

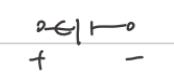
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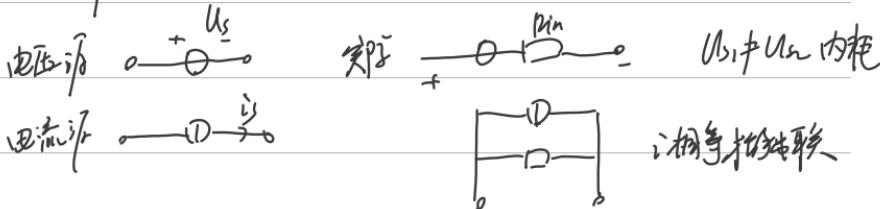
第一、二章 基本概念和模型

一、参考方向

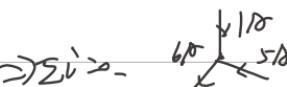
关联参考方向： $U_{i,j}$ 方向一致  无源元件 $P=U_{i,j}I$. 吸收能量(吸收)

非关联参考方向： $U_{i,j}$ 方向不一致  $P=U_{i,j}I$. 释放能量(发出)

二、电源、受控源



三、基尔霍夫定律. 本质：电荷守恒

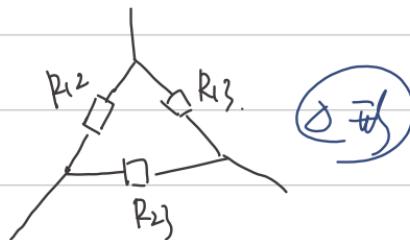
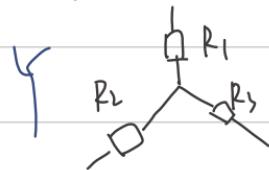
$$KCL: \text{对某节点 } \left\{ \begin{array}{l} \sum I_{出} = \sum I_{入} \\ (+) \quad (-) \end{array} \right. \Rightarrow \sum I = 0$$


$$KVL: \text{对任一回路, 所有支路电压代数和} = 0, \sum U = 0$$

回路顺+逆-

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四: $Y-\Delta$ 等效变换



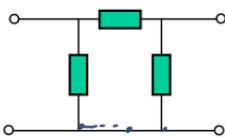
Δ 形

$$Y \rightarrow \Delta: Y = \frac{\Delta \text{相阻抗}}{\Delta \text{电势降}}$$

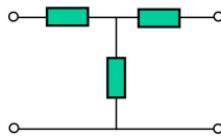
$$R_1 = \frac{R_{12} \cdot R_{13}}{R_{12} + R_{13} + R_{11}}$$

$$Y \rightarrow \Delta \quad \Delta = \frac{\Sigma \text{两两相阻}}{Y \text{的不相邻电阻}}$$

$$R_{12} = \frac{R_1 R_2 + R_2 R_3 + R_1 R_3}{R_3}$$

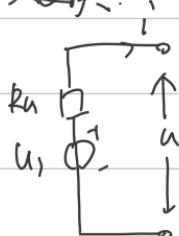


π型网络 (Δ)

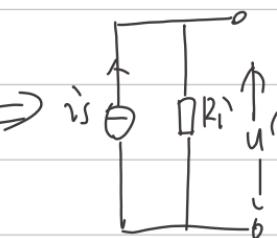


T型网络 (Y)

五. 电源等效变换: \rightarrow 戴维南 \rightarrow 虚地源 (源流)



\Leftrightarrow

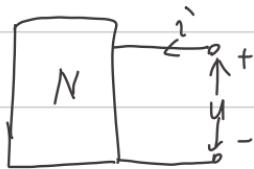


$$\left\{ \begin{array}{l} i_1 = \frac{u_s}{R_1} \\ u_o = R_1 \end{array} \right.$$

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(待测物设置计算)

六、电源-端口网络



端口输入阻抗 $R_i = \frac{U}{I} \Rightarrow$ 等效电阻 R_{eq} .

设 U, I 求 R_i . $\frac{U}{I} = R_i$

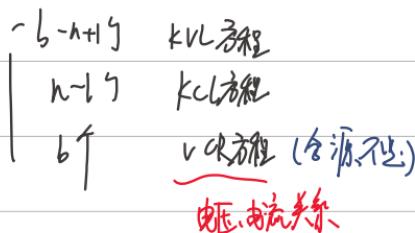
第二章：电阻电路的分析与解法

一、电路的图

支路：一个二端元件构成的支路（也可合併）

网孔：顶点区域不再含有支路 网孔数=独立回路数

没 V 结点， b 个支路



二、支路电流法：

利用VR方程将各支路以支路电流表示，代入KVL方程。

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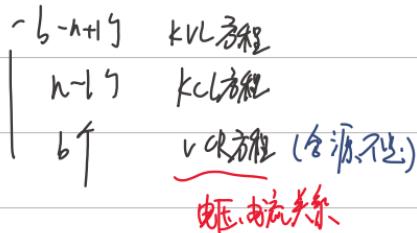
第二章：电阻电路的分析

一、电路的图

支路：一个结点叫构成一个支路（也可合称）

网孔：限走既或不再有支路 网孔数 = 网孔数

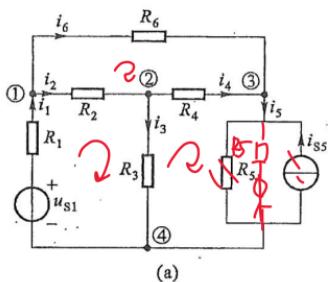
n个结点，b个支路



二、支路电流法：

利用VCR方程将各支路以支路电流表示，代入KVL方程。

W6 --- X6 W6



$$\begin{cases} ①: -i_1 + i_2 + i_6 = 0 \\ ②: -i_2 + i_3 + i_4 = 0 \\ ③: -i_4 + i_5 - i_6 = 0 \end{cases}$$

$$\begin{cases} -u_{S1} + R_1 i_1 + R_2 i_2 + R_3 i_3 = 0 \\ -R_3 i_3 + R_4 i_4 + R_5 i_5 + R_6 i_6 = 0 \\ -R_2 i_2 - R_4 i_4 + R_6 i_6 = 0 \end{cases}$$

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三. 网孔电流法(回路电流法)

适用. 平面电路.

自阻. 互阻

— =

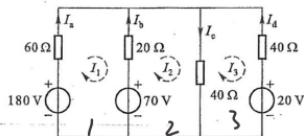


图 3-10 例 3-1 图

$$R_{11} = 60 + 20 = 80 \Omega$$

$$R_{22} = 20 + 40 = 60 \Omega$$

$$R_{33} = 40 + 40 = 80 \Omega$$

$$R_{12} = -20 \Omega \quad R_{23} = -40 \Omega \quad R_{13} = 0 \Omega$$

$$U_{S11} = 180 - 70 = 110 \text{ V}$$

$$U_{S22} = 70 \text{ V}$$

$$U_{S33} = -20 \text{ V}$$

$$\begin{aligned} 1 \quad & R_{11}I_1 + R_{12}I_2 + R_{13}I_3 = U_{S11} \\ 2 \quad & R_{12}I_1 + R_{22}I_2 + R_{23}I_3 = U_{S22} \\ 3 \quad & R_{13}I_1 + R_{23}I_2 + R_{33}I_3 = U_{S33} \end{aligned} \quad \Rightarrow \quad \left\{ \begin{array}{l} 80I_1 - 20I_2 = 110 \\ -20I_1 + 60I_2 = 70 \\ -40I_2 + 80I_3 = -20 \end{array} \right.$$

四. 节点电压法

R₁₂₃₄

G₁₂₃₄

$R = \frac{1}{q}$

Q: 画: 32 (5)

$$G_{11} = \frac{1}{R_1} + \frac{1}{R_{12}R_{13}} + \frac{1}{R_4}$$

$$(G_{11}U_{n1} + G_{12}U_{n2} + G_{13}U_{n3}) = i_{s11}$$

$$G_{12} = -\frac{1}{R_{12}R_{13}}$$

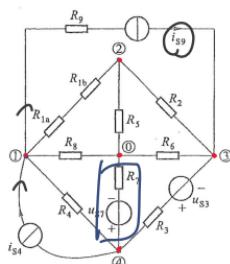
$$G_{21}U_{n1} + G_{22}U_{n2} + G_{23}U_{n3} = i_{s22}$$

$$G_{13} = 0$$

$$G_{31}U_{n1} + G_{32}U_{n2} + G_{33}U_{n3} = i_{s33}$$

$$G_{14} = -\frac{1}{R_4}$$

$$R \rightarrow \left(\frac{1}{R_1} + \frac{1}{R_{12}R_{13}} + \frac{1}{R_4} \right) U_{n1} - \frac{1}{R_{12}R_{13}} U_{n2} - \frac{1}{R_4} U_{n4} = i_{s44}$$



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$$-\frac{1}{R_4}U_{n1} - \frac{1}{R_3}U_{n3} + \left(\frac{1}{R_3} + \frac{1}{R_4} + \frac{1}{R_7}\right)U_{n4} = -i_{s4} + \frac{U_{s7}}{R_7} + \frac{U_{s3}}{R_3}$$

第四章：电路原理：

| kVL, KCL

一、叠加定理

1. 反映了电路的线性性质

2. 某处电压或电流都是电路中若干电源单独作用时在该处分别

产生的电压或电流的叠加。(代数和) ①

3. 叠加原理只适用于线性电路。

4. 不作用的电压源、短路
不作用的电流源、断路开



总功率不等于按各分电路计算所得功率的叠加

A+B

$$P = I^2 R = \frac{V^2}{R} \quad i_2' \quad i_2'' \quad i_2 = i_2' + i_2''$$

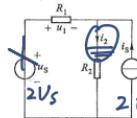
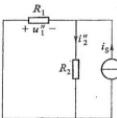


图 4-1 叠加定理

$$i_2' = 2i_2$$

电流分配法



$$I_2 = 1A$$



$$i_2'' = 3A$$

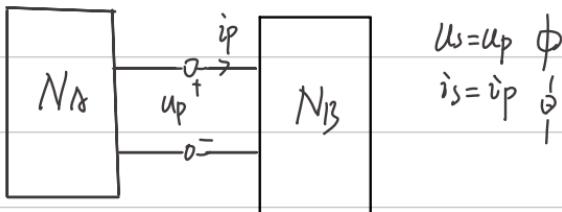
电压分配法

$$\therefore \text{在 (a) 中 } i_2' = i_2' + i_2'' \\ = 1A + 3A = 4A$$

5. 分压原理。在线性电路中，所有激励源同时增大(或减小) k 倍，响应也将同样增大(或减小) k 倍。

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二. 替代定理：

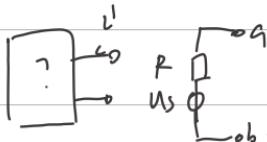


三. 戴维南定理和诺顿定理

开路电压、短路电流、等效电阻 (3选2)

1. 戴维南定理：

对外等效为电压源和电阻



电源电压和激励电压等于端口的开路电压

电阻等于端内全部独立电源置零后输入电阻。

2. 诺顿定理：

对外等效为电流源和电阻。

$\text{Req} \neq 0$, 但 U_o 都相等

理想电压源

激励电流等于端口的短路电流

电阻等于端内全部独立电源置零后输入电阻。

$\text{Req} = 0$ 且相等

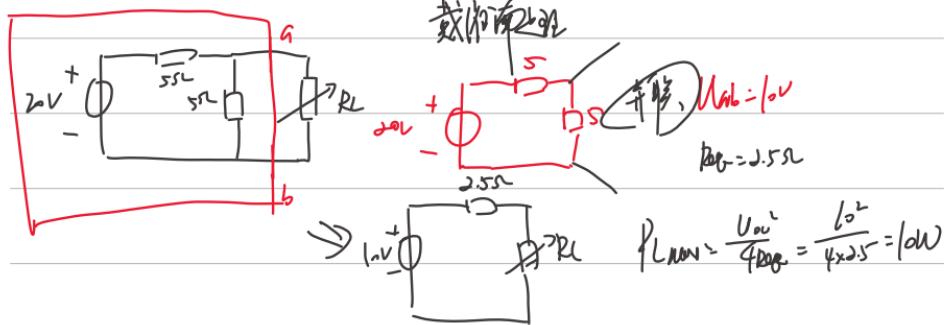
理想电流源

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四、最大功率传输定理

$$P_{max} = \frac{U_{av}^2}{4R_{eq}}$$

$P_L = R_{eq}$ 输入电阻匹配



第3章：储能元件

一、电容(记忆)

恒定电流源

$$i = C \frac{du}{dt}$$

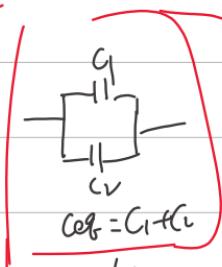
二、电感(记忆)

L

$$u = L \frac{di}{dt}$$

三、串并联:

$$\frac{1}{C_{eq}} = \frac{1}{C_1} + \frac{1}{C_2}$$



$$L_{eq} = L_1 + L_2$$

$$\frac{1}{L_{eq}} = \frac{1}{L_1} + \frac{1}{L_2}$$

$$L_{eq} = L_1 + L_2$$

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源保留在各分电路中进行分析。

【例 4-1】试用叠加定理计算图 4-2(a)中的 u 和 i 。

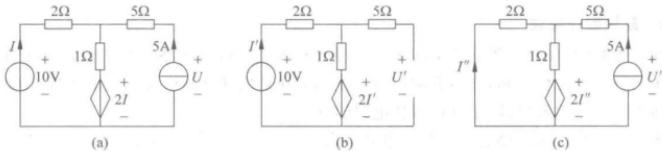


图 4-2 叠加定理计算

解 应用叠加定理，分别画出电压源和电流源单独作用时的分电路如图 4-2(b)、(c)所示，受控源均保留在各分电路中。图 4-2(b)的分响应求得为

$$I' = \frac{10}{2+1+2} A = 2A$$

$$U' = 1 \times I' + 2I' = 6V$$

图 4-2(c)的分响应求得为

$$-2I'' = 1 \times (5 + I'') + 2I''$$

$$I'' = -1A$$

$$U'' = 5 \times 5 - 2I'' = 27V$$

电路的总响应为

$$I = I' + I'' = (2 + (-1))A = 1A$$

$$U = U' + U'' = (6 + 27)V = 33V$$

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第8章：一阶动态电路

一、概念

1. 含有一个动态元件的电路

$$u(t) = u(0) + \int_{t_0}^t i \cdot dt$$

2. 换路定则

$t=0^-$ 换路前的暂态时刻

$$\underline{u}(0^+) = \underline{u}_c(0^-)$$

$t=0^+$ 换路后的暂态时刻

$$\underline{i}(0^+) = \underline{i}_L(0^-)$$

二、一阶电路的零输入响应，没输入

衰减

$$u_c = u_s e^{-\frac{t}{\tau}}$$

$\tau = RC$ (时间常数)

通过3.5τ衰减为0.



$$i_L = I_s e^{-\frac{t}{\tau}}$$

$$\tau = \frac{L}{R} = LG$$



三、一阶电路的零状态响应。
激励能

$$u_c = u_s (1 - e^{-\frac{t}{\tau}})$$

$$\tau = RC$$

$$i_L = I_s (1 - e^{-\frac{t}{\tau}})$$

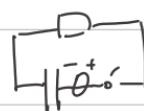
$$\tau = \frac{L}{R}$$



$$Us(1 - e^{-\frac{t}{\tau}})$$

四、一阶电路的全响应：

非零初值状态后一阶电路受到激励



$$u_c = u_s e^{-\frac{t}{\tau}} + u_s (1 - e^{-\frac{t}{\tau}})$$

零输入+零状态

时序叠加

$$u_c = u_s + (u_0 - u_s) e^{-\frac{t}{\tau}} \xrightarrow{\text{齐次解}} \text{三要素法}$$

$$f(t) = f(\infty) + [f(0^+) - f(\infty)] \cdot e^{-\frac{t}{\tau}}$$

U(0) 齐次解

初始值

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$$f(t) = f'(t) + [f(0^+) - f'(0^+)] e^{-\frac{t}{\tau}} \quad u(t) = t - 5$$

稳态分量：将电容视为开路，将电感视为短路

一阶电路的全响应

解题步骤： $r(t) = [r(0^+) - r(\infty)]e^{-t/\tau} + r(\infty)$ $t > 0$

1. 初始值 $r(0^+)$ 的计算

- 画 0^- 电路图 (电容开路，电感短路，开关未动)，求得 $u_C(0^-)$ 和 $i_L(0^-)$
- 换路定则，得 $u_C(0^+)$ 和 $i_L(0^+)$ $U_C(0^+) = U_C(0^-), i_L(0^+) = i_L(0^-)$
- 画 0^+ 电路图 (电容 $u_C(0^+)$ 电压源，电感 $i_L(0^+)$ 电流源，开关已动)，得其他初始值 $r(0^+)$

零状态分量 稳态值 $r(\infty)$ 的计算

画 ∞ 电路图 (电容开路，电感短路，开关已动)，求得 $r(\infty)$

3. 时间常数 τ 的计算

- 画 R_o 电路图 (开关已作用，直流通路置零)，计算电容/电感端口 (看进去) 的等效电阻 R_o
- 计算 τ : $\tau = R_o C$ 或 $\tau = L/R_o = GL$

4. 将 $r(0^+)$, $r(\infty)$ 和 τ 代入三要素公式

(1) 求 $I(0^+), U(0^+)$

画 $0^-, 0^+$ 图

(2) 求 $I(\infty), U(\infty)$

画 ∞ 图

(3) 求 Γ

(4) 代入公式

计算 τ : 开关闭合，置零

$$\text{若 } R_{eq} \Rightarrow \tau = R_{eq} \cdot C = \frac{L}{R_{eq}}$$

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第八章 相量法

指物形式 → 三角函数

$$|A|e^{j\theta} = |A|\cos\theta + (|A|j)\sin\theta$$

改挂公式: $e^{j\pi} = -1 \quad e^{j\frac{\pi}{2}} = j$ 复数因子 $e^{j\theta}$ 逆向旋转 θ

$$e^{-j\frac{\pi}{2}} = -j \quad e^{j0^\circ} = 1 \quad \times J \frac{\pi}{2}$$

$$x(-J) + j - \frac{\pi}{2}$$

二、正弦量:

初相角

± 1 $\pm \pi$

$$i = \underline{I_m} \cdot \cos(\omega t + \varphi_i)$$

频率

I_m : 振幅 ω : 角频率 $|I_m| \leq 18^\circ$

$$\text{有效值: } I = \frac{\sqrt{2}}{2} I_m = 0.707 I_m$$

$$i_i = \underline{I} \cos(\omega t + \varphi_i)$$

① 正弦量之间的转化:

(角频率不变要求)

$$A = |A|e^{j\omega t} \quad i_i = \underline{I} \cos(\omega t + \varphi_i) \rightarrow i_i = \underline{|I|} \cos(\omega t + \varphi_i)$$

$$|A| < 0$$

相量法

正弦量

幅值

最大值

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3. 相序、滞后

$$\varphi_1 - \varphi_2 > 0 \quad \text{超前 2}$$

< - 滞后

$$|\varphi_1 - \varphi_2| = \frac{\pi}{2} \quad \text{正交}$$

$$|\varphi_1 - \varphi_2| = \pi \quad \text{反相}$$

4. 相量表示 U, I

$$i = U_s \angle \varphi_s \quad \text{幅相}$$

$$i = I \angle \varphi_i$$

2. 电路定理的相量形式

$$KCL: \sum I = 0$$

$$KVL: \sum u = 0$$

$$\text{电阻: } U_R = R \cdot I_R$$

$$\text{电感: } U_L = j\omega L \cdot I_L$$

$$\text{电容: } U_C = \frac{1}{j\omega C} I_C \\ = -j \cdot \frac{1}{\omega C} I_C$$

$$\text{感抗 } X_L = \omega L = 2\pi f L$$

$$\text{容抗 } X_C = -\frac{1}{\omega C} = -\frac{1}{2\pi f C}$$

$$U_R = R \cdot I_R$$

$$U_L = \omega L \cdot I_L$$

$$\bar{U}_i = \bar{I}_i$$

$$\bar{U}_u - \bar{U}_i = \frac{\pi}{2}$$

互感

$$U_C = \frac{1}{j\omega C} I_C$$

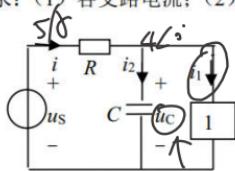
$$\bar{U}_u - \bar{U}_i = -\frac{\pi}{2}$$

互感

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5. 已知图中 $u_s = 25\sqrt{2} \cos(10^6 t - 126.87^\circ) V$, $u_C = 20\sqrt{2} \cos(10^6 t - 90^\circ) V$, $R = 3\Omega$, $C = 0.2\mu F$.

求：(1) 各支路电流；(2) 框 1 可能是什么元件？(注： $\cos 53.13^\circ = 0.6$)



电感

找电流与电压

同相位

(π - 37°)

$$(1), U_C = \int_0^t i(t) dt$$

$$i(t) = \frac{dU_C}{dt} = \int_0^t \omega C \cdot U_C$$

$$= 0.2 \times 10^{-6} \times 10^6 \times 20\sqrt{2} \cos(10^6 t - 90^\circ) V$$

$$= 4\sqrt{2} \cos(10^6 t) V = (4 \angle 0^\circ)$$

$$U_R = U_s - U_C$$

$$= 25 \angle -126.87^\circ - 20 \angle -90^\circ$$

$$= 25(0.6 - \sqrt{2}/2) - 20(0 - \sqrt{2}/2)$$

$$= (15) V \quad i = \frac{15V}{3\Omega} = (5) A$$

$$U_1 = i - U_2$$

$$= -9 V$$

负负 ⇒ 正正

相同相位

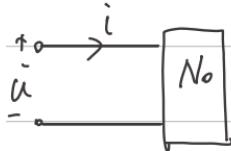
$$i_R = 3\Omega \cos(10^6 t \pm 18^\circ)$$

$$i_1 = 9\Omega \cos(10^6 t \pm 18^\circ)$$

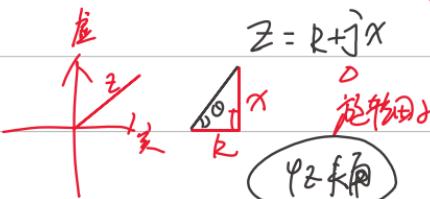
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第6章：正弦稳态电路的分析：

- 阻抗和导纳：



$$\text{阻抗 } Z = \frac{u}{i} = \frac{u}{I} \angle \varphi_u - \varphi_i = \frac{u}{I} \angle \varphi_Z$$



$$\frac{u}{I} = \sqrt{R^2 + X^2}$$

$$\tan \theta = \frac{X}{R}$$

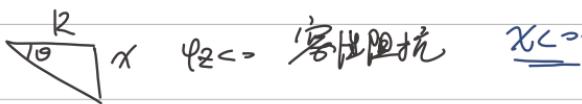
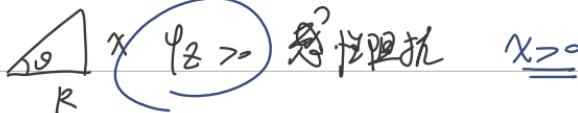
$$\varphi_Z = \arctan \left(\frac{X}{R} \right)$$

$$Z_R = \frac{u}{I} = R \rightarrow X=0$$

$$Z_L = j\omega L \quad Z_C = -j\frac{1}{\omega C} \rightarrow X^2 = \frac{1}{\omega^2 C^2}$$

Z

$$X = \omega L$$



$$\text{由 } Y = \frac{i}{u} \quad \text{导纳: } Y = \frac{i}{u} = |Y| \angle \varphi_Z$$

$$Y = G + jB$$

$$\text{电阻 } Y_R = \frac{1}{R}$$

$B > 0$ 时 容性电纳

$$\text{电容: } Y_C = \frac{1}{j\omega L} = -j\frac{1}{\omega L}$$

$B < 0$ 时 感性电纳

$$\text{电感: } Y_L = j\omega C$$

日期:

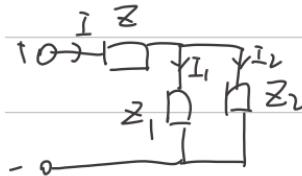
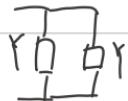
第5章 电阻元件

导纳与阻抗关系:

$$|Z| |Y| = 1$$

2 中性点接法的等效电路图

$$Y_2 + Y_3 = 0$$



$$Z_{eq} = Z + Z_1 \parallel Z_2 = Z + \frac{Z_1 Z_2}{Z_1 + Z_2}$$

二、正弦稳态电路的功率:

单位: W

有功功率: $P = UI \cos \varphi_Z$

($\Phi_Z = \Phi_U - \Phi_I$)

无功功率: 感性

$\cos \varphi_Z \Rightarrow$ 电能消耗

无功功率: $(\varphi_Z = \varphi_U - \varphi_I)$

$$\therefore P = S \lambda$$

2. 视在功率: 单位 VAR

$$Q = UI \sin \varphi_Z = S \cdot \underline{\sin \varphi_Z}$$

3. 视在功率 单位 VA

$$S = UI \quad S = \sqrt{P^2 + Q^2}$$

$$Z = R + jX \quad i = \begin{pmatrix} i_R \\ i_X \end{pmatrix}$$

$$P = UI \cos \varphi_Z = I^2 R = I \cdot U_R \quad | \quad U_R = U \cdot \underline{\cos \varphi_Z} \quad U_R \text{ 有功分量}$$

$$Q = UI \sin \varphi_Z = I^2 X = I \cdot U_X \quad | \quad U_X = U \cdot \underline{\sin \varphi_Z} \quad U_X \text{ 无功分量}$$

日期: /

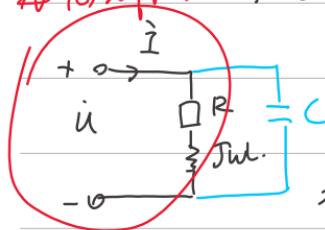
4. 复功率

$$\begin{aligned} \bar{S} &= u \cdot i^* = u \cdot i \angle \varphi_u \angle i^* = u \cdot i \cdot \cos \varphi + j \cdot u \cdot i \sin \varphi \\ &= P + j Q \end{aligned}$$

R	P	Q	\bar{S}
$I^2 R$	0	$I^2 R$	
L	0		$I^2 wL = \frac{U^2}{wL}$
C	0		$J Q_L$

$$-wCU^2 = -\frac{I^2}{wC} \quad J Q_C$$

④ 无功补偿: 提高功率因数: 同并联电容器办法.



$$\lambda_1 = 0.6 \rightarrow \lambda = 0.9$$

功率因数: $\bar{S} = \bar{S}_1 + \bar{S}_C$

$$\left. \begin{array}{l} S \cdot \cos \varphi_2 = S_1 \cdot \cos \varphi_2 + 0 \\ S \cdot \sin \varphi_2 = S_1 \cdot \sin \varphi_2 - wCU^2 \end{array} \right\} \quad \text{①}$$

$$\therefore \frac{\textcircled{2}}{\textcircled{1}} \Rightarrow C = \frac{P_1}{wU^2} (-\tan \varphi_2 - \tan \varphi_{2u})$$

$$\varphi_2 = \arccos \lambda$$

$$\varphi_{2u} = \arccos \lambda_1$$

日期: /

第十三章、二端口网络:

(1) 用电压表示电流:

Y参数方程(即等效内阻方程)

$$\begin{cases} i_1 = Y_{11}U_1 + Y_{12}U_2 \\ i_2 = Y_{21}U_1 + Y_{22}U_2 \end{cases}$$

写成矩阵形式 $\begin{bmatrix} i_1 \\ i_2 \end{bmatrix} = \begin{bmatrix} Y_{11} & Y_{12} \\ Y_{21} & Y_{22} \end{bmatrix} \begin{bmatrix} U_1 \\ U_2 \end{bmatrix}$

$$Y_{11}: \frac{i_1}{U_1} \Big|_{U_2=0} \text{ 转换等效}$$

$$Y_{21}: \frac{i_2}{U_1} \Big|_{U_2=0} \text{ 转换等效}$$

$$Y_{12}: \frac{i_1}{U_2} \Big|_{U_1=0} \text{ 转换等效}$$

$$Y_{22}: \frac{i_2}{U_2} \Big|_{U_1=0} \text{ 转换等效}$$

其中 $[Y] = \begin{bmatrix} Y_{11} & Y_{12} \\ Y_{21} & Y_{22} \end{bmatrix}$

\uparrow
Y参数矩阵

$$[Y] = \begin{bmatrix} Y_a + Y_b & -Y_L \\ -Y_b & Y_b + Y_L \end{bmatrix}$$

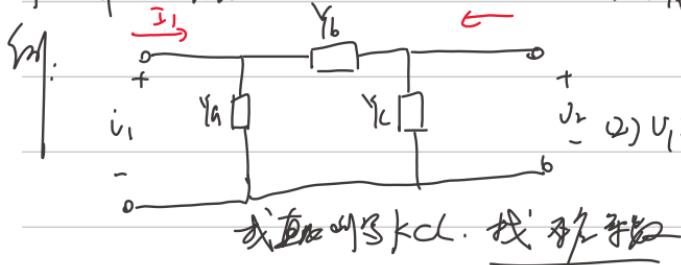
注: 互易 = 对称: $Y_{12} = Y_{21}$

对称二端口: $\begin{cases} Y_{12} = Y_{21} \\ Y_{11} = Y_{22} \end{cases}$

由互易性 $\frac{X}{V}$ (互换对称).

短路外特性.

求二端口的Y参数:



$$Y_{11} = \frac{I_1}{U_1} = Y_a + Y_b$$

$$Y_{21} = \frac{I_2}{U_1} = -Y_b$$

$$Y_{12} = \frac{I_1}{U_2} \Big|_{U_1=0} = -Y_b$$

$$Y_{22} = \frac{I_2}{U_2} \Big|_{U_1=0} = Y_b + Y_c$$

日期: /

(2) 用电流表表示:

三端口方程 (即阻抗参数方程)

$$\begin{cases} U_1 = Z_{11} \cdot I_1 + Z_{12} \cdot I_2 \\ U_2 = Z_{21} \cdot I_1 + Z_{22} \cdot I_2 \end{cases}$$

矩阵形式: $\begin{bmatrix} U_1 \\ U_2 \end{bmatrix} = \begin{bmatrix} Z_{11} & Z_{12} \\ Z_{21} & Z_{22} \end{bmatrix} \begin{bmatrix} I_1 \\ I_2 \end{bmatrix}$

$$Z_{11} = \frac{U_1}{I_1} \Big|_{I_2=0} \quad \text{输入阻抗}$$

$$Z_{21} = \frac{U_2}{I_1} \Big|_{I_2=0} \quad \text{转移阻抗}$$

$$Z_{12} = \frac{U_1}{I_2} \Big|_{I_1=0} \quad \text{转移阻抗}$$

阻抗矩阵
↓
 $= [Z] \begin{bmatrix} I_1 \\ I_2 \end{bmatrix}$

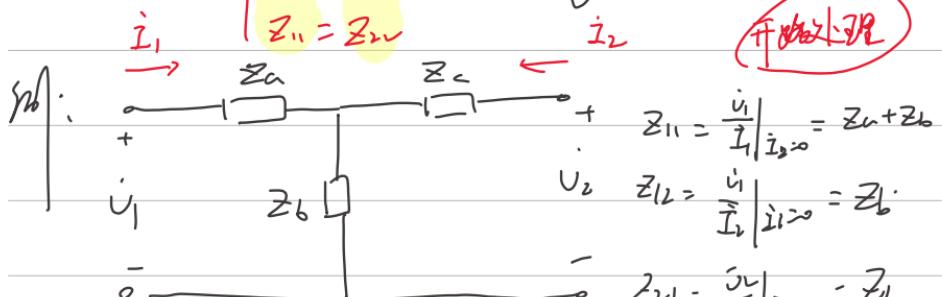
$$[Z] = [Y]^{-1}$$

$$Z_{21} = \frac{U_2}{I_1} \Big|_{I_2=0} \quad \text{输入阻抗}$$

$$[Z] = \begin{bmatrix} Z_a + Z_b & Z_b \\ Z_b & Z_b + Z_c \end{bmatrix}$$

注: 端口 = 端口: $Z_{12} = Z_{21}$

对称二端口: $\begin{cases} Z_{12} = Z_{21} \\ Z_{11} = Z_{22} \end{cases}$ 由对称 $\xrightarrow{\quad} \xleftarrow{\quad}$ (对称形式)



$$Z_{11} = \frac{U_1}{I_1} \Big|_{I_2=0} = Z_a + Z_b$$

$$Z_{12} = \frac{U_1}{I_2} \Big|_{I_1=0} = Z_b$$

$$Z_{21} = \frac{U_2}{I_1} \Big|_{I_2=0} = Z_b$$

$$Z_{22} = \frac{U_2}{I_2} \Big|_{I_1=0} = Z_b + Z_c$$

日期: / /

H 混合微分方程: 质量: i_1, i_2

$$i_1 = \dots -$$

$$i_2 = \dots -$$

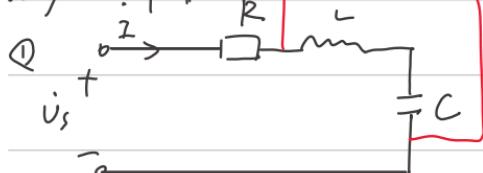
T 微分方程组:

$$i_1 = \dots -$$

$$i_2 = \dots -$$

日期: /

谐振 (串联并联)



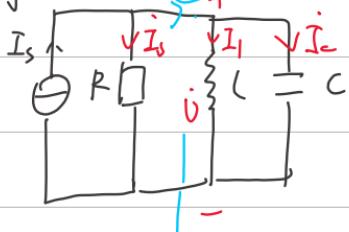
相干于谐振。

$$Z_{eq} = R + j\omega L + \frac{1}{j\omega C} = R + j\omega L - j\frac{1}{\omega C} = R + j(\omega L - \frac{1}{\omega C})$$

若虚部为0. 即 $\omega L - \frac{1}{\omega C} = 0 \Rightarrow \omega^2 = \frac{1}{LC}$ 成立. 则 | 谐振

$$\therefore I = \frac{Us}{Z_{eq}} = \frac{Us}{R + j(\omega L - \frac{1}{\omega C})} = \frac{Us}{R}$$

② 并联谐振 开路



$$Y = \frac{1}{R} + \frac{j}{\omega L} + \frac{1}{j\omega C}$$

$$= \frac{1}{R} + j\frac{1}{\omega C} - j\frac{1}{\omega L}$$

$$= \frac{1}{R} + j(\frac{1}{\omega C} - \frac{1}{\omega L})$$

虚部为0

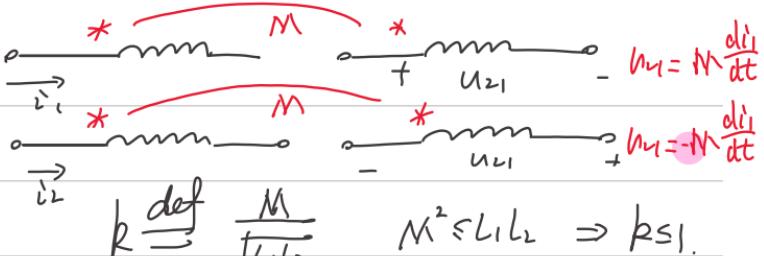
若 $\omega C - \frac{1}{\omega L} = 0 \Rightarrow \omega^2 = \frac{1}{LC}$ 成立 \Rightarrow

$$Y = \frac{1}{R} \quad / I_L = \frac{U}{j\omega L}, \quad I_C = \frac{U}{j\omega C} = Uj\omega C$$

$$I_L + I_C = jU(\frac{1}{\omega C} - \frac{1}{\omega L}) = 0$$

$$品质因数 Q = \frac{1}{R} \sqrt{\frac{L}{C}} (\text{或} \omega L)$$

日期:



耦合系数 k

$$k \stackrel{\text{def}}{=} \frac{M}{\sqrt{L_1 L_2}}$$

$$M^2 \leq L_1 L_2 \Rightarrow k \leq 1.$$

回路端:

时域: $u_1 = L_1 \cdot \frac{di_1}{dt} + M \frac{di_2}{dt}$

$u_2 = M \cdot \frac{di_1}{dt} + L_2 \frac{di_2}{dt}$

相量: $\begin{cases} u_1 = j\omega L_1 i_1 + j\omega M i_2 \\ u_2 = j\omega M i_1 + j\omega L_2 i_2 \end{cases}$

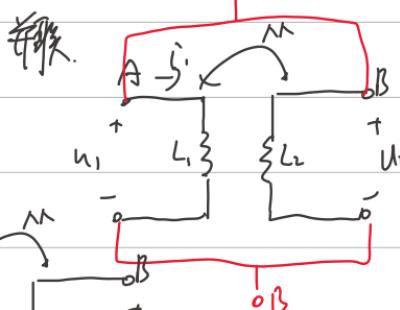
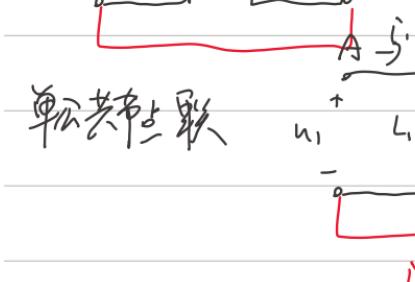
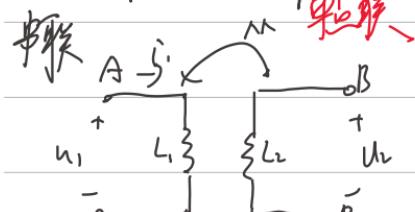
$u_1 = L_1 \frac{di_1}{dt} - M \frac{di_2}{dt}$

$u_2 = -M \frac{di_1}{dt} + L_2 \frac{di_2}{dt}$

$u_1 = L_1 \frac{di_1}{dt} + M \frac{di_2}{dt}$

$u_2 = -M \frac{di_1}{dt} - L_2 \frac{di_2}{dt}$

逐项去耦等效. { 串联
并联
单端形 }

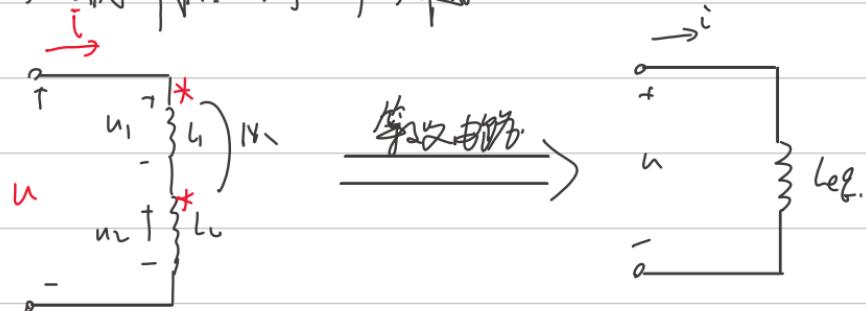


单端共地耦

$i_1 \downarrow o <$

日期: /

(1) 互感线圈的串联: 同名端必须连通



$$L_{eq} = L_1 + L_2 + 2M$$

$$\text{反}: L_{eq} = L_1 + L_2 - 2M > 0$$

如图 测量互感值，只测一次

$$M = \frac{L_{\text{互感}} - L_{\text{反}}}{4}$$

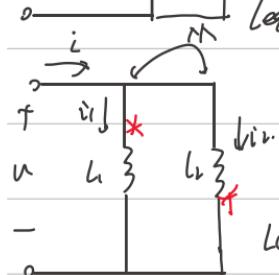
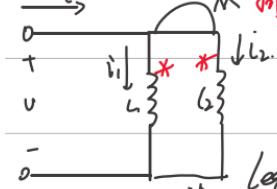
$$\text{全耦合: } M = \sqrt{L_1 L_2}$$

$\because L_1 = L_2 = L$ 且 $M = L$.

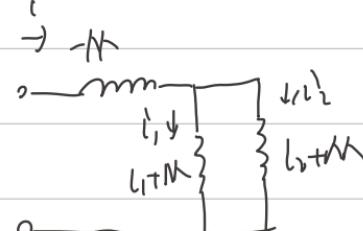
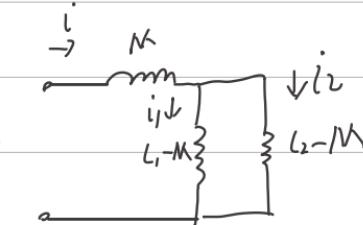
$$L_{eq} = \begin{cases} 4M & \text{同名端} \\ 0 & \text{反} \end{cases}$$

(2) 互感线圈的并联:

同名端同向



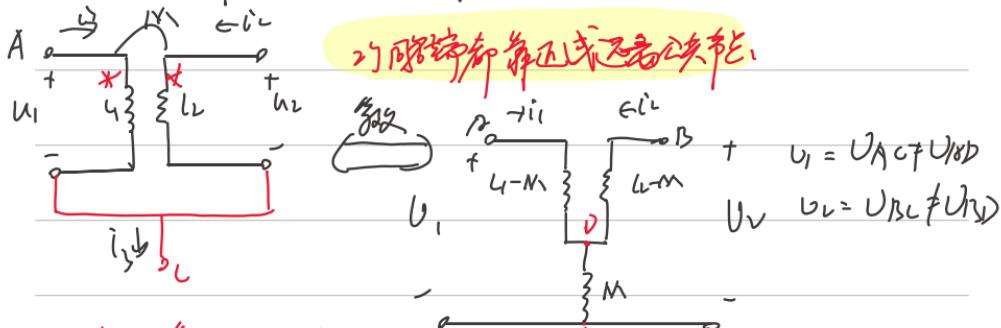
$$L_{eq} = \frac{(L_1 L_2 - M^2)}{L_1 + L_2 - 2M}$$



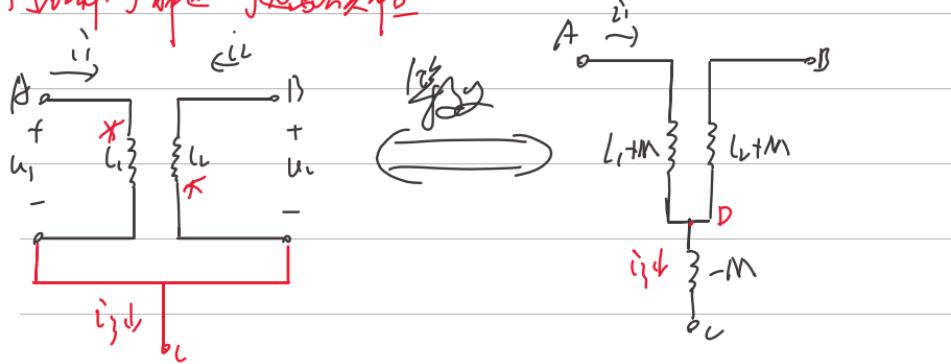
$$L_{eq} = \frac{L_1 L_2 - M^2}{L_1 + L_2 + 2M}$$

日期: /

(3) 有一个公共节点, 继续依圆周去耦等效电路:



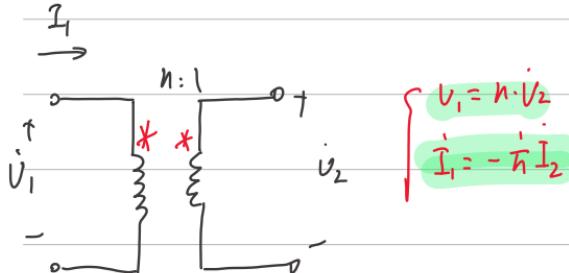
同右端→靠近→形成公共节点



日期: /

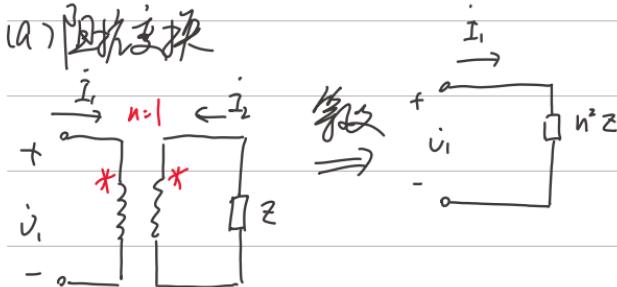
空心变压器: 引入阻抗 $Z_L = \frac{(LWM)^2}{Z_{L2}}$

理想变压器:



理想变压器的性质:

(a) 阻抗变换



$$\frac{U_1}{I_1} = \frac{n U_2}{-n I_2} = n^2 \left(-\frac{U_2}{I_2} \right) = n^2 \cdot Z$$

(b) 功率消耗:

$$P = U_1 i_1 + U_2 i_2 = n U_2 \cdot (-\frac{1}{n} i_2) + U_2 i_2 = 0$$

∴ 理想变压器既不能能，也不能耗能。

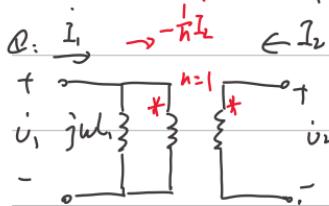
在电路中只起传递信号和能量的作用。

日期: /

全耦合变压器 转换成理想变压器

$$① \left\{ \begin{array}{l} \dot{U}_1 = n \dot{U}_2 \\ \dot{I}_1 = \frac{\dot{U}_1}{j\omega L_1} - \frac{1}{n} \dot{I}_2 \end{array} \right.$$

$$\left\{ \begin{array}{l} \dot{U}_2 = \frac{1}{n} \dot{U}_1 \\ \dot{I}_2 = \frac{\dot{U}_2}{j\omega L_2} - n \dot{I}_1 \end{array} \right.$$

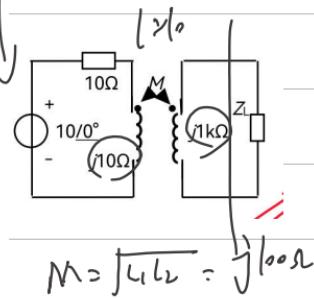


$$② \left\{ \begin{array}{l} \dot{U}_2 = \frac{1}{n} \dot{U}_1 \\ \dot{I}_2 = \frac{\dot{U}_2}{j\omega L_2} - n \dot{I}_1 \end{array} \right.$$



全耦合变压器: $M = \sqrt{L_1 L_2}$

$$n = \sqrt{\frac{U_2}{U_1}}$$



$$M = \sqrt{L_1 L_2} = \sqrt{100 \Omega}$$

41. 图 7-54 所示电路中变压器为全耦合变压器, Z_L 为何值获最大功率, 最大功率为多少?

答: 把全耦合变压器等效为如图 7-55 所示理想变压器模型。其中

$$n = \sqrt{\frac{L_2}{L_1}} = \sqrt{\frac{\omega L_2}{\omega L_1}} = \sqrt{\frac{1000}{10}} = 10$$

(1) 求 \dot{U}_{oc} 。因为 $\dot{i}_z = 0$, 所以 $\dot{i}_1 = n \dot{i}_z = 0$ 。

分压公式

$$\dot{U}_1 = \frac{j10}{10 + j10} \dot{U}_s = \frac{j10}{10 + j10} 10 \angle 0^\circ = 5\sqrt{2} \angle 45^\circ \text{V}$$

$$\dot{U}_{oc} = \dot{U}_2 |_{i_z=0} = 10 \dot{U}_1 = 50\sqrt{2} \angle 45^\circ \text{V}$$

(2) 求 Z_0 。把初级阻抗折合到次级

$$Z_0 = n^2 (10/j10) = 500\sqrt{2} \angle 45^\circ \Omega = 500 + j500 \Omega$$

144

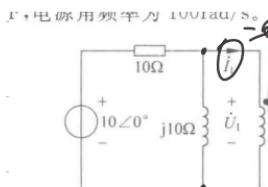


图 7-55 解题 41 图

$$\begin{aligned} \dot{U}_1 &= 5\sqrt{2} \angle 45^\circ \\ \dot{U}_L &= 10\dot{U}_1 = 50\sqrt{2} \angle 45^\circ \text{V} \\ n^2 (10/j10) &= Z_0 \\ Z_L &= Z_0 \quad \Rightarrow P = \frac{|U_L|^2}{4R} \end{aligned}$$

日期： /

耦合变压器的去耦等效：①端⇒三端

这里， $R=1$ ，即 $IV = \sqrt{L_1 L_2}$ ； $L_1 \neq \infty$ ， $n = \sqrt{L_1 / L_2}$ 。

耦合变压器也可以进行 T 型去耦等效变换，只要把变压器的两个负极连接起来看即可，如图 7-8 所示。注意，不能把变压器的两个正极连接在一起。

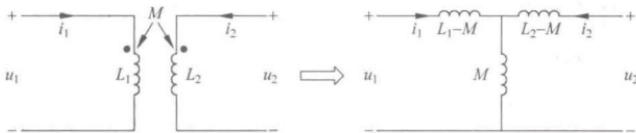
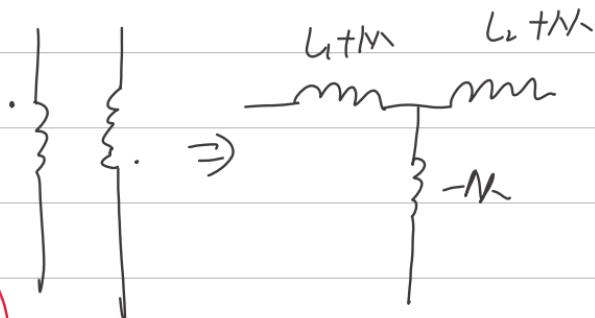


图 7-8 耦合变压器的去耦等效变换

⇒ 同名端在左



品质因数：

$$Q = \frac{1}{R} \sqrt{\frac{L}{C}} = \frac{w_o L}{R} = \frac{1}{w_o R C}$$

$$= \frac{X_L}{R} = \frac{X_C}{R}$$

$$\underline{X_L = X_C}$$