

Distance and curvature

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1 Normals and curvature

There is a deep link between the evolution of the normal along a curve and the curvature.

Let C be a planar curve. To define the curvature at a point, we can consider the case of a straight line. We can admit that in this case the curvature is zero along the line. For a portion of a circle, the curvature is defined to be inversely proportional to the radius of the circle:

$$\kappa = \frac{1}{R} \quad (1)$$

More precisely, for any curve, we can locally approximate a sufficiently regular curve (\mathcal{C}^2 is enough) at a point by a circle that best approximates it locally (see Fig. 1. This circle is tangent to C and is called an *osculating circle*. The radius of this circle defines the curvature.

Another way to define the curvature is to consider a point moving at a constant speed along the curve C . The variation of the tangent vector along the curve defines the curvature. This is equivalent to specifying the acceleration of the point.

$$\kappa = \frac{d\mathbf{T}}{ds}, \quad (2)$$

where s is a parametrisation of the curve. Both definition of the curvature are in fact equivalent (see Fig. 2).

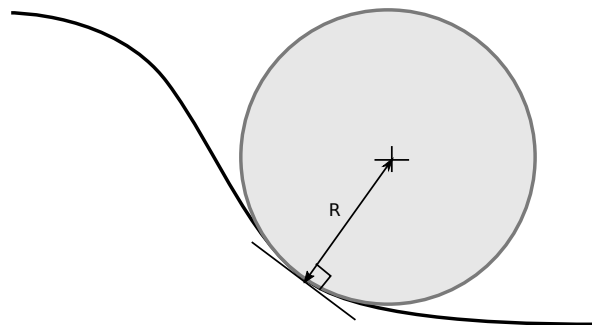


Figure 1: The notion of an osculating circle (best local approximation) defines the curvature as the inverse of the radius of the circle.

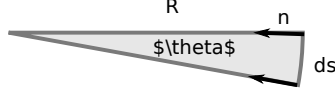


Figure 2: We can write $\sin d\theta \approx d\theta = \frac{ds}{R}$. As ds tends to zero, we have $R = \frac{d\theta}{ds} = \frac{d\mathbf{T}}{ds}$.

Parametrisation

Let $\gamma(t)$ be a parametrisation of the curve C , i.e.

$$\gamma(t) = (x(t), y(t)) \quad (3)$$

This defines the position of a point on the curve over time. We assume an injective parametrisation, i.e. such that the speed $\gamma'(t)$ is never zero. This means

$$\forall t, \|\gamma'(t)\|^2 = x'(t)^2 + y'(t)^2 > 0 \quad (4)$$

In this case, we can re-parametrise the curve with curvilinear abscissa s in such a way that the speed is constant and equal to one.

$$\forall s, \gamma'(s)^2 = x'(s)^2 + y'(s)^2 = 1 \quad (5)$$

In this parametrisation, γ' is the unit tangent velocity vector \mathbf{T} . If \mathbf{N} is the unit normal vector to the curve, we have

$$\mathbf{T}'(s) = \kappa(s)\mathbf{N}(s) \quad (6)$$

We note that instead of deriving the unit tangent vector, we can also consider deriving the unit normal vector. This is because \mathbf{N} is \mathbf{T} rotated by $\frac{\pi}{2}$, i.e. $\mathbf{N}(x, y) = (-y'(s), x'(s))$. This yields

$$\mathbf{N}'(s) = \kappa(s)\mathbf{T}(s) \quad (7)$$

We will make use of that fact in the next section.

Level sets

In imaging it can be difficult to represent a parametric curve because of discretization effects. It is common to represent it by a *level set* (see Fig. 3).

Let $\phi(x, y)$ be a \mathcal{C}^2 function in a domain Ω . We define the curve Γ as the zero-level-set of this function

$$\Gamma = \{(x, y), \phi(x, y) = 0\} \quad (8)$$

Γ is a set and no longer a parametrized curve, however we can manipulate it by working on the underlying ϕ function. This is the main idea behind the level-set method [?].

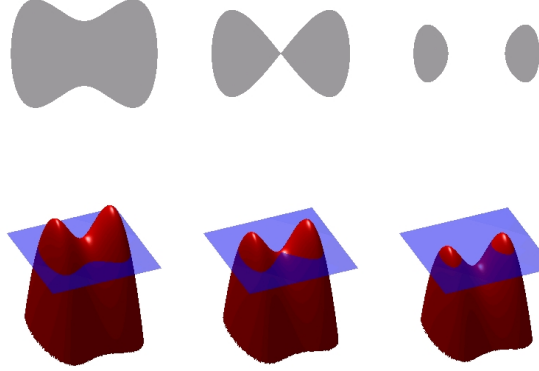


Figure 3: Representing a curve by a level set.

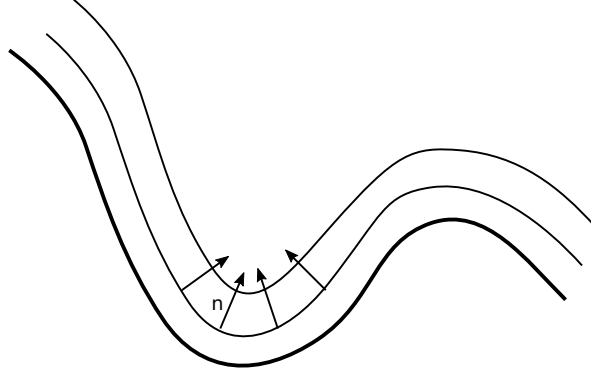


Figure 4: The faster the normal evolves along a curve, the higher the curvature.

Level sets and curvature

Curvature is easy to define in the level set case. For any point (x, y) in Ω , $\nabla\phi(x, y)$ is the gradient at (x, y) . If we consider the level-set at $(x, y, \phi(x, y))$, i.e. the curve that passes through (x, y) at level $\phi(x, y)$, then $\nabla\phi(x, y)$ is the normal vector to this curve at (x, y) . The unit normal is given by

$$\mathbf{n}(x, y) = \frac{\nabla\phi}{|\nabla\phi|}(x, y) \quad (9)$$

The curvature is given by the derivative of this expression. However this is a multidimensional derivative. Since $\nabla\phi$ is a vector, we must use the divergence operator:

$$\kappa = \nabla \cdot \frac{\nabla\phi}{|\nabla\phi|} \quad (10)$$

This is in particular true for the computation of the curvature of Γ .

2 Application to our problem

We want to define how to sample a segment p_1p_2 so that checking at each sampling point if it is located outside the perfusion territory, we can conclude the segment belongs inside the territory or not. The number of checking ($n + 1$), shall be optimized in order to avoid too many tests (minimize computation time) but also to guarantee the result with a tolerance reasonable enough (maximize test accuracy).

2.1 First approach

We can estimate n , the number of tests along the segment, from:

$$n \propto \frac{|p_1 - p_0|}{R} \quad (11)$$

R is an approximation of the local curvature along the segment by estimating the divergence at each point p_1 and p_2 , called R_1 and R_2 respectively :

$$R = \max(|R_1|, |R_2|) \quad (12)$$

The figure 5 illustrates the relationship between $D = |p_1 - p_0|$, R_1 , R_2 and n .

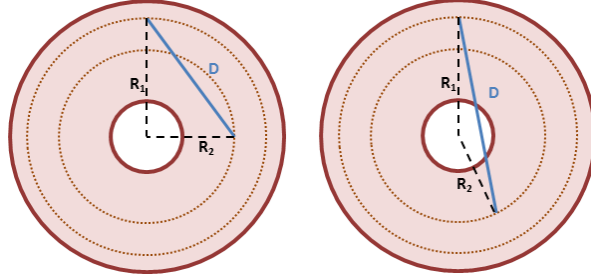


Figure 5: When D gets bigger relatively to $\max(|R_1|, |R_2|)$, the value of n is also higher to detect if the segment crosses the perfusion territory.

The divergence of a continuously differentiable vector field ω is equal to the scalar value function:

$$\text{div}(\omega) = \left(\frac{\partial}{\partial x}, \frac{\partial}{\partial y} \right) \cdot (\omega_x, \omega_y) \quad (13)$$

$$\text{div}(\omega) = (\omega_x(x, y) - \omega_x(x - 1, y)) + (\omega_y(x, y) - \omega_y(x, y - 1)) \quad (14)$$

with

$$\omega_x = \nabla_x \omega = \omega(x + 1, y) - \omega(x, y) \quad (15)$$

and

$$\omega_y = \nabla_y \omega = \omega(x, y + 1) - \omega(x, y) \quad (16)$$

2.2 Second approach

We are in the case of measuring the curvature along a segment, so we could use the segment information within an iterative process.

2.2.1 Interpolating the point along the segment line that crosses the concavity

We calculate the distances λ_i that solves:

$$\omega(p_1) + \lambda_1 \frac{\langle \nabla \omega(p_1), p_1 p_2 \rangle}{\|p_1 p_2\|} = 0 \quad (17)$$

$$\omega(p_2) + \lambda_2 \frac{\langle \nabla \omega(p_2), p_2 p_1 \rangle}{\|p_1 p_2\|} = 0 \quad (18)$$

Then we select:

$$\lambda = \min(\lambda_1, \lambda_2) \quad (19)$$

to obtain :

$$n = \left\lceil \frac{1}{\lambda} \right\rceil \quad (20)$$

If $\lambda > 1$ it means the line $p_1 p_2$ crosses the concavity outside of the segment $p_1 p_2$. We would approximate that there is actually no need of computing test along the segment. But we have to keep in mind that this interpretation comes only from a local approximation.

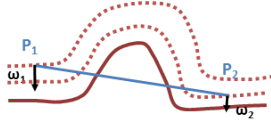


Figure 6: Specific situation where the local gradient doesn't help detecting the concavity.

Also, this method would fail for any case where the dot product $\langle \nabla \omega(p_1), p_1 p_2 \rangle \simeq 0$, and in some specific situations such as the figure 2.2.1. Hence we need to define a global boundary:

$$n \geq \frac{\|p_1 p_2\|}{R_{max}} \quad (21)$$

with R_{max} the maximal curvature radius of both inner and outer surfaces.

Note: because of the segmentation, we might actually obtain R_{max} close to zero, hence it is necessary to consider a tolerance s so that

$$R_{max}^* = R_{max} + s \quad (22)$$

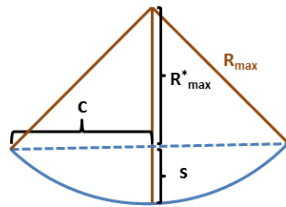


Figure 7: The maximally inscribed radius and tolerance s define a semi-cord c .

The semi-cord c defined by R_{max}^* and s is calculated as:

$$c = \sqrt{(R_{max}^* - s)^2 - R_{max}^2} \quad (23)$$

That can be simplified as:

$$c = \sqrt{R_{max}^2 - (R_{max} + s)^2} \quad (24)$$

The global boundary follows this tolerance:

$$n \geq \frac{\|p_1 p_2\|}{c} \quad (25)$$

We take the biggest n between maximal curvature and gradient method. This provides a robust sampling definition considering both local and global informations, see figure 2.2.1.

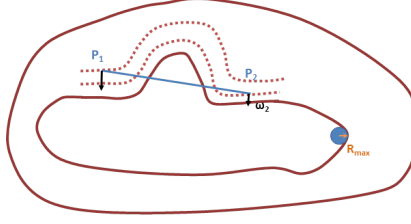


Figure 8: Specific situation where the local gradient doesn't help detecting the concavity.

2.2.2 Projecting Newton's method gradient result on the segment

If we want to find the first point along the gradient direction, starting from p_1 , that reaches the border of the perfusion territory we look for γ_1 that solves:

$$\omega(p_1) + \gamma_1 \Delta\omega = 0 \quad (26)$$

The gap of potential $\Delta\omega$ is calculated along the gradient:

$$\Delta\omega = \omega(p_1 + \nabla\omega(p_1)) - \omega(p_1) \quad (27)$$

The process is similar to calculate γ_2 from P_2 .

If $|\gamma_1|$ is small, p_1 is close to a concavity. Then we can use its projection on the segment $p_1 p_2$ to determine if the segment is how fast the segment is going toward the concavity.

$$d_{proj1} = \gamma_1 \frac{\langle \nabla\omega(p_1), p_1 p_2 \rangle}{\|p_1 p_2\|} \quad (28)$$

Similarly for the p_2 segment end, it would be calculated as:

$$\gamma_2 = -\frac{\omega(p_2)}{\omega(p_2 + \nabla\omega(p_2)) - \omega(p_2)} \quad (29)$$

and then

$$d_{proj2} = \gamma_2 \frac{\langle \nabla\omega(p_2), p_2 p_1 \rangle}{\|p_1 p_2\|} \quad (30)$$

If any of the d_{proj_i} is negative we know that the segment is locally going away from the concavity.

We select the smallest of the two sampling distance:

$$d_{proj} = \min(d_{proj1}, d_{proj2}) \quad (31)$$

The distance $|d_{proj}|$ is efficient to sample the segment, so n is defined as:

$$n = \left\lceil \frac{\|p_1 p_2\|}{|d_{proj}|} \right\rceil \quad (32)$$

We need to use the same boundaries than defined in 2.2.1.

These two methods are expected to be more accurate than the previous one 2.1, because they consider the potential along the segment (not only at the tips), but also both local and global curvatures. It will be interesting to compare these two last method.