## Results for ifipeout0.98: Crack Propagation Int. Pipe **Surface Flaw**

Author: edit file makereport3 to change

Affiliation:

Sun Jul 28 12:37:45 EDT 2013

Simulation input data:

**B=** 10.0 mm

 $r_i = 50$ . mm

 $a_0 = 0.5 \text{ mm}$ 

 $c_0 = 4.0 \text{ mm}$ 

#MATERIAL= merged\_a36\_fitted.html

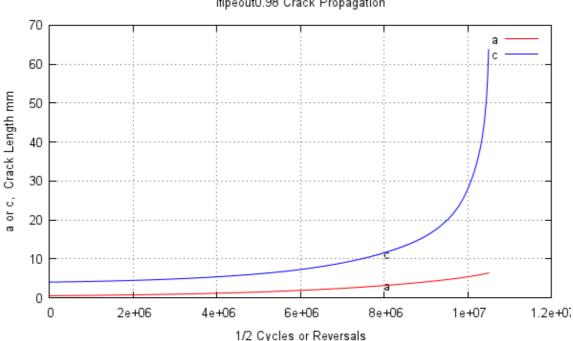
#TYPE= pipe\_inside\_surface\_flaw

#ACTIVATE\_MmMb= 1 \_\_\_\_\_#ACTIVATE\_MkmMkb= 0 \_\_\_\_\_#ACTIVATE\_fw= 0

#### **Crack Propagation Results:**

(#pipeIntSurfFlaw.f vers. 3.06

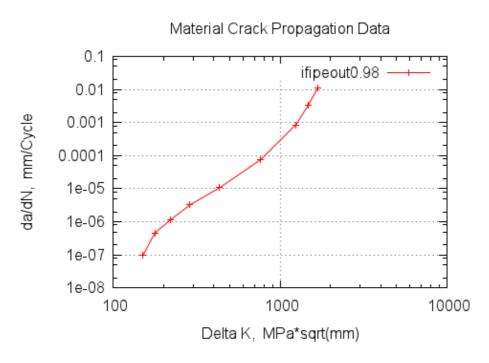
- No. of Reversals= 10501379 revs. or 5.25069e+06 cycles
- Final \_\_\_\_  $\mathbf{a} = 0.637E + 01 \text{ mm}$
- Final \_\_\_\_ c = 0.637E+02 mm
- No. of History Reps.= 750099 reps. + 7 revs.
- No. records = 10501380 in random access data file



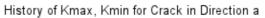
ifipeout0.98 Crack Propagation

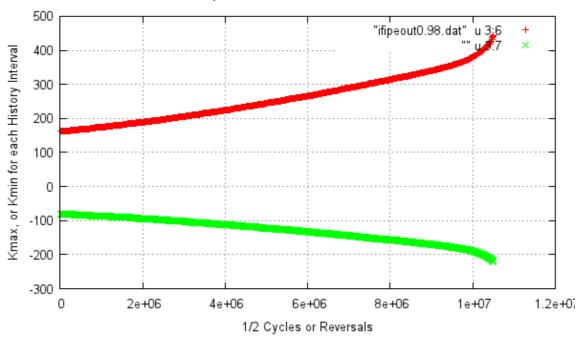
## Results for ifipeout0.98 : Crack Propagation Int. Pipe Surface Flaw



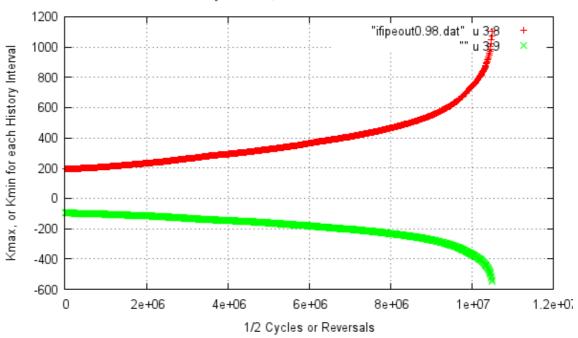


### Results for ifipeout0.98 : Crack Propagation Int. Pipe Surface Flaw

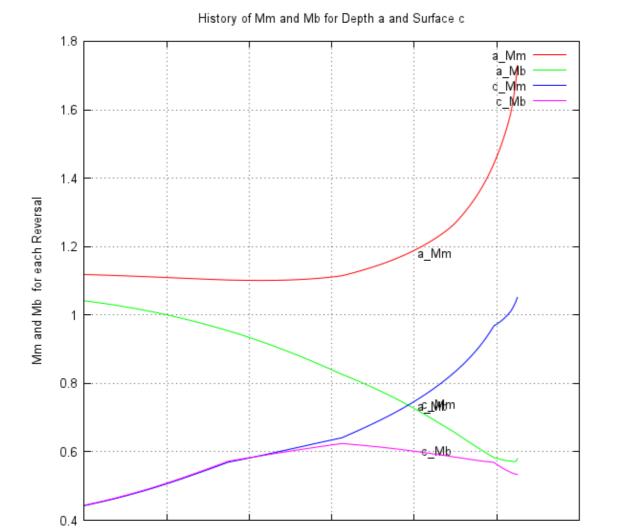




### History of Kmax, Kmin for Crack in Direction c



## Results for ifipeout0.98 : Crack Propagation Int. Pipe Surface Flaw



6e+06

1/2 Cycles or Reversals

8e+06

1e+07

1.2e+07

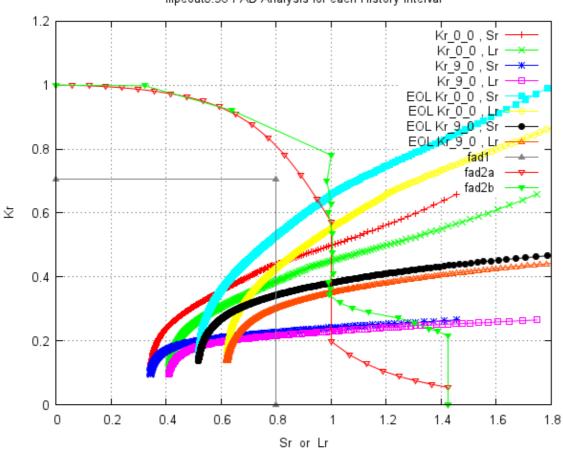
0

2e+06

4e+06

# FAD Results for ifipeout0.98 #TensileFile= a36\_Mattos\_mono\_engrSS\_FLAT.txt

#PmEOL= 70. #PbEOL= 100. #Kmat= 1675.



ifipeout0.98 FAD Analysis for each History Interval

# Crack Initiation Life Results for ifipeout0.98 (Assume Kt= 1.8 for welds)

Files Used:

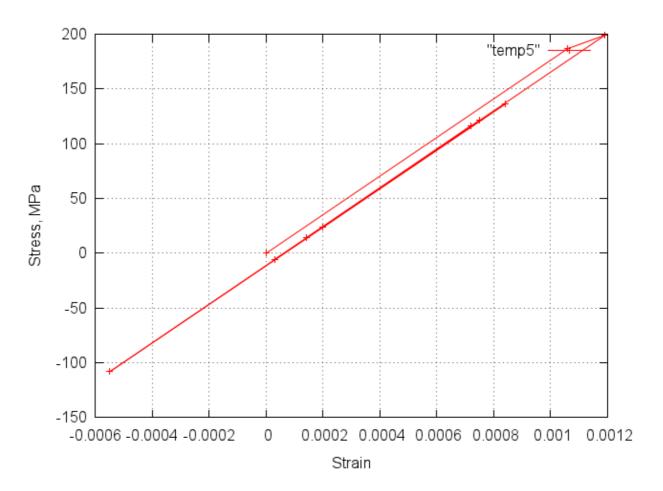
- Stress History (Sb+Sm)
- Rainflow File
- Material File

Loop	p Sma:	x Smin	N	Sigmax	Sigm	in De	lta Epsma	x Epsmin	DeltaEps	%Eps	%SWaT	%Sts	%Morr
1	219.6	-110.3	1.0	199.	-108.	307.	0.00119	00055	0.00174	0.0	0.0	0.0	0.0
2	152.3	-110.3	1.0	136.	-108.	244.	0.00084	00055	0.00139	0.0	0.0	0.0	0.0
3	152.3	-0.1	1.0	136.	-6.	142.	0.00084	0.00003	0.00080	0.0	0.0	0.0	0.0
4	131.2	20.9	2.0	117.	14.	103.	0.00072	0.00014	0.00058	0.0	0.0	0.0	0.0
5	136.4	31.5	2.0	121.	24.	98.	0.00075	0.00020	0.00055	0.0	0.0	0.0	0.0

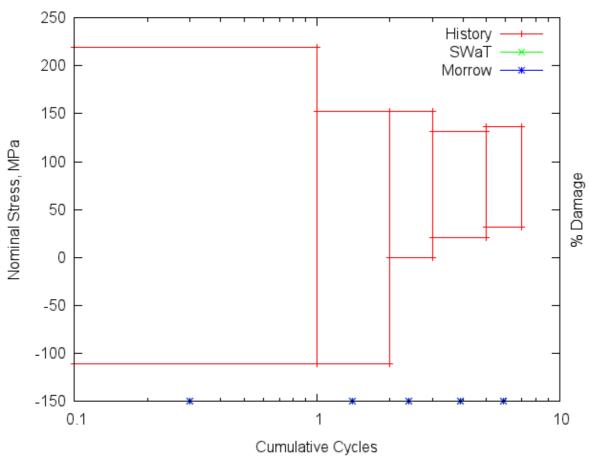
Predicted History Repetitions to Initiation:

StrainLife\_Reps SWaT\_Life\_Reps StressLife\_Reps Morrow\_Reps Goodman\_Reps (Reps= Repetions)
Infinity Infinity Infinity Infinity Infinity

## **Local Stress and Strain Response:**



## **Cumulative Cycle Plot of History and Damage:**



(Rectangles are Rainflow Cycle Sets: Sorted by Range: largest on Left)

## Appendix 1: Print of "pdprop.env" Simulation Control file

```
# This file contains the starting filenames, variables etc
# for the Crack Propagation programs. It should be edited by the
# user before each simulation run. It can also be generated from web
# page at: to be determined
#TYPE= pipe_inside_surface_flaw
                                   #with or without weld using ACTIVATEs:
#ACTIVATE_MmMb= 1 # Deactivate = 0
#ACTIVATE_MkmMkb= 0
                      # Set to off for inside surf. flaw.( not available )
                         Set to off for inside surf. flaw. (fw=1.0)
#ACTIVATE_fw=
                  0
                                #Other
                                           #TYPE= options:
                                # plate_surface_flaw
                                # plate_long_surface_flaw
                                 plate_tru_flaw
                                 plate_embedded_flaw
                                 plate_edge_flaw
                               # pipe_inside_surface_flaw
                                # pipe_long_inside_surface_flaw
                                # pipe_full_inside_flaw
                                # pipe_full_outside_flaw
```

#### Results for ifipeout0.98: Crack Propagation Int. Pipe Surface Flaw

```
#
#
                                                       # rod_surface_flaw
#
                                                       # rod_full_outside_flaw
                                                       # These problem types are used to pull in the
#
                                                       # appropriate Fw, Mm, Mb, files etc.
# The factors described in this section may be ignored if not applicable to
# the particular problem type described above.
# (All dimensions in mm)
\#B = 10.0
                 # plate (or pipe wall) thickness
\#W= 0.0 \# plate width
                 # Internal diameter if pipe problem
#ri=50.
#azero= 0.5 # initial crack depth
#czero= 4.0 # initial 1/2 crack width at surface
                 # Weld Feature width. Set to 0.0 if no Mkm or Mkb (weld)
#HISTORYFILE= load1.txt
                                               # historyFileName
                   # Adjustments to load file variables:
                    # Note that the MEANADD (below) is added AFTER the MAGFACTOR is applied.
#MAGFACTOR_m= 1.0
                                    # Multiply factor on membrane load. Result should be MPa
#MAGFACTOR_b= 1.0
                                    # Multiply factor on bending load term. Result should be MPa
                                  # Mean shift in MPa added to membrane stress.
#MEANADD_m= 0.0
                                   # Mean shift in MPa added to bending stress.
#MEANADD_b= 0.0
#MAXREPS= 10
                               # Max no. history repeats in simulation.
                                      # One repetition or application of the load history is
                                      # also called a "block" of cycles.
                                      # Normally this would be some large number.
#MATERIAL= merged_a36_fitted.html #File name of material fitted data
                                                          This file is used to define the cyclic
                                                          stress-strain curve, and the Neuber Product curve.
                                                         # Can be "table" or "Paris"
#DADN= table
!! specify: mpa_m or ksi_in or mpa_mm
                                                     ksi_in: ksi stress, inch crack length, inches in delta_K
                                                     \label{eq:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:mpa_m:
                                                     same as N/(mm**(3/2))
                                                   # da/dN digitized da/dN curve for material,
#DADN_TABLE= a36+1015.dadn
                                                          including the threshold, and KIc.
                                                           If a threshold exists, put in a vertical line
                                                           (with two identical X-axis points).
                                                          If the threshold needs to be "turned off" then
                                                          do NOT put in a vertical line at low da/dN.
                                                           (Ignored when #DADN= PARIS )
#FAD Stuff:
#TensileFile= a36_Mattos_mono_engrSS_FLAT.txt
                                                                                    #enter "none" if no FAD
#PmEOL= 70.
                                          #Set these so that Pm+Pb= 0.82*Syield for default.
#PbEOL= 100.
#Kmat= 1675.
#Pin_Joint = 0
                                                #Set = 1 if struture is pinJointed (for bending)
#BLOCKSKIP= 1.0 percent
                                                       # At the end of each block check if the previous
                                                          two blocks of cycles had similar damage (crack
                                                          extension) within this percentage. If TRUE then
                                                          simply skip the simulation of the next block,
                                                          but just add the expected damage. Continue by
                                                          simulating the block after the skip.
```

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```
# A value of 0.0 will disallow skipping blocks.

#SAVELEVEL= 0  #Amout of output saved to disk:

# 3=lots 2=medium 1=minimal

# 0= save #crk= data into binary direct access file only

# No #crk= data will be written into the text logfile.

# Use for large output files with lots of cycles.
```

# Appendix 2: Print of da/dn vs DeltaK Table in file ifipeout0.98

## Appendix 3: Print of Stress-Strain-Init.Life file: "matfile"

```
#SAE Standard Fatigue Data File format
```

##

#### Pick one: #FDE\_plot #FDE\_fit # #

```
#Copyright (C) 2012 F.D.E. Committee
#This data file is free software - you can redistribute it and/or
#modify it under the terms of the GNU General Public License as
#published by the Free Software Foundation; either version 2 of the
#license, or (at your option) any later version.
#This data file is distributed in the hope that it will be useful,
#but WITHOUT ANY WARRANTY - without even the implied warranty of
#MERCHANTABILITY or FITNESS FOR A PARTICULAR PURPOSE. See the
#GNU General PUblic License for more details.
#You should have received a copy of the GNU General PUblic License
#along with this program - if not, write to the Free Software
#Foundation, Inc., 59 Temple Place - Suite 330, Boston, MA 02111-1307, USA
#Try also their web site: http://www.gnu.org/copyleft/gpl.html
# NOTE: Fitted Data !!
# A36 Steel Merged Data Sets from Refs. 1 and 2:
# Ref.1: P.Dindinger report to Fat.Des.+Eval. Comm. Apr.2012
# Ref.2: G.A.Miller and H.S.Reemsnyder, "Strain-Cycle Fatigue of Sheet and
# Plate Steels I: Test Method Development and Data Presentation,"
# SAE Paper 830175, Detroit MI, Feb28-Mar.4, 1983
\# NOTE that original test data ends at 2Nf = 1.3million.
#FileType= strain_life
#DataType= fitted
#TIMEcol= 0
#NAME= ASTM-A36
```

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```
#NAME= Structural
#NAME= Steel
#Stress_units= ksi
#Strain_units= strain
#Sy= 38.4 0.2pc offset, 265 mpa
#Su= 69. ksi from Miller/Reemsnyder = 475 mpa
#eu= 0 #strain at Su not reported
\#E=29528. \text{ ksi} = 203600 \text{ mpa}
#FractureStrain= 0 not reported
#FractureStress= 0. not reported
#monotonic_K= 0 not reported
#monotonic_n= 0 not reported
#BHN= 138.
#%RA= 0. % not reported
#saedigcurve_v2.2.f starts.
# NOTE!! The Following Points are FITTED DATA: #NOTE!! Fitted Stress computed using Experm.
# Total Strain 2Nf Stress Mean Plastic Strain Initial
 #Original test data ends at 2Nf = 1.3million.
#Points below are extrapolation:
  0.00125 2000000 29.6 0. 0.00025 29528. #Fitted_point 0.00106 5000000 27.1 0. 0.00014 29528. #Fitted_point
```