

Recap:

- $p = f(\theta_1, \theta_2)$

$$\begin{bmatrix} \dot{x} \\ \dot{y} \end{bmatrix} = \begin{bmatrix} \quad \quad \end{bmatrix} \begin{bmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \end{bmatrix}$$

\searrow
 J_v

- dimensions of J_v : $(3 \times n)$
 $n \rightarrow$ degrees of freedom.

- differentiate position $\dot{p} = J_v \dot{\theta}$ to get velocity Jacobian.

- if singular configuration,
 $\det(J) = 0$

$$\Rightarrow \dot{\theta} = J^{-1} \dot{p}$$

\Rightarrow infinity.

SINGULARITIES

- i) wrist singularity
- ii) elbow singularity
- iii) shoulder singularity

\rightarrow in singularity, joint space velocity is ∞ theoretically

STATICS

• study of forces acting on the body without any motion (or acceleration)

• torque : $\vec{\tau} = \vec{r} \times \vec{F}$ (rotational equivalent of force)

• mechanical power : $P = \frac{W}{t}$

for linear motion, $P = \frac{Fd}{t} = \underline{\underline{F \cdot v}}$

PRINCIPLE OF CONSERVATION OF POWERS:

power at joints = power to move robot +
(power at end effector)

Because of statics, power to move robot = 0

\Rightarrow power at joints = power at end-effector

now, power at joints = $\vec{\tau}^T \dot{\theta}$
power at end-effector = $\vec{F}^T \vec{v}$

Thus, $\vec{\tau}^T \dot{\theta} = \vec{F}^T \vec{v}$

$$\vec{\tau}^T \dot{\theta} = \vec{F}^T \vec{J}_v \dot{\theta}$$

$$[\vec{v} = \vec{J}_v \dot{\theta}]$$

$$\vec{\tau}^T = \vec{J}_v^T \vec{F}^T$$

$$\boxed{\vec{\tau} = \vec{J}_v^T \vec{F}}$$

if it jiggles when she walks,
i listen when she talks.

$$\text{Thus, } \vec{\tau} = \vec{J}_v^T \vec{F}$$

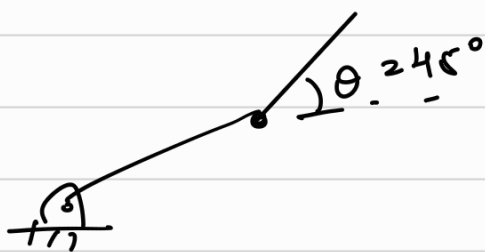
Test 1
Test 2

The quick brown fox
jumped over the lazy dog

- humanoids have non-singular Jacobians for walking because of manipulability ellipsoid.

eg -

(1) 2R planar



$$\theta_1 = 0^\circ, \quad \theta_2 = 45^\circ,$$

$$F_y = -1\text{N}$$

$$l_1 = l_2 = 1$$

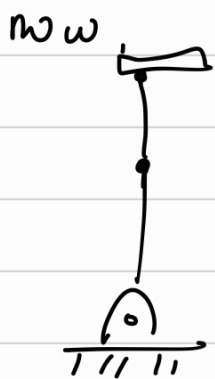
$$F = \begin{bmatrix} 0 \\ -1 \end{bmatrix} \quad \hat{c} = J^T F$$

$$\text{now } J_0 = \begin{bmatrix} -l_1 s\theta_1 - l_2 s\theta_{12} & -l_2 s\theta_{12} \\ l_1 c\theta_1 + l_2 c\theta_{12} & l_2 c\theta_{12} \end{bmatrix}$$

$$= \begin{bmatrix} -1/\sqrt{2} & -1/\sqrt{2} \\ (1 + 1/\sqrt{2}) & 1/\sqrt{2} \end{bmatrix}$$

$$J_0^T = \begin{bmatrix} -1/\sqrt{2} & (1 + 1/\sqrt{2}) \\ -1/\sqrt{2} & 1/\sqrt{2} \end{bmatrix}$$

$$\text{Thus, } \hat{c} = J_0^T F$$



$\rightarrow \dot{\mathcal{L}} = 0$ (singular configuration)

- For a spatial manipulator, use a full Jacobian matrix.

$$\mathbf{F} = \mathbf{J}^{-T} \dot{\mathcal{L}}$$

- velocity ellipsoid is \perp to configuration while force ellipsoid is in the direction.

\rightarrow Trajectory: path parameterized wrt time t .

Motion planning: finding robot's motion from a start position to an end position.

Path planning: finding a collision-free path from initial to final configuration.

$$\theta(s) : [0, 1] \rightarrow \Theta$$

$$\begin{aligned} \text{When } s=0 &\Rightarrow \theta(0) : \theta_{\text{initial}} \\ s=1 &\Rightarrow \theta(1) : \theta_{\text{final}} \end{aligned}$$

- linear motion in task space will have non-linear motion in joint space (and vice-versa)

- if we take linear motion in task space \Rightarrow velocity and acceleration will be non-linear
- to have smooth velocity & acceleration \Rightarrow cubic polynomial.

Let : $p_0 = (x_0, y_0)$
 $p_f = (x_f, y_f)$

$$p_s = (x(s), y(s))$$

$$\Rightarrow p(s) = (1-s) p_0 + s p_f$$

- When doing linear configuration, the intermediate points may be out of the reachable workspace.

- To satisfy n constraints, we need to consider ' n ' independent coefficients.

Say, $s(t) = a_0 + a_1 t + a_2 t^2 + a_3 t^3$
 $\dot{s}(t) = a_1 + 2a_2 t + 3a_3 t^2$

$$s(t_0) ; s(t_f) ; \dot{s}(t_0) = 0 ; \dot{s}(t_f) = 0$$

$$= n \quad = n_f$$

Now, $s(0) = a_0$ (initial posⁿ)
 $\dot{s}(0) = a_1$

$$s(t_f) = \quad ; \quad \dot{s}(t_f) =$$

- no. of constraints = 6 (considering acceleration & velocity constraints)

$$\Rightarrow \text{order of polynomial} = 6 - 1 = 5$$

you physically only feel acceleration
that's why you want to keep it smooth.
But just that your soul shudders.

- $\det(M) = -4(t_f - t_0)^9$

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