

Goldstein Ch 10 #12

$$V(r) = \begin{cases} -V_0 & 0 < r < r_0 \\ 0 & r > r_0 \end{cases} \quad V_0 > 0$$

(a) use polar coords in plane (r, θ) & (p_r, p_θ)
want oscillation or rotation

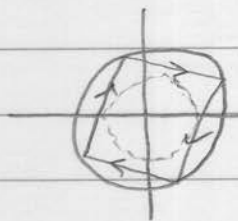
$$H = \frac{p_r^2}{2m} + \frac{p_\theta^2}{2mr^2} + V(r) = E \quad (\text{conservative } H=T+V)$$

Case $E < 0$ since $T > 0$ need $V < 0$ so $0 < r < r_0$ to start

since E conserved always have $0 \leq r(t) \leq r_0$

θ cyclic so $p_\theta = d_\theta = \text{constant}$

Could be (i) rotation in (θ, p_θ)



θ increases

$p_\theta = \text{const} = \text{periodic}$

here $r_1 < r < r_0$

constrained away from zero

$$E = \frac{p_r^2}{2m} + \frac{d_\theta^2}{2mr^2} - V_0, \quad p_r = \pm \sqrt{2m(V_0 + E) - \frac{d_\theta^2}{r^2}}$$

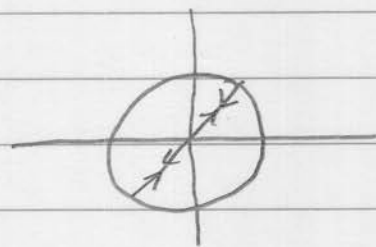
p_r also periodic

(r, p_r) is oscillation

(ii) special case, (θ, p_θ) is oscillation

θ periodic (either 0 or $\pi + \theta_0$)

$d_\theta = p_\theta = 0$ so periodic



So for $-V_0 \leq E < 0$ can always define action angle variables
initial conditions here: $0 < r(t=0) \leq r_0$

$$-V_0 \leq \frac{p_r^2}{2m} + \frac{d_\theta^2}{2mr^2} - V_0 < 0 \rightarrow 0 < p_r^2 < 2mV_0 - \frac{d_\theta^2}{r^2}$$

$$0 < p_r^2 < 2mV_0 - \frac{d_\theta^2}{r_0^2}$$

$p_r^2 > 0$ so $d_\theta^2 < 2mr_0^2 V_0$ required for negative E

Case $E \geq 0$ r is unbounded. Only possibility for action-angle vars is r increasing, p_r periodic
 If $\theta = \text{constant}$, $p_\theta = d\theta = 0$, then $p_r = \text{constant}$
 hence periodic

Here (θ, p_θ) is dot in phase space (call it oscillation with 0 amplitude)
 (r, p_r) is rotation

(Any other motion for $E \geq 0$ is unsuitable to action-angle vars)

Initial conditions here:

$$t=0 \quad p_r^2 = \begin{cases} (E+V_0) 2m & r < r_0 \\ E (2m) & r > r_0 \end{cases} \quad p_\theta = 0$$

$$\text{then } p_\theta = 0 \Rightarrow p_\theta(t) = 0$$

p_r either constant if $t=0$ has $r > r_0$, or increases by one jump if $r < r_0$.

(b) $E < 0$, $r_1 < r < r_0$ case

$$J_\theta = \oint p_\theta d\theta = 2\pi \alpha_0$$

$$J_r = \oint p_r dr = \pm \oint dr (2m(V_0+E) - \frac{\alpha_0^2}{r^2})^{1/2}$$

$$= \pm (2m(V_0+E))^{1/2} \oint dr \frac{1}{r} (r^2 - r_1^2)^{1/2}$$

$$\text{since } p_r = 0 \text{ at } r = r_1, \quad r_1^2 = \frac{\alpha_0^2}{2m(V_0+E)}$$

one period is $r_0 \rightarrow r_1 \rightarrow r_0$ doubles $r_1 \rightarrow r_0$
 $p_r < 0$ $p_r > 0$ result

$$J_r = 2 (2m(V_0+E))^{1/2} \int_{r_1}^{r_0} \frac{1}{r} (r^2 - r_1^2)^{1/2} dr$$

$$= 2 (2m(V_0+E))^{1/2} \left[\left(r_0^2 - \frac{\alpha_0^2}{2m(V_0+E)} \right)^{1/2} - \frac{\alpha_0}{\sqrt{2m(V_0+E)}} \cos^{-1} \left(\frac{\alpha_0}{r_0 \sqrt{2m(V_0+E)}} \right) \right]$$

to get the frequency use $\frac{1}{\nu_r} = \frac{\partial J_r}{\partial E}$

Goldstein

Ch 12 #7

$$\Delta H = b p_x^2 p_y^2$$

$$H_0 = \frac{p_x^2}{2m} + \frac{p_y^2}{2m} + \frac{1}{2} m \omega^2 (x^2 + y^2)$$

$$\text{one } J = \frac{\omega}{2\pi}$$

$$x = \sqrt{\frac{J_x}{\pi m \omega}} \sin(2\pi(\omega t + \beta_x)) \quad , \quad y = \sqrt{\frac{J_y}{\pi m \omega}} \sin(2\pi(\omega t + \beta_y))$$

$$p_x = \sqrt{\frac{m J_x \omega}{\pi}} \cos(2\pi(\omega t + \beta_x)) \quad p_y = \sqrt{\frac{m J_y \omega}{\pi}} \cos(2\pi(\omega t + \beta_y))$$

new vars $\{J_x, \beta_x\}, \{J_y, \beta_y\}$

$$H_0 = \frac{\omega}{2\pi} (J_x + J_y)$$

$$\dot{\beta}_x^{(1)} = \left. \frac{\partial \Delta H}{\partial J_x} \right|_0 = \frac{2}{2J_x} b \left(\frac{m J_x \omega}{\pi} \right) \left(\frac{m J_y \omega}{\pi} \right) \cos^2(2\pi(\omega t + \beta_x)) \cos^2(2\pi(\omega t + \beta_y))$$

$$= b \frac{m^2 \omega^2}{\pi^2} J_y^{(0)} \cos^2(2\pi(\omega t + \beta_x^{(0)})) \cos^2(2\pi(\omega t + \beta_y^{(0)}))$$

$$x = y = 0 \text{ at } t = 0 \text{ so } \beta_x^{(0)} = \beta_y^{(0)} = 0, \quad \overset{t=0}{p_x = p_y} \Rightarrow J_x^{(0)} = J_y^{(0)} = \frac{\pi}{\omega} E$$

over one period

$$\overline{\dot{\beta}_x^{(1)}} = \frac{b m^2 \omega^2}{\pi^2} J_y^{(0)} \underbrace{\frac{1}{2\pi} \int_0^{2\pi} d\theta \cos^4(\theta)}_{= 3/8}$$

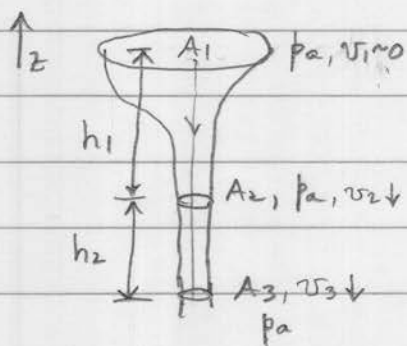
$$= \frac{3 b m^2 \omega^2 J_y^{(0)}}{8 \pi^2}$$

$$J_x^0 \rightarrow J_x + \overline{\dot{\beta}_x^{(1)}}$$

is shift in J_x

by symmetry its same for J_y

Smits 4.36 (a)



continuity $\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \vec{v}) = 0$, $\text{Div. Thm} \Rightarrow \rho \int_S dS \hat{n} \cdot \vec{v} = 0$

continuity $A_1 v_1 = A_2 v_2 = A_3 v_3$

Bernoulli (equal pressure)

$$\frac{v_1^2}{2} + g z_1 = \frac{v_2^2}{2} + g z_2 = \frac{v_3^2}{2} + g z_3$$

Water at rest
in funnel basin

$$z_1 - z_2 = h_1, \quad z_2 - z_3 = h_2$$

(a) $\frac{A_3}{A_2} = \frac{v_2}{v_3}$, $v_2^2 = 2gh_1$, $v_3^2 - v_2^2 = 2gh_2$, $v_3^2 = 2g(h_1 + h_2)$
 $v_2 = \sqrt{2gh_1}$, $v_3 = \sqrt{2g(h_1 + h_2)}$

$$\frac{A_3}{A_2} = \sqrt{\frac{h_1}{h_1 + h_2}}$$

(b) Mom. Conservation: $\frac{\partial}{\partial t} (\rho \vec{v}) + \nabla \cdot \hat{T} = \vec{f} = \rho \vec{g}$

$$\int_S dS \hat{n} \cdot \hat{T} = \int_{\text{Vol}} dV \nabla \cdot \hat{T} = \int_{\text{Vol}} dV \rho \vec{g} = V \rho \vec{g}$$

$\hat{T}_{ki} = \delta_{ki} p + v_k v_i \rho$, take surface

fluid passes only through A_2 & A_3

so only these have non-zero velocities

$$\hat{n} \cdot \hat{T}|_2 = \hat{z} p + \underbrace{\vec{v}_2}_{(-v_2 \hat{z})} \cdot \underbrace{\hat{z}}_{(-v_2)} \rho, \quad \hat{n} \cdot \hat{T}|_3 = -\hat{z} \cdot \hat{T}|_3 = -\hat{z} p + \underbrace{\vec{v}_3}_{(-v_3 \hat{z})} \cdot \underbrace{(-\hat{z})}_{(+v_3)} \rho$$

pressure terms equal with opposite signs so cancel

$v_2 = \text{constant across } A_2 \text{ for ideal fluid}$, $v_3 = \text{constant on } A_3$

So

$$V \rho (-g \hat{z}) = \int_{A_2} dS \hat{n} \cdot \hat{T} + \int_{A_3} dS \hat{n} \cdot \hat{T} = (v_2^2 A_2 - v_3^2 A_3) \hat{z} \rho$$

$$\text{Volume} = \frac{A_2 v_2^2}{(-g)} \left(1 - \frac{v_3^2 A_3}{v_2^2 A_2} \right) = \frac{A_2 (2gh_1)}{(-g)} \left(1 - \frac{(h_1 + h_2)}{h_1} \sqrt{\frac{h_1}{h_1 + h_2}} \right)$$

$$= 2 A_2 h_1 \left(\sqrt{\frac{h_1 + h_2}{h_1}} - 1 \right)$$

7.12 Smit's

$$u = v_x = 2cxy$$

$$v_z = 0$$

$$v = v_y = c(a^2 + x^2 - y^2)$$

a) Incompressible?

$$\vec{\nabla} \cdot \vec{v} = \frac{\partial v_x}{\partial x} + \frac{\partial v_y}{\partial y} = 2cy - 2cy = 0 \quad \text{Yes.}$$

$$\begin{aligned} \text{b) } \vec{\nabla} \times \vec{v} &= ? \\ \vec{\nabla} \times \vec{v} &= \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ v_x & v_y & 0 \end{vmatrix} = \hat{x}(0) - \hat{y}(0) + \hat{z}\left(\frac{\partial v_y}{\partial x} - \frac{\partial v_x}{\partial y}\right) \\ &= \hat{z}(c \cdot 2x - 2cx) = 0 \quad \text{so irrotational} \end{aligned}$$

c) $\vec{v} = \vec{\nabla} \phi$, $v_x = \frac{\partial \phi}{\partial x}$ so $\phi = cx^2y + g(y)$

$v_y = \frac{\partial \phi}{\partial y}$, $\phi = c(a^2 + x^2)y - \frac{cy^3}{3}$ \leftarrow this agrees with above, so works

\leftarrow (fixed)

8.24 Smit's

$$F_D = f(V, L, B, \rho, \mu, g)$$

$\mu = "v"$

a) $[F_D] = \frac{kg \cdot m}{s^2}$, $[V] = \frac{m}{s}$, $[L] = m$, $[B] = m$, $[\rho] = \frac{kg}{m^3}$, $[\mu] = \frac{m^2}{s}$
 $[g] = m/s^2$

dimless: L/B , $R = \frac{VL}{\mu}$, $[e v^2 L^2] = [F_D]$
 v^2/gL

\leftarrow also could take $\mu = \eta = \rho \nu$ as valid interpretation

a) $F_D = \rho v^2 L^2 h\left(\frac{L}{B}, \frac{VL}{\mu}, \frac{v^2}{gL}\right)$

b) need some $\left(\frac{L}{B} \text{ \& } \frac{VL}{\mu} \text{ \& } \frac{v^2}{gL}\right)$ as the ship

c) $L' = \frac{1}{25} L = 4m$, $B' = \frac{1}{25} B$ $\rightarrow v'^2 = v^2 \frac{L'}{L} = 100/25 = 4$
 $v = 10m/s$, $v^2/L = v'^2/L'$ $v' = 2m/s$

$$\frac{v'L'}{\mu'} = \frac{vL}{\mu}, \quad \frac{\mu'}{\mu} = \frac{v'L'}{vL} = \frac{2}{10} \frac{1}{25} = \frac{1}{125}$$

With same ρ
 $\frac{F_D'}{F_D} = \frac{v'^2 L'^2}{v^2 L^2} = \frac{1}{(125)^2}$

9.37 Smits, steady flow

$$\omega \gg D$$

Navier Stokes

$$(\vec{v} \cdot \vec{\nabla}) \vec{v} = -\frac{1}{\rho} \nabla p + \nu \nabla^2 \vec{v}$$

$$\vec{v} = v_x(y) \hat{x}$$

$$v_x(y) = U = U_0 \left[1 - \left(\frac{2y}{D} \right)^2 \right]$$

$$(\vec{v} \cdot \vec{\nabla}) \vec{v} \propto \frac{\partial v_x(y)}{\partial x} = 0$$

$$\textcircled{a} \quad \frac{1}{\rho} \frac{\partial p}{\partial x} = \nu \frac{\partial^2 v_x(y)}{\partial y^2} = \nu U_0 \left(-\frac{4}{D^2} \right) \frac{\partial^2}{\partial y^2} y^2 = -\frac{8 \nu U_0}{D^2}$$

shear stress $\sigma_{ix} = \eta \left(\frac{\partial v_i}{\partial x} + \frac{\partial v_x}{\partial i} - \frac{2}{3} \delta_{ix} \frac{\vec{\nabla} \cdot \vec{v}}{0} \right)$

at wall: $\sigma_{xy} = \sigma_{yx} = \eta \frac{\partial v_x}{\partial y} \Big|_{y=\pm D/2} = \eta \left(-\frac{4}{D^2} \right) \left(\pm \frac{D}{2} \right) U_0$

\hat{x} friction force on wall from shear

$$\tau_w = (-\hat{y}) \cdot \sigma_{yx} \Big|_{y=D/2} + (+\hat{y}) \cdot \sigma_{yx} \Big|_{y=-D/2} = \eta \left(-\frac{4}{D^2} \right) \left(-\frac{D}{2} - \frac{D}{2} \right) U_0$$

$$\tau_w = \eta \frac{4 U_0}{D^2} D = \frac{\eta 8 U_0}{D^2} \frac{D}{2}$$

$$\text{so } \frac{\partial p}{\partial x} = -\frac{8 \eta U_0}{D^2} = -\frac{2}{D} \tau_w \quad \checkmark$$

$$\textcircled{b} \quad \frac{\partial p}{\partial x} = -\frac{8 U_0 \nu}{D^2} \quad \text{found in } \textcircled{a} \quad \nu = \mu$$

$$\textcircled{c} \quad \vec{\nabla} \times \vec{v} \Big|_z = \frac{\partial v_x}{\partial y} = \eta \left(-\frac{4}{D^2} \right) y \quad \text{linearly with } y$$

Strogatz 3.4.4

$$\dot{x} = x + \frac{rx}{1+x^2} = x \left(1 + \frac{r}{1+x^2} \right)$$

$$\dot{x} = x \left(\frac{1+r+x^2}{1+x^2} \right)$$

numerator has subcritical pitchfork form

fixed pts: $x=0$ (always), $1+r < 0$ then $x = \pm \sqrt{-(1+r)}$
so $r < -1$

check stability:

near $x \approx 0$

$$\dot{x} = x(1+r)$$

stable $1+r < 0$

ie $r < -1$

unstable $1+r > 0$

$r > -1$

$$x = +\sqrt{-(1+r)} + \eta \quad \text{for } r < -1$$

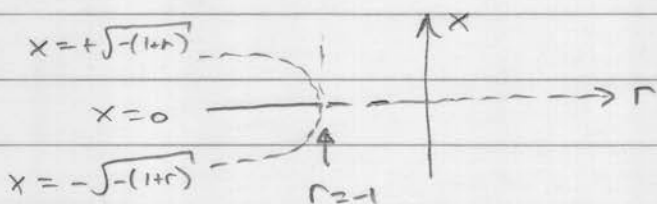
$$\dot{x} = \frac{x(x + \sqrt{-(1+r)})(x - \sqrt{-(1+r)})}{1+x^2}$$

$$\text{so } \dot{\eta} = \frac{\sqrt{-(1+r)}}{-r} 2\sqrt{-(1+r)} (\eta) = \frac{2(1+r)}{-r} \eta$$

$$\underbrace{-r}_{>0}$$

unstable

$$x = -\sqrt{-(1+r)} + \eta \quad , \text{ similar } , \text{ unstable}$$



Strogatz 5.2.5

$$\dot{x} = 3x - 4y$$

$$\dot{y} = x - y$$

$$\begin{pmatrix} \dot{x} \\ \dot{y} \end{pmatrix} = \underbrace{\begin{pmatrix} 3 & -4 \\ 1 & -1 \end{pmatrix}}_M \begin{pmatrix} x \\ y \end{pmatrix}$$

$$\tau = \text{tr } M = 2$$

$$\Delta = \det M = -3 + 4 = +1$$

$$\tau^2 - 4\Delta = 0, \tau > 0$$

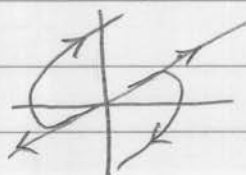
$\dot{x}=0$ is an unstable degenerate node

$$\lambda_{\pm} = \tau_{\pm} = +1$$

$$(M - \lambda I) \Rightarrow \begin{pmatrix} 2 & -4 \\ 1 & -2 \end{pmatrix} \begin{pmatrix} a_1 \\ a_2 \end{pmatrix} = 0$$

$$a_1 = 2a_2$$

$$\begin{pmatrix} 2 \\ 1 \end{pmatrix} \text{ only eigenvector}$$



Strogatz 6.3.9

$$\dot{x} = y^3 - 4x$$

$$\dot{y} = y^3 - y - 3x$$

(a) $\dot{x}=0$ fixed
 $\dot{y}=0$ pts

$$y^3 = 4x$$

$$4x - 3x - y = 0 \text{ so } x = y, \quad x^3 = 4x$$

$$\bullet \quad x = y = 0 \quad \text{or} \quad x = y = +2 \quad \text{or} \quad x = y = -2$$

$$\underline{x=y=0}$$

$$\dot{x} = -4x$$

$$\dot{y} = -y - 3x$$

$$\begin{pmatrix} \dot{x} \\ \dot{y} \end{pmatrix} = \begin{pmatrix} -4 & 0 \\ -1 & -3 \end{pmatrix}$$

$$\tau = -7, \quad \tau^2 - 4\Delta = 1$$

$$\Delta = 12$$

stable node

$$\underline{x=y=2}$$

$$x = 2 + \eta$$

$$y = 2 + \eta$$

$$\dot{\eta} = (2+\eta)^3 - 4(2+\eta) \approx 8 + 12\eta - 8 - 4\eta$$

$$\dot{\eta} = (2+\eta)^3 - (2+\eta) - 3(2+\eta) \approx 8 + 12\eta - 2 - \eta - 6 - 3\eta$$

$$= 11\eta - 3\eta$$

$$M = \begin{pmatrix} -4 & 12 \\ -3 & 11 \end{pmatrix}$$

$$\tau = 7$$

$$\tau^2 - 4\Delta = 49 + 36 = 85$$

$$\Delta = -44 + 36 = -8, \quad \text{saddle node}$$

$$\lambda = -1 \text{ has } \begin{pmatrix} -3 & 12 \\ -3 & 12 \end{pmatrix} \begin{pmatrix} a_1 \\ a_2 \end{pmatrix} = 0 \quad a_1 = 4a_2 \quad \begin{pmatrix} 4 \\ 1 \end{pmatrix}, \quad \lambda_{\pm} = \frac{7}{2} \pm \frac{1}{2}9 = -1 \text{ or } (+8) \quad \begin{pmatrix} 1 \\ 1 \end{pmatrix}$$

$$\underline{x=y=-2}$$

Note: $x \rightarrow -x$ & $y \rightarrow -y$ is symmetry of eqns

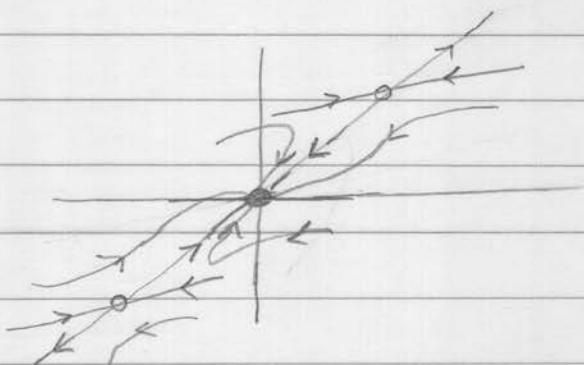
so saddle node here too

(b) $x=y \Rightarrow \dot{x} = x^3 - 4x = x(x^2 - 4)$

$$\dot{y} = x^3 - 4x \text{ too} \quad \text{so } \dot{x} = \dot{y} \quad \& \quad x=y \text{ as time increases}$$

(c) let $w = x - y$, $\dot{w} = \dot{x} - \dot{y} = (y^3 - 4x) - (y^3 - y - 3x) = -(x - y) = -w$
 $\therefore w = A e^{-t}$ decreases

(d)



6.5.4 Strogatz

$$\ddot{x} = ax - x^2$$

find conserved quantity & sketch

$$\dot{x} = w \quad \equiv f_x$$

$$\dot{w} = ax - x^2 \quad \equiv f_w$$

$$H(x, w) = \int^w dw' f_x - \int^x dx' f_w = \frac{w^2}{2} - \left(\frac{ax^2}{2} - \frac{x^3}{3} \right)$$

$$= \frac{w^2}{2} + \frac{x^2}{3} \left(x - \frac{3a}{2} \right) = \frac{w^2}{2} + \frac{x^3}{3} - \frac{ax^2}{2}$$

fixed pts $w=0$ & $x=0$ or $x=a$

$$\frac{\partial^2 H}{\partial x^2} = -a < 0 \text{ for } a > 0 \text{ max/unstable}$$

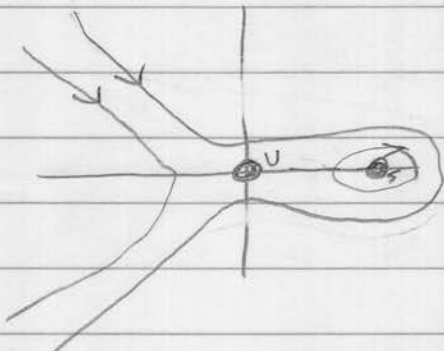
$$> 0 \text{ for } a < 0 \text{ min/stable}$$

$$\frac{\partial^2 H}{\partial x^2} = 2x - a$$

$$\frac{\partial^2 H}{\partial x^2} = a, > 0 \text{ } a > 0 \text{ unstable}$$

$$< 0 \text{ } a < 0 \text{ stable}$$

$a > 0$



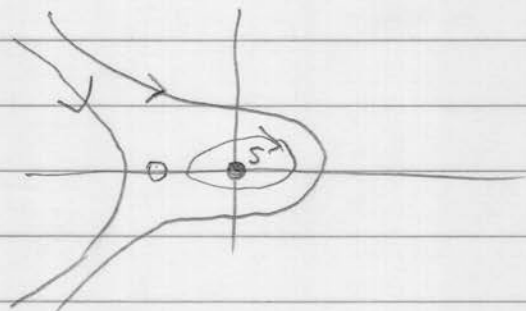
Hamiltonian / Conservative E system

so stable center about s

$u = \text{unstable}$

$s = \text{stable}$

$a < 0$

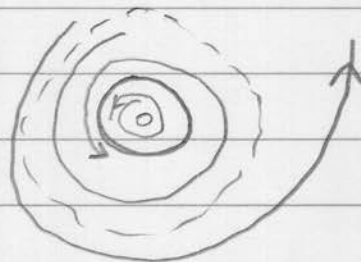
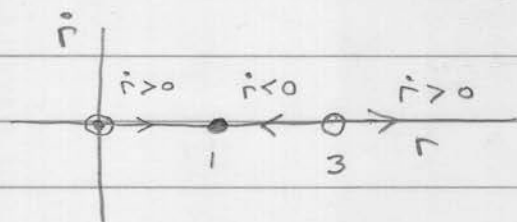


7.1.2 Strogatz

$$r \geq 0$$

$$\dot{r} = r(1-r^2)(9-r^2) \quad \dot{\theta} = 1$$

$r=1$ & $r=3$ are limit cycles, $r=0$ fixed pt



$$\ddot{x} = \cancel{ax - x^2} a - e^x$$

Find conserved quantity

$$\cancel{\ddot{x}} \ddot{x} = \cancel{ax - x^2} a - e^x$$

$$\cancel{\ddot{x}} \ddot{x} = -\frac{d}{dx} [-ax + e^x]$$

$$\text{Let } V(x) = -ax + e^x$$

Hence we have

$$\ddot{x} = -\frac{dV}{dx}$$

$$\dot{x} \ddot{x} = -\dot{x} \frac{dV}{dx}$$

$$\Rightarrow \frac{d}{dt} \left(\frac{\dot{x}^2}{2} \right) = -\frac{d}{dt} V(x)$$

$$\Rightarrow \frac{d}{dt} \left(\frac{\dot{x}^2}{2} + V(x) \right) = 0$$

$$\text{Hence } E = \frac{\dot{x}^2}{2} + V(x) = \frac{\dot{x}^2}{2} - ax + e^x$$

is conserved.

$$\text{Let } y = \dot{x} \Rightarrow \dot{y} = a - e^x$$

$$\text{Jacobian matrix for this system is } A = \begin{pmatrix} \frac{\partial \dot{x}}{\partial x} & \frac{\partial \dot{x}}{\partial y} \\ \frac{\partial \dot{y}}{\partial x} & \frac{\partial \dot{y}}{\partial y} \end{pmatrix} = \begin{pmatrix} 0 & 1 \\ -e^x & 0 \end{pmatrix}$$

$$\dot{x} = y$$

$$\dot{y} = a - e^x$$

$$A = \begin{pmatrix} 0 & 1 \\ -e^x & 0 \end{pmatrix}$$

(2)

Hence if ~~there~~ there are fixed points then they are centers

as $\Delta = \det A = e^x > 0$

Recall that for a conservative system we only have centers and saddles as fixed points.

$\Delta > 0 \Rightarrow$ centers [only if there are fixed points in the first place!]

Now let's find the fixed points for this system

$$\dot{x} = y$$

$$\dot{y} = a - e^x$$

$$\dot{x} = \dot{y} = 0 \Rightarrow y = 0, x = \ln a$$

Only when $a > 0$

For $a = 0$ or $a < 0$

\longrightarrow No fixed points

Let's consider the case of $a > 0$ first.

$$a > 0 \rightarrow \text{~~the~~ } (\ln a, 0)$$

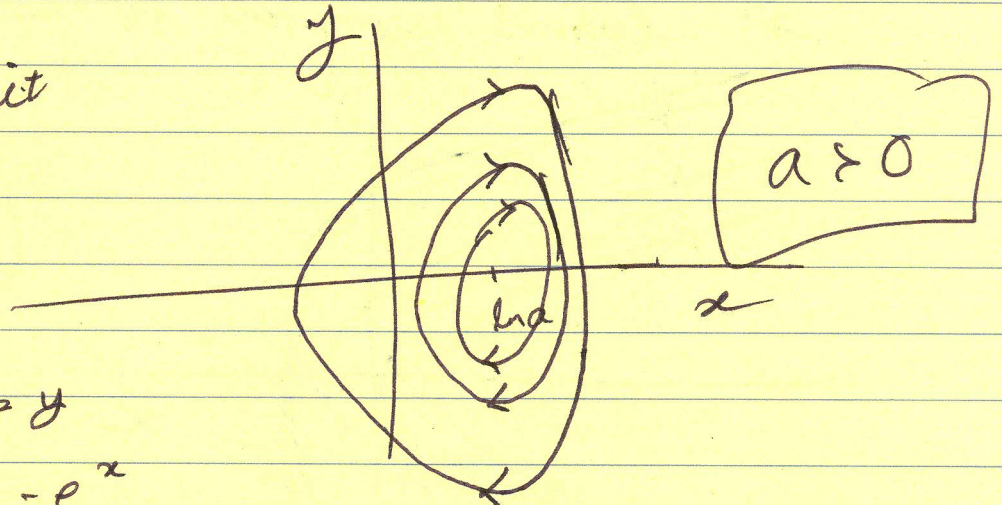
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Center

(3)

$E = \frac{y^2}{2} - ax + e^x$ is constant along the closed contours

$$\left. \frac{d^2 E}{dx^2} \right|_{x=\ln a} = a > 0 \rightarrow E \text{ has a minimum at } (0, \ln a)$$

Phase portrait



Note that $\dot{x} = y$

$$\dot{y} = a - e^x$$

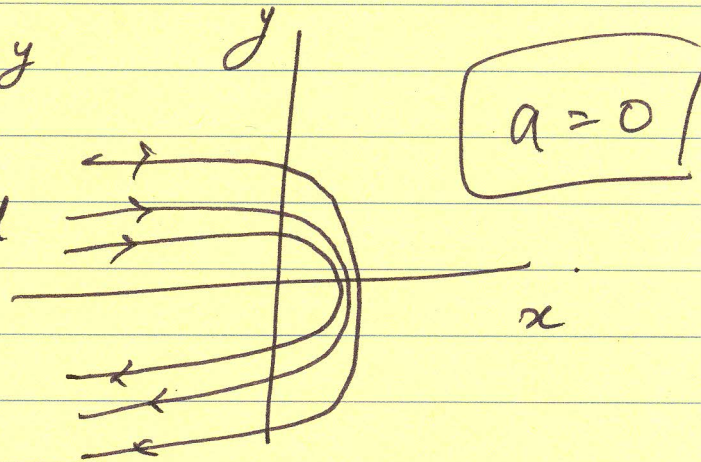
Note For large x , $-e^x$ dominates in \dot{y} and we get very steep descent. The curve turns right ~~or~~ left only when y is large enough.

For $a = 0$

$$\dot{x} = y$$

$$\dot{y} = -e^x$$

We have no fixed points



Note

For $x \rightarrow -\infty$

$\dot{y} \rightarrow 0 \Rightarrow$ the curves get horizontal for $x \rightarrow -\infty$

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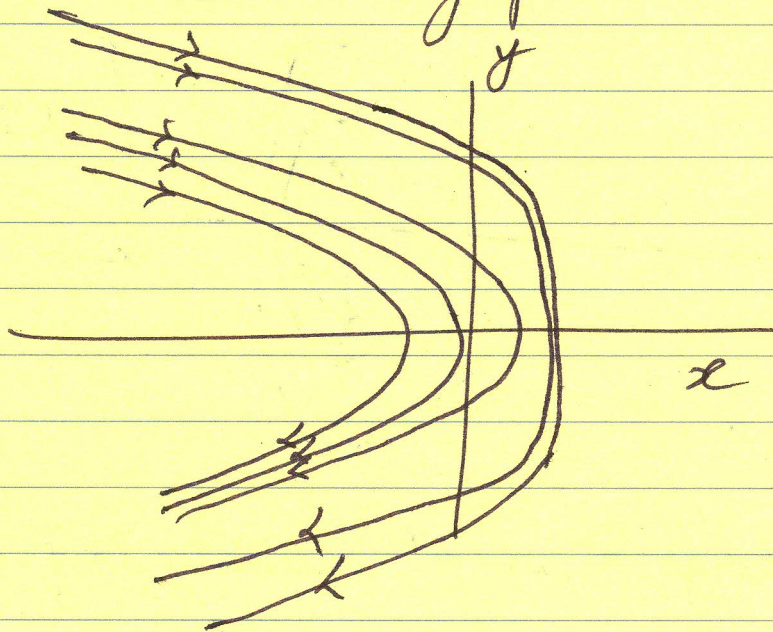
$$a < 0$$

$$\dot{x} = y$$

$$\dot{y} = -|a| - e^x$$

$$\text{as } x \rightarrow -\infty \quad y \rightarrow -|a|$$

⇒ curves asymptote to lines $y = -|a|x + \text{const}$



$$a < 0$$

~~For Contour plots for conservative system~~