# Power Electronics Education Electronic Book



### Welcome to PEEEB



Lecture 8: DC-AC Converters

Presenter: Dr. Firuz Zare

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Lecture 8

### **DC-AC Converters**

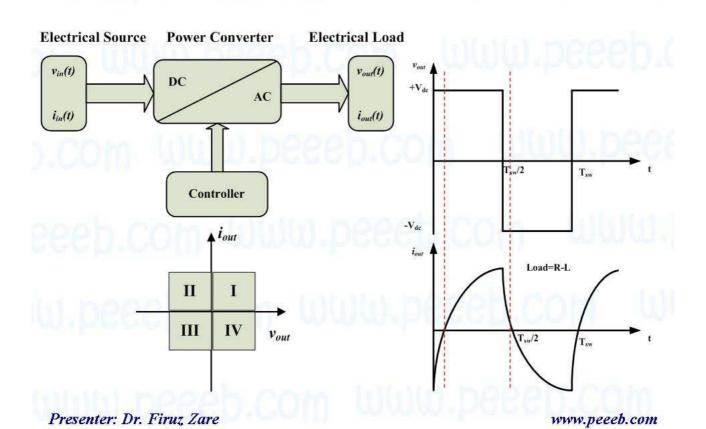
### Introduction

- Current Source or Voltage Source Inverters
- Single-phase or Three-phase Inverter
- Modulation Strategies
- Two-level or Multilevel
- Close loop or Open loop Control

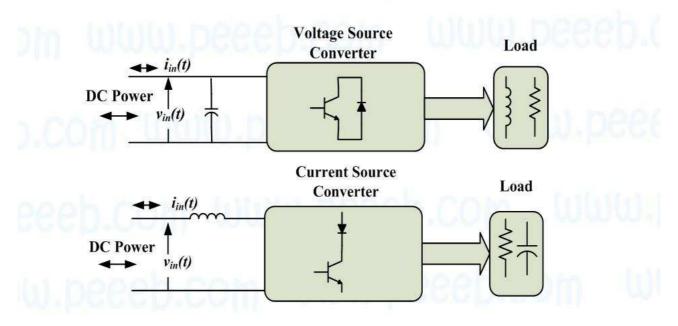
### • Single-phase Inverter

- Bipolar and Unipolar Modulations
- Three-phase Inverter
  - Leg, Line and Phase Voltages
  - Active and Zero Switching
  - Common-mode Voltage

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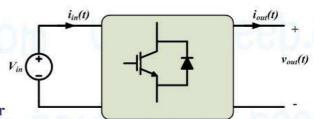
### **Current Source or Voltage Source**



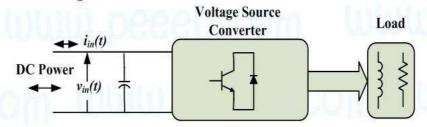
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### Power supplies in DC-AC converters:

- ·Battery
- •PV
- •(Grid and Wind Generator) & Rectifier

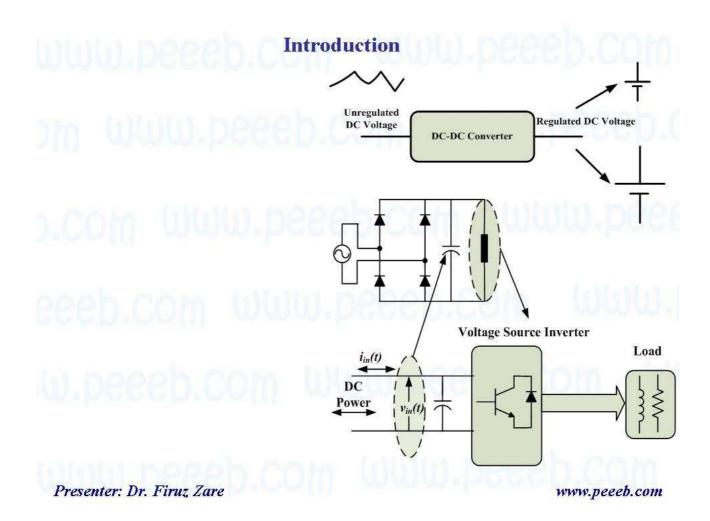


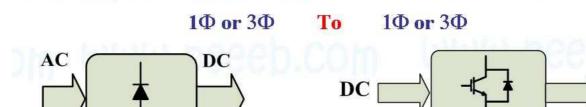
### Capacitor



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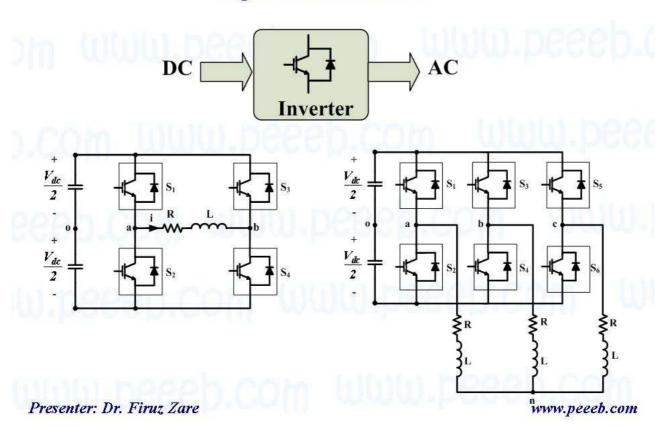


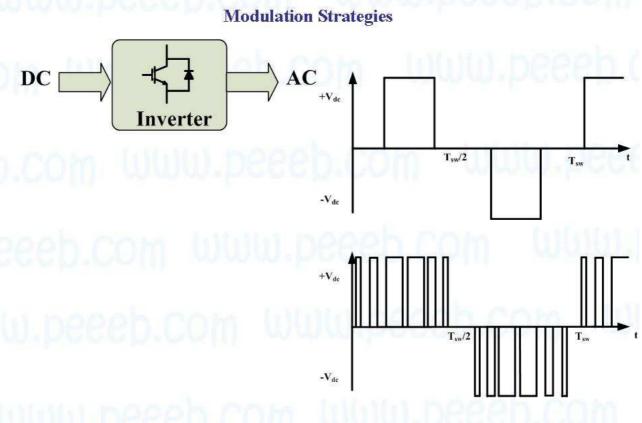
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Inverter

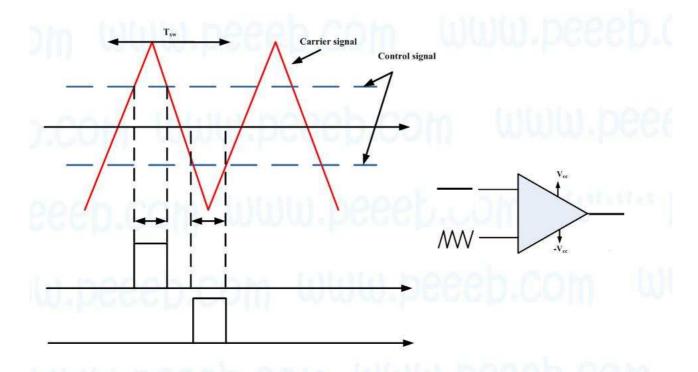
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### Single-Phase & Three-Phase





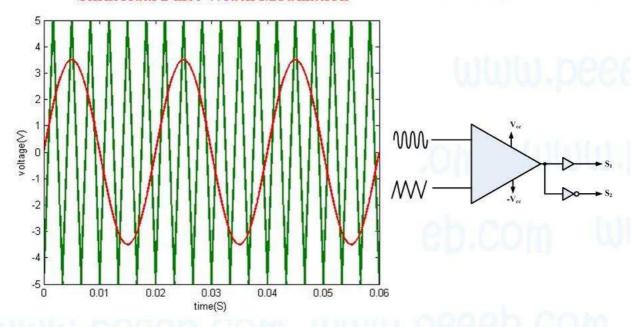
# Introduction Modulation Strategies



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# Introduction Modulation Strategies

### Sinusoidal Pulse Width Modulation

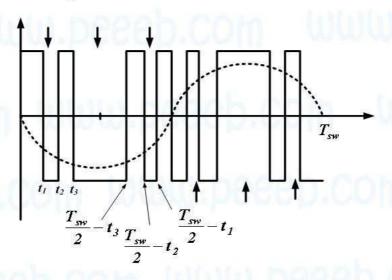


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### **Modulation Strategies**

### **Harmonic Elimination Technique**

In this technique, we can switching times, t1, t2 and t3 to control output voltage and cancel harmonics. This is an off-line switching method in which switching times are stored in a memory.

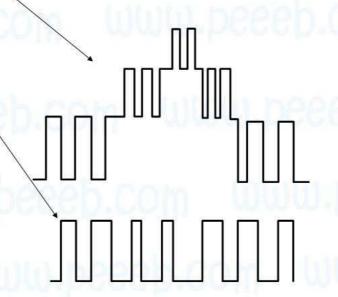


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### Two-level or Multi-level Inverter

### **Multi-level Converter**

- •Less voltage stress
- •Better quality and less switching losses
- •Suitable for high voltage applications
- •Complex circuit and control
- •More components

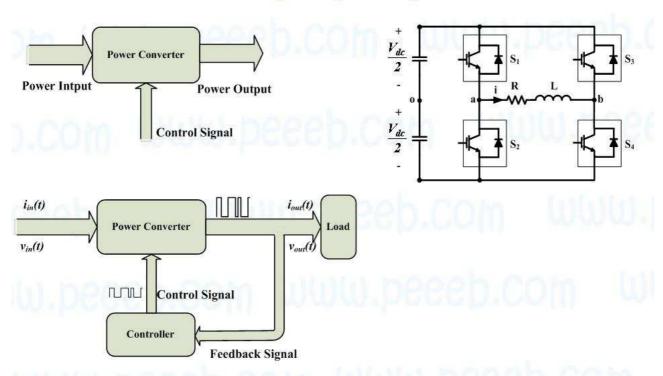


An output voltage generated by an inverter

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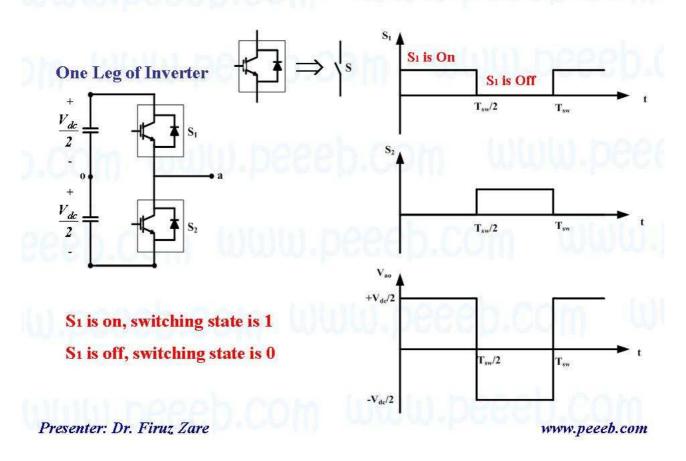
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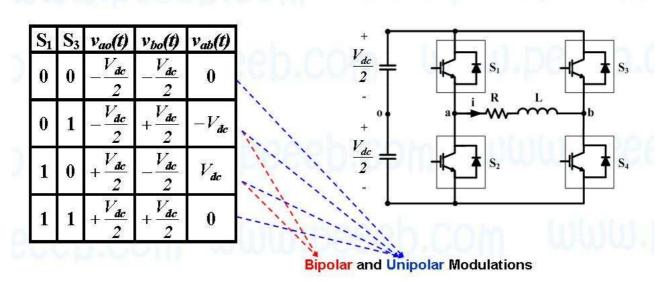
### **Close Loop or Open Loop Control**



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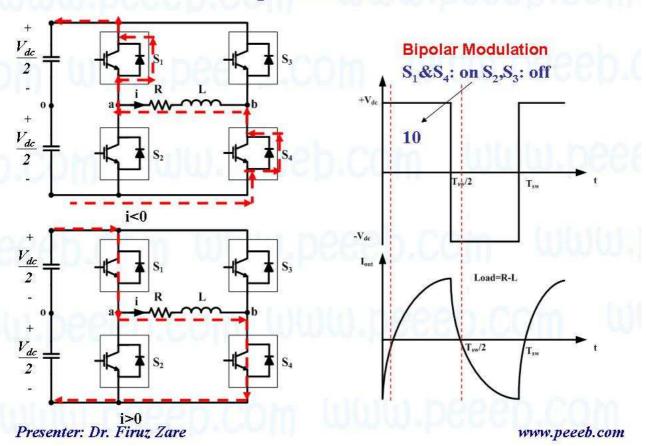
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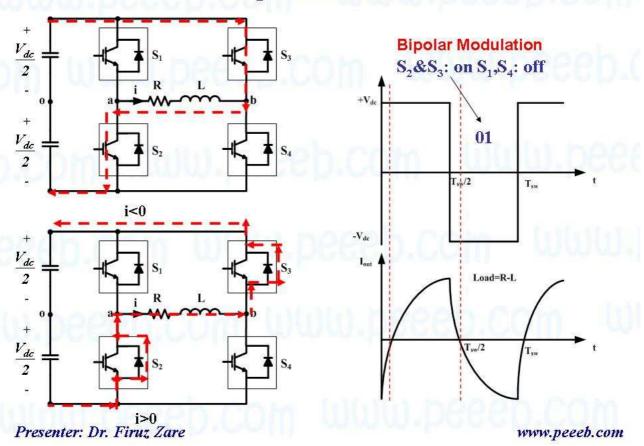




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### **Bipolar Modulation**

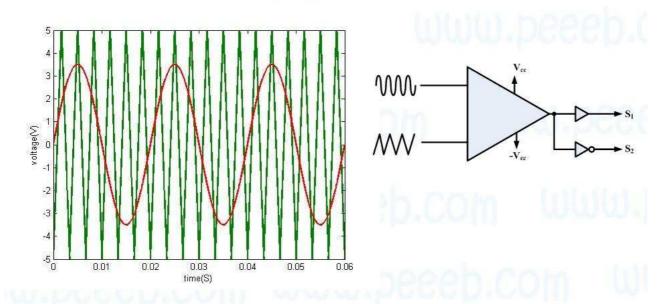
We can only control the output voltage by changing  $V_{\text{dc}}!$  BUT we can control the output frequency.

Increasing switching frequency and applying Pulse Width Modulation (PWM) make it possible to change the rms and frequency of output voltage.

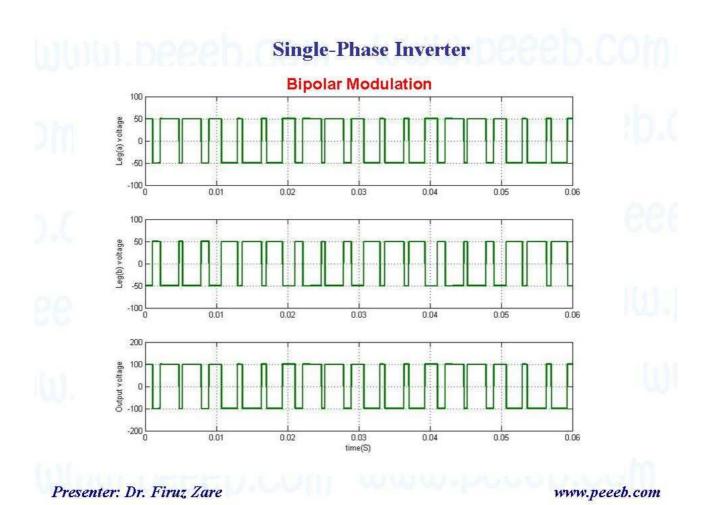
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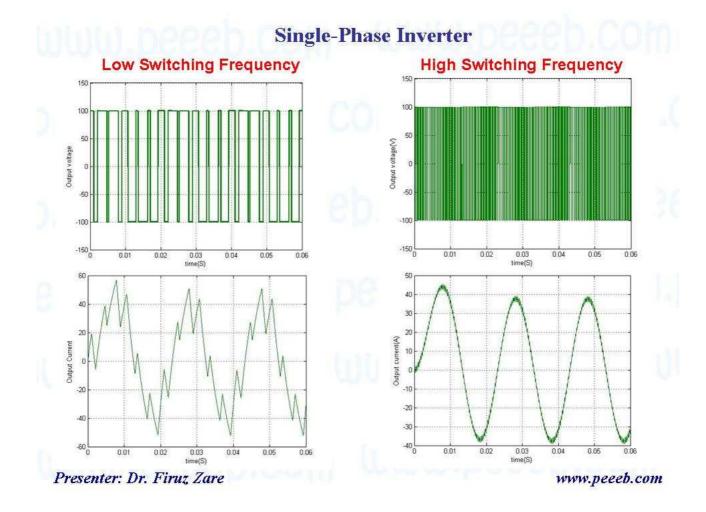
Lecture 8

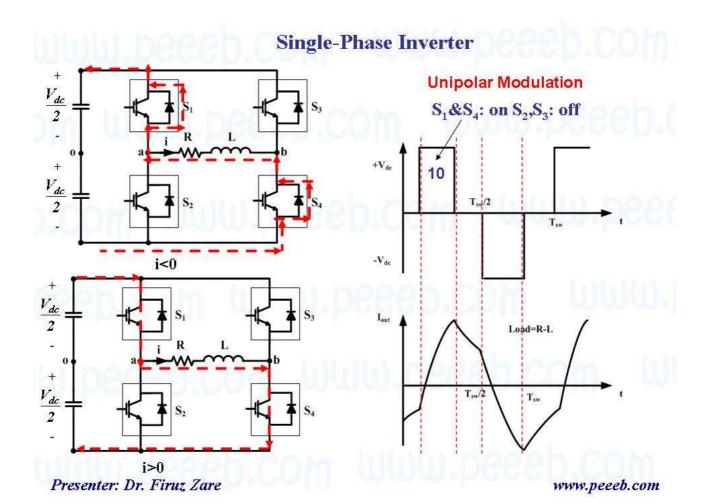
### **Bipolar Modulation**



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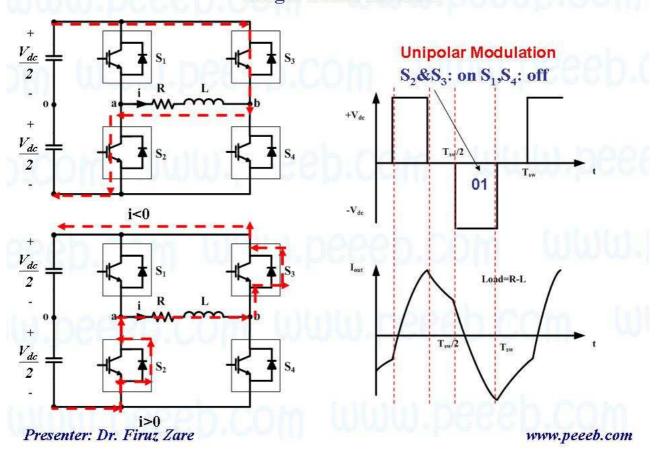
# Single-Phase Inverter Unipolar Modulation $S_1 \& S_3$ : on $S_2, S_4$ : off $S_1 & S_2 & S_4 & S$

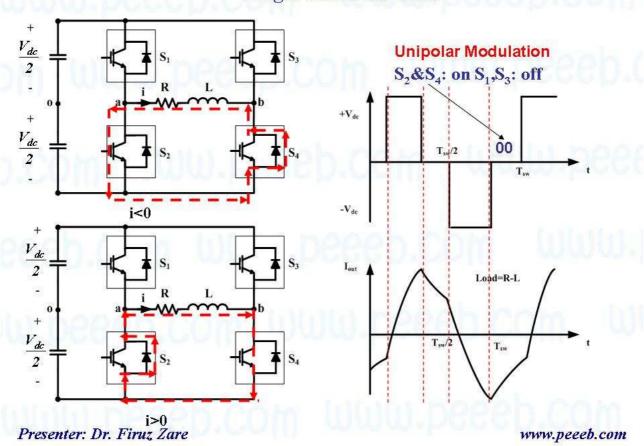
 $V_{dc}$   $V_{dc}$  V

 $V_{dc}$ 

+

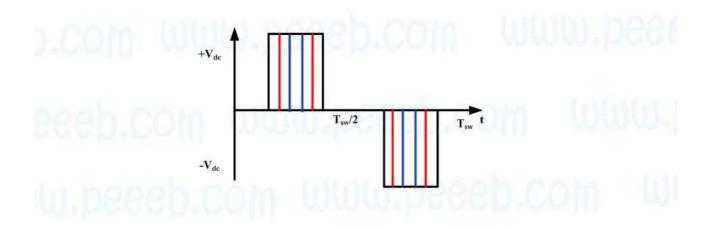
 $V_{dc}$ 





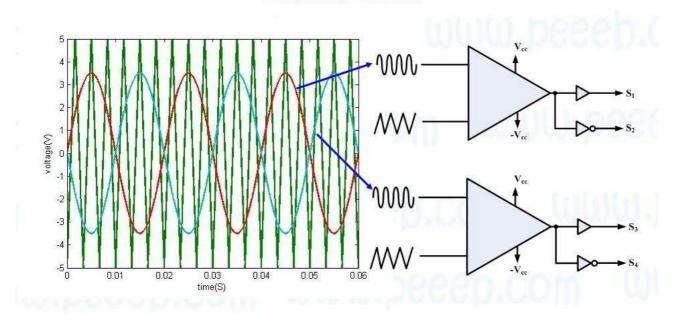
### **Unipolar Modulation**

We can control the output voltage and frequency by changing the pulse width without changing the DC link voltage.

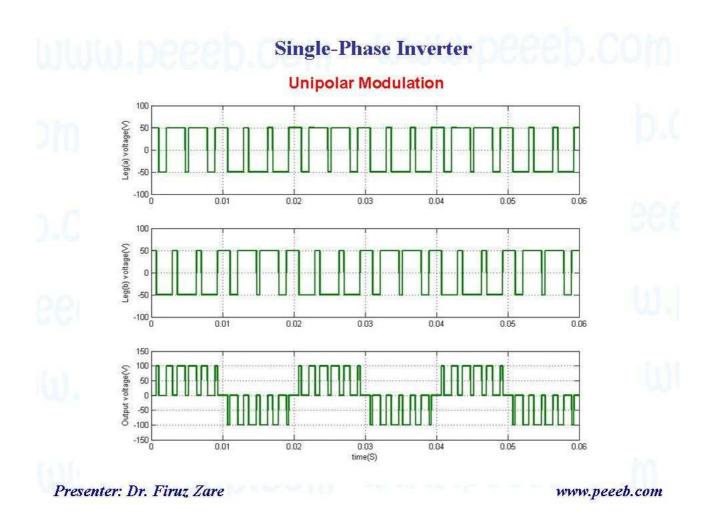


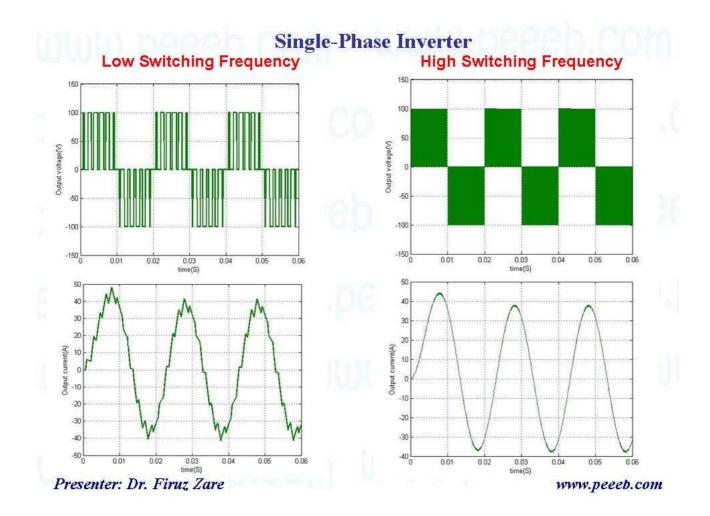
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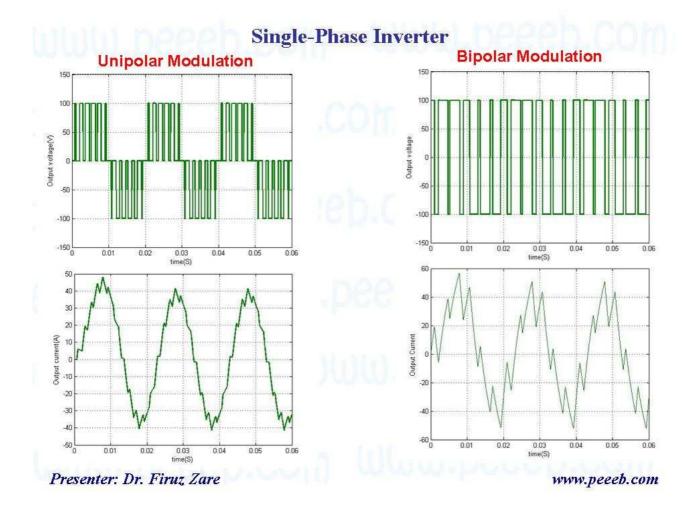
### **Unipolar Modulation**



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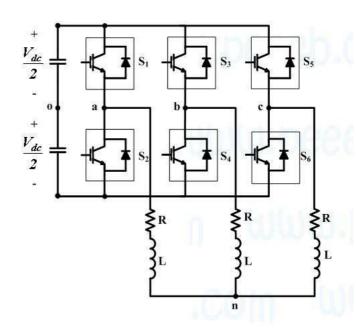






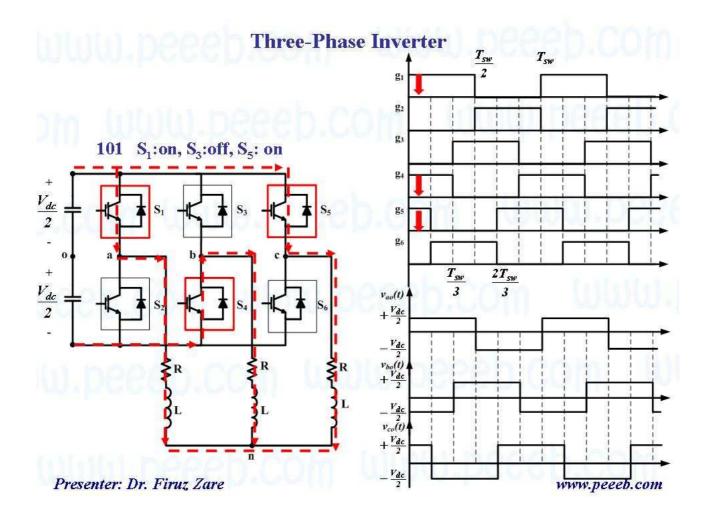
### Three-Phase Inverter

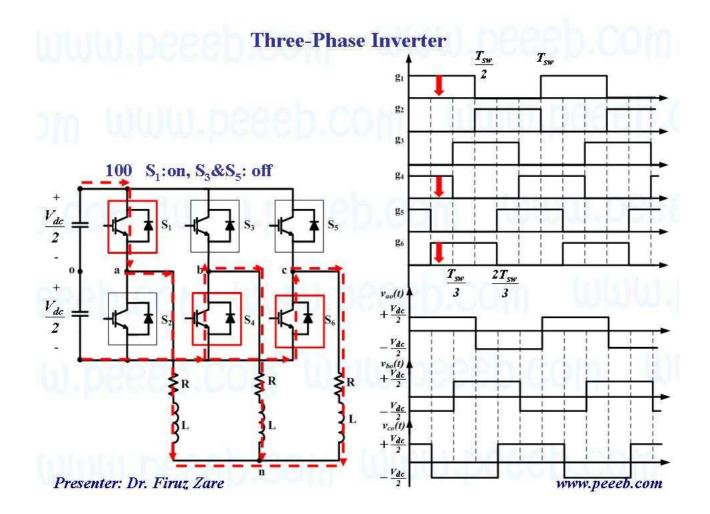
$S_1$	$S_3$	$S_5$	vao(t)	$v_{bo}(t)$	$v_{co}(t)$
0	0	0	$-\frac{V_{dc}}{2}$	$-\frac{V_{dc}}{2}$	$-\frac{V_{dc}}{2}$
0	0	1	$-\frac{V_{dc}}{2}$	$-\frac{V_{dc}}{2}$	$+\frac{V_{dc}}{2}$
0	1	0	$-\frac{V_{dc}}{2}$	$+\frac{V_{dc}}{2}$	$-\frac{V_{dc}}{2}$
0	1	1	$-\frac{V_{dc}}{2}$	$+\frac{V_{dc}}{2}$	$+\frac{V_{dc}}{2}$
1	0	0	$+\frac{V_{dc}}{2}$	$-\frac{V_{dc}}{2}$	$-\frac{V_{dc}}{2}$
1	0	1	$+\frac{V_{dc}}{2}$	$-\frac{V_{dc}}{2}$	$+\frac{V_{dc}}{2}$
1	1	0	$+\frac{V_{dc}}{2}$	$+\frac{V_{dc}}{2}$	$-\frac{V_{dc}}{2}$
1	1	1	$+\frac{V_{dc}}{2}$	$+\frac{V_{dc}}{2}$	$+\frac{V_{dc}}{2}$

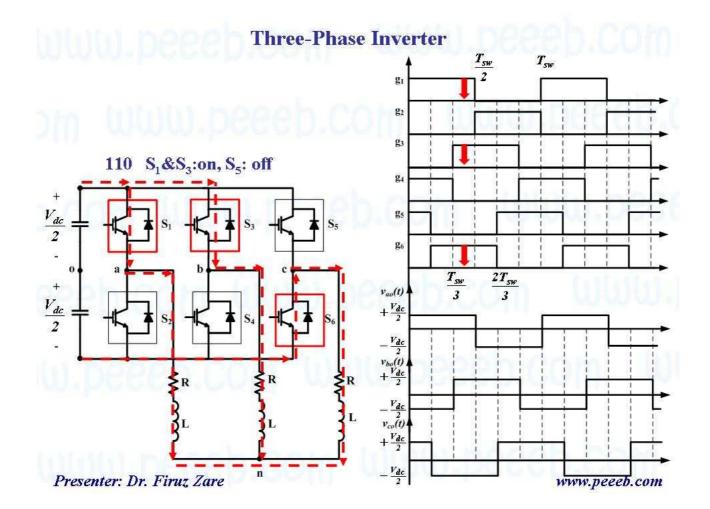


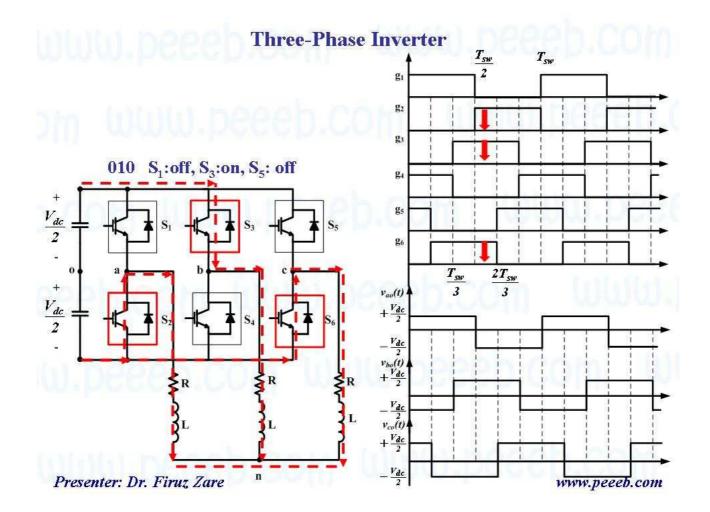
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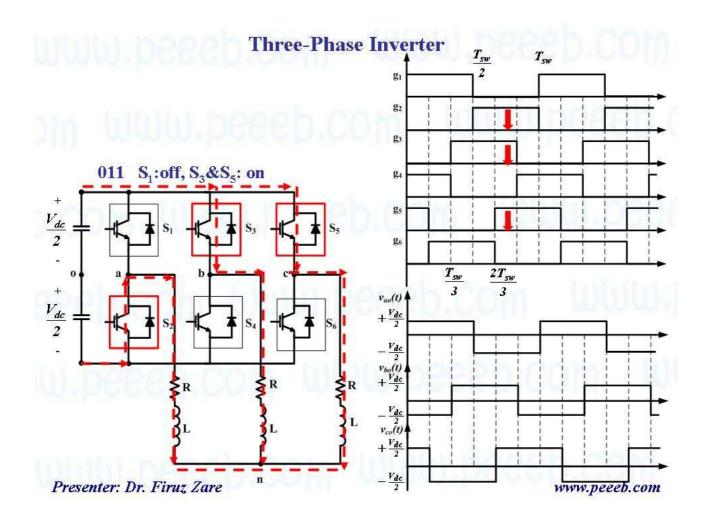
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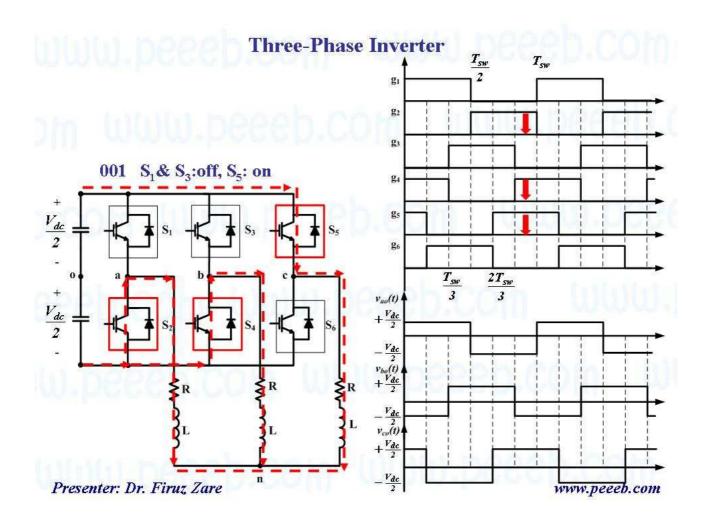


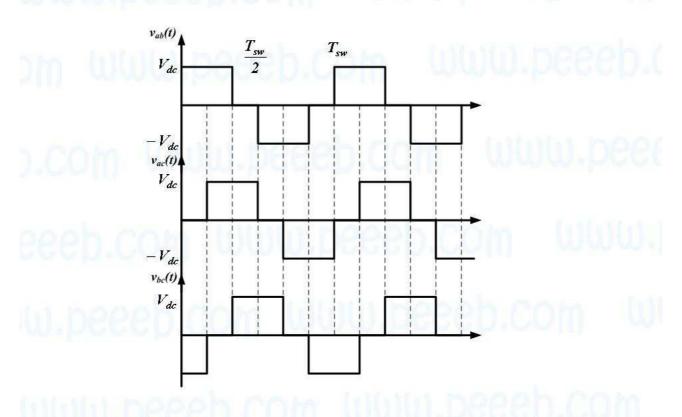






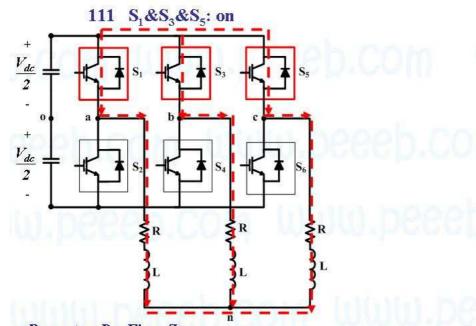






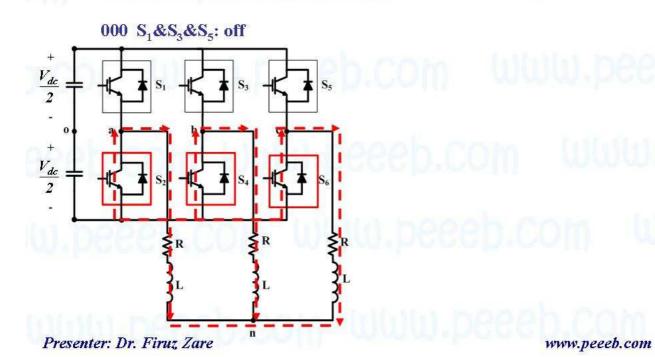
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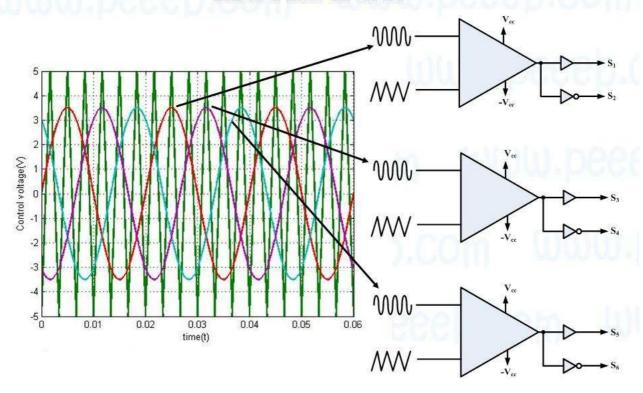




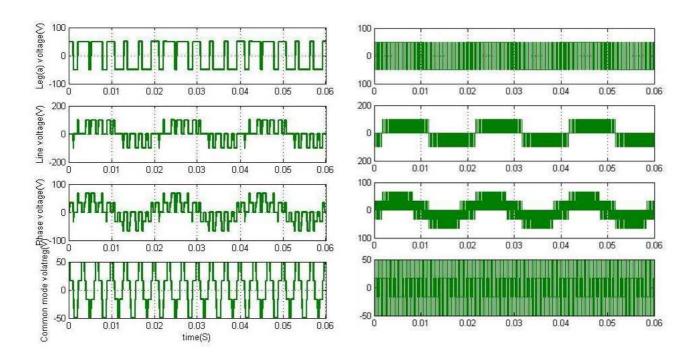
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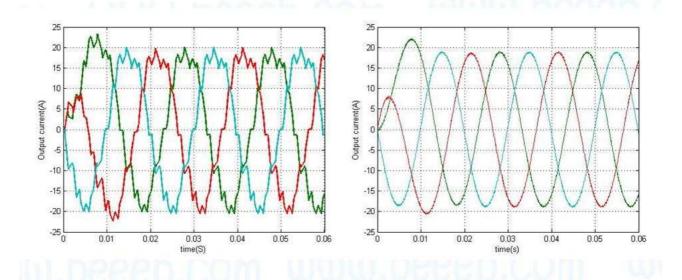


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Increasing switching frequency improves load current and decreases harmonics.



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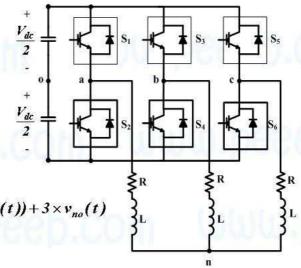
$$\begin{cases} v_{ao}(t) = v_{an}(t) + v_{no}(t) \\ v_{bo}(t) = v_{bn}(t) + v_{no}(t) \end{cases}$$

$$\begin{cases} v_{ao}(t) = v_{bn}(t) + v_{no}(t) \\ v_{co}(t) = v_{cn}(t) + v_{no}(t) \end{cases}$$

$$v_{ao}(t) + v_{bo}(t) + v_{co}(t) = (v_{an}(t) + v_{bn}(t) + v_{cn}(t)) + 3 \times v_{no}(t)$$

$$v_{an}(t) + v_{bn}(t) + v_{cn}(t) = 0$$

$$v_{no}(t) = \frac{(v_{ao}(t) + v_{bo}(t) + v_{co}(t))}{3}$$



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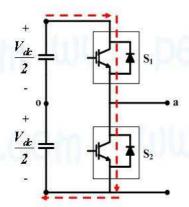
Three-Phase Inverter  $v_{no}(t) = \frac{(v_{ao}(t) + v_{bo}(t) + v_{co}(t))}{3}$ 

a	a	$S_5$ $v_{ao}(t)$ $v_{bo}(t)$ $v_{co}(t)$ $v_{no}(t)$ $v_{an}(t)$ $v_{an}(t)$							(1)
$S_1$	$S_3$	55	$v_{ao}(t)$	$v_{bo}(t)$	$v_{co}(t)$	$v_{no}(t)$	$v_{an}(t)$	$v_{bn}(t)$	$v_{cn}(t)$
0	0	0	$-\frac{V_{dc}}{2}$	$-\frac{V_{dc}}{2}$	$-\frac{V_{dc}}{2}$	$-\frac{V_{dc}}{2}$	0	0	0
0	0	1	$-\frac{V_{dc}}{2}$	$-\frac{V_{dc}}{2}$	$+\frac{V_{dc}}{2}$	$-\frac{V_{dc}}{6}$	$-\frac{V_{dc}}{3}$	$-\frac{V_{dc}}{3}$	$\frac{2V_{dc}}{3}$
0	1	0	$-\frac{V_{dc}}{2}$	$+\frac{V_{dc}}{2}$	$-\frac{V_{dc}}{2}$	$-\frac{V_{dc}}{6}$	$-\frac{V_{dc}}{3}$	$\frac{2V_{dc}}{3}$	$-\frac{V_{dc}}{3}$
0	1	1	$-\frac{V_{dc}}{2}$	$+\frac{V_{dc}}{2}$	$+\frac{V_{dc}}{2}$	$+\frac{V_{dc}}{6}$	$-\frac{2V_{dc}}{3}$	$\frac{V_{dc}}{3}$	$\frac{V_{dc}}{3}$
1	0	0	$+\frac{V_{dc}}{2}$	$-\frac{V_{dc}}{2}$	$-\frac{V_{dc}}{2}$	$-\frac{V_{dc}}{6}$	$\frac{2V_{dc}}{3}$	$-\frac{V_{dc}}{3}$	$-\frac{V_{dc}}{3}$
1	0	1	$+\frac{V_{dc}}{2}$	$-\frac{V_{dc}}{2}$	$+\frac{V_{dc}}{2}$	$+\frac{V_{dc}}{6}$	$\frac{V_{dc}}{3}$	$-\frac{2V_{dc}}{3}$	$\frac{V_{dc}}{3}$
1	1	0	$+\frac{V_{dc}}{2}$	$+\frac{V_{dc}}{2}$	$-\frac{V_{dc}}{2}$	$+\frac{V_{dc}}{6}$	$\frac{V_{dc}}{3}$	$\frac{V_{dc}}{3}$	$-\frac{2V_{dc}}{3}$
1	1	1	$+\frac{V_{dc}}{2}$	$+\frac{V_{dc}}{2}$	$+\frac{V_{dc}}{2}$	$+\frac{V_{dc}}{2}$	0	0	0

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### **Dead-time in Inverters**



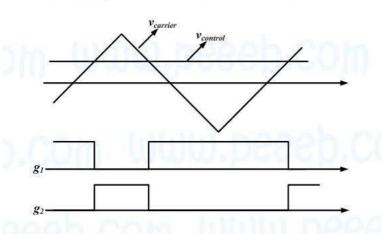
Two switches in each leg should not be turned on simultaneously. This case, makes a short circuit across the DC supply and may damage the power converter due to a significant short circuit current through the power switches.

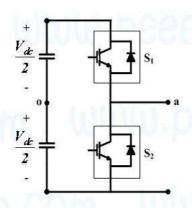
 $T_{sw}/2$   $T_{sw}$  t  $T_{sw}/2$   $T_{sw}$  t  $T_{sw}/2$   $T_{sw}$  t  $T_{sw}/2$   $T_{sw}$  t

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## **Dead-time in Inverters**

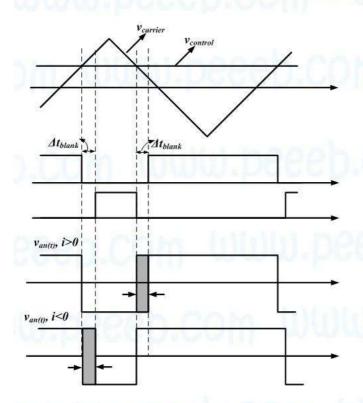


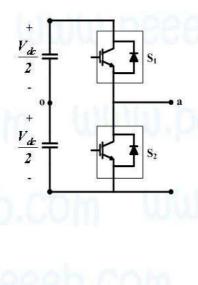


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# **Dead-time in Inverters**

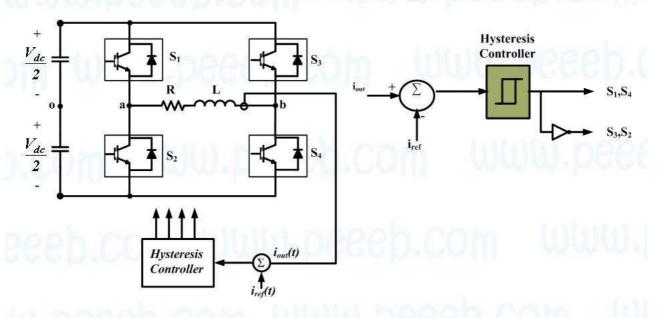




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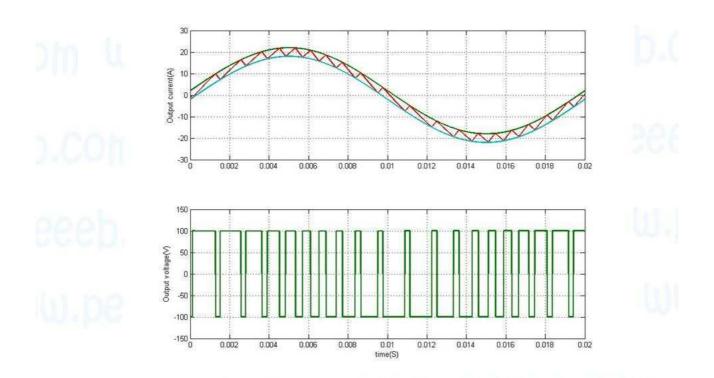
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## **Hysteresis Current Control for a Single-Phase Inverter**



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## **Hysteresis Current Control for a Single-Phase Inverter**



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