                                                                                 19584.619
19588.692
19592.816
19596.992
                                                                         67
68
                                                                                                                                              119
                                                                                                                                                         19849.390
                                                                                                                                              120
121
                                                                                                                                                         19854.948
                                                                         69
70
71
72
73
74
75
76
77
                                                                                                                                                         19860.467
                                                                                                                                                         19865.936
           19455.852
19457.117
                                              19508.792
19511.643
                                                                                  19601.218
19605.494
                                                                                                                                              123
124
                                                                                                                                                         19871 337
                                                                                                            98
                                                                                                                                                         19876.643
           19458.445
19459.836
                                              19514.552
19517.520
                                                                                  19609.820
                                                                                                          99
100
                                                                                                                                                         19881.820
                                                                                  19614, 196
                                                                                                                                                         19886.844
           19461.289
19462.804
                                     49
50
                                              19520.546
19523.629
                                                                                 19618.620
19623.092
                                                                                                          101
102
           19464.381
                                     51
                                              19526.770
                                                                                  19627.612
                                                                                                          103
                                                                                                                     19759.649
                                              ...... skip 230 lines summarizing results for v= 35-39 .....
*** For J= 74 E= 19742.97 R(3-rd) > RMAX & E < V(N) so try WKB B.C. @ RMAX *** For J= 74 E= 19742.96 R(3-rd) > RMAX & E < V(N) so try WKB B.C. @ RMAX *** For J= 74 E= 19742.96 R(3-rd) beyond range so tunneling calculation uses
*** For J= 74 E= 19742.96 R(3-rd) beyond range so tunneling calculation uses pure centrifugal potential with J(app)= 72.87 for R > R(max)= 15.00

*** For J= 75 E= 19746.03 R(3-rd) > RMAX & E < V(N) so try WKB B.C. @ RMAX

*** For J= 75 E= 19746.02 R(3-rd) > RMAX & E < V(N) so try WKB B.C. @ RMAX

*** For J= 75 E= 19746.02 R(3-rd) beyond range so tunneling calculation uses pure centrifugal potential with J(app)= 73.89 for R > R(max)= 15.00

*** For J= 76 E= 19749.10 R(3-rd) > RMAX & E < V(N) so try WKB B.C. @ RMAX

*** For J= 76 E= 19749.09 R(3-rd) > RMAX & E < V(N) so try WKB B.C. @ RMAX
*** For J= 76 E= 19749.09 R(3-rd) > RMAX & E \ V(N) SO LIY WED D.O. S INTER-
*** For J= 76 E= 19749.09 R(3-rd) beyond range so tunneling calculation uses
pure centrifugal potential with J(app)= 74.90 for R > R(max)= 15.00

*** For J= 77 E= 19752.19 R(3-rd) > RMAX & E < V(N) so try WKB B.C. @ RMAX

*** For J= 77 E= 19752.18 R(3-rd) > RMAX & E < V(N) so try WKB B.C. @ RMAX

*** For J= 77 E= 19752.18 R(3-rd) > RMAX & E < V(N) SO TRY WKB B.C. @ RMAX

*** For J= 77 E= 19752.18 R(3-rd) > RMAX & E < V(N) SO TRY WKB B.C. @ RMAX
pure centrifugal potential with J(app)= 75.92 for R > R(max)= 15.00

For J= 93 ETRY= 19800.6818 > VMAX= 19800.4705 find onee turn point: R= 2.35

For J= 93 ETRY= 19800.6892 > VMAX= 19800.4705 find onee turn point: R= 2.35

For J= 93 ETRY= 19800.6892 > VMAX= 19800.4705 find onee turn point: R= 2.35

For J= 93 ETRY= 19800.6892 > VMAX= 19800.4705 find onee turn point: R= 2.35
For vibrational level v = 40
J
E
                                                                      of Potential-1
                                     19 19626.163
20 19627.136
21 19628.157
22 19629.225
                                                                                 19652.625
19654.470
19656.358
19658.289
                                                                                                                     19694.708
19697.304
19699.935
                                                                                                                                                        19749.092
           19616.922
19617.020
19617.168
19617.364
                                                                                                                                                         19752.181
19755.283
                                                                         39
                                                                                                            58
59
60
61
62
63
64
65
66
67
                                                                         40
41
42
                                                                                                                     19702,600
                                                                                                                                                         19758.395
                                               19630.341
                                                                                  19660.263
                                                                                                                      19705.297
                                                                                                                                                         19761.516
           19617.609
19617.904
                                              19631.503
19632.713
                                                                                  19662.279
19664.337
                                                                                                                     19708.027
19710.788
                                                                                                                                                         19764.642
19767.771
            19618.247
19618.639
                                              19633.970
19635.273
                                                                                  19666.437
19668.577
                                                                                                                     19713.579
19716.401
19719.250
                                                                                                                                                         19770.899
19774.022
            19619.081
19619.571
                                                                                  19670.759
19672.980
                                               19636.623
                                                                                                                                                         19777.138
                                               19638.019
                                                                                                                                                         19780.239
                                                                                                            68
69
70
71
72
73
           19620.109
19620.697
                                              19639.461
19640.949
                                                                                  19675.242
19677.543
                                                                                                                     19725.033
19727.963
                                                                                                                                                        19783.320
19786.373
           19621.333
19622.017
19622.750
19623.531
                                                                                 19677.343
19679.882
19682.260
19684.676
19687.130
                                                                                                                     19730.918
19733.896
19736.896
19739.918
                                                                         51
52
53
54
                                                                                                                                                        19789.385
19792.337
19795.203
                                               19642.482
                                              19644.061
19645.685
19647.353
                                                                                                                                                      19797.968
           19624.360
19625.238
                                           19649.066
19650.824
                                                                        55 19689.620
56 19692.146
                                                                                                            74 19742.958
75 19746.017
                                                                                                                                       ·++++++++++++++
Find 41 Potential-1 vibrational levels with J= v E(v) v E(v) v E(v)
         0
                15985.8099
                                                       17599.2328
                                                                                               18743.5515
                                                                                                                                       19404.8742
                                                      17599.2328
17723.5255
17843.8623
17960.1998
18072.4992
18180.7266
18284.8542
                                                                                      23
24
25
26
                                                                                                                              34
35
36
37
                                                                                               18822.9413
18898.2750
                16150.1163
                                                                                                                                       19443.8033
                16311.0672
                                                                                                                                       19479.6566
19512.5503
                                                                                             18969.6004
19036.9760
                16468.6043
                16622.6712
                                                                                                                                       19542.6009
                                              15
                                                                                             19100.4706
19160.1627
```

```
7 17063.4841 18 18384.8610 29 19216.1394 40 19616.8729
8 17203.1035 19 18480.7338 30 19268.4954
9 17338.9707 20 18572.4682 31 19317.3318
10 17471.0312 21 18660.0691 32 19362.7547
```

An n= 5 N-D theory extrapolation from v= 39 & 40 implies vD = 59.899

# Standard Channel-8 output for Illustrative linelist "production run"

Case 3: Predict emission for B-X Br2 based on Gerstenkorn (1987) constants

Note that (v',J') & (v",J") strictly label the upper and lower levels, resp., and E(lower)=E"

but E(2)-E(1) is: (energy of State-2 level) - (energy of State-1 level)

| dJ  | (J") | Ban<br>v' | d<br>v" | E(lower) | E(2)-E(1)   | A(Einstein) | F-C Factor  | <v'j' m v"j"></v'j' m v"j"> |
|-----|------|-----------|---------|----------|-------------|-------------|-------------|-----------------------------|
| P(  | 1)   | 0 -       | 0       | 162.54   | -15823.27   | 7.51655D-05 | 3.26301D-10 | 7.77793D-06                 |
| P(  | 1)   | 0 -       | 1       | 485.69   | -15500.12   | 1.98479D-03 | 9.03473D-09 | 4.12243D-05                 |
| P(  | 1)   | 0 -       | 2       | 806.67   | -15179.14   | 2.56291D-02 | 1.22429D-07 | 1.52860D-04                 |
| P(  | 1)   | 0 -       | 3       | 1125.45  | -14860.36   | 2.15688D-01 | 1.08216D-06 | 4.57792D-04                 |
| P(  | 1)   | 0 -       | 4       | 1442.03  | -14543.78   | 1.33030D+00 | 7.01609D-06 | 1.17424D-03                 |
| P(  | 1)   | 0 -       | 5       | 1756.40  | -14229.41   | 6.41089D+00 | 3.55737D-05 | 2.66365D-03                 |
| P(  | 1)   | 0 -       | 6       | 2068.54  | -13917.27   | 2.51332D+01 | 1.46864D-04 | 5.45245D-03                 |
| P(  | 1)   | 0 -       | 7       | 2378.43  | -13607.38   | 8.24026D+01 | 5.07537D-04 | 1.02119D-02                 |
| P(  | 1)   | 0 -       | 8       | 2686.06  | -13299.75   | 2.30523D+02 | 1.49801D-03 | 1.76763D-02                 |
| P(  | 1)   | 0 -       | 9       | 2991.42  | -12994.39   | 5.58669D+02 | 3.83406D-03 | 2.84933D-02                 |
| P(  | 1)   | 0 -       | 10      | 3294.49  | -12691.32   | 1.18684D+03 | 8.61075D-03 | 4.30264D-02                 |
| P(  | 1)   | 0 -       | 11      | 3595.25  | -12390.56   | 2.23108D+03 | 1.71302D-02 | 6.11533D-02                 |
| P(  | 1)   | 0 -       | 12      | 3893.69  | -12092.12   | 3.73965D+03 | 3.04191D-02 | 8.21222D-02                 |
| P(  | 1)   | 0 -       | 13      | 4189.78  | -11796.03   | 5.62413D+03 | 4.85201D-02 | 1.04526D-01                 |
|     |      |           |         |          |             |             |             |                             |
|     |      |           |         | omit     | 267521 line | es          |             |                             |
| • • |      |           | • • • • |          |             |             |             |                             |
|     | 91)  | 40 -      | 5       | 2427.17  | -17370.80   | 4.55940D+01 | 3.22713D-04 |                             |
|     | 93)  | 40 -      | 5       | 2456.75  | -17341.21   | 4.45961D+01 | 3.13842D-04 | -7.36500D-03                |
|     | 91)  | 40 -      | 6       | 2736.53  | -17061.44   | 1.63941D+01 | 1.20264D-04 | 4.60057D-03                 |
|     | 93)  | 40 -      | 6       | 2765.99  | -17031.98   | 1.74563D+01 | 1.27340D-04 | 4.73392D-03                 |
|     | 91)  | 40 -      | 7       | 3043.63  | -16754.34   | 8.11570D+01 | 6.22525D-04 | 1.05187D-02                 |
| -   | 93)  | 40 -      | 7       | 3072.96  | -16725.00   | 8.14359D+01 | 6.21159D-04 | 1.05076D-02                 |
|     | 91)  | 40 -      | 8       | 3348.45  | -16449.52   | 6.05804D+00 | 4.87388D-05 | 2.95411D-03                 |
|     | 93)  | 40 -      | 8       | 3377.66  | -16420.31   | 5.45704D+00 | 4.36756D-05 | 2.79608D-03                 |
|     | 91)  | 40 -      | 9       | 3650.98  | -16146.99   | 4.46439D+01 | 3.71936D-04 | -8.24583D-03                |
|     | 93)  | 40 -      | 9       | 3680.06  | -16117.91   | 4.60071D+01 | 3.81203D-04 | -8.34820D-03                |
|     | 91)  |           | 10      | 3951.19  | -15846.78   | 4.35551D+01 | 3.79843D-04 | -8.37720D-03                |
|     | 93)  | 40 -      |         | 3980.15  | -15817.82   | 4.27258D+01 | 3.70610D-04 | -8.27501D-03                |
|     | 91)  | 40 -      |         | 4249.08  | -15548.89   | 4.25958D+00 | 3.84497D-05 | 2.69541D-03                 |
|     | 93)  | 40 -      |         | 4277.91  | -15520.06   | 4.87948D+00 | 4.38321D-05 | 2.87733D-03                 |
|     | 91)  | 40 -      |         | 4544.62  | -15253.35   | 5.56357D+01 | 5.28869D-04 | 1.00258D-02                 |
|     | 93)  | 40 -      |         | 4573.32  | -15224.64   | 5.60365D+01 | 5.29892D-04 | 1.00359D-02                 |
|     | 91)  | 40 -      |         | 4837.80  | -14960.17   | 6.82655D+00 | 6.82839D-05 | 3.61565D-03                 |
|     | 93)  | 40 -      |         | 4866.37  | -14931.60   | 6.15591D+00 | 6.12800D-05 | 3.42476D-03                 |
|     | 91)  | 40 -      |         | 5128.60  | -14669.37   | 2.97279D+01 | 3.08674D-04 | -7.77062D-03                |
| P(  | 93)  | 40 -      | 14      | 5157.04  | -14640.93   | 3.09159D+01 | 3.19393D-04 | -7.90463D-03                |

#### Appendix D: Program Structure

The present section lists the names and outlines the functions of the various subroutines used by **LEVEL**, and indicates their hierarchy. In particular, the level of indentation in this list indicates which subroutines call which others; unless stated otherwise, each subroutine is called exclusively by the immediately preceding routine having one lower level of indentation.

- **LEVEL:** The main program which reads input data and instructions, and calls the potential preparation, eigenfunction determination, and overlap integral routines.
  - MASSES: A data subroutine containing accurate atomic masses and other properties of all stable atomic isotopes. For normal cases, its presence obviates the need for a user to look up and type precise particle masses into the input data file. It is loo called by POTGEN to define mass-scaling of BOB functions.
  - **ALF:** For any smooth single-minimum, shelf-state or double-minimum potential, ALF (Automatic Level Finder) uses multiple calls to subroutine SCHRQ (see below) to determine the vibrational energies of all levels from v=0 up to some maximum v specified by its input parameter KVMAX. If fewer than the specified number of levels are found, warnings are printed.
    - **SCECOR:** uses first-order semiclassical estimates of (v + 1/2) and dG(v)/dv (see Eqs. (10) and (11), and sometimes more brute force methods, to generate a trial eigenvalue for the 'next' level of interest.
  - **SCHRQ:** Solves the Schrödinger equation to determine the eigenvalue and (unit normalized) eigenfunction of the vibrational level lying closest to the input trial energy.
    - **QBOUND:** For quasibound levels (those lying above the potential asymptote, but behind a potential barrier), applies the Airy function boundary condition at the third turning point to initiate the inward inward integration of the wave function for such levels [8, 9].
    - **WIDTH:** Calculates the tunneling predissociation lifetime or width of a quasibound level [9–11].
      - **LEVQAD:** Called by WIDTH to evaluate the near-turning-point contributions to the semiclassical quadratures over the potential well and the barrier to tunneling which are required for calculating the predissociation rate.
  - **CDJOEL:** Calculates the diatomic molecule centrifugal distortion constants of Eq. (8). The required input is the effective (centrifugally-distorted, if appropriate) radial potential, and the eigenvalue and eigenfunction of the level in question (as calculated by SCHRQ).
  - **LEVXPC:** Calculates the desired diagonal expectation values of powers of the specified distance coordinate or (interpolated) radial function RFN(r) (see READ #26 in Appendix B).
  - **MATXEL:** Calculates the desired off-diagonal matrix elements of powers of the specified radial function or distance coordinate, and the radiative lifetime or Einstein emission coefficient  $\mathcal{A}$  [s<sup>-1</sup>].
  - **PREPOT:** The subroutine that oversees reading of the parameters defining the potential and generating the required potential array at the N distances specified by the input distance array.

- GENINT: Uses piecewise polynomial or cubic spline functions to interpolate over a set of read-in turning points to yield the potential function array at the equally-spaced radial mesh required by SCHRQ. If necessary, it extrapolates beyond the range of the given points with analytic functions (see options for parameter ILR of READ #7).
  - **PLYINTRP:** Performs piecewise polynomial interpolation on a given array of point, and returns the function value and (if desired) its derivatives at a specified point. It is used by GENINT to interpolate for the potential for cases with  $\mathtt{NUSE} > 0$ . This routine is also used by SPLINT to define the first derivatives at the inner and outer ends of the interpolation region,  $R = \mathtt{XI}(1)$  and  $\mathtt{XI}(\mathtt{NTP})$ , respectively.
  - **SPLINT:** Calls subroutine SPLINE to generate the  $4 \times (NTP 1)$  coefficients required to define the cubic spline through the NTP given turning points, and then uses these coefficients to generate the desired interpolated function values at the specified integration mesh points.
    - **SPLINE:** Generates the coefficients defining the cubic spline function through the given NTP turning points.
- **POTGEN:** For the various analytic potential function specified by input parameter IPOTL (see Read #10), reads in the parameters defining those functions and generates the desired array of potential function values on the specified radial grid. If BOB correction functions are to be included, also reads in the parameters defining them and incorporates them into the effective adiabatic potential used by SCHRQ.
  - **DAMPF:** Generates the damping functions of Eqs. (25) and (26) utilized in defining the tails of the MLR, DELR and HPP potential energy functions.
  - **AFdiag:** Performs the  $2 \times 2$  or  $3 \times 3$  diagonalization used to define the long-range tail of a potential energy function the case or interstate coupling near the nS+nP asymptote of a homonuclear alkali dimer [33, 49–51].
  - **LKoef:** Asen Pashov's subroutine to generate the array of Nbeta × Nbeta coefficients that define his spline 'basis functions' [45].
  - **Scalc:** A function subroutine to generate the  $S_m(x)$  'basis functions' used by Pashov to generate values of a spline function.

ludcmp: A subroutine used by LKoef.