

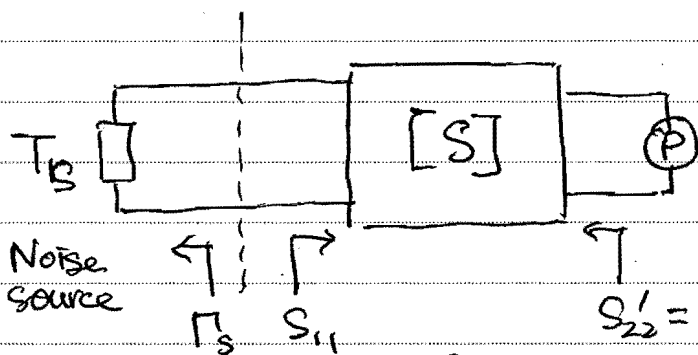
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Parameter Noise Wave Extraction

ET 5/26/2018

Consider a network connected to a matched power measurement device.

- * This network is characterized by a scattering matrix $[S]$
- * The network is reasonably well matched at output (say with attenuators)
- * The network has $S_{12} \approx 0$



$$S_{22}' = S_{22} + \frac{S_{22}S_{21}\Gamma_L}{1 - S_{11}\Gamma_L}$$

Available gain of network

$$G_{av} = \frac{|S_{21}|^2}{|1 - \Gamma_s S_{11}|^2} \cdot \frac{1 - |\Gamma_s|^2}{1 - |S_{22}'|^2} = |S_{21}|^2 \frac{1 - |\Gamma_s|^2}{|1 - \Gamma_s S_{11}|^2}$$

Noise Temp. of network

$$T_n = T_{min} + T_o \frac{R_N}{G_s} |Y_s - Y_{opt}|^2 \quad \text{To ambient temp. (K)}$$

where T_{min} , R_N and Y_{opt} are the 4 noise parameters
 $Y_s = G_s + jB_s$ is the source admittance

Power measured at output

$$P = k B G_{av} (T_s + T_n)$$

↑ Boltzmann constant
 ↑ Noise equivalent BW

• BMDM •

$$P = k_B \frac{|S_{21}|^2}{|1 - \Gamma_S S_{11}|^2} \left[(1 - |\Gamma_S|^2) (T_S + T_{min}) + T_0 R_N \frac{1 - |\Gamma_S|^2}{G_S} |Y_S - Y_{opt}|^2 \right]$$

We note that

$$1 - |\Gamma_S|^2 = \frac{4 G_S Y_0}{|Y_0 + Y_S|^2}$$

$$\text{where } Y_0 = \frac{1}{50 \Omega}$$

$$\begin{aligned} P &= k_B \frac{|S_{21}|^2}{|1 - \Gamma_S S_{11}|^2} \left[\frac{4 G_S Y_0}{|Y_0 + Y_S|^2} (T_S + T_{min}) + \frac{4 Y_0 R_N}{|Y_0 + Y_S|^2} T_0 |Y_S - Y_{opt}|^2 \right] \\ &= k_B \underbrace{\frac{|S_{21}|^2}{|1 - \Gamma_S S_{11}|^2} \frac{4 Y_0}{|Y_0 + Y_S|^2}}_{G_{net}} \left[G_S (T_S + T_{min}) + R_N T_0 |Y_S - Y_{opt}|^2 \right] \end{aligned}$$

The network gain G_{net} can be found using a hot/cold measurement with a matched calibrated noise source (no impedance diff ON/OFF)

$$\begin{aligned} P_{hot} &= G_{net} [G_S (T_{hot} + T_{min}) + R_N T_0 |Y_S - Y_{opt}|^2] \\ P_{cold} &= G_{net} [G_S (T_{cold} + T_{min}) + R_N T_0 |Y_S - Y_{opt}|^2] \end{aligned}$$

$$P_{hot} - P_{cold} = G_{net} G_S (T_{hot} - T_{cold})$$

$$\begin{aligned} P &= G_{net} [G_S (T_S + T_{min}) + R_N T_0 ((G_S - G_{opt})^2 + (B_S - B_{opt})^2)] \\ &= G_{net} [G_S T_S + G_S (T_{min} - 2 R_N G_{opt} T_0) + R_N (G_{opt}^2 + B_{opt}^2) T_0 \\ &\quad + R_N (G_S^2 + B_S^2) T_0 - 2 R_N B_S B_{opt} T_0] \end{aligned}$$

There are 4 independent unknowns

$$C_1 = \frac{T_{min}}{T_0} - 2 R_N G_{opt}$$

$$C_2 = R_N$$

$$C_3 = (G_{opt}^2 + B_{opt}^2) R_N$$

$$C_4 = -R_N B_{opt}$$

$$R = G_{\text{net}} \left[G_S T_S + G_S C_1 + (G_S^2 + B_S^2) C_2 T_0 \right]$$

$$P = G_{\text{net}} T_0 \left[G_S \frac{T_S}{T_0} + G_S C_1 + (G_S^2 + B_S^2) C_2 + C_3 + 2B_S C_4 \right]$$

If we make 4 power measurements with different T_S or $G_S + jB_S$, the above equations can be solved for C_1, C_2, C_3 and C_4 .

from which T_{min} , R_N and $Y_{\text{opt}} = G_{\text{opt}} + jB_{\text{opt}}$ can be solved.

Note: For passive terminations, $T_S = T_0$

If more than 4 measurements are made, then one arrives at an over-determined system, which can be tackled by error minimization.

Reference: Juan M O'Callaghan, and Jyoti P Mondal.

"A vector approach for noise parameter fitting and selection of source admittances."

IEEE MTT-39, pp. 1376-1382, Aug 1991