

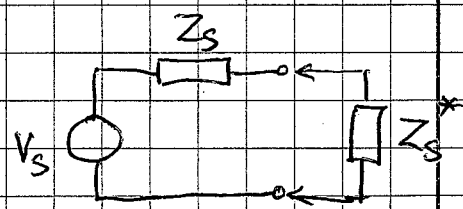
Input match $\Gamma_{in} = S_{11} + \frac{S_{12}S_{21}\Gamma_L}{1 - S_{22}\Gamma_L}$

Output match $\Gamma_{out} = S_{22} + \frac{S_{12}S_{21}\Gamma_s}{1 - S_{11}\Gamma_s}$

Available Gain $G_{av} = \frac{|S_{21}|^2}{|1 - \Gamma_s S_{11}|^2} \cdot \frac{1 - |\Gamma_s|^2}{1 - |\Gamma_{out}|^2}$

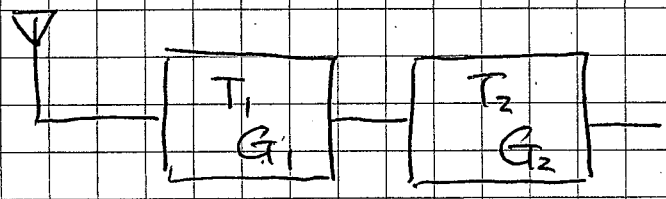
Definition of Available Gain

$$G_{av} = \frac{P_{out-av}}{P_{in-av}}$$



Maximum Available power from source

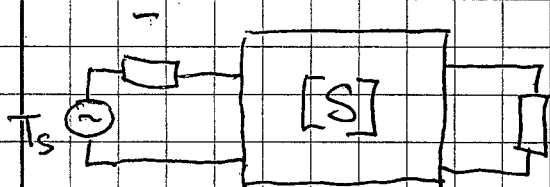
$$P_{av} = \frac{|V_s|^2}{8 \operatorname{Re}(Z_s)} = \frac{|V_s|^2}{8 Z_0} \frac{|1 - \Gamma_s|^2}{1 - |\Gamma_s|^2}$$



$$T_{sys} = T_1 + \frac{T_2}{G_1} + \frac{T_3}{G_1 G_3}$$

Available gain

Noise Parameters



$$T = T_{min} + T_0 \frac{R_N}{G_s} |Y_s - Y_{opt}|^2 = T_{min} + \frac{T_0 r_n Z_0}{G_s} |Y_s - Y_{opt}|^2$$

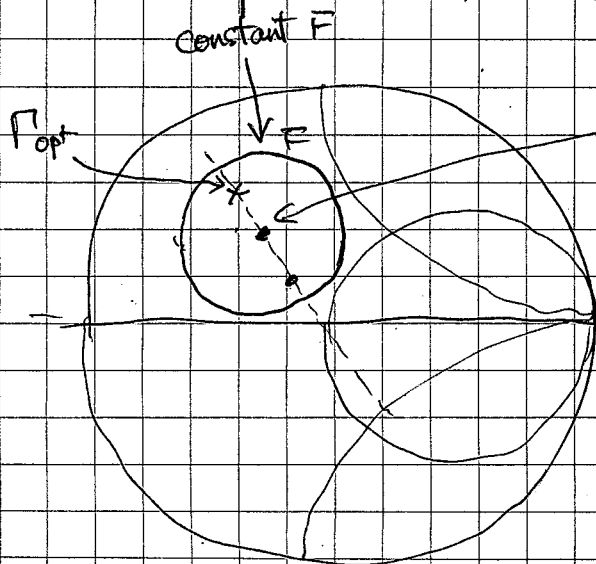
$$= T_{min} + \frac{4R_N}{Z_0} \frac{T_0 |\Gamma_s - \Gamma_{opt}|^2}{(1 - |\Gamma_s|^2)(1 + |\Gamma_{opt}|^2)}$$

Noise
figure

$$F = \frac{T_n}{T_0} + 1$$

Constant noise temp / figure appears as circles on Smith Chart

4 Noise parameters T_{min} , Γ_{opt} (Y_{opt}) and R_N (r_n)

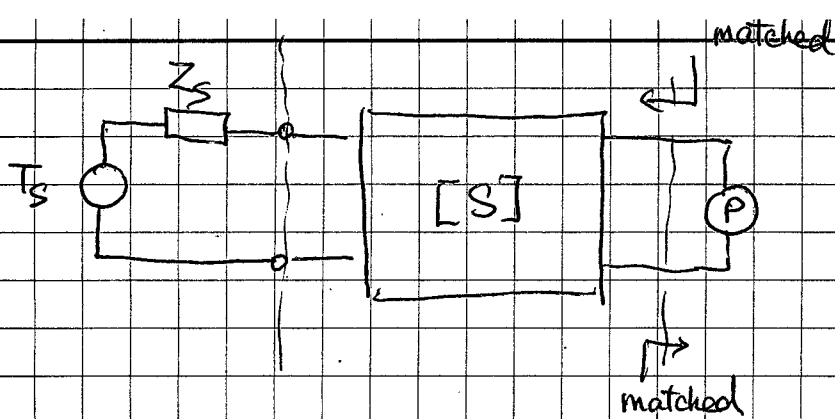


$$C_F = \frac{\Gamma_{opt}}{N+1}$$

$$R_F = \frac{\sqrt{N(N+1 - |\Gamma_{opt}|^2)}}{N+1}$$

$$N = (F - F_{min}) \frac{1 + |\Gamma_{opt}|^2}{4r_n}$$

Input Toner used to derive these parameters



$$P_{out} = k G_{av} B (T_s + T_n)$$

$$G_{av} = \frac{|S_{21}|^2}{|1 - \Gamma_s S_{11}|^2} [1 - |\Gamma_s|^2]$$

$$= k B \frac{|S_{21}|^2}{|1 - \Gamma_s S_{11}|^2} [1 - |\Gamma_s|^2] \left[T_s + T_{min} + T_0 \frac{R_N}{G_s} |Y_s - Y_{opt}|^2 \right]$$

$$1 - |\Gamma_s|^2 = \frac{4 G_s Y_0}{|Y_0 + Y_s|^2}$$

$$Y_0 = \frac{1}{Z_0} = \frac{1}{50 \Omega}$$

$$P_{out} = k B \frac{|S_{21}|^2}{|1 - \Gamma_s S_{11}|^2} \left[\frac{4 G_s Y_0}{|Y_0 + Y_s|^2} (T_s + T_{min}) + \frac{4 Y_0 R_N}{|Y_0 + Y_s|^2} T_0 |Y_s - Y_{opt}|^2 \right]$$

$$= k B \frac{|S_{21}|^2}{|1 - \Gamma_s S_{11}|^2} \cdot \frac{4 Y_0}{|Y_0 + Y_s|^2} \left[G_s (T_s + T_{min}) + R_N T_0 |Y_s - Y_{opt}|^2 \right]$$

$\underbrace{\hspace{10em}}_{G_{net}}$

$$P_{hot} - P_{cold} = \underbrace{G_{net} G_s}_{\rightarrow \text{derived}} (T_{hot} - T_{cold})$$

$$G_s \approx \frac{1}{Z_0} \approx 50 \Omega$$

$$P_{out} = G_{net} \left[G_s (T_s + T_{min}) + R_N T_0 ((G_s - G_{opt})^2 + (B_s - B_{opt})^2) \right]$$

$$= G_{net} \left[G_s T_s + G_s (T_{min} - 2 R_N T_0 G_{opt}) + R_N T_0 (G_{opt}^2 + B_{opt}^2) \right. \\ \left. + R_N T_0 (G_s^2 + B_s^2) - 2 R_N T_0 B_s B_{opt} \right]$$

Write $Q_1 = \frac{T_{min}}{T_0} - 2 R_N G_{opt}$

$$Q_2 = R_N$$

$$Q_3 = R_N (G_{opt}^2 + B_{opt}^2)$$

$$Q_4 = - R_N B_{opt}$$

$$P_{out} = G_{net} T_0 \left[G_s \frac{T_s}{T_0} + G_s Q_1 + Q_2 (G_s^2 + B_s^2) + Q_3 + 2 B_s Q_4 \right]$$

$$P_{out} = k G_{av} B (T_s + T_n)$$

$$= k B \frac{|S_{21}|^2}{|1 - \Gamma_S S_{11}|^2} [1 - |\Gamma_S|^2] \left[T_s + T_{min} + T_0 \frac{R_N}{G_S} |Y_S - Y_{opt}|^2 \right]$$

$$= k B \frac{|S_{21}|^2}{|1 - \Gamma_S S_{11}|^2} \cdot \frac{4 G_S Y_0}{|Y_S + Y_0|^2} \left[T_s + T_{min} + T_0 \frac{R_N}{G_S} |Y_S - Y_{opt}|^2 \right]$$

$$= k B |S_{21}|^2 \left[\frac{4 G_S Y_0}{|Y_S + Y_0|^2} \cdot \frac{1}{|1 - \Gamma_S S_{11}|^2} (T_s + T_{min}) \right.$$

$$\left. + \frac{1}{|1 - \Gamma_S S_{11}|^2} \frac{4 R_N Y_0}{|Y_S + Y_0|^2} T_0 |Y_S - Y_{opt}|^2 \right]$$

For hot/cold measurement with constant source impedance

$$P_{hot} - P_{cold} = k B |S_{21}|^2 \cdot \frac{4 G_S Y_0}{|Y_S + Y_0|^2} \cdot \frac{1}{|1 - \Gamma_S S_{11}|^2} (T_{hot} - T_{cold})$$

Assume further that $Y_S = Y_0$ for this meas.

$$G_T \triangleq \frac{P_{hot} - P_{cold}}{T_{hot} - T_{cold}} = k B |S_{21}|^2 \cdot \frac{4 G_S Y_0}{|1 - \Gamma_S S_{11}|^2} \quad (\Gamma_S = 0)$$

$$P_{out} = G_T \left[\frac{4 G_S Y_0}{|Y_S + Y_0|^2} \cdot \frac{T_s + T_{min}}{|1 - \Gamma_S S_{11}|^2} + \frac{1}{|1 - \Gamma_S S_{11}|^2} \cdot \frac{4 R_N Y_0}{|Y_S + Y_0|^2} T_0 |Y_S - Y_{opt}|^2 \right]$$

$$= \frac{G_T}{|1 - \Gamma_S S_{11}|^2} \cdot 4 Y_0 \left[\frac{G_S (T_s + T_{min})}{|Y_S + Y_0|^2} \right]$$

$$\begin{aligned}
 1 - |\Gamma_s|^2 &= 1 - \left| \frac{Y_0 - Y_s}{Y_s + Y_0} \right|^2 = 1 - \frac{|Y_0 - Y_s|^2}{|Y_s + Y_0|^2} \\
 &= \frac{(Y_s + Y_0)(Y_s^* + Y_0^*) - (Y_s - Y_0)(Y_s^* - Y_0^*)}{|Y_s + Y_0|^2} \\
 &= \frac{(Y_s Y_0 + Y_s^* Y_0^*) + (Y_s Y_0 + Y_s^* Y_0^*)}{|Y_s + Y_0|^2} \\
 &= \frac{2Y_0(Y_s + Y_s^*)}{|Y_s + Y_0|^2} = \frac{4G_s Y_0}{|Y_s + Y_0|^2}
 \end{aligned}$$

$$\begin{aligned}
 |Y_s - Y_{opt}|^2 &= (G_s - G_{opt})^2 + (B_s - B_{opt})^2 \\
 &= (G_s^2 + B_s^2) + (G_{opt}^2 + B_{opt}^2) - 2G_s G_{opt} - 2B_s B_{opt}
 \end{aligned}$$

Assuming that $|\Gamma_s| \approx 0$ for hot-cold measurement

$$P_{\text{hot}} - P_{\text{cold}} = \frac{kB|S_{21}|^2}{4|1 - S_{11}|^2} (T_{\text{hot}} - T_{\text{cold}})$$

$$P_T = \frac{P_{\text{hot}} - P_{\text{cold}}}{T_{\text{hot}} - T_{\text{cold}}} = kB|S_{21}|^2$$

$$P_{\text{out}} = G_{av} kB (T_s + T_n)$$

$$= \frac{kB|S_{21}|^2}{|1 - \Gamma_s S_{11}|^2} (1 - |\Gamma_s|^2) \left[T_s + T_{\text{min}} + \frac{4R_n}{G_s} |Y_s - Y_{\text{opt}}|^2 T_0 \right]$$

$$T_{\text{out}} = \frac{P_{\text{out}}}{kB|S_{21}|^2} |1 - \Gamma_s S_{11}|^2$$

$$1 - |\Gamma_s|^2 = \frac{4G_s Y_0}{|Y_0 + Y_s|^2}$$

$$T_{\text{out}} = (1 - |\Gamma_s|^2) (T_s + T_{\text{min}}) + \frac{4R_n Y_0}{|Y_0 + Y_s|^2} |Y_s - Y_{\text{opt}}|^2 T_0$$

$$|Y_s - Y_{\text{opt}}|^2 = (G_s^2 + B_s^2) + (G_{\text{opt}}^2 + B_{\text{opt}}^2) - 2G_s G_{\text{opt}} - 2B_s B_{\text{opt}}$$

$$\frac{T_{\text{out}} - (1 - |\Gamma_s|^2) T_s}{T_0} = \frac{4G_s Y_0}{|Y_0 + Y_s|^2} \frac{T_{\text{min}}}{T_0} + \frac{4R_n Y_0}{|Y_0 + Y_s|^2} |Y_s - Y_{\text{opt}}|^2$$

$$Q = \frac{G_s T_{\text{min}}}{T_0}$$

$$Q_1 = \frac{T_{\min}}{T_0} - 2R_N G_{\text{opt}}$$

$$Q_2 = R_N$$

$$Q_3 = R_N (G_{\text{opt}}^2 + B_{\text{opt}}^2)$$

$$Q_4 = -R_N B_{\text{opt}}$$

$$\frac{T_{\text{out}} - (1 - |S_{11}|^2) T_s}{T_0} = \frac{4G_s Y_0}{|Y_0 + Y_s|^2} Q_1 + \frac{4Y_0}{|Y_0 + Y_s|^2} (G_s^2 + B_s^2) Q_2$$

$$+ \frac{4Y_0}{|Y_0 + Y_s|^2} Q_3 + \frac{4Y_0 B_s}{|Y_0 + Y_s|^2} Q_4$$

$$\frac{T_{\text{out}} - (1 - |S_{11}|^2) T_s}{4Y_0 T_0} = \frac{G_s}{|Y_0 + Y_s|^2} Q_1 + \frac{G_s^2 + B_s^2}{|Y_0 + Y_s|^2} Q_2 + \frac{Q_3}{|Y_0 + Y_s|^2} + \frac{B_s}{|Y_0 + Y_s|^2} Q_4$$

$$R_N = Q_2 \quad B_{\text{opt}} = -\frac{Q_4}{Q_2}$$

$$G_{\text{opt}} = \sqrt{\frac{Q_3}{Q_2} - \left(\frac{Q_4}{Q_2}\right)^2} = \frac{1}{Q_2} \sqrt{Q_2 Q_3 - Q_4^2}$$

$$T_{\min} = T_0 \left[Q_1 + 2Q_2 G_{\text{opt}} \right] = T_0 \left[Q_1 + 2\sqrt{Q_2 Q_3 - Q_4^2} \right]$$

For short-circuit

$$B_s \rightarrow \infty \quad \frac{1}{|Y_0 + Y_s|^2} \rightarrow 0 \quad \frac{B_s}{|Y_0 + Y_s|^2} \rightarrow 0 \quad \frac{G_s}{|Y_0 + Y_s|^2} \rightarrow 0$$

$$\frac{G_s^2 + B_s^2}{|Y_0 + Y_s|^2} = \frac{|Y_s|^2}{|Y_0 + Y_s|^2} \rightarrow 1$$

Short-circuit

$$\frac{T_{\text{out-sh}}}{4Y_0 T_0} = Q_2 = R_N$$

$$R_N = P_{\text{out-sh}} \frac{T_{\text{hot}} - T_{\text{cold}}}{P_{\text{hot}} - P_{\text{cold}}} |1 - S_{11}|^2 \frac{1}{4Y_0 T_0} =$$

For open-circuit $G_S = 0$ $B_S = 0$

$$\frac{T_{\text{out-open}}}{4Y_0 T_0} = \frac{Q_3}{Y_0^2}$$

$$Q_3 = \frac{T_{\text{out-open}}}{4T_0} Y_0$$

For matched load at T_0 (cold) $G_S = Y_0$ $B_S = 0$

$$\frac{T_{\text{out}} - T_{\text{cold}}}{4Y_0 T_0} = \frac{Q_1}{4Y_0} + \frac{Q_2}{4} + \frac{Q_3}{4Y_0^2}$$

$$\frac{T_{\text{out}} - T_{\text{cold}}}{T_0} = Q_1 + Y_0 Q_2 + \frac{Q_3}{Y_0}$$

$$\frac{T_{\text{out}} - T_{\text{cold}}}{T_0} = Q_1 +$$

$$[C] = kT_0 [I - SS^*]$$

$$SS^* = \begin{bmatrix} S_{11}S_{11}^* & S_{11}S_{21}^* \\ S_{21}S_{11}^* & S_{21}S_{21}^* \end{bmatrix}$$

$$SS^* = \begin{bmatrix} S_{11}S_{11}^* + S_{12}S_{21}^* & S_{11}S_{21}^* + S_{12}S_{22}^* \\ S_{21}S_{11}^* + S_{22}S_{21}^* & S_{21}S_{21}^* + S_{22}S_{22}^* \end{bmatrix}$$

$$= \begin{bmatrix} |S_{11}|^2 + |S_{21}|^2 & S_{11}S_{21}^* + S_{21}S_{22}^* \\ S_{21}S_{11}^* + S_{22}S_{21}^* & |S_{21}|^2 + |S_{22}|^2 \end{bmatrix}$$

$$\langle C_1 C_1^* \rangle = kT_0 (1 - |S_{11}|^2 - |S_{21}|^2)$$

$$\langle C_2 C_2^* \rangle = kT_0 (1 - |S_{22}|^2 - |S_{21}|^2)$$

$$\langle C_1 C_2^* \rangle = -kT_0 (S_{11}S_{21}^* + S_{21}S_{22}^*)$$

Noise Temp $T_n = \frac{\beta C \beta^\dagger}{k}$

$$\beta = \begin{bmatrix} \end{bmatrix}$$

Fitting of over-constrained linear system

$$y = a_1 X_1 + a_2 X_2 + a_3 X_3 + \dots$$

$$n = 1 \dots N$$

a_n — unknown coefficients

X_n — experimental parameters

y_n — measurement data

If M measurements are made ($M > N$)
 $m = 1, \dots, M$

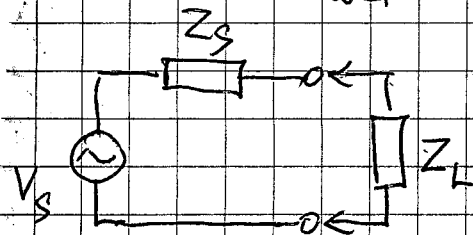
we have an over-constrained system
 which is solved in the least square sense

$$\sigma^2 = \sum_m [(a_1(x_1)_m + a_2(x_2)_m + a_3(x_3)_m + \dots) - y_m]^2$$

$$\frac{\partial \sigma^2}{\partial a_1} = 2 \sum_m [(a_1(x_1)_m + a_2(x_2)_m + a_3(x_3)_m + \dots) - y_m] \cdot (x_1)_m = 0$$

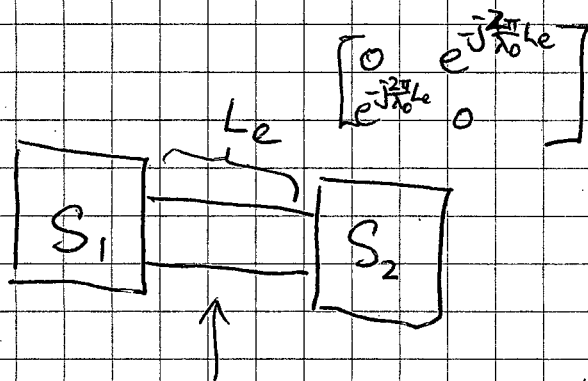
$$\begin{bmatrix} a_1 \\ a_2 \\ a_3 \\ \vdots \end{bmatrix} = \begin{bmatrix} \sum_m (x_1)_m^2 & \sum_m (x_1)_m (x_2)_m & \sum_m (x_1)_m (x_3)_m & \dots \\ \sum_m (x_1)_m (x_2)_m & \sum_m (x_2)_m^2 & \sum_m (x_2)_m (x_3)_m & \dots \\ \sum_m (x_1)_m (x_3)_m & \sum_m (x_2)_m (x_3)_m & \sum_m (x_3)_m^2 & \dots \\ \vdots & \vdots & \vdots & \ddots \end{bmatrix}^{-1} \begin{bmatrix} \sum_m (x_1)_m y_m \\ \sum_m (x_2)_m y_m \\ \sum_m (x_3)_m y_m \\ \vdots \end{bmatrix}$$

Available Power



Max power $Z_s = Z_L^*$

$$P_{av} = \frac{1}{8} \frac{|V_s|^2}{\text{Re}(Z_s)}$$



$$|S_{21}| = 1$$

$$|1 - S_{11}\Gamma_s| = 1$$

$$S_{11} = 0$$

$$\Gamma_s = S_{11}|_{out}$$

$$\Gamma_{out} = 0 + \frac{e^{-j\frac{4\pi}{\lambda_0} Le}}{\phi} \Gamma_s$$

$$G_{av} = \frac{1 - |\Gamma_{out}|^2}{1 - |\Gamma_{out}|^2 e^{-j\frac{4\pi}{\lambda_0} Le}} = 1 = \Gamma_s e^{-j\frac{4\pi}{\lambda_0} Le}$$