

8.333 : STATISTICAL MECHANICS 1

Midterm # 3: Nov 22, 2021

Name: Riean A. Bri

(1)

(7)

Attractive shell potential

$$(2) \quad V(r) = \begin{cases} +\infty & 0 < r < a \\ -\varepsilon & a < r < b \\ 0 & b < r < \infty \end{cases}$$

$$B_2 = -\frac{1}{2} \int d^3 r_{12} \left[ \exp(-\beta V(r_{12})) - 1 \right]$$

$$= -\frac{1}{2} 4\pi \int_0^\infty dr r^2 \left( \exp(-\beta V(r)) - 1 \right)$$

$$= -\frac{1}{2} (4\pi) \int_0^a dr r^2 [-1]$$

$$- \frac{1}{2} (4\pi) \int_a^b dr r^2 \left[ \exp(+\beta \varepsilon) - 1 \right]$$

$$- \frac{1}{2} (4\pi) \int_b^\infty dr r^2 [1 - 1]$$

$$= \frac{2a^3\pi}{3} + \frac{2}{3} (a^3 - b^3) (-1 + e^{\beta \varepsilon}) \pi$$

$$= \boxed{\frac{2\pi}{3} \left[ b^3 + (a^3 - b^3) e^{\beta \varepsilon} \right]}$$

$$\textcircled{b} \quad B_2(T) = \frac{2\pi}{3} (b^3 + (a^3 - b^3)e^{\beta\epsilon})$$

• In the high-temp limit,  $\beta \rightarrow 0$ , so

$$\lim_{T \rightarrow \infty} B_2(T) = \frac{2\pi}{3} (b^3 + (a^3 - b^3)(1 + \beta\epsilon))$$

$$= \left[ \frac{2\pi}{3} a^3 + \frac{2\pi}{3} (a^3 - b^3) \beta\epsilon \right]$$

~~At  $R \rightarrow 0$ ,  $C \rightarrow 0$ , so we get~~

attractive components

• At low temperatures, ~~hard core~~ ~~part~~ takes over...

$$B_2(T) \sim \left[ \frac{2\pi}{3} (a^3 - b^3) e^{\beta\epsilon} \right]$$

$$a < b \Rightarrow B_2(T) < 0$$

• @ high temps, the hard core part of the potential is dominant

$$\left[ B_2(T \rightarrow \infty) \sim \frac{2\pi}{3} b^3 \right]$$

③ High  $T$  limit again...

③

$$(P + a^2)(V - Nb) = Nk_B T$$

Recall that

$$\frac{PV}{Nk_B T} = 1 + \frac{N}{V} B_2(T)$$

$$\Rightarrow \frac{PV}{Nk_B T} = 1 + \frac{N}{V} \left[ \frac{2\pi}{3} (a^3 + (d^3 - b^3) \beta \epsilon) \right]$$

→  ~~$Nk_B T$~~

$$P = Nk_B T \left[ \frac{1}{V} + \frac{N}{V^2} \left( \frac{2\pi}{3} (a^3 + (a^3 - b^3) \beta \epsilon) \right) \right]$$

$$P + \cancel{Nk_B T} \cdot \frac{N}{V^2} \frac{2\pi}{3} (b^3 - a^3) \beta \epsilon = k_B T \frac{N}{V} \left( 1 + \frac{N}{V} \frac{2\pi}{3} a^3 \right)$$

$$P + \frac{N^2}{V^2} \epsilon \frac{2\pi}{3} (b^3 - a^3) = k_B T \frac{N}{V} \left( 1 + \frac{N}{V} \frac{2\pi}{3} a^3 \right)$$

$$\text{Now ... } 1 + \frac{N}{V} \frac{2\pi}{3} a^3 = 1 + \frac{1}{2} n \left( \frac{4\pi}{3} a^3 \right)$$

$$\approx V \left( V - \frac{N}{2} \frac{4\pi}{3} a^3 \right)^{-1}$$

So

$$\left( P + \frac{n^2 \epsilon}{2} \frac{4\pi}{3} (b^3 - a^3) \right) \left( V - \frac{N}{2} \frac{4\pi}{3} a^3 \right) = Nk_B T$$

→

Van der Waals params

(4)

$$\left\{ \begin{array}{l} a = \frac{\epsilon}{2} \frac{4\pi}{3} (L^3 - a^3) = \frac{2\pi\epsilon}{3} (L^3 - a^3) \\ b = \frac{2\pi}{3} a^3 \end{array} \right.$$

(5)

(2) Interesting point particles

$$Z(T, N, V) = Z_{\text{ideal}}(T, N, V) \exp(\beta N u(V))$$

$$\textcircled{a} \quad Z_{\text{ideal}}(T, N, V) \approx \frac{V^N}{N! \lambda^{3N}} \approx V^N T^{\frac{3N}{2}}$$

where  $V$  is the volume

$$\lambda = \frac{h}{\sqrt{2\pi m k_B T}} \rightarrow \text{thermal wavelength} \sim T^{-1/2}$$

$$\underline{s_0}, \quad \begin{cases} X = N \\ Y = +3N/2 \end{cases}$$

\textcircled{b} Energy is given by

$$E = \langle H \rangle = - \frac{\partial \ln Z}{\partial \beta} \quad \ln\left(\frac{1}{k_B \beta}\right)$$

$$= - \frac{\partial}{\partial \beta} \left[ N \ln V + \left(\frac{3N}{2}\right) \ln T + \beta N u(V) \right]$$

$$= \left[ -N u(V) + \frac{3N}{2\beta} \right]$$

(i)

(c) Heat capacity @ constant volume ...

$$C_V = \left. \frac{\partial E}{\partial T} \right|_V = \frac{\partial \langle \mathcal{H} \rangle}{\partial T} = \frac{\partial}{\partial T} \left[ -N u(\gamma) + \frac{3N}{2} k_B T \right]$$

$$\boxed{dV = 0} = + \boxed{\frac{3N}{2} k_B}$$

(d) To find pressure, need to go to free energy ...

$$F = -k_B T \ln Z = \dots \text{ (mathematician)}$$

$$\boxed{P} = \left. \frac{\partial F}{\partial V} \right|_{T, N} =$$

$$= \left. \frac{\partial}{\partial V} \left[ -k_B T \ln Z \right] \right|_{T, N}$$

$$= k_B T \left. \frac{\partial}{\partial V} \ln Z \right|_{T, N} \quad \gamma = \frac{V}{N}$$

$$= \frac{k_B T}{V} \left( N + V \beta u' \left( \frac{V}{N} \right) \right)$$

$$= \frac{k_B T N}{V} + u' \left( \frac{V}{N} \right)$$

$$n = \frac{N}{V}$$

$$= \boxed{k_B T n + u' \left( \frac{1}{n} \right)}$$

(e) Isothermal compressibility

(7)

$$\kappa_T = -\frac{1}{V} \left. \frac{\partial V}{\partial P} \right|_T$$

$$= -\frac{1}{V} \left( \frac{\partial P}{\partial V} \right)^{-1} \Big|_T$$

$$= -\frac{n}{N} \frac{N \partial(1/n)}{\partial P}$$

$$= +n n^{-2} \left( \frac{\partial P}{\partial n} \right)^{-1} \Big|_T$$

$$= \left[ \frac{1}{n} \left[ \frac{k_B T}{n} - \frac{1}{n^2} u'(1/n) \right] \right]$$

$$\left[ \frac{k_B T}{n} - \frac{1}{n^2} u'(1/n) \right]$$

$$\kappa_T = \frac{n}{k_B T n^2 - u'(1/n)}$$



(f) Necessary condition for  $u(v)$  for stability of particles? (8)

To get ~~static~~ mechanically stable system of particles, we ~~must~~ <sup>must</sup> have that

$$K_T > 0 \Rightarrow n^2 k_B T - \cancel{\text{something}} u'(1/n) > 0$$

~~$$K_T = n^2 k_B T - \frac{1}{n^2} \frac{d}{dn} (n^2 u'(1/n))$$~~

$$\Rightarrow \boxed{n^2 k_B T > u'(1/n)}$$

$$v = 1/n$$

or  $\boxed{u'(v) < \frac{k_B T}{v^2}}$