

Lift Force on an Aerofoil

(lab experiment)

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1 Outline

In this laboratory experiment, the focus is on determining the lift force acting on an airfoil using the Air Flow bench in a vertical wind tunnel. By examining the pressure distribution across the airfoil's surface at varying angles of attack, the experiment helps to relate these pressure to the overall lift produced by the airfoil.

2 Theory

Lift on an airfoil is important for aircraft elevation, which can be interpreted by the Coanda effect and the different pressures between top and bottom surfaces.

For a symmetric airfoil in zero angle, the lift generated is zero. After rising the angle of airfoil, the pressure variaty and producing more lift.

However, at significant angles, the airflow over the top of the wing can detach due to boundary layer effects, altering the pressure distribution and resulting in lower lift coefficients. This phenomenon is known as "stalling".

3 Method

- a. An accurate value for the density of air was determined using room temperature and atmospheric pressure, as cited in Rogers and Mayhew (1992 pp.157-8).
- b. With the aerofoil positioned at a 0° angle of attack, pressure measurements were recorded.
- c. The effective static pressure should be computed by using the atmospheric and duct inlet pressures.

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- d. Using the effective static pressure (p_{eff}) and the airbox pressure reading, calculate the free stream velocity and determined the Reynolds number with chord length.
- e. For each pressure tapping reading, the corresponding value of pressure ratio($C_{p,n}$) was calculated, and these values were plotted against ($\frac{x}{c}$). The curves were extended to represent a chord ratio of 0 and 1. Noticed that the pressure coefficient near the leading edge is approaching zero, which indicate the directing of the air is disappeared at this point. The exact position of this stagnation point changes with incident angle.
- f. From the generated curves of C_p , the lift coefficient (C_L) can be numerically integrated to derive its value.
- g. The measurements have been repeated for increasing angles of attack (in steps of 5°) up to 25° , with additional measurements at 17.5° and 22.5° . Following this, the lift coefficients were computed and a graph illustrating C_L vs. α for the aerofoil was plotted.

4 Results

The density of mercury and air and atmospheric pressure at this time can be determined from the thermometers (23.5°) and manometers ($754mmHg$).

The air and mercury densities are ($1.2kg/m^3$ and $13.534 \times 10^3kg/m^3$) and the atmospheric pressure is ($100107.4792Pa$), as shown by equation $P_a = \rho_{Hg}gh$ and by consulting the density - temperature table of mercury.

The following table shows the data recorded from the experiment.

5 Analysis

| | 1 | 3 | 5 | 7 | 9 | 11 | 2 | 4 | 6 | 8 | 10 | 12 | Atm | Airbox | Inlet |
|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|--------|-------|
| 0 | 196 | 158 | 152 | 158 | 167 | 177 | 184 | 156 | 155 | 164 | 170 | 182 | 186 | 244 | 190 |
| 5 | 236 | 195 | 175 | 175 | 178 | 182 | 124 | 118 | 132 | 148 | 168 | 180 | 186 | 244 | 192 |
| 10 | 146 | 220 | 197 | 187 | 188 | 187 | 58 | 88 | 106 | 146 | 164 | 180 | 186 | 244 | 194 |
| 15 | 244 | 235 | 212 | 199 | 194 | 189 | 13 | 54 | 116 | 146 | 166 | 178 | 186 | 244 | 198 |
| 17.5 | 242 | 239 | 217 | 203 | 196 | 190 | 8 | 42 | 119 | 148 | 165 | 178 | 186 | 244 | 200 |
| 20 | 247 | 236 | 217 | 205 | 197 | 190 | 156 | 154 | 154 | 153 | 154 | 158 | 186 | 244 | 210 |
| 22.5 | 248 | 238 | 220 | 209 | 200 | 192 | 164 | 162 | 162 | 160 | 160 | 162 | 186 | 244 | 214 |
| 25 | 247 | 242 | 226 | 217 | 205 | 196 | 172 | 170 | 169 | 168 | 164 | 164 | 186 | 246 | 218 |

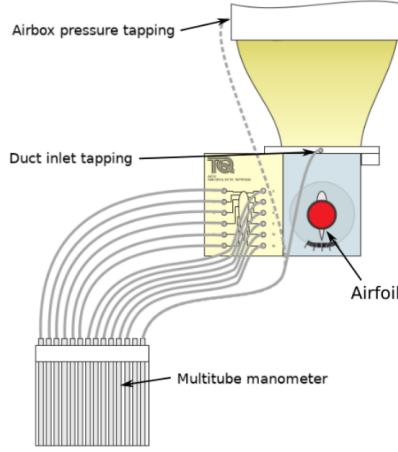


Figure 5.1: Pressure tappings for AF18 Experiment

Next the experimental data were processed. Firstly the difference in water head was calculated for each sampling point by using the Pitot tube at atmospheric pressure as a standard value. The difference in water head was then converted to a difference in pressure by equation $P_n = \rho gh$, as shown in table b below.

Based on the data, it was able to calculate the effective static pressure (p_{eff}) in different angle.

$$p_{eff} = p_0 + \frac{85}{135} \times (p_a - p_0) \quad (5.1)$$

And calculate free stream velocity U_∞ by following formular in different angle.

$$U_\infty = \sqrt{\frac{2 \times (p_{airbox} - p_{eff})}{\rho}} \quad (5.2)$$

The results are shown in the following table.

And from

$$C_{p,n} = \frac{p_n - p_{eff}}{\frac{1}{2} \rho u_\infty^2} \quad (5.3)$$

| | 1 | 3 | 5 | 7 | 9 | 11 | 2 | 4 | 6 | 8 | 10 | 12 | Atm | Airbox | Inlet |
|------|--------|---------|---------|---------|---------|--------|----------|----------|---------|---------|---------|---------|-----|--------|--------|
| 0 | 98.1 | -274.68 | -333.54 | -274.68 | -186.39 | -88.29 | -19.62 | -294.3 | -304.11 | -215.82 | -156.96 | -39.24 | 0 | 568.98 | 39.24 |
| 5 | 490.5 | 88.29 | -107.91 | -107.91 | -78.48 | -39.24 | -608.22 | -667.08 | -529.74 | -372.78 | -176.58 | -58.86 | 0 | 568.98 | 58.86 |
| 10 | -392.4 | 333.54 | 107.91 | 9.81 | 19.62 | 9.81 | -1255.68 | -961.38 | -784.8 | -392.4 | -215.82 | -58.86 | 0 | 568.98 | 78.48 |
| 15 | 568.98 | 480.69 | 255.06 | 127.53 | 78.48 | 29.43 | -1697.13 | -1294.92 | -686.7 | -392.4 | -196.2 | -78.48 | 0 | 568.98 | 117.72 |
| 17.5 | 549.36 | 519.93 | 304.11 | 166.77 | 98.1 | 39.24 | -1746.18 | -1412.64 | -657.27 | -372.78 | -206.01 | -78.48 | 0 | 568.98 | 137.34 |
| 20 | 598.41 | 490.5 | 304.11 | 186.39 | 107.91 | 39.24 | -294.3 | -313.92 | -313.92 | -323.73 | -313.92 | -274.68 | 0 | 568.98 | 235.44 |
| 22.5 | 608.22 | 510.12 | 333.54 | 225.63 | 137.34 | 58.86 | -215.82 | -235.44 | -235.44 | -255.06 | -255.06 | -235.44 | 0 | 568.98 | 274.68 |
| 25 | 598.41 | 549.36 | 392.4 | 304.11 | 186.39 | 98.1 | -137.34 | -156.96 | -166.77 | -176.58 | -215.82 | -215.82 | 0 | 588.6 | 313.92 |

| | 0 | 5 | 10 | 15 | 17.5 | 20 | 22.5 | 25 | | | | |
|------------|----------|----------|----------|----------|----------|----------|----------|----------|--|--|--|--|
| p_{eff} | 24.70667 | 37.06 | 49.41333 | 74.12 | 86.47333 | 148.24 | 172.9467 | 197.6533 | | | | |
| U_∞ | 30.11847 | 29.77471 | 29.42693 | 28.71875 | 28.35803 | 26.48081 | 25.69155 | 25.52602 | | | | |

| | 1 | 3 | 5 | 7 | 9 | 11 | 2 | 4 | 6 | 8 | 10 | 12 |
|------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | 0.016 | 0.071 | 0.175 | 0.317 | 0.510 | 0.698 | 0.032 | 0.119 | 0.230 | 0.413 | 0.603 | 0.794 |
| 0 | 0.135 | -0.560 | -0.613 | -0.505 | -0.342 | -0.162 | -0.036 | -0.541 | -0.559 | -0.397 | -0.288 | -0.072 |
| 5 | 0.852 | 0.110 | -0.203 | -0.203 | -0.148 | -0.074 | -1.143 | -1.254 | -0.996 | -0.701 | -0.332 | -0.111 |
| 10 | -0.850 | 0.585 | 0.208 | 0.019 | 0.038 | 0.019 | -2.417 | -1.850 | -1.510 | -0.755 | -0.415 | -0.113 |
| 15 | 1.000 | 0.913 | 0.515 | 0.258 | 0.159 | 0.059 | -3.430 | -2.617 | -1.388 | -0.793 | -0.396 | -0.159 |
| 17.5 | 0.959 | 1.019 | 0.630 | 0.346 | 0.203 | 0.081 | -3.619 | -2.928 | -1.362 | -0.773 | -0.427 | -0.163 |
| 20 | 1.070 | 1.103 | 0.723 | 0.443 | 0.256 | 0.093 | -0.699 | -0.746 | -0.746 | -0.769 | -0.746 | -0.653 |
| 22.5 | 1.099 | 1.223 | 0.842 | 0.570 | 0.347 | 0.149 | -0.545 | -0.594 | -0.594 | -0.644 | -0.644 | -0.594 |
| 25 | 1.025 | 1.340 | 1.004 | 0.778 | 0.477 | 0.251 | -0.351 | -0.401 | -0.427 | -0.452 | -0.552 | -0.552 |

the pressure ratio in different angle can be calculated. Additionally, the tapping position and airfoil chord for the different sampling points can be obtained from the appendix, and the $\frac{x}{c}$ can be calculated.

6 Conclusions

References