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# RESEARCH MEMORANDUM

PRESSURE DISTRIBUTIONS ON THE BLADE SECTIONS  
OF THE NACA 10-(3)(90)-03 PROPELLER  
UNDER OPERATING CONDITIONS

By Peter J. Johnson

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## NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS

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## RESEARCH MEMORANDUM

## PRESSURE DISTRIBUTIONS ON THE BLADE SECTIONS

## OF THE NACA 10-(3)(090)-03 PROPELLER

## UNDER OPERATING CONDITIONS

By Peter J. Johnson

## SUMMARY

This paper is the third of a series which present the results of pressure-distribution measurements on five related propellers. All five propellers were designed to have NACA 16-series airfoil sections over the entire blade except a small region at the tip. Chordwise distributions of pressure are presented for the NACA 10-(3)(090)-03 propeller at nine radial stations. At the innermost station investigated, which had a thickness ratio of 0.300, the section helical Mach number varied from 0.28 to 0.70; for the section nearest the tip, which had a thickness ratio of 0.053, the helical Mach number varied from 0.57 to 1.18. The pressure distributions have been reduced by integration to the form of blade-section aerodynamic coefficients. The tables which form the essential part of this paper present the basic pressure data, the aerodynamic coefficients, and a complete description of the operating conditions for each test point.

## INTRODUCTION

The development of efficient propellers for use on high-speed aircraft has been impeded by a lack of airfoil data at transonic and supersonic speeds. The scarcity of information at transonic speeds was due principally to the natural limitations of conventional wind tunnels in this speed range. Inasmuch as the aerodynamic characteristics of propeller-blade sections are not necessarily identical with two-dimensional airfoil characteristics, the idea of determining propeller section characteristics directly by means of pressure measurements appeared attractive, especially because such work could be done in a conventional wind tunnel. Accordingly, the NACA initiated an

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investigation of high-speed propeller-blade section characteristics for the NACA 10-(3)(08)-03 propeller, results of which are reported in reference 1. Encouraged by these results, a new program was authorized for the design and testing of five related propellers embodying NACA 16-series blade sections.

The five propellers had identical rectangular blade plan forms with 8-inch chord and 10-foot diameter, and all had the same design blade twist. The designations for these blade designs are:

- (1) NACA 10-(3)(066)-03
- (2) NACA 10-(3)(049)-03
- (3) NACA 10-(3)(090)-03
- (4) NACA 10-(5)(066)-03
- (5) NACA 10-(0)(066)-03

The solidities of all five blades are the same. References 2 and 3 have erroneous solidities in the propeller-blade designations. Reference 2 presents a complete description of the test apparatus and reduction of data with the tabular data from tests of the NACA 10-(3)(066)-03 propeller, and reference 3 presents the data obtained from the tests of the NACA 10-(3)(049)-03 propeller. The purpose of this paper is to present in tabular form the data obtained with the NACA 10-(3)(090)-03 blade design which had thicker blade sections than did the other propellers in this series of five. No attempt has been made to analyze the data thoroughly or to formulate conclusions. In order to expedite the transfer of the information contained in this paper to the agencies concerned with its ultimate use, the data have been analyzed only to the extent necessary to ensure their validity and to facilitate their use.

It is important to note that the values of induced angle presented in the tables are calculated as for a propeller operating with Betz loading by use of Goldstein tip correction factors. Because, in general, the blade loading was not optimum, the values of induced angle must be calculated for the actual arbitrary loading.

#### SYMBOLS

The symbols used throughout this paper, some of which are defined in figure 1, are defined as follows:

- |   |                   |
|---|-------------------|
| B | number of blades  |
| b | blade chord, feet |

c	distance from section leading edge to any point on chord, feet
$c_c$	section chordwise-force coefficient
$c_l$	section lift coefficient
$c_{l_d}$	blade-section design lift coefficient
$c_m$	section pitching-moment coefficient about quarter-chord point
$c_n$	section normal-force coefficient
D	propeller diameter, feet
$F_c$	section chordwise pressure force, pounds
$F_n$	section normal pressure force, pounds
G	Goldstein induced-velocity correction factor for finite number of blades
h	blade-section maximum thickness, feet
J	advance ratio ( $V/nD$ )
M	Mach number of advance
$M_x$	helical section Mach number $\left( M \sqrt{1 + \left( \frac{\pi x}{J} \right)^2} \right)$
m	section pitching moment, pound-feet
N	propeller rotational speed, rpm
n	propeller rotational speed, rps
P	pressure coefficient $\left( \frac{p - p_o}{q_x} \right)$
p	static pressure at point on airfoil surface, pounds per square foot

$p_o$	free-stream static pressure, pounds per square foot
$q_x$	resultant dynamic pressure at radial station $x$ , pounds per square foot $\left(\frac{1}{2} \rho W_o^2\right)$
$R$	propeller-tip radius, feet
$r$	radius to blade element, feet
$r_p$	polar ordinate, feet
$s$	distance along surface of blade section, feet
$V$	velocity of advance (corrected for wind-tunnel-wall interference effects), feet per second
$W_o$	velocity vector $\left(V \sqrt{1 + \left(\frac{\pi x}{J}\right)^2}\right)$
$W$	resultant velocity at blade section, feet per second
$w_i$	induced velocity at blade section, feet per second
$x$	fraction of propeller-tip radius ( $r/R$ )
$y$	normal distance from chord line to upper or lower surface of airfoil, inches
$\alpha_i$	induced angle of attack, degrees
$\alpha_x$	angle of attack of blade element, corrected for induced flow and blade deflection, at radial station $x$ , degrees $(\beta_x - \phi + \Delta\beta)$
$\alpha_x'$	geometric angle of attack of blade element at radial station $x$ , degrees $(\beta_x - \phi_o)$
$\beta$	blade angle, degrees
$\beta_{0.75R}$	blade angle at 0.75 tip radius, degrees
$\Delta\beta$	change in blade angle caused by operation loads, degrees
$\theta$	polar angular ordinate, radians

$\rho$	mass density of air in free stream, slugs per cubic foot
$\sigma$	solidity $\left( B \frac{b}{D} / \pi x \right)$
$\phi$	helix angle, degrees $(\phi_0 + \alpha_1)$
$\phi_0$	geometric helix angle, degrees $(\tan^{-1}(J/\pi x))$
$\psi$	slope angle at surface of section; referenced to chord, degrees

## Subscripts:

L	lower-surface value
U	upper-surface value

## APPARATUS

The 2000-horsepower propeller dynamometer used in making these propeller tests in the Langley 16-foot high-speed tunnel is described in detail in reference 4. Reference 2 presents a description of the propeller spinner and hubs used, a description and diagram of the pressure-transfer device and pressure-measuring apparatus, and the details of the optical deflectometer used to measure the torsional deflection of the blade. Figure 2 is a diagram of the pressure-distribution propeller test installation.

Propeller blades.— The test data presented herein were obtained by taking pressure-distribution measurements at nine blade sections of the NACA 10-(3)(090)-03 propeller. The foregoing designation indicates a 10-foot-diameter propeller having values of the design parameters at the 0.70 radius station as follows: section design lift coefficient, 0.30; section thickness ratio, 0.090; and solidity per blade, 0.03. NACA 16-series airfoil sections were used throughout the blade except very near the tip. The propeller-blade form characteristics are presented in figure 3 with the section locations where pressure measurements were taken indicated on the blade plan form. The portion of the blade enclosed by the spinner is also indicated. The lift-coefficient curve shows a sharp decrease from design value of 0.3 at the  $x = 0.95$  station to 0.223 at  $x = 0.975$ . Owing to the fairing down of the blade to a fine edge at the tip in the final manufacturing processes, the dimensions

were slightly changed. Measurements at  $x = 0.975$  showed the blade section to be approximately of the NACA 16-series with a design lift coefficient of 0.223. Details of the blade construction, pressure tube and orifice installation, and temperature measurements are described in reference 2.

### TESTS

All tests on the NACA 10-(3)(090)-03 propeller were made with the blade angle at the 0.75 tip radius set at  $45^\circ$ . Since the blade section angle of attack is a function of the section blade angle and advance ratio, the angle of attack was varied during a run by changing the advance ratio. For the low-speed tests, the propeller rotational speed was held constant and the advance ratio (section angle of attack) was changed by varying the tunnel airspeed. At the higher speeds, tunnel air-stream Mach number was held constant and the advance ratio varied by varying the propeller rotational speed. Because each test covered approximately the same range of advance ratio, the data provide blade section characteristics over a given range of angle of attack at different values of section helical Mach number. The range covered and operating conditions for each test are specified in the data tables 1 to 10. The table index presents an outline of the test schedule.

In order to extend the test range of the data to higher section angles of attack beyond the power limitations of the two-blade propeller configuration, some one-blade propeller tests were run and pressure data were obtained for the  $x = 0.85$  section. The procedures employed in making these tests are described in reference 2.

### REDUCTION OF DATA

The usual wind-tunnel-wall corrections described in reference 4 have been applied to the data to obtain equivalent free airspeed.

The following equations, repeated from reference 1 with abbreviated explanation, have been used in the reduction of the data presented herein.

The pressure coefficient

$$P = \frac{p - p_o}{q_x}$$

The normal force

$$F_n = \int_0^b p \cos \psi \, ds = \int_0^b \left[ (p_L - p_o) - (p_U - p_o) \right] dc$$

making the normal-force coefficient

$$c_n = \frac{F_n}{q_\infty b} \int_0^{1.0} (p_L - p_U) d \frac{c}{b}$$

The chordwise force

$$F_c = \int_0^b p \sin \psi \, ds = \int_0^b \left[ (p_U - p_o) \tan \psi_U - (p_L - p_o) \tan \psi_L \right] dc$$

making the chordwise-force coefficient

$$c_c = \frac{F_c}{q_\infty b} \int_0^{1.0} (p_U \tan \psi_U - p_L \tan \psi_L) d \frac{c}{b} \quad (1)$$

or, in polar coordinates

$$c_c = \int_0^{2\pi} (P) \left( \frac{\sin \psi}{\sin (\theta - \psi)} \right) \left( \frac{r_p}{b} \right) d\theta \quad (2)$$



where equation (1) is used to evaluate that portion of chordwise-force coefficient from  $\frac{c}{b} = 0.025$  to  $\frac{c}{b} = 1.0$  and equation (2) is used to evaluate the chordwise-force coefficient from  $\frac{c}{b} = 0$  to  $\frac{c}{b} = 0.025$ .

The pitching-moment coefficient

$$c_m = \frac{m}{q_\infty b^2} = \frac{\bar{c}}{b} \int_0^{1.0} (P_L - P_U) d \frac{c}{b} - \int_0^{1.0} (P_L - P_U) \frac{c}{b} d \frac{c}{b}$$

and the moments have been taken about  $\frac{\bar{c}}{b} = 0.25$ .

The induced angle

$$\alpha_1 = \tan^{-1} \left( \frac{\sigma c_l}{4G \sin \phi} \right)$$

For the first approximation in the calculation of the angle, it is assumed that  $c_l$  is equal to  $c_n$  and  $\phi$  is equal to  $\phi_0$ .

## RESULTS AND DISCUSSION

The data obtained from measuring blade-section pressure distribution at nine radial stations of the NACA 10-(3)(090)-03 propeller are presented in tabular form as itemized in the table index.

Pressure distribution.— For each value of advance ratio at which pressure measurements were recorded, there are tabulated the values of pressure coefficient for all orifice locations on the blade section instrumented. There is also listed the value of stagnation pressure computed for the section Mach number. There is negligible error in assuming the stagnation point to occur on the leading edge for all except the highest angles of attack on the most inboard sections. The trailing-edge pressure coefficient is listed as the faired intersection of the upper-surface and lower-surface distributions at the trailing edge except where they cannot be reasonably assumed to coincide. In this case, the value tabulated is taken from the lower-surface fairing and a note of the fact appears at the bottom of the table. In all cases

where faulty readings were obtained because of leaking or stopped pressure tubes, faired values are tabulated and noted.

Figure 4 illustrates the form used in obtaining the pressure distribution as a function of the pressure coefficient  $P$  and orifice location  $c/b$ . The values from which the distributions were plotted were obtained from table 8 for the NACA 16-(3)(06.50) blade section at  $x = 0.95$ . These plots show the variation with Mach number of the pressure distribution on this section at a constant angle of attack of approximately  $0.8^\circ$  (including the Goldstein correction for induced angle) and give the consequent change in section normal-force and pitching-moment coefficients. At a section helical Mach number of 0.64, the pressure distribution is obtained with the entire section operating in a subsonic field. When the Mach number is increased to 0.89 the effects of shock appear on the upper surface at about 0.75 chord. At speeds in the low supersonic range where  $M_x = 1.09$ , the shock moves back to the trailing edge.

The section normal-force and pitching-moment coefficient were derived by integration of the pressure-distribution plots and are listed for all test points in the tables. The method for obtaining the chordwise-force coefficients tabulated is described in detail in reference 2. For one test (table 6(e)), a plot of the normal-force, pitching-moment, and chordwise-force coefficients together with section Mach number and angle of attack are shown in figure 5 to illustrate a convenient form for use in further analysis of the blade-section data.

Blade-angle deflection.— The physical deflection of the propeller blade during the tests was measured by means of an optical deflectometer. These measurements were closely checked by independent computations, and the accuracy of this correction is believed to be within  $0.1^\circ$ . Owing to the thickness of the sections incorporated in the NACA 10-(3)(090)-03 propeller blade, the deflections measured are less than on the other blades in the series tested, and  $\Delta\beta$  in no case exceeds  $1^\circ$  in the tests on this blade.

Induced-angle correction.— The correction for induced angle tabulated in the paper was computed using Goldstein's correction as would be applied to a propeller having an optimum loading. Since the propeller did not operate with an optimum loading, this induced angle may be somewhat in error. A study of references 5 and 6 has indicated that the corrections used may be close to being correct for the arbitrary loadings obtained in these tests at radii up to  $x = 0.70$  but may be considerably in error near the tip. A detailed analysis of the problem of the induced-angle correction to be applied to the data from this series of tests is not within the scope of this paper and is the subject of further work.

Figure 6 shows the effect of the induced-angle correction on the normal-force-coefficient curve for the NACA 16-309 airfoil section at the 0.7 radius station operating at a helical Mach number of 0.70. The slope  $dc_n/d\alpha$  increased from 0.085 for the uncorrected angle ( $\alpha = \beta_x - \phi_0 + \Delta\beta$ ) to 0.115 for the corrected angle of attack ( $\alpha_x = \beta_x - \phi_0 + \Delta\beta - \alpha_1$ ). For reference, the Langley 24-inch-tunnel data (reference 7) for the same airfoil section are plotted in the figure. The induced-angle correction brings the propeller data closer to agreement with that from the Langley 24-inch tunnel although it is not certain that the data from airfoils operating as propeller-blade sections can be practically and consistently corrected to agree with two-dimensional airfoil data.

Blade loadings.— The variation of the normal-force coefficient along the blade radius at an advance ratio of 2.2 for three values of stream Mach number is shown in figure 7. At a forward Mach number of 0.38 all the blade sections operate at subcritical speeds and the load distribution is free from abrupt changes. When the air-stream Mach number is increased to 0.56 the lift distribution at radii between  $x = 0.60$  and  $x = 0.80$  undergoes little change, but inboard of  $x = 0.60$ , where thickness ratio varies from 0.10 to greater than 0.30 and helical Mach number varies from about 0.60 to 0.75, compressibility effects result in a loss of lift; outboard of  $x = 0.80$  where the helical Mach number varies from 0.85 to 0.97, a loss of lift is also experienced. With a further increase in air-stream Mach number to 0.65, a further loss of lift occurs over most of the blade; the loss is most pronounced in the region operating at helical Mach numbers between 0.85 and 0.97 ( $x = 0.60$  to 0.80), but outboard of  $x = 0.80$  where the section speeds are slightly supersonic the loss is relatively less than for other portions of the blade. This tendency toward loss of lift at section Mach numbers between 0.85 and 1.00 and subsequent recovery of lift at supersonic speeds is indicated by the data obtained with this thick propeller blade, as well as in the cases of the thinner propellers (references 2 and 3). The severe loss of lift over the inboard sections of this propeller indicates the very adverse effects of compressibility which result from operation of thick sections at supercritical subsonic speeds. This fact becomes apparent upon comparison of the radial load distributions obtained with this thick propeller with those obtained with the thinner propellers of references 2 and 3. The loss of lift at relatively low Mach numbers on the inboard portions of this thick propeller points to the desirability of using as thin sections as possible over the entire length of the blade, inboard as well as near the tip.

The distortion of the blade load distribution with changes in speed, shown in figure 7, points to one of the problems encountered in the

determination of the induced angle of attack. The loading does not correspond to a Betz or Goldstein loading, even at low speeds, and changes with Mach number. A sound approach to the determination of the induced angle will involve application of a method such as is presented in reference 5, to a large number of actual load distributions obtainable from these data, so that the effects of systematic changes in Mach number and advance ratio upon the induced angle may be ascertained.

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## REFERENCES

1. Evans, Albert J., and Limer, George: Preliminary Investigation to Determine Propeller Section Characteristics by Measuring the Pressure Distribution on an NACA 10-(3)(08)-03 Propeller under Operating Conditions. NACA RM L8E11, 1948.
2. Maynard, Julian D., and Murphy, Maurice P.: Pressure Distributions on the Blade Sections of the NACA 10-(3)(066)-033 Propeller under Operating Conditions. NACA RM L9L12, 1950.
3. Gray, W. H., and Hunt, Robert M.: Pressure Distributions on the Blade Sections of the NACA 10-(3)(049)-033 Propeller under Operating Conditions. NACA RM L9L23, 1950.
4. Corson, Blake W., Jr., and Maynard, Julian D.: The NACA 2000-Horsepower Propeller Dynamometer and Tests at High Speed of an NACA 10-(3)(08)-03 Two-Blade Propeller. NACA RM L7L29, 1948.
5. Theodorsen, Theodore: The Theory of Propellers. II - Method for Calculating the Axial Interference Velocity. NACA Rep. 776, 1944.
6. Kawada, Sandi: Calculation of Induced Velocity by Helical Vortices and Its Application to Propeller Theory. Rep. No. 172 (vol. XIV, 1), Aero. Res. Inst., Tokyo Imperial Univ., Jan. 1939.
7. Lindsey, W. F., Stevenson, D. B., and Daley, Bernard N.: Aerodynamic Characteristics of 24 NACA 16-Series Airfoils at Mach Numbers between 0.3 and 0.8. NACA TN 1546, 1948.

<sup>b</sup>Paired value.

TABLE 1.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(30.00) PROPELLER BLADE SECTION ( $x = 0.30$ ) - Continued

(b)  $M = 1350$  rpm.

J	2.533	2.389	2.266	2.076	1.940	1.791	1.657	1.492	1.415	1.565	1.715	1.863	1.998	2.159	2.309	2.471
$M_x$	.552	.521	.496	.462	.435	.407	.384	.357	.343	.370	.395	.423	.448	.477	.505	.537
$\alpha_x$	-.79	.33	1.38	3.22	4.71	6.55	8.43	11.08	12.47	9.86	7.59	5.63	4.05	2.38	1.00	-.32
$\Delta\theta$	0	0	0	0	0	.01	.01	.01	.01	.01	.01	.01	.01	0	0	0
$\alpha_1$	-.16	-.09	0	.04	.30	.53	.80	1.12	1.31	.96	.71	.42	.15	-.02	-.04	-.11
$c_n$	-.0723	-.0406	-.0013	.0161	.1258	.2194	.3277	.4445	.5142	.3865	.2910	.1755	.0645	-.0097	-.0161	-.0490
$c_m$	-.0080	.0170	.0537	.0931	.0998	.1118	.1180	.1311	.1321	.1255	.1114	.1055	.1000	.0798	.0292	.0029
$c_c$																
c/b	Pressure coefficient, P															
Upper surface	*0.000	1.078	1.069	1.063	1.055	1.049	1.042	1.038	1.032	1.030	1.035	1.040	1.046	1.052	1.059	1.065
	.025	.334	.194	.041	-.204	-.439	-.746	-1.099	-1.575	-1.828	-1.332	-.945	-.590	-.324	-.076	.099
	.050	-.034	-.188	-.323	-.568	-.787	-1.066	-1.371	-1.758	-1.971	-1.561	-.925	-.686	-.447	-.273	-.101
	.100	-.237	-.354	-.445	-.630	-.781	-.983	-1.184	-1.441	-1.579	-1.307	-.892	-.688	-.473	-.287	-.128
	.200	-.567	-.645	-.685	-.816	-.905	-1.035	-1.146	-1.262	-1.350	-1.194	-.892	-.687	-.475	-.286	-.130
	.300	-.726	-.766	-.769	-.863	-.908	-1.004	-1.045	-1.114	-1.164	-1.073	-.818	-.688	-.488	-.290	-.134
	.400	-.810	-.823	-.797	-.847	-.871	-.934	-.932	-.940	-.968	-.932	-.819	-.689	-.483	-.290	-.133
	.500	-.847	-.830	-.769	-.785	-.787	-.816	-.788	-.743	-.739	-.757	-.790	-.684	-.487	-.286	-.137
	.600	-.814	-.768	-.670	-.624	-.619	-.638	-.571	-.453	-.419	-.502	-.591	-.636	-.612	-.446	-.179
	.700	-.513	-.428	-.284	-.171	-.197	-.255	-.214	-.189	-.233	-.173	-.226	-.246	-.255	-.214	-.138
	.800	-.093	-.066	-.016	-.021	-.023	-.033	-.105	-.184	-.233	-.139	-.071	-.016	-.025	-.017	-.059
Lower surface	.900	-.068	-.048	-.004	-.035	-.045	-.026	-.113	-.189	-.243	-.148	-.075	.001	-.046	-.017	-.040
	.950	-.099	-.039	.006	-.013	-.001	-.047	-.113	-.184	-.233	-.143	-.083	-.006	-.022	-.030	-.049
	.0375	-.383	-.213	-.024	.139	.325	.482	.649	.822	.875	.749	.592	.408	.233	.051	-.126
	.075	-.511	-.371	-.205	-.078	.083	.221	.381	.563	.626	.486	.330	.155	.002	-.147	-.297
	.150	-.649	-.537	-.400	-.314	-.194	-.074	.047	.227	.283	.157	.021	-.124	-.250	-.365	-.482
	.250	-.709	-.624	-.512	-.458	-.349	-.269	-.159	-.023	.020	-.077	-.189	-.308	-.407	-.492	-.581
	.350	-.728	-.668	-.579	-.551	-.464	-.409	-.318	-.207	-.171	-.256	-.340	-.433	-.514	-.574	-.636
	.450	-.755	-.714	-.648	-.644	-.573	-.534	-.462	-.372	-.348	-.410	-.477	-.551	-.615	-.654	-.693
	.550	-.760	-.748	-.707	-.723	-.681	-.666	-.614	-.636	-.539	-.573	-.617	-.669	-.719	-.730	-.744
	.650	-.718	-.748	-.744	-.804	-.775	-.781	-.753	-.781	-.720	-.731	-.753	-.774	-.802	-.783	-.756
	.750	-.438	-.553	-.611	-.720	-.716	-.750	-.753	-.757	-.777	-.752	-.738	-.731	-.730	-.691	-.590
	.850	-.022	-.167	-.289	-.458	-.466	-.579	-.625	-.658	-.691	-.640	-.595	-.528	-.484	-.404	-.232
	.925	-.070	-.034	-.031	-.255	-.278	-.342	-.408	-.488	-.548	-.448	-.370	-.288	-.184	-.028	-.053
	.975	-.074	-.030	.018	-.086	-.066	-.120	-.210	-.309	-.367	-.260	-.164	-.081	-.093	-.047	-.055
	*1.000	-.076	-.017	.038	.010	.086	-.031	-.106	-.187	-.219	-.135	-.091	-.010	.025	.020	-.060

\*No orifice.

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TABLE 1.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(30.00) PROPELLER BLADE SECTION ( $x = 0.30$ ) - Continued

(c)  $N = 1500$  rpm.

$\frac{C_p}{C_{p0}}$	1.653 .429 8.49 0	1.786 .432 6.62 0	1.899 .475 5.19 0	2.029 .503 3.72 0	2.145 .526 2.52 0	2.282 .555 1.26 0	2.395 .580 .28 0	2.514 .607 -.65 0	2.454 .593 -.19 0	2.352 .569 .64 0	2.218 .540 1.82 0	2.094 .514 3.03 0	1.968 .486 4.37 0	1.849 .465 5.81 0	1.736 .440 7.30 0
$\frac{C_{p0}}{C_p}$	.79 .3260 .1234	.57 .2348 .1124	.34 .1432 .1085	.14 .0581 .0936	.01 .0032 .0778	-.16 -.0677 .0639	-.20 -.0877 .0436	-.30 -.1323 .0282	-.24 -.1039 .0372	-.23 -.0994 .0771	-.08 -.0342 .0736	.07 .0297 .0864	.24 .1013 .1008	.47 .1941 .1093	.67 .2761 .1178
$c/b$	Pressure coefficient, $P$														
Upper surface	$a_0$ .000	1.047	1.053	1.058	1.065	1.071	1.079	1.086	1.095	1.091	1.083	1.075	1.068	1.061	1.056
	.025	-1.091	-.770	-.518	-.262	-.070	.110	.223	.431	.282	.181	.018	-.168	-.373	-.633
	.050	-1.392	-1.112	-.883	-.640	-.449	-.271	-.156	-.032	-.093	-.197	-.361	-.544	-.745	-.986
	.100	-1.211	-1.026	-.870	-.698	-.562	-.433	-.350	-.251	-.302	-.378	-.500	-.634	-.773	-.941
	.200	-1.167	-1.069	-.970	-.866	-.780	-.702	-.657	-.588	-.624	-.667	-.739	-.827	-.912	-1.013
	.300	-1.063	-1.023	-.965	-.902	-.852	-.810	-.799	-.758	-.781	-.792	-.829	-.878	-.932	-.988
	.400	-.930	-.940	-.907	-.876	-.852	-.841	-.860	-.845	-.855	-.840	-.843	-.867	-.892	-.922
	.500	-.781	-.810	-.801	-.801	-.801	-.814	-.860	-.868	-.867	-.828	-.805	-.804	-.806	-.808
	.600	-.546	-.629	-.616	-.637	-.667	-.710	-.778	-.804	-.794	-.735	-.686	-.653	-.624	-.628
	.700	-.163	-.267	-.211	-.202	-.248	-.288	-.362	-.392	-.386	-.319	-.254	-.214	-.191	-.262
	.800	-.099	-.060	-.024	-.019	-.001	-.008	-.045	-.050	-.051	-.020	-.006	-.019	-.024	-.032
	.900	-.112	-.071	-.044	-.050	-.028	-.022	-.063	-.061	-.065	-.031	-.025	-.057	-.052	-.043
	.950	-.109	-.080	-.043	-.026	-.012	-.010	-.042	-.045	-.045	-.020	-.010	-.029	-.032	-.057
Lower surface	.0375	b.648	.507	.375	.217	.073	-.086	-.217	-.328	-.275	-.165	-.010	.138	.282	.434
	.075	.401	.247	.126	-.014	-.135	-.271	-.383	-.478	-.432	-.338	-.205	-.078	.044	.182
	.150	.081	-.051	-.154	-.264	-.364	-.475	-.564	-.642	-.604	-.529	-.418	-.319	-.219	-.106
	.250	-.157	-.255	-.336	-.423	-.502	-.590	-.659	-.719	-.691	-.631	-.547	-.467	-.388	-.298
	.350	-.305	-.396	-.460	-.532	-.596	-.659	-.709	-.751	-.731	-.688	-.628	-.565	-.505	-.431
	.450	-.454	-.528	-.579	-.635	-.680	-.727	-.760	-.788	-.776	-.747	-.705	-.660	-.614	-.553
	.550	-.610	-.667	-.703	-.734	-.760	-.788	-.799	-.804	-.802	-.796	-.775	-.750	-.722	-.683
	.650	-.762	-.793	-.806	-.813	-.818	-.814	-.799	-.783	-.791	-.810	-.818	-.816	-.800	-.772
	.750	-.765	-.761	-.756	-.734	-.711	-.690	-.680	-.592	-.643	-.708	-.700	-.727	-.748	-.755
	.850	-.616	-.635	-.558	-.474	-.402	-.351	-.337	-.282	-.310	-.358	-.369	-.449	-.510	-.600
	.925	-.403	-.353	-.315	-.221	-.146	-.124	-.141	-.109	-.125	-.149	-.136	-.200	-.270	-.331
	.975	-.214	-.174	-.130	-.055	-.030	-.029	-.049	-.050	-.047	-.043	-.034	-.052	-.088	-.145
	a1.000	-.043	-.103	-.043	.005	.011	.017	-.012	.002	-.006	-.017	.009	.017	.012	-.063

<sup>a</sup>No orifice.<sup>b</sup>Paired value.

NACA



TABLE 1.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-(3)(30.00) PROPELLER BLADE SECTION ( $x = 0.30$ ) -- Continued(d)  $N = 1600$  rpm.

	$c_u$	$c_{u_1}$	$c_{u_2}$	$c_{u_3}$	$c_{u_4}$	$c_{u_5}$	$c_{u_6}$	$c_{u_7}$	$c_{u_8}$	$c_{u_9}$	$c_{u_{10}}$	$c_{u_{11}}$	$c_{u_{12}}$
	2.465	2.419	2.364	2.310	2.244	2.192	2.135	2.070	2.017	1.952	1.902	1.846	
	.638	.627	.614	.600	.586	.574	.560	.544	.534	.519	.508	.494	
	-.28	.09	.54	.99	1.58	2.07	2.62	3.28	3.85	4.57	5.16	5.85	
	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	
	-.05	0	.03	.02	0	.02	.04	.09	.17	.28	.35	.43	
	-.0213	.0019	.0110	.0103	.0013	.0071	.0168	.0387	.0716	.1174	.1484	.1774	
	-.0170	-.0108	-.0023	.0203	.0493	.0655	.0783	.0896	.0962	.1014	.1100	.1196	
	$c/b$	Pressure coefficient, P											
Upper surface	0.000	1.104	1.102	1.097	1.093	1.088	1.085	1.080	1.076	1.073	1.069	1.066	1.062
	0.025	.390	.283	.217	.151	.076	.004	-.077	-.176	-.266	-.389	-.502	-.601
	0.050	-.051	-.099	-.171	-.240	-.315	-.389	-.472	-.569	-.659	-.777	-.884	-1.000
	0.100	-.258	-.294	-.349	-.403	-.463	-.516	-.578	-.649	-.712	-.795	-.872	-.926
	0.200	-.624	-.644	-.682	-.715	-.751	-.781	-.822	-.863	-.903	-.949	-.998	-1.015
	0.300	-.808	-.812	-.831	-.842	-.859	-.870	-.895	-.917	-.936	-.961	-.991	-.988
	0.400	-.898	-.889	-.891	-.888	-.886	-.881	-.889	-.897	-.903	-.912	-.929	-.909
	0.500	-.928	-.908	-.896	-.877	-.856	-.834	-.828	-.821	-.813	-.814	-.817	-.777
	0.600	-.865	-.841	-.818	-.792	-.721	-.681	-.653	-.628	-.611	-.612	-.610	-.551
	0.700	-.577	-.558	-.532	-.458	-.305	-.238	-.191	-.165	-.158	-.182	-.188	-.132
	0.800	-.185	-.168	-.146	-.103	-.070	-.053	-.051	-.047	-.044	-.037	-.042	-.020
	0.900	-.095	-.080	-.070	-.048	-.041	-.038	-.045	-.049	-.044	-.030	-.038	-.022
	0.950	-.090	-.077	-.070	-.051	-.036	-.032	-.039	-.040	-.039	-.033	-.045	-.027
Lower surface	0.0375	-.280	-.221	-.160	-.088	-.028	.037	.098	.163	.229	.317	.377	.469
	0.075	-.447	-.396	-.342	-.280	-.229	-.171	-.122	-.062	-.004	.071	.124	.211
	0.150	-.634	-.586	-.542	-.488	-.446	-.397	-.360	-.312	-.263	-.200	-.154	-.079
	0.250	-.729	-.685	-.648	-.605	-.573	-.532	-.504	-.469	-.428	-.377	-.343	-.276
	0.350	-.769	-.733	-.707	-.673	-.651	-.618	-.598	-.575	-.540	-.497	-.469	-.410
	0.450	-.813	-.783	-.765	-.738	-.725	-.701	-.690	-.673	-.646	-.609	-.590	-.539
	0.550	-.818	-.800	-.795	-.784	-.787	-.775	-.775	-.768	-.751	-.724	-.714	-.670
	0.650	-.754	-.755	-.774	-.787	-.820	-.823	-.832	-.842	-.837	-.823	-.824	-.789
	0.750	-.385	-.418	-.475	-.539	-.634	-.671	-.718	-.745	-.750	-.749	-.760	-.740
	0.850	-.090	-.080	-.087	-.124	-.263	-.342	-.397	-.435	-.463	-.497	-.529	-.559
	0.925	-.100	-.084	-.082	-.104	-.066	-.104	-.146	-.172	-.204	-.267	-.312	-.320
	0.975	-.103	-.089	-.066	-.104	-.038	-.032	-.037	-.038	-.044	-.083	-.135	-.146
	1.000	-.093	-.098	-.086	-.085	-.030	-.024	.006	.013	-.014	-.038	.009	0

<sup>a</sup>No orifice.<sup>b</sup>Reaired value.

NACA

TABLE 1.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(30.00) PROPELLER BLADE SECTION ( $x = 0.30$ ) - Continued

(a)  $M = 0.36$ .

	2.508	2.462	2.414	2.368	2.325	2.279	2.231	2.179	2.138	2.097	2.058	2.017	1.977	1.931
$J$	.601	.605	.606	.608	.610	.611	.613	.612	.614	.616	.618	.619	.620	.624
$M_x$	-.60	-.24	.10	.50	.83	1.24	1.70	2.19	2.59	3.00	3.40	3.80	4.29	4.58
$\Delta\delta$	0	0	0	.01	.01	.01	.02	.02	.02	.02	.02	.02	.03	.03
$\alpha_1$	-.19	-.15	-.12	.02	.03	.06	.05	.02	.04	.08	.13	.20	.26	.30
$\alpha_n$	-.0819	-.0639	-.0523	.0065	.0148	.0245	.0200	.0090	.0161	.0361	.0568	.0832	.1084	.1252
$\alpha_m$	.0051	.0087	.0141	-.0007	.0084	.0192	.0367	.0600	.0711	.0729	.0760	.0834	.0867	.0934
$\alpha_o$														
$a/b$	Pressure coefficient, P													
Upper surface	<sup>a</sup> 0.000	1.093	1.094	1.095	1.095	1.096	1.096	1.097	1.096	1.097	1.098	1.099	1.099	1.101
	.025	b.225	b.175	.266	.224	.188	.136	.089	.039	-.011	-.054	-.103	-.162	-.273
	.050	-.032	-.065	-.112	-.159	-.201	-.254	-.306	-.361	-.418	-.464	-.517	-.585	-.711
	.100	-.237	-.262	-.300	-.341	-.373	-.419	-.460	-.504	-.552	-.591	-.631	-.686	-.785
	.200	-.537	-.606	-.636	-.670	-.698	-.732	-.764	-.800	-.839	-.871	-.904	-.949	-.1.019
	.300	-.756	-.769	-.790	-.818	-.838	-.865	-.884	-.909	-.942	-.966	-.988	-1.019	-1.081
	.400	-.847	-.850	-.860	-.880	-.892	-.904	-.909	-.920	-.938	-.950	-.960	-.972	-.1.000
	.500	-.879	-.873	-.874	-.889	-.886	-.884	-.870	-.860	-.866	-.866	-.864	-.855	-.852
	.600	-.827	-.816	-.802	-.820	-.799	-.778	-.731	-.663	-.642	-.629	-.620	-.594	-.587
	.700	-.502	-.503	-.473	-.542	-.499	-.436	-.328	-.182	-.164	-.165	-.165	-.159	-.168
	.800	-.119	-.115	-.105	-.156	-.128	-.111	-.089	-.094	-.106	-.107	-.101	-.093	-.073
Lower surface	.900	-.079	-.065	-.058	-.070	-.062	-.057	-.048	-.069	-.083	-.080	-.073	-.078	-.089
	.950	-.076	-.061	-.057	-.070	-.064	-.061	-.048	-.057	-.067	-.068	-.066	-.070	-.075
	.0375	-.348	-.291	-.227	-.177	-.121	-.068	-.006	.040	.081	.127	.177	.235	.319
	.075	-.497	-.449	-.395	-.335	-.307	-.265	-.209	-.170	-.138	-.100	-.055	-.006	.071
	.150	-.658	-.621	-.580	-.549	-.513	-.479	-.437	-.405	-.383	-.349	-.312	-.274	-.210
	.250	-.730	-.704	-.673	-.654	-.625	-.601	-.570	-.548	-.533	-.508	-.480	-.449	-.401
	.350	-.759	-.742	-.722	-.706	-.689	-.674	-.651	-.639	-.631	-.612	-.592	-.568	-.533
	.450	-.752	-.781	-.770	-.761	-.750	-.743	-.731	-.727	-.727	-.713	-.699	-.681	-.659
	.550	-.759	-.796	-.795	-.790	-.789	-.794	-.793	-.801	-.811	-.803	-.797	-.787	-.750
	.650	-.759	-.760	-.767	-.766	-.776	-.798	-.815	-.844	-.864	-.863	-.867	-.869	-.892
	.750	-.486	-.494	-.510	-.467	-.497	-.539	-.587	-.651	-.690	-.696	-.711	-.726	-.770
	.850	-.150	-.153	-.166	-.184	-.094	-.116	-.163	-.281	-.344	-.354	-.375	-.395	-.439
	.925	-.114	-.106	-.101	-.079	-.077	-.073	-.061	-.089	-.115	-.125	-.125	-.143	-.170
	.975	-.108	-.097	-.093	-.084	-.080	-.077	-.057	-.053	-.057	-.058	-.052	-.060	-.068
	1.000	-.090	-.085	-.080	-.090	-.085	-.080	-.055	-.040	-.040	-.040	-.040	-.035	-.035

<sup>a</sup>No orifice.  
<sup>b</sup>Paired value.

NACA

TABLE 1.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(30.00) PROPELLER BLADE SECTION ( $x = 0.30$ ) - Continued

( $r$ )  $M = 0.60$ .

	$J$	$M_x$	$C_{x'}$	$\Delta p$	$C_{L1}$	$C_{L2}$	$C_{L3}$	$C_{L4}$	$C_{L5}$	$C_{L6}$	$C_{L7}$	$C_{L8}$	$C_{L9}$
	2.426	2.397	2.361	2.312	2.268	2.225	2.200	2.150	2.116	2.081	2.048	2.020	1.984
	.649	.650	.652	.653	.655	.655	.660	.657	.659	.660	.662	.669	.670
	.03	.27	.56	.98	1.37	1.76	1.99	2.47	2.81	3.17	3.51	3.81	4.21
	-.01	-.01	0	0	0	.01	.01	.01	.02	.02	.02	.02	.02
	-.14	-.12	-.09	-.05	.01	.03	.06	.11	.13	.17	.21	.24	.28
	-.0600	-.0503	-.0387	-.0232	-.0045	.0123	.0252	.0452	.0561	.0716	.0884	.1032	.1187
	.0134	.0161	.0187	.0220	.0252	.0431	.0451	.0587	.0636	.0688	.0737	.0732	.0760
													.0297
Pressure coefficient, $P$													
$a/b$													
Upper surface	$a_{0.000}$	1.110	1.110	1.111	1.111	1.112	1.112	1.113	1.112	1.113	1.113	1.114	1.117
	$b_{.120}$	.120	.145	.257	.217	.184	.128	.104	.046	-.020	-.066	-.087	-.130
	.050	-.067	-.089	-.130	-.174	-.211	-.246	-.300	-.370	-.402	-.443	-.518	-.569
	.100	-.272	-.290	-.324	-.359	-.392	-.446	-.464	-.522	-.549	-.583	-.642	-.682
	.200	-.644	-.657	-.687	-.713	-.744	-.796	-.809	-.866	-.892	-.889	-.940	-.1.001
	.300	-.833	-.841	-.864	-.881	-.910	-.956	-.967	-1.016	-1.046	-1.072	-1.113	-1.147
	.400	-.924	-.926	-.939	-.946	-.966	-.999	-.996	-1.029	-1.048	-1.064	-1.081	-1.129
	.500	-.943	-.932	-.935	-.923	-.934	-.946	-.933	-.942	-.944	-.909	-.933	-.917
	.600	-.824	-.799	-.790	-.755	-.762	-.749	-.720	-.710	-.696	-.680	-.653	-.604
	.700	-.342	-.306	-.303	-.264	-.292	-.280	-.255	-.247	-.236	-.230	-.218	-.209
Lower surface	.800	-.128	-.122	-.122	-.112	-.113	-.117	-.103	-.107	-.102	-.095	-.099	-.119
	.900	-.097	-.089	-.089	-.078	-.075	-.083	-.071	-.082	-.085	-.115	-.108	-.117
	.950	-.084	-.076	-.080	-.072	-.075	-.082	-.074	-.085	-.085	-.085	-.091	-.092
	.0375	-.256	-.211	-.166	-.099	-.062	-.014	.034	.075	.111	.155	.194	.268
	.075	-.432	-.391	-.354	-.296	-.268	-.227	-.179	-.146	-.114	-.077	-.043	-.024
	.150	-.627	-.592	-.563	-.514	-.493	-.464	-.422	-.399	-.373	-.344	-.316	-.299
	.250	-.730	-.702	-.679	-.641	-.628	-.607	-.574	-.559	-.541	-.518	-.496	-.452
	.350	-.777	-.755	-.741	-.712	-.705	-.696	-.666	-.661	-.649	-.634	-.620	-.588
	.450	-.829	-.812	-.806	-.784	-.786	-.785	-.760	-.763	-.759	-.750	-.743	-.719
	.550	-.841	-.832	-.835	-.826	-.834	-.846	-.832	-.850	-.853	-.854	-.857	-.849
NACA	.650	-.790	-.757	-.801	-.805	-.821	-.855	-.848	-.885	-.903	-.920	-.937	-.962
	.750	-.487	-.494	-.514	-.532	-.553	-.604	-.602	-.664	-.686	-.706	-.726	-.740
	.850	-.155	-.157	-.167	-.180	-.191	-.243	-.230	-.296	-.316	-.335	-.352	-.375
	.925	-.122	-.115	-.111	-.101	-.088	-.106	-.095	-.111	-.112	-.118	-.129	-.151
	.975	-.112	-.105	-.101	-.091	-.079	-.085	-.074	-.072	-.064	-.071	-.078	-.101
	1.000	-.069	-.080	-.095	-.087	-.060	-.082	-.075	-.068	-.052	-.058	-.068	-.089

<sup>a</sup>No orifice.

<sup>b</sup>Paired value.

TABLE 1.-- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(30.00) PROPELLER BLADE SECTION ( $x = 0.30$ ) -- Concluded

(g)  $M = 0.64$ 

	2.374	2.344	2.319	2.286	2.255	2.231	2.199	2.172	2.142	2.125	2.095	2.069	2.042	2.020	1.999	1.984
$\frac{J}{M_\infty}$	.680	.683	.687	.689	.691	.691	.692	.694	.694	.698	.698	.700	.701	.701	.701	.701
$\alpha_{x'}$	.45	.70	.87	1.20	1.48	1.70	2.00	2.26	2.56	2.70	3.00	3.29	3.58	3.80	4.00	4.20
$\Delta\theta$	.01	.02	.02	.02	.02	.02	.02	.03	.03	.03	.04	.04	.04	.04	.04	.04
$\alpha_i$	-.21	-.20	-.17	-.13	-.09	-.04	.02	.06	.10	.11	.18	.30	.30	.31	.35	.42
$c_n$	-.0897	-.0877	-.0723	-.0581	-.0374	-.0174	.0065	.0277	.0419	.0458	.0781	.1277	.1258	.1297	.1465	.1768
$c_m$	.0361	.0415	.0454	.0485	.0475	.0505	.0505	.0531	.0537	.0577	.0551	.0397	.0485	.0515	.0516	.0460
$c_o$	.0357	.0367	.0376	.0371	.0371	.0365	.0380	.0393	.0398	.0402	.0427	.0381	.0395	.0401	.0389	.0391
$o/b$	Pressure coefficient, P															
Upper surface	0.000	1.121	1.123	1.124	1.125	1.126	1.126	1.126	1.127	1.127	1.128	1.128	1.129	1.130	1.130	1.130
	.025	1.250	1.295	.253	.230	.200	.177	.150	.127	.102	.086	.055	.020	.009	-.012	-.035
	.050	-.085	-.111	-.137	-.164	-.196	-.223	-.254	-.280	-.308	-.327	-.363	-.383	-.413	-.435	-.475
	.100	-.286	-.308	-.329	-.352	-.378	-.401	-.426	-.449	-.470	-.485	-.514	-.532	-.553	-.590	-.599
	.200	-.676	-.697	-.715	-.737	-.761	-.783	-.809	-.834	-.856	-.865	-.898	-.914	-.915	-.934	-.985
	.300	-.879	-.899	-.918	-.941	-.961	-.976	-.995	-.1.011	-.1.027	-.1.035	-.1.068	-.1.087	-.1.115	-.1.133	-.1.174
	.400	-.975	-.991	-.1.005	-.1.015	-.1.026	-.1.043	-.1.060	-.1.084	-.1.110	-.1.129	-.1.167	-.1.177	-.1.170	-.1.161	-.1.204
	.500	-.991	-.955	-.949	-.955	-.962	-.970	-.986	-.997	-.995	-.991	-.1.007	-.1.026	-.1.009	-.1.003	-.1.002
	.600	-.721	-.690	-.667	-.656	-.663	-.671	-.688	-.691	-.671	-.660	-.676	-.703	-.666	-.651	-.638
	.700	-.220	-.206	-.200	-.201	-.223	-.244	-.275	-.289	-.287	-.287	-.312	-.354	-.311	-.303	-.293
	.800	-.132	-.141	-.145	-.152	-.151	-.145	-.143	-.140	-.141	-.139	-.152	-.158	-.151	-.150	-.169
	.900	-.132	-.129	-.127	-.128	-.122	-.111	-.114	-.116	-.128	-.129	-.147	-.150	-.176	-.181	-.191
	.950	-.099	-.097	-.095	-.098	-.099	-.102	-.111	-.118	-.128	-.127	-.144	-.150	-.151	-.149	-.174
Lower surface	.0375	-.171	-.136	-.097	-.065	-.028	.008	.036	.068	.094	.124	.152	.179	.202	.233	.264
	.075	-.359	-.329	-.294	-.265	-.235	-.201	-.179	-.150	-.125	-.100	-.076	-.050	-.031	-.004	.025
	.150	-.588	-.567	-.535	-.513	-.486	-.460	-.439	-.419	-.399	-.375	-.356	-.332	-.318	-.294	-.266
	.250	-.715	-.699	-.676	-.658	-.636	-.615	-.600	-.583	-.567	-.549	-.533	-.512	-.505	-.481	-.463
	.350	-.782	-.771	-.753	-.740	-.729	-.709	-.699	-.688	-.674	-.660	-.653	-.635	-.631	-.614	-.597
	.450	-.847	-.843	-.831	-.827	-.818	-.806	-.794	-.784	-.784	-.804	-.771	-.759	-.758	-.744	-.735
	.550	-.885	-.888	-.887	-.889	-.892	-.890	-.892	-.895	-.895	-.898	-.887	-.887	-.889	-.892	-.891
	.650	-.857	-.870	-.879	-.889	-.901	-.908	-.921	-.939	-.949	-.971	-.982	-.965	-.998	-.1.010	-.1.006
	.750	-.584	-.592	-.604	-.618	-.627	-.632	-.643	-.650	-.657	-.663	-.669	-.697	-.613	-.634	-.596
	.850	-.273	-.281	-.290	-.297	-.300	-.303	-.309	-.316	-.320	-.318	-.324	-.337	-.250	-.267	-.246
	.925	-.144	-.142	-.140	-.143	-.143	-.140	-.140	-.143	-.149	-.142	-.152	-.135	-.152	-.152	-.186
	.975	-.111	-.106	-.098	-.094	-.088	-.088	-.091	-.096	-.105	-.101	-.114	-.120	-.133	-.132	-.175
	1.000	-.080	-.082	-.082	-.065	-.060	-.072	-.083	-.081	-.087	-.100	-.104	-.120	-.135	-.130	-.170

\*No orifice.

bPaired value.

NACA



TABLE 2.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(17.30) PROPELLER BLADE SECTION ( $x = 0.45$ ) - Continued

(b)  $N = 1350$  rpm.

	2.558	2.408	2.268	2.097	1.971	1.817	1.676	1.480	1.564	1.759	1.891	2.011	2.181	2.344	2.484
$J$	.585	.577	.530	.502	.477	.456	.433	.398	.419	.448	.472	.490	.520	.547	.572
$\alpha_{x1}$	-1.77	-.28	1.24	3.29	5.23	7.18	9.45	14.17	11.41	8.09	6.08	4.41	2.25	.40	-1.06
$\Delta\theta$	.02	.02	.03	.04	.05	.06	.06	.08	.07	.06	.05	.04	.04	.02	.02
$\alpha_1$	-.11	.12	.38	.74	1.00	1.31	1.67	2.41	1.98	1.45	1.15	.89	.57	.24	-.01
$c_n$	-.0481	.0510	.1294	.3069	.4242	.5335	.6729	.9484	.7948	.5903	.4716	.3671	.2368	.0997	-.0042
$c_m$	-.0354	-.0197	-.0084	.0055	.0233	.0388	.0490	.0470	.0519	.0436	.0323	.0154	-.0048	-.0152	-.0258
$c_c$															
$a/b$	Pressure coefficient, $P$														
Upper surface	0.000	1.088	1.079	1.072	1.064	1.058	1.053	1.048	1.041	1.035	1.028	1.027	1.022	1.019	1.014
	.025	.478	.138	-.112	-.512	-.920	-1.384	-1.990	-2.982	-2.450	-1.640	-1.149	-.732	-.305	.023
	.050	.090	-.130	-.343	-.667	-.983	-1.330	-1.736	-2.450	-2.065	-1.519	-1.151	-.843	-.503	-.230
	.100	-.130	-.307	-.471	-.699	-.910	-1.133	-1.373	-1.860	-1.594	-1.234	-1.018	-.817	-.585	-.384
	.200	-.314	-.442	-.550	-.694	-.825	-.934	-1.094	-1.564	-1.205	-1.007	-.880	-.772	-.624	-.493
	.300	-.439	-.536	-.609	-.706	-.786	-.866	-.969	-1.131	-1.069	-.919	-.812	-.762	-.661	-.569
	.400	-.506	-.577	-.625	-.689	-.733	-.786	-.852	-.934	-.870	-.816	-.750	-.721	-.659	-.594
	.500	-.549	-.593	-.620	-.655	-.675	-.701	-.727	-.737	-.717	-.710	-.674	-.676	-.640	-.603
	.600	-.576	-.597	-.605	-.619	-.607	-.593	-.578	-.515	-.531	-.527	-.522	-.613	-.615	-.598
	.700	-.500	-.520	-.526	-.476	-.441	-.371	-.312	-.270	-.246	-.339	-.400	-.464	-.503	-.523
	.800	-.287	-.291	-.279	-.246	-.154	-.058	-.057	-.198	-.093	-.048	-.091	-.206	-.273	-.303
	.900	.033	.026	.036	.064	.083	.030	-.032	-.198	-.083	-.001	-.064	.077	.035	.029
	.950	.208	.175	.154	.132	.094	.030	-.038	-.219	-.093	-.001	-.067	.100	.138	.172
Lower surface	.0375	-.574	-.342	-.114	.173	.394	.574	.740	.961	.870	.652	.490	.289	.035	-.228
	.075	-.544	-.381	-.200	.023	.199	.354	.511	.765	.641	.428	.284	.112	-.085	-.287
	.150	-.479	-.379	-.259	-.095	.036	.155	.278	.502	.395	.211	.099	-.029	-.176	-.318
	.250	-.449	-.385	-.299	-.173	-.072	.019	.117	.305	.212	.064	-.023	-.125	-.236	-.342
	.350	-.424	-.387	-.321	-.224	-.122	-.067	.002	.160	.086	-.036	-.101	-.186	-.278	-.354
	.450	-.435	-.418	-.369	-.287	-.222	-.160	-.107	.021	-.033	-.131	-.183	-.257	-.328	-.392
	.550	-.435	-.434	-.400	-.338	-.288	-.243	-.206	-.106	-.149	-.225	-.299	-.317	-.374	-.417
	.650	-.416	-.432	-.416	-.367	-.335	-.308	-.287	-.216	-.242	-.295	-.316	-.358	-.392	-.422
	.750	-.327	-.371	-.374	-.357	-.346	-.340	-.333	-.303	-.305	-.337	-.340	-.358	-.365	-.371
	.850	-.099	-.181	-.211	-.229	-.259	-.280	-.299	-.314	-.292	-.289	-.264	-.252	-.218	-.190
	.925	.147	.079	.040	-.008	-.062	-.106	-.138	-.198	-.153	-.082	-.050	.021	.063	.092
	.975	.216	.195	.188	.127	.036	-.035	-.097	-.208	-.153	-.066	-.004	.062	.173	.188
	1.000	.240	.225	.220	.165	.075	0	-.085	-.230	-.140	-.060	.025	.100	.200	.210

\*No orifice.

NACA

TABLE 2.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(17.30) PROPELLER BLADE SECTION ( $x = 0.45$ ) - Continued

(c)  $N = 1500$  rpm.

$J$	2.535	2.402	2.221	2.087	1.963	1.854	1.731	1.599	1.662	1.792	1.906	1.958	2.012	2.143	2.311	2.478	
$M_{\infty}$	.653	.621	.583	.558	.535	.516	.492	.473	.483	.503	.524	.535	.545	.571	.601	.638	
$\Delta\theta$	-1.55	-.22	1.78	3.41	5.06	6.63	8.54	10.78	9.68	7.57	5.87	5.13	4.39	2.71	.75	-.99	
$c_l$	.01	.01	.02	.03	.04	.05	.05	.06	.06	.05	.04	.04	.04	.03	.02	.01	
$c_m$	-.21	0	.45	.72	.94	1.25	1.57	1.92	1.79	1.41	1.09	.97	.85	.62	.27	-.01	
$c_c$	-.0888	0	.1903	.3006	.3877	.5097	.6361	.7697	.7206	.5723	.4458	.4006	.3510	.2594	.1139	-.0548	
	-.0158	.0014	.0013	.0167	.0326	.0426	.0483	.0564	.0547	.0464	.0383	.0338	.0272	.0082	-.0080	-.0042	
$c/b$	Pressure coefficient, $P$																
Upper surface	0.000	1.111	1.100	1.088	1.080	1.073	1.068	1.062	1.057	1.060	1.065	1.070	1.073	1.076	1.084	1.093	1.106
	.025	.371	.168	-.176	-.514	-.873	-1.295	-1.805	-2.692	-2.217	-1.530	-1.089	-.898	-.722	-.404	.004	.275
	.050	.076	-.113	-.414	-.693	-.975	-1.297	-1.675	-2.004	-1.899	-1.473	-1.146	-.998	-.860	-.572	-.257	-.015
	.100	-.156	-.308	-.535	-.732	-.923	-1.127	-1.315	-1.589	-1.483	-1.242	-1.033	-.937	-.849	-.649	-.418	-.232
	.200	-.356	-.459	-.611	-.732	-.849	-.953	-1.082	-1.218	-1.157	-1.004	-.912	-.854	-.807	-.682	-.532	-.412
	.300	-.495	-.561	-.668	-.746	-.818	-.881	-.969	-1.050	-1.009	-.925	-.844	-.823	-.794	-.716	-.613	-.534
	.400	-.569	-.605	-.677	-.724	-.761	-.799	-.849	-.893	-.868	-.826	-.777	-.760	-.756	-.702	-.635	-.592
	.500	-.622	-.629	-.660	-.681	-.689	-.706	-.727	-.736	-.722	-.720	-.703	-.688	-.692	-.670	-.640	-.632
	.600	-.646	-.626	-.632	-.624	-.613	-.597	-.577	-.549	-.553	-.591	-.606	-.610	-.616	-.633	-.624	-.640
	.700	-.532	-.499	-.507	-.495	-.412	-.358	-.299	-.251	-.238	-.334	-.386	-.409	-.436	-.467	-.510	-.517
	.800	-.242	-.210	-.260	-.159	-.073	-.039	-.049	-.091	-.066	-.040	-.053	-.069	-.100	-.223	-.268	-.220
	.900	.082	.099	.042	.053	.066	.028	-.024	-.080	-.050	.003	.049	.066	.066	.047	.095	
	.950	.127	.109	.120	.049	.066	.026	-.029	-.091	-.055	-.002	.049	.066	.070	.082	.151	.113
Lower surface	.0375	-.629	-.373	-.047	.183	.370	.538	.694	.776	.752	.608	.458	.378	.292	.092	-.196	-.512
	.075	-.614	-.418	-.154	.088	.178	.326	.466	.597	.552	.387	.253	.186	.116	-.044	-.268	-.525
	.150	-.553	-.418	-.237	-.100	.016	.131	.244	.353	.317	.181	.073	.023	-.036	-.154	-.317	-.497
	.250	-.527	-.428	-.290	-.184	-.093	0	.089	.174	.148	.037	-.046	-.086	-.133	-.225	-.351	-.487
	.350	-.503	-.432	-.324	-.239	-.165	-.088	-.014	.033	.036	-.057	-.125	-.158	-.199	-.272	-.371	-.478
	.450	-.521	-.466	-.378	-.306	-.246	-.181	-.119	-.067	-.076	-.156	-.215	-.243	-.275	-.335	-.414	-.503
	.550	-.524	-.490	-.423	-.367	-.318	-.265	-.217	-.185	-.180	-.245	-.291	-.313	-.341	-.387	-.449	-.517
	.650	-.505	-.492	-.444	-.404	-.370	-.334	-.294	-.275	-.266	-.319	-.352	-.366	-.387	-.418	-.458	-.510
	.750	-.411	-.432	-.408	-.392	-.381	-.362	-.344	-.338	-.326	-.358	-.372	-.379	-.390	-.396	-.407	-.433
	.850	-.185	-.248	-.243	-.272	-.290	-.297	-.307	-.313	-.300	-.305	-.293	-.287	-.284	-.253	-.220	-.232
	.925	.044	-.010	.004	-.066	-.191	-.116	-.142	-.161	-.146	-.129	-.104	-.091	-.083	-.028	.037	.005
	.975	.126	.099	.150	.028	-.001	-.041	-.087	-.140	-.107	-.064	-.021	-.001	.006	.098	.166	.102
	1.000	.148	.120	.177	.042	.049	0	-.051	-.113	-.097	-.038	.019	.057	.060	.230	.136	.136

<sup>a</sup>No orifice.

NACA

TABLE 2.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(17,30) PROPELLER BLADE SECTION ( $x = 0.45$ ) - Continued

(d)  $N = 1600$  rpm.

J	2.492	2.423	2.342	2.280	2.173	2.088	2.088	1.941	1.772	1.837	1.959	2.048	2.136	2.223	2.300	2.374	2.470	
M <sub>x</sub>	.680	.666	.647	.632	.610	.593	.581	.564	.530	.543	.568	.588	.603	.623	.639	.655	.676	
α <sub>x</sub>	-1.13	-.44	.42	1.10	2.35	3.40	4.18	5.37	7.88	6.88	5.12	3.92	2.80	1.75	.88	.07	-.92	
Δθ	.06	.06	.07	.07	.08	.09	.09	.10	.11	.11	.10	.09	.08	.08	.07	.06	.06	
α <sub>1</sub>	-.24	-.10	.07	.22	.44	.66	.80	1.03	1.50	1.29	.99	.76	.54	.34	.14	.01	-.18	
c <sub>n</sub>	-.1045	-.0406	.0306	.0913	.1845	.2742	.3323	.4213	.6071	.5265	.4052	.3129	.2258	.1423	.0574	.0035	-.0761	
c <sub>m</sub>	.0048	.0052	.0118	.0184	.0244	.0308	.0367	.0428	.0516	.0470	.0415	.0341	.0285	.0210	.0168	.0103	.0017	
c <sub>c</sub>																		
c/b	Pressure coefficient, P																	
Upper surface	0.000	1.121	1.116	1.109	1.103	1.096	1.090	1.087	1.082	1.072	1.075	1.063	1.069	1.094	1.100	1.106	1.112	
	.025	.335	.291	.097	-.029	-.244	-.499	-.664	-.955	-1.650	-1.350	-.899	-.597	-.352	-.140	.020	.150	
	.050	.037	-.059	-.181	-.293	-.482	-.666	-.829	-1.064	-1.595	-1.371	-1.022	-.778	-.572	-.394	-.253	-.134	
	.100	-.196	-.276	-.370	-.454	-.599	-.748	-.841	-.995	-1.329	-1.195	-.970	-.808	-.663	-.532	-.429	-.337	
	.200	-.398	-.453	-.515	-.567	-.666	-.757	-.814	-.903	-1.068	-1.006	-.891	-.810	-.702	-.619	-.555	-.495	
	.300	-.542	-.581	-.615	-.648	-.720	-.774	-.810	-.877	-.971	-.925	-.855	-.799	-.739	-.683	-.644	-.604	
	.400	-.624	-.648	-.658	-.671	-.720	-.748	-.770	-.788	-.855	-.840	-.785	-.767	-.720	-.687	-.671	-.652	
	.500	-.670	-.673	-.664	-.659	-.684	-.694	-.697	-.708	-.727	-.729	-.706	-.703	-.681	-.668	-.671	-.668	
	.600	-.670	-.661	-.640	-.621	-.634	-.612	-.611	-.603	-.577	-.598	-.609	-.612	-.619	-.623	-.638	-.649	
	.700	-.480	-.486	-.470	-.446	-.437	-.417	-.398	-.364	-.296	-.336	-.372	-.412	-.419	-.437	-.463	-.476	
.800	-.095	-.155	-.161	-.140	-.099	-.050	-.024	-.020	-.041	-.032	-.021	-.038	-.063	-.118	-.150	-.159		
.900	.069	.073	.076	.070	.047	.058	.064	.049	-.015	.010	.050	.059	.052	.050	.071	.075		
.950	.079	.082	.090	.084	.042	.054	.064	.049	-.019	.006	.050	.059	.045	.051	.083	.083		
Lower surface	.0375	-.557	-.430	-.277	-.145	.018	.192	.286	.419	.649	.550	.390	.242	.101	-.056	-.209	-.335	
	.075	-.586	-.480	-.350	-.237	-.109	.032	.106	.222	.428	.337	.197	.072	-.038	-.162	-.296	-.401	
	.150	-.544	-.471	-.380	-.300	-.209	-.100	.041	.067	.211	.138	.029	-.072	-.155	-.245	-.342	-.415	
	.250	-.531	-.475	-.406	-.343	-.276	-.187	-.139	-.068	.061	.002	-.085	-.166	-.233	-.304	-.379	-.434	
	.350	-.519	-.479	-.422	-.372	-.319	-.245	-.204	-.146	-.037	-.088	-.158	-.227	-.280	-.338	-.402	-.444	
	.450	-.547	-.513	-.468	-.426	-.382	-.319	-.285	-.235	-.139	-.183	-.245	-.302	-.312	-.397	-.452	-.487	
	.550	-.559	-.538	-.502	-.468	-.436	-.380	-.354	-.313	-.238	-.275	-.323	-.370	-.406	-.445	-.492	-.518	
	.650	-.548	-.537	-.514	-.490	-.461	-.425	-.404	-.372	-.316	-.345	-.378	-.416	-.444	-.473	-.512	-.527	
	.750	-.454	-.460	-.455	-.444	-.439	-.414	-.404	-.386	-.360	-.377	-.390	-.412	-.424	-.437	-.458	-.479	
	.850	-.247	-.262	-.274	-.281	-.297	-.291	-.294	-.297	-.309	-.309	-.295	-.295	-.293	-.283	-.287	-.271	-.244
	.925	-.032	-.033	-.040	-.052	-.079	-.087	-.089	-.104	-.139	-.130	-.102	-.093	-.081	-.066	-.062	-.041	-.018
	.975	.061	.071	.071	.055	.011	.006	.005	-.016	-.077	-.054	-.013	0	.007	.034	.046	.068	.075
	1.000	.084	.084	.097	.086	.022	.040	.032	.017	-.058	-.020	.012	.041	.027	.050	.079	.090	.063

\*No orifice.

NACA



TABLE 2.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(17.30) PROPELLER BLADE SECTION ( $\alpha = 0.45$ ) - Continued

(a)  $M = 0.56$ .

	$\frac{C_p}{\rho V^2}$	$\frac{C_{p,x}}{\rho V^2}$	$\frac{C_{p,y}}{\rho V^2}$	$\frac{C_{p,z}}{\rho V^2}$	$\frac{C_{p,w}}{\rho V^2}$	$\frac{C_{p,u}}{\rho V^2}$	$\frac{C_{p,v}}{\rho V^2}$	$\frac{C_{p,w}}{\rho V^2}$	$\frac{C_{p,u}}{\rho V^2}$	$\frac{C_{p,v}}{\rho V^2}$	$\frac{C_{p,w}}{\rho V^2}$	$\frac{C_{p,u}}{\rho V^2}$	$\frac{C_{p,v}}{\rho V^2}$	$\frac{C_{p,w}}{\rho V^2}$	$\frac{C_{p,u}}{\rho V^2}$	$\frac{C_{p,v}}{\rho V^2}$	$\frac{C_{p,w}}{\rho V^2}$	$\frac{C_{p,u}}{\rho V^2}$
$\frac{c}{b}$	Pressure coefficient, $P$																	
Upper surface	0.000	1.127	1.125	1.124	1.123	1.122	1.121	1.121	1.120	1.119	1.117	1.117	1.115	1.114	1.113	1.112	1.111	1.109
	0.025	-0.614	-0.576	-0.527	-0.468	-0.401	-0.341	-0.279	-0.233	-0.167	-0.123	-0.090	0	0.054	0.106	0.180	0.222	0.279
	0.050	-0.888	-0.844	-0.789	-0.727	-0.661	-0.599	-0.539	-0.494	-0.432	-0.391	-0.322	-0.272	-0.221	-0.172	-0.105	-0.066	-0.012
	0.100	-0.997	-0.927	-0.886	-0.831	-0.775	-0.726	-0.673	-0.634	-0.582	-0.549	-0.490	-0.448	-0.409	-0.366	-0.312	-0.278	-0.232
	0.200	-1.000	-0.963	-0.925	-0.880	-0.845	-0.806	-0.765	-0.731	-0.688	-0.658	-0.611	-0.576	-0.548	-0.515	-0.475	-0.450	-0.379
	0.300	-1.071	-1.046	-1.018	-0.960	-0.919	-0.878	-0.839	-0.807	-0.772	-0.745	-0.704	-0.672	-0.647	-0.620	-0.589	-0.567	-0.509
	0.400	-1.127	-1.061	-0.995	-0.927	-0.887	-0.855	-0.829	-0.801	-0.775	-0.761	-0.726	-0.703	-0.687	-0.665	-0.643	-0.630	-0.605
	0.500	-0.742	-0.745	-0.755	-0.748	-0.754	-0.754	-0.745	-0.735	-0.722	-0.714	-0.698	-0.686	-0.681	-0.668	-0.659	-0.653	-0.638
	0.600	-0.556	-0.573	-0.588	-0.590	-0.606	-0.616	-0.627	-0.626	-0.633	-0.638	-0.636	-0.633	-0.641	-0.639	-0.640	-0.643	-0.637
	0.700	-0.199	-0.230	-0.257	-0.277	-0.310	-0.338	-0.356	-0.365	-0.389	-0.409	-0.421	-0.425	-0.448	-0.460	-0.468	-0.482	-0.495
	0.800	0	0.005	0.006	0.012	0.008	0.004	-0.008	-0.012	-0.037	-0.061	-0.090	-0.087	-0.126	-0.145	-0.153	-0.169	-0.189
	0.900	-0.045	-0.080	0.002	0.018	0.023	0.025	0.027	0.034	0.027	0.023	0.037	0.053	0.081	0.082	0.082	0.081	0.085
	0.950	0.006	0.013	0.017	0.024	0.024	0.024	0.027	0.034	0.031	0.026	0.045	0.068	0.089	0.092	0.090	0.090	0.098
Lower surface	0.0375	0.354	0.320	0.282	0.249	0.197	0.153	0.104	0.070	0.012	-0.027	-0.097	-0.147	-0.211	-0.266	-0.335	-0.423	-0.484
	0.075	0.165	0.138	0.105	0.078	0.032	-0.004	-0.044	-0.072	-0.118	-0.151	-0.207	-0.247	-0.296	-0.341	-0.416	-0.469	-0.510
	0.150	-0.003	-0.026	-0.053	-0.073	-0.107	-0.133	-0.165	-0.185	-0.219	-0.242	-0.283	-0.309	-0.345	-0.374	-0.424	-0.458	-0.527
	0.250	-0.121	-0.141	-0.162	-0.175	-0.203	-0.223	-0.250	-0.264	-0.290	-0.307	-0.337	-0.358	-0.383	-0.401	-0.438	-0.463	-0.479
	0.350	-0.207	-0.221	-0.240	-0.247	-0.271	-0.283	-0.305	-0.317	-0.337	-0.350	-0.375	-0.397	-0.409	-0.420	-0.448	-0.464	-0.473
	0.450	-0.310	-0.319	-0.337	-0.337	-0.357	-0.367	-0.383	-0.393	-0.408	-0.419	-0.437	-0.444	-0.461	-0.466	-0.487	-0.498	-0.500
	0.550	-0.407	-0.415	-0.425	-0.421	-0.435	-0.441	-0.455	-0.460	-0.469	-0.476	-0.488	-0.492	-0.502	-0.503	-0.516	-0.524	-0.518
	0.650	-0.487	-0.489	-0.495	-0.486	-0.493	-0.496	-0.505	-0.506	-0.509	-0.512	-0.518	-0.517	-0.521	-0.517	-0.522	-0.524	-0.513
	0.750	-0.499	-0.497	-0.497	-0.485	-0.487	-0.482	-0.484	-0.482	-0.479	-0.476	-0.474	-0.469	-0.467	-0.457	-0.452	-0.450	-0.434
	0.850	-0.373	-0.370	-0.366	-0.354	-0.349	-0.341	-0.336	-0.328	-0.321	-0.313	-0.303	-0.295	-0.287	-0.274	-0.263	-0.257	-0.237
	0.925	-0.151	-0.144	-0.140	-0.128	-0.122	-0.116	-0.111	-0.104	-0.096	-0.086	-0.076	-0.068	-0.055	-0.042	-0.032	-0.029	-0.012
	0.975	-0.049	-0.045	-0.042	-0.032	-0.029	-0.023	-0.018	-0.009	-0.002	0.007	0.023	0.036	0.053	0.069	0.073	0.074	0.090
	1.000	0.065	0.052	0.023	-0.002	0.029	0.014	0.027	0.031	0.031	0.023	0.053	0.077	0.085	0.095	0.096	0.087	0.109

\*No orifice.

NACA

TABLE 2.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(17.30) PROPELLER BLADE SECTION ( $x = 0.45$ ) - Continued

( $r$ )  $M = 0.60$ .

J	1.961	1.985	2.017	2.042	2.073	2.106	2.131	2.158	2.192	2.223	2.264	2.294	2.328	2.358	2.390	2.434
$M_x$	.740	.737	.734	.728	.727	.725	.722	.719	.716	.715	.713	.711	.708	.703	.701	.699
$\alpha_x'$	5.09	4.76	4.32	3.98	3.60	3.17	2.87	2.52	2.11	1.74	1.27	.94	.56	.24	-.10	-.56
$\Delta\theta$	.11	.10	.09	.09	.08	.07	.06	.05	.04	.03	.02	.01	0	-.01	-.02	-.03
$\alpha_1$	.77	.74	.66	.60	.49	.42	.36	.30	.23	.18	.09	.06	.01	-.04	-.11	-.17
$\alpha_n$	.3187	.3039	.2729	.2497	.2032	.1755	.1497	.1232	.0955	.0748	.0394	.0258	.0038	-.0174	-.0459	-.0697
$\alpha_m$	.0493	.0511	.0527	.0511	.0539	.0519	.0462	.0424	.0429	.0390	.0338	.0213	.0154	.0121	.0085	.0057
$\alpha_0$	.0168	.0128	.0096	.0086	.0082	.0088	.0089	.0104	.0117	.0138						
$a/b$	Pressure coefficient, P															
Upper surface	.0000	1.145	1.144	1.143	1.141	1.140	1.139	1.138	1.137	1.135	1.135	1.134	1.133	1.132	1.131	1.129
	.0025	-.375	-.361	-.316	-.283	-.228	-.176	-.133	-.102	-.041	-.003	.065	.110	.166	.199	.247
	.050	-.654	-.641	-.596	-.559	-.506	-.453	-.412	-.379	-.321	-.284	-.219	-.176	-.125	-.091	-.045
	.100	-.771	-.767	-.735	-.705	-.661	-.619	-.581	-.553	-.505	-.472	-.413	-.379	-.333	-.309	-.268
	.200	-.893	-.904	-.882	-.841	-.789	-.748	-.716	-.691	-.652	-.623	-.575	-.551	-.514	-.492	-.460
	.300	-.998	-.992	-.960	-.943	-.921	-.893	-.862	-.827	-.790	-.758	-.709	-.691	-.655	-.634	-.603
	.400	-1.143	-1.148	-1.124	-1.108	-1.072	-1.028	-.976	-.914	-.866	-.823	-.777	-.765	-.736	-.715	-.687
	.500	-1.098	-1.080	-1.073	-.954	-.875	-.851	-.834	-.810	-.793	-.774	-.749	-.754	-.737	-.730	-.711
	.600	-.462	-.483	-.504	-.535	-.544	-.579	-.597	-.607	-.623	-.634	-.638	-.669	-.674	-.683	-.681
	.700	-.232	-.221	-.223	-.239	-.209	-.241	-.263	-.288	-.318	-.341	-.359	-.419	-.438	-.457	-.468
	.800	-.109	-.089	-.063	-.047	-.024	-.018	-.013	-.011	-.018	-.026	-.027	-.093	-.115	-.139	-.144
Lower surface	.900	-.139	-.111	-.062	-.036	-.013	0	.010	-.006	.024	.031	.047	.030	.053	.074	.086
	.950	-.106	-.088	-.052	-.033	-.010	.001	.010	-.007	.024	.030	.044	.040	.068	.086	.093
	.0375	.279	.250	.212	.178	.132	.082	.043	.014	-.051	-.097	-.153	-.222	-.275	-.335	-.395
	.075	.099	.075	.044	.014	-.024	-.067	-.097	-.121	-.177	-.215	-.260	-.319	-.363	-.414	-.465
	.150	-.060	-.081	-.105	-.128	-.157	-.191	-.214	-.231	-.273	-.299	-.328	-.370	-.399	-.435	-.468
	.250	-.178	-.196	-.215	-.232	-.255	-.280	-.298	-.310	-.343	-.363	-.382	-.416	-.433	-.463	-.484
	.350	-.267	-.281	-.294	-.308	-.324	-.346	-.377	-.367	-.392	-.407	-.418	-.445	-.456	-.480	-.495
	.450	-.380	-.392	-.399	-.408	-.423	-.439	-.447	-.451	-.472	-.481	-.486	-.508	-.514	-.533	-.540
	.550	-.498	-.506	-.508	-.509	-.519	-.530	-.531	-.529	-.544	-.546	-.544	-.559	-.560	-.570	-.574
	.650	-.624	-.620	-.611	-.598	-.602	-.604	-.597	-.587	-.595	-.589	-.578	-.585	-.577	-.580	-.573
	.750	-.640	-.624	-.597	-.580	-.571	-.558	-.544	-.544	-.541	-.535	-.516	-.514	-.500	-.495	-.481
	.850	-.443	-.440	-.413	-.398	-.396	-.385	-.371	-.358	-.352	-.344	-.322	-.310	-.286	-.277	-.258
	.925	-.212	-.202	-.176	-.164	-.159	-.148	-.136	-.124	-.119	-.112	-.092	-.076	-.049	-.039	-.022
	.975	-.133	-.122	-.094	-.075	-.060	-.047	-.035	-.025	-.020	-.011	.007	.027	.032	.062	.074
	1.000	-.115	-.097	-.040	-.030	-.010	0	.011	-.010	.023	.018	.033	.050	.070	.090	.090

\*No orifice.

NACA

TABLE 2.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(17.30) PROPELLER BLADE SECTION ( $x = 0.45$ ) - Concluded

(g)  $M = 0.63$ .

$J$	1.973	1.992	2.056	2.089	2.109	2.146	2.161	2.188	2.213	2.248	2.275	2.308	2.336	2.376
$\alpha_x$	.780	.774	.765	.762	.756	.756	.748	.745	.740	.741	.736	.733	.730	.727
$\Delta\delta$	.492	.466	.381	.338	.313	.268	.249	.217	1.87	1.46	1.16	.79	.48	.05
$\alpha_i$	.11	.11	.09	.09	.08	.08	.07	.07	.06	.06	.06	.05	.04	.04
$c_l$	.54	.56	.50	.44	.39	.32	.26	.23	.17	.12	.07	.01	-.05	-.12
$c_n$	.2200	.2297	.2077	.1845	.1626	.1335	.1097	.0942	.0729	.0497	.0297	.0045	-.0206	-.0516
$c_m$	.0519	.0444	.0354	.0362	.0347	.0364	.0362	.0321	.0277	.0249	.0226	.0226	.0197	.0164
$c_c$	.0454	.0425	.0321	.0311	.0278	.0249	.0234	.0217	.0194	.0186	.0181	.0181	.0173	.0174
$c/b$	Pressure coefficient, P													
Upper surface	$\infty$ .000	1.162	1.159	1.155	1.154	1.152	1.152	1.149	1.148	1.145	1.146	1.144	1.142	1.140
	.025	-.198	-.183	-.107	-.082	-.053	-.017	.009	.038	.071	.114	.146	.186	.217
	.050	-.475	-.465	-.387	-.365	-.336	-.301	-.274	-.250	-.217	-.174	-.144	-.107	-.076
	.100	-.617	-.613	-.556	-.536	-.515	-.485	-.464	-.445	-.419	-.383	-.357	-.323	-.295
	.200	-.793	-.798	-.735	-.699	-.665	-.636	-.602	-.609	-.588	-.560	-.541	-.514	-.489
	.300	-.874	-.869	-.833	-.822	-.813	-.794	-.782	-.773	-.749	-.722	-.703	-.677	-.655
	.400	-1.029	-1.038	-1.007	-1.000	-.991	-.966	-.938	-.919	-.895	-.868	-.843	-.799	-.735
	.500	-1.031	-1.084	-1.108	-1.092	-1.072	-1.029	-1.003	-.983	-.957	-.944	-.919	-.862	-.823
	.600	-.499	-.544	-.771	-.700	-.745	-.730	-.743	-.752	-.765	-.758	-.751	-.748	-.747
	.700	-.314	-.324	-.332	-.287	-.292	-.297	-.307	-.333	-.370	-.393	-.411	-.421	-.434
	.800	-.263	-.265	-.177	-.175	-.137	-.088	-.067	-.076	-.099	-.110	-.109	-.106	-.102
Lower surface	.900	-.249	-.234	-.116	-.131	-.103	-.062	-.043	-.026	.006	.032	.060	.071	.078
	.950	-.234	-.213	-.089	-.101	-.073	-.038	-.025	-.007	.031	.053	.070	.077	.081
	.0375	.235	.213	.130	.095	.052	.017	-.031	-.074	-.115	-.169	-.209	-.258	-.310
	.075	.059	.042	-.026	-.056	-.092	-.124	-.164	-.202	-.237	-.283	-.317	-.357	-.403
	.150	-.086	-.103	-.157	-.180	-.213	-.234	-.267	-.295	-.322	-.354	-.380	-.405	-.437
	.250	-.203	-.214	-.260	-.279	-.305	-.322	-.349	-.374	-.395	-.419	-.437	-.454	-.478
	.350	-.287	-.291	-.333	-.347	-.369	-.380	-.403	-.424	-.438	-.455	-.466	-.479	-.495
	.450	-.401	-.406	-.442	-.453	-.472	-.480	-.498	-.514	-.523	-.537	-.545	-.547	-.558
	.550	-.528	-.530	-.558	-.566	-.581	-.582	-.595	-.605	-.607	-.613	-.611	-.607	-.606
	.650	-.706	-.708	-.723	-.721	-.726	-.715	-.712	-.707	-.690	-.677	-.664	-.645	-.633
	.750	-.851	-.833	-.798	-.721	-.684	-.647	-.622	-.605	-.583	-.567	-.553	-.537	-.527
	.850	-.522	-.488	-.408	-.401	-.386	-.369	-.364	-.358	-.341	-.332	-.323	-.310	-.303
	.925	-.273	-.238	-.167	-.164	-.146	-.128	-.121	-.108	-.086	-.077	-.066	-.054	-.051
	.975	-.218	-.187	-.079	-.079	-.057	-.033	-.025	-.007	.027	.037	.048	.060	.065
	1.000	-.210	-.184	-.056	-.056	-.030	.006	-.003	.019	.050	.064	.068	.083	.085

\*No orifice.



TABLE 3.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-(3)(10.40) PROPELLER BLADE SECTION ( $x = 0.60$ )

$$\left[ \beta_{0.75R} = 45^\circ; \beta_x = 51.4^\circ; B = 2 \right]$$

(a)  $N = 1140$  rpm.

	$J$	1.540	1.671	1.779	1.894	1.972	2.074	2.191	2.318	2.443	2.569	2.510	2.412	2.379	2.270	2.138	2.019	1.901	1.768	1.654
$M_x$		.401	.421	.433	.444	.457	.468	.484	.500	.515	.536	.528	.512	.508	.494	.476	.461	.449	.433	.418
$\alpha_x'$		12.15	9.84	8.06	6.86	5.11	3.66	2.11	.52	-.95	-.233	-1.69	-.59	-.21	1.11	2.80	4.43	6.16	8.23	10.13
$\alpha_1$		.19	.16	.14	.13	.11	.10	.08	.05	.02	-.01	.01	.03	.04	.06	.08	.11	.12	.15	.17
$\alpha_1$		2.50	2.80	1.91	1.57	1.37	1.11	.81	.49	.25	.02	.13	.30	.38	.64	.93	1.24	1.57	1.94	2.26
$c_n$		.9540	.8426	.7316	.6065	.5310	.4310	.3197	.1916	.0990	.0097	.0529	.1174	.1484	.2519	.3652	.4839	.6090	.7458	.8632
$c_m$		.0036	-.0121	-.0157	-.0192	-.0190	-.0269	-.0323	-.0387	-.0452	-.0558	-.0518	-.0437	-.0409	-.0329	-.0292	-.0228	-.0188	-.0162	-.0100
$c_c$																				
$c/h$		Pressure coefficient, $P$																		
Upper surface	0.000	1.041	1.045	1.048	1.051	1.053	1.056	1.062	1.064	1.068	1.073	1.071	1.067	1.066	1.062	1.058	1.055	1.052	1.048	1.045
	.025	-2.631	-2.491	-1.772	-1.474	-1.176	-.802	-.449	-.105	.139	.365	.268	.089	.015	-.246	-.594	-.997	-1.476	-1.837	-2.662
	.050	-2.585	-1.772	-1.474	-1.173	-.980	-.732	-.495	-.253	-.070	.105	.027	-.108	-.162	-.350	-.594	-.854	-1.161	-1.512	-1.843
	.100	-2.059	-1.361	-1.182	-.978	-.844	-.672	-.513	-.346	-.209	-.078	-.138	-.239	-.278	-.412	-.575	-.754	-.966	-1.192	-1.407
	.200	-1.107	-1.003	-.889	-.778	-.701	-.602	-.498	-.389	-.297	-.221	-.254	-.320	-.344	-.430	-.538	-.651	-.769	-.904	-1.027
	.300	-.861	-.836	-.758	-.686	-.636	-.561	-.493	-.411	-.342	-.286	-.314	-.364	-.377	-.440	-.515	-.593	-.678	-.773	-.845
	.400	-.735	-.737	-.693	-.642	-.610	-.558	-.503	-.450	-.400	-.360	-.392	-.418	-.424	-.465	-.523	-.582	-.636	-.698	-.742
	.500	-.608	-.642	-.618	-.592	-.568	-.537	-.503	-.460	-.425	-.405	-.417	-.439	-.440	-.470	-.503	-.548	-.583	-.623	-.643
	.600	-.496	-.533	-.528	-.518	-.508	-.491	-.475	-.445	-.425	-.420	-.424	-.434	-.433	-.450	-.472	-.493	-.513	-.529	-.527
	.700	-.362	-.395	-.415	-.423	-.428	-.428	-.426	-.414	-.404	-.416	-.415	-.413	-.405	-.410	-.417	-.420	-.418	-.416	-.389
	.800	-.197	-.202	-.228	-.252	-.263	-.279	-.298	-.300	-.306	-.329	-.321	-.311	-.297	-.286	-.277	-.264	-.247	-.225	-.194
	.900	-.067	-.028	-.004	-.002	-.002	-.016	-.041	-.047	-.067	-.093	-.085	-.071	-.056	-.038	-.013	.003	.009	-.003	-.028
	.950	-.039	.009	.049	.079	.095	.108	.114	.116	.107	.094	.100	.103	.114	.121	.124	.109	.082	.047	.001
Lower surface	.0375	.853	.777	.660	.504	.388	.225	.031	-.195	-.400	-.668	-.546	-.371	-.287	-.087	.132	.326	.507	.673	.794
	.075	.681	.603	.498	.368	.274	.132	.011	-.140	-.292	-.468	-.390	-.271	-.212	-.072	.082	.225	.368	.510	.619
	.150	.480	.413	.327	.226	.155	.065	-.035	-.144	-.239	-.399	-.303	-.229	-.188	-.087	.018	.120	.227	.335	.424
	.250	.336	.275	.205	.123	.067	0	-.077	-.156	-.223	-.303	-.268	-.220	-.186	-.112	-.032	.042	.127	.213	.286
	.350	.231	.183	.127	.058	.013	-.038	-.100	-.159	-.209	-.268	-.245	-.208	-.181	-.127	-.063	-.006	.062	.135	.193
	.450	.147	.110	.062	.005	-.033	-.076	-.125	-.173	-.209	-.253	-.234	-.211	-.188	-.142	-.092	-.047	.006	.066	.117
	.550	.059	.022	-.004	-.051	-.078	-.111	-.151	-.188	-.209	-.242	-.230	-.220	-.198	-.163	-.124	-.089	-.047	0	.041
	.650	0	-.021	-.047	-.087	-.113	-.135	-.167	-.190	-.205	-.223	-.219	-.211	-.198	-.177	-.140	-.117	-.082	-.047	-.019
	.750	-.067	-.067	-.082	-.110	-.124	-.138	-.161	-.173	-.170	-.175	-.176	-.180	-.169	-.162	-.143	-.125	-.106	-.081	-.065
	.850	-.060	-.047	-.021	-.066	-.076	-.073	-.077	-.074	-.063	-.056	-.058	-.073	-.068	-.070	-.066	-.072	-.062	-.050	-.048
	.925	-.032	-.008	-.004	-.022	-.022	.011	.021	.035	.052	.065	.058	.040	.043	.032	.024	.003	-.018	-.006	-.012
	.975	-.025	.012	.021	.031	.047	.065	.096	.116	.139	.148	.140	.129	.128	.111	.082	.061	.038	.017	.005
	1.000	-.022	.045	.076	.094	.135	.135	.197	.177	.213	.190	.184	.183	.208	.179	.180	.137	.099	.060	.010

<sup>a</sup>No orifice.

NACA

TABLE 3.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(10.40) PROPELLER BLADE SECTION ( $x = 0.60$ ) - Continued

(b)  $N = 1350$  rpm.

J	2.551	2.423	2.271	2.142	2.025	1.905	1.792	1.652	1.427	1.525	1.710	1.850	1.948	2.095	2.211	2.362	2.498
$M_x$	.643	.617	.591	.574	.556	.539	.520	.502	.472	.483	.512	.531	.544	.566	.582	.608	.626
$\alpha_x$	-2.14	-.72	1.09	2.75	4.35	6.10	7.85	10.17	14.27	12.43	9.19	6.94	5.46	3.38	1.85	-.01	-1.56
$\Delta\theta$	.01	.05	.10	.13	.16	.19	.22	.25	.28	.27	.24	.21	.18	.14	.11	.07	.03
$C_l$	-.06	.22	.57	.91	1.26	1.62	1.99	2.34	2.77	2.57	2.24	1.78	1.49	1.09	.78	.39	.07
$C_m$	-.0245	.0852	.2242	.3561	.4903	.6265	.7671	.8974	1.0471	.9768	.8686	.6903	.5787	.4257	.3055	.1532	.0282
$C_{m'}$	-.0511	-.0429	-.0320	-.0265	-.0188	-.0134	-.0023	.0048	-.0487	0	.0018	-.0079	-.0147	-.0215	-.0294	-.0391	-.0464
$C_c$																	
c/b	Pressure coefficient, P																
Upper surface	0.000	1.108	1.098	1.090	1.085	1.079	1.074	1.069	1.064	1.057	1.050	1.067	1.072	1.076	1.082	1.087	1.095
	.025	.385	.160	-.179	-.562	-1.012	-1.602	-2.070	-3.200	-1.450	-2.513	-3.165	-2.161	-1.362	-.782	-.381	.005
	.050	.115	-.071	-.331	-.603	-.908	-1.242	-1.475	-2.368	-1.522	-2.423	-2.046	-1.486	-1.132	-.758	-.481	-.193
	.100	-.082	-.223	-.414	-.603	-.806	-1.044	-1.227	-1.974	-1.573	-2.119	-1.361	-1.194	-.967	-.709	-.522	-.317
	.200	-.236	-.328	-.454	-.576	-.706	-.833	-.943	-1.068	-1.558	-1.261	-1.028	-.987	-.792	-.649	-.526	-.391
	.300	-.316	-.383	-.474	-.562	-.645	-.734	-.804	-.882	-1.330	-.923	-.864	-.868	-.707	-.608	-.526	-.428
	.400	-.401	-.449	-.513	-.576	-.629	-.687	-.727	-.766	-1.060	-.749	-.765	-.804	-.669	-.604	-.541	-.471
	.500	-.449	-.476	-.518	-.560	-.594	-.627	-.645	-.655	-.822	-.613	-.663	-.735	-.618	-.582	-.547	-.496
	.600	-.463	-.471	-.493	-.516	-.531	-.545	-.543	-.531	-.641	-.482	-.550	-.642	-.544	-.528	-.513	-.480
	.700	-.449	-.442	-.445	-.452	-.449	-.439	-.416	-.391	-.302	-.357	-.411	-.528	-.445	-.453	-.458	-.444
	.800	-.337	-.319	-.308	-.301	-.276	-.248	-.214	-.207	-.392	-.234	-.211	-.327	-.257	-.291	-.311	-.313
Lower surface	.900	-.052	-.040	-.025	-.012	.004	.006	-.005	-.035	-.301	-.147	-.023	-.093	.009	-.002	-.025	-.034
	.950	.115	.120	.116	.107	.093	.062	.034	.006	-.264	-.111	.015	-.046	.075	.099	.110	.122
	.0375	-.754	-.449	-.150	.089	.306	.491	.650	.785	.861	.862	.734	.477	.430	.198	-.018	-.294
	.075	-.521	-.328	-.124	.047	.212	.360	.493	.613	.703	.693	.564	.329	.307	.129	-.033	-.225
	.150	-.403	-.276	-.130	-.014	.106	.217	.323	.424	.513	.498	.383	.172	.176	.044	-.070	-.207
	.250	-.350	-.259	-.161	-.066	.024	.114	.198	.284	.356	.345	.246	.057	.081	-.024	-.110	-.211
	.350	-.314	-.245	-.170	-.097	-.023	.050	.120	.246	.246	.159	.015	.020	-.061	-.134	-.209	-.287
	.450	-.301	-.249	-.190	-.128	-.068	-.009	.052	.110	.147	.150	.083	-.077	-.031	-.101	-.161	-.221
	.550	-.288	-.250	-.209	-.165	-.115	-.067	-.016	.030	.049	.058	.010	-.139	-.086	-.141	-.189	-.229
	.650	-.268	-.245	-.220	-.188	-.145	-.105	-.064	-.033	-.037	-.019	-.049	-.183	-.120	-.164	-.206	-.230
	.750	-.216	-.207	-.198	-.180	-.155	-.131	-.102	-.081	-.122	-.086	-.093	-.214	-.141	-.170	-.191	-.202
	.850	-.083	-.090	-.097	-.097	-.090	-.084	-.070	-.064	-.149	-.093	-.070	-.174	-.090	-.099	-.091	-.089
	.925	.043	.032	.013	0	-.007	-.034	-.025	-.026	-.154	-.075	-.027	-.128	-.027	-.006	.007	.026
	.975	.128	.120	.092	.070	.040	.015	.002	-.001	-.200	-.091	-.004	-.091	.020	.048	.086	.116
	1.000	.208	.215	.174	.180	.150	.085	.057	.040	-.231	-.101	.048	-.025	.110	.150	.148	.181

\*No orifice.

NACA

TABLE 3.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(10.40) PROPELLER BLADE SECTION ( $x = 0.60$ ) - Continued

(c)  $N = 1500$  rpm.

	1.663	1.777	1.899	1.985	2.121	2.259	2.393	2.523	2.655	2.734	2.192	2.069	1.951	1.834	1.701
$J$	.561	.575	.597	.612	.634	.660	.684	.709	.696	.672	.646	.625	.604	.587	.564
$M_x$	9.98	8.41	6.19	4.92	3.03	1.24	-.37	-1.84	-1.08	.32	2.09	3.73	5.41	7.19	9.34
$\alpha_1$	.23	.20	.15	.13	.10	.08	.04	-.01	.02	.06	.09	.12	.14	.17	.22
$\alpha_2$	2.53	2.22	1.79	1.44	1.03	.66	.27	-.06	.10	.40	.81	1.20	1.56	1.98	2.37
$c_m$	.9703	.8961	.6910	.5626	.4035	.2584	.1065	-.0219	.0384	.1597	.3194	.4665	.6084	.7665	.9116
$c_o$	.0146	.2175	-.0054	-.0151	-.0248	-.0297	-.0396	-.0500	-.0449	-.0362	-.0277	-.0200	-.0108	.0008	.0100
$o/b$	Pressure coefficient, P														
Upper surface	0.000	1.081	1.085	1.092	1.097	1.104	1.114	1.123	1.133	1.128	1.118	1.109	1.101	1.094	1.089
	.025	-3.060	-2.810	-2.023	-1.208	-.648	-.214	-.142	-.397	.882	.017	-.393	-.827	-1.414	-2.366
	.050	-2.848	-2.663	-1.358	-1.068	-.697	-.379	-.099	.120	.021	-.199	-.510	-.817	-1.191	-1.892
	.100	-1.875	-1.294	-1.143	-.925	-.688	-.469	-.299	-.084	-.167	-.337	-.565	-.769	-1.010	-1.200
	.200	-1.086	-1.009	-.897	-.785	-.645	-.507	-.372	-.250	-.306	-.421	-.565	-.693	-.824	-.954
	.300	-.880	-.857	-.780	-.711	-.617	-.521	-.430	-.344	-.305	-.464	-.562	-.645	-.733	-.818
	.400	-.759	-.737	-.716	-.679	-.618	-.554	-.496	-.438	-.466	-.520	-.585	-.637	-.688	-.742
	.500	-.645	-.660	-.646	-.631	-.598	-.559	-.529	-.501	-.516	-.541	-.578	-.607	-.630	-.659
	.600	-.511	-.537	-.547	-.548	-.538	-.519	-.514	-.509	-.511	-.517	-.529	-.539	-.542	-.549
	.700	-.362	-.386	-.421	-.442	-.451	-.450	-.463	-.478	-.470	-.460	-.453	-.446	-.427	-.412
	.800	-.176	-.175	-.206	-.237	-.265	-.279	-.303	-.325	-.316	-.295	-.275	-.254	-.218	-.192
Lower surface	.900	-.025	-.005	.030	.037	.031	.027	.008	-.010	-.007	.010	.024	.038	.039	.012
	.950	.013	.028	.071	.099	.117	.131	.137	.143	.140	.133	.127	.117	.089	.046
	.0375	-.799	.703	.540	.387	.163	-.087	-.408	-.795	-.598	-.285	.027	.256	.454	.617
	.075	.631	.547	.405	.279	.106	-.075	-.300	-.537	-.423	-.217	.006	.177	.334	.467
	.150	.446	.369	.258	.159	.031	-.101	-.299	-.409	-.340	-.202	-.039	.084	.202	.306
	.250	.305	.241	.146	.069	-.033	-.139	-.296	-.364	-.312	-.212	-.085	.012	.104	.186
	.350	.211	.177	.078	.012	-.069	-.153	-.246	-.331	-.293	-.215	-.116	-.034	.042	.111
	.450	.130	.080	.016	-.039	-.109	-.180	-.256	-.318	-.290	-.229	-.148	-.079	-.015	.042
	.550	.048	.006	-.047	-.096	-.153	-.202	-.262	-.308	-.290	-.243	-.184	-.129	-.071	-.026
	.650	-.015	-.050	-.091	-.136	-.180	-.216	-.258	-.287	-.278	-.246	-.204	-.161	-.109	-.075
	.750	-.070	-.093	-.120	-.151	-.178	-.196	-.221	-.230	-.230	-.217	-.192	-.165	-.132	-.111
	.850	-.052	-.068	-.076	-.085	-.091	-.094	-.096	-.085	-.095	-.100	-.096	-.086	-.080	-.073
	.925	-.013	-.021	-.023	-.004	.006	.019	.029	.052	.039	.023	.011	.007	-.012	-.028
	.975	.007	-.002	.023	.046	.074	.101	.119	.147	.130	.106	.083	.065	.030	.005
	1.000	.018	.007	.070	.120	.150	.172	.193	.229	.207	.192	.175	.143	.101	.061

<sup>a</sup>No airfoil.

NACA

TABLE 3.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(10,40) PROPELLER BLADE SECTION ( $x = 0.60$ ) - Continued

(d)  $N = 1600$  rpm.

$J$	1.840	1.922	1.980	2.058	2.137	2.231	2.301	2.371	2.494	2.422	2.350	2.273	2.196	2.105	2.041	1.962	1.892
$M_\infty$	.623	.639	.690	.663	.677	.698	.710	.722	.747	.731	.715	.702	.685	.669	.696	.642	.628
$\Delta P$	7.09	5.84	4.99	3.89	2.81	1.59	.73	-.12	-1.52	-.71	.13	1.07	2.04	3.24	4.12	5.25	6.29
$P_1$	.28	.26	.22	.18	.14	.11	.08	.05	0	.03	.06	.09	.12	.16	.19	.24	.26
$P_2$	1.98	1.73	1.53	1.27	1.04	.74	.52	.31	0	.17	.40	.58	.84	1.13	1.31	1.57	1.80
$C_D$	.7658	.6710	.5961	.4948	.4077	.2903	.2035	.1210	-.0019	.0677	.1568	.2303	.3297	.4432	.5084	.6090	.6961
$C_L$	.0016	-.0070	-.0121	-.0166	-.0228	-.0289	-.0352	-.0377	-.0585	-.0451	-.0366	-.0325	-.0238	-.0210	-.0175	-.0136	-.0069
$c/b$	Pressure coefficient, $P$																
Upper surface	$0.000$	1.100	1.106	1.110	1.115	1.120	1.128	1.133	1.138	1.148	1.141	1.135	1.130	1.123	1.117	1.112	1.107
	$.025$	-2.194	-1.761	-1.274	-.889	-.579	-.292	-.042	-.140	.383	.248	.066	-.101	-.364	-.704	-.980	-1.359
	$.050$	-1.973	-1.521	-1.203	-.902	-.664	-.414	-.249	-.099	.111	-.007	-.159	-.293	-.495	-.755	-.963	-1.262
	$.100$	-1.447	-1.151	-1.010	-.858	-.696	-.518	-.391	-.275	-.101	-.199	-.322	-.425	-.576	-.763	-.896	-1.092
	$.200$	-.973	-.919	-.850	-.759	-.667	-.562	-.479	-.398	-.272	-.345	-.429	-.497	-.592	-.704	-.778	-.868
	$.300$	-.855	-.807	-.762	-.704	-.645	-.580	-.525	-.471	-.377	-.432	-.490	-.533	-.597	-.668	-.714	-.773
	$.400$	-.778	-.747	-.723	-.690	-.654	-.618	-.582	-.524	-.490	-.529	-.562	-.584	-.624	-.668	-.697	-.729
	$.500$	-.689	-.671	-.662	-.649	-.631	-.618	-.602	-.595	-.573	-.588	-.594	-.599	-.618	-.639	-.651	-.665
	$.600$	-.570	-.561	-.563	-.566	-.558	-.564	-.559	-.565	-.521	-.571	-.559	-.554	-.556	-.563	-.567	-.563
	$.700$	-.421	-.425	-.438	-.453	-.456	-.471	-.476	-.487	-.514	-.500	-.480	-.470	-.464	-.459	-.454	-.435
	$.800$	-.186	-.194	-.215	-.240	-.251	-.271	-.281	-.293	-.317	-.306	-.287	-.277	-.264	-.250	-.237	-.208
Lower surface	$.900$	.009	.035	.043	.046	.047	.037	.036	.035	.022	.023	.033	.039	.042	.049	.043	.026
	$.950$	.045	.072	.088	.104	.120	.123	.129	.135	.144	.142	.135	.132	.122	.116	.100	.058
	$.0375$	.584	.502	.406	.270	.137	-.064	-.225	-.411	-.842	-.558	-.327	-.168	.015	.198	.307	.437
	$.075$	.442	.376	.298	.189	.090	-.063	-.176	-.305	-.564	-.400	-.246	-.135	-.004	.133	.218	.320
	$.150$	.286	.234	.173	.093	.020	-.094	-.176	-.272	-.424	-.330	-.228	-.143	-.049	.052	.113	.192
	$.250$	.171	.131	.084	.014	-.048	-.138	-.199	-.266	-.384	-.314	-.234	-.174	-.101	-.016	.031	.094
	$.350$	.094	.063	.020	-.036	-.085	-.160	-.209	-.263	-.354	-.297	-.237	-.188	-.131	-.059	-.021	.033
	$.450$	.028	.002	-.036	-.083	-.124	-.189	-.228	-.272	-.344	-.300	-.249	-.209	-.163	-.103	-.070	.006
	$.550$	-.041	-.061	-.093	-.135	-.165	-.218	-.251	-.286	-.338	-.306	-.269	-.235	-.197	-.152	-.124	-.058
	$.650$	-.092	-.109	-.138	-.172	-.190	-.234	-.258	-.283	-.316	-.296	-.269	-.245	-.218	-.182	-.163	-.106
	$.750$	-.126	-.137	-.155	-.177	-.187	-.217	-.229	-.241	-.250	-.245	-.235	-.220	-.206	-.182	-.170	-.136
	$.850$	-.087	-.084	-.088	-.095	-.096	-.110	-.109	-.109	-.096	-.103	-.107	-.103	-.093	-.094	-.089	-.050
	$.925$	-.037	-.015	-.010	.004	.006	.015	.023	.044	.031	.021	.018	.018	.007	.006	.005	-.011
	$.975$	-.003	.020	.038	.058	.079	.088	.101	.111	.134	.119	.105	.099	.081	.066	.049	.023
	$1.000$	.053	.091	.096	.124	.176	.211	.201	.191	.207	.189	.181	.201	.173	.171	.127	.090

\*No orifice.

NACA

TABLE 3.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(10,40) PROPELLER BLADE SECTION ( $\alpha = 0.60$ ) - Continued

(c)  $M = 0.56$ .

	$\Gamma$	$M_{\infty}$	$\alpha$	$\Delta\theta$	$\alpha_1$	$\alpha_m$	$\alpha_c$										
	.1.972	1.986	2.022	2.053	2.091	2.125	2.165	2.205	2.241	2.284	2.326	2.371	2.410	2.476	2.517		
	.784	.775	.770	.762	.757	.751	.745	.742	.736	.730	.725	.722	.715	.714	.703		
	5.11	4.91	4.39	3.96	3.43	2.98	2.45	1.93	1.47	.93	.42	-.11	-.57	-1.32	-1.77		
	.26	.25	.24	.22	.20	.18	.17	.14	.13	.11	.09	.07	.05	.02	0		
	1.50	1.44	1.33	1.23	1.09	1.02	.90	.79	.68	.53	.44	.33	.22	.09	-.03		
	.5839	.5613	.5174	.4774	.4252	.4000	.3503	.3077	.2665	.2090	.1729	.1297	.0892	.0355	-.0129		
	-.0346	-.0295	-.0234	-.0202	-.0206	-.0231	-.0236	-.0254	-.0285	-.0356	-.0380	-.0401	-.0442	-.0500	-.0506		
	.0014	-.0018															
$a/b$		Pressure coefficient, P															
Upper surface	0.000	1.163	1.160	1.158	1.154	1.152	1.150	1.147	1.146	1.143	1.141	1.139	1.138	1.135	1.135	1.131	
	.025	-.751	-.742	-.708	-.699	-.667	-.503	-.425	-.343	-.258	-.170	-.088	-.013	.072	.178	.246	
	.050	-.920	-.916	-.882	-.825	-.729	-.669	-.601	-.528	-.457	-.384	-.314	-.250	-.177	-.085	-.024	
	.100	-.935	-.886	-.850	-.840	-.810	-.773	-.718	-.660	-.597	-.534	-.477	-.423	-.363	-.283	-.232	
	.200	-1.026	-1.027	-1.011	-.983	-.881	-.829	-.782	-.734	-.685	-.633	-.587	-.545	-.499	-.435	-.401	
	.300	-1.054	-1.051	-.995	-.917	-.885	-.858	-.814	-.775	-.734	-.688	-.651	-.615	-.578	-.524	-.491	
	.400	-1.069	-1.052	-.995	-.942	-.885	-.842	-.808	-.763	-.728	-.688	-.651	-.615	-.578	-.524	-.491	
	.500	-1.154	-1.147	-1.120	-1.099	-1.051	-.976	-.918	-.880	-.838	-.795	-.754	-.710	-.664	-.615	-.589	
	.600	-.975	-1.158	-.975	-.973	-.870	-.803	-.778	-.766	-.750	-.730	-.720	-.707	-.697	-.671	-.658	
	.700	-.523	-.499	-.508	-.527	-.564	-.580	-.595	-.609	-.623	-.622	-.629	-.630	-.638	-.632	-.629	
	.800	-.350	-.282	-.273	-.291	-.315	-.332	-.352	-.373	-.394	-.404	-.426	-.440	-.458	-.465	-.478	
	.900	-.200	-.140	-.109	-.080	-.079	-.073	-.075	-.080	-.087	-.090	-.104	-.117	-.135	-.144	-.164	
	.950	-.167	-.107	-.080	-.049	-.041	-.030	-.024	-.020	-.016	-.010	-.012	-.010	-.008	-.001	-.007	
Lower surface	.0375	.187	.143	.104	.062	-.012	-.056	-.123	-.193	-.277	-.354	-.451	-.541	-.661	-.795	-.944	
	.075	.109	.069	.035	.003	-.055	-.091	-.142	-.193	-.257	-.310	-.379	-.440	-.520	-.601	-.692	
	.150	0	-.053	-.059	-.083	-.128	-.153	-.190	-.229	-.274	-.311	-.364	-.406	-.457	-.501	-.557	
	.250	-.094	-.123	-.142	-.163	-.202	-.220	-.250	-.281	-.315	-.340	-.376	-.405	-.441	-.470	-.509	
	.350	-.159	-.184	-.200	-.215	-.247	-.260	-.283	-.308	-.334	-.352	-.380	-.401	-.427	-.445	-.476	
	.450	-.229	-.249	-.261	-.272	-.298	-.307	-.324	-.343	-.364	-.376	-.396	-.412	-.430	-.439	-.460	
	.550	-.307	-.323	-.329	-.333	-.352	-.358	-.368	-.383	-.397	-.402	-.416	-.424	-.436	-.436	-.452	
	.650	-.372	-.381	-.379	-.376	-.389	-.389	-.395	-.403	-.410	-.411	-.419	-.423	-.427	-.419	-.430	
	.750	-.397	-.397	-.389	-.381	-.385	-.381	-.382	-.385	-.386	-.381	-.383	-.383	-.382	-.367	-.373	
	.850	-.302	-.296	-.286	-.275	-.267	-.265	-.265	-.263	-.255	-.255	-.250	-.247	-.228	-.228	-.230	
	.925	-.204	-.192	-.180	-.165	-.152	-.153	-.148	-.143	-.138	-.127	-.126	-.122	-.115	-.096	-.096	
	.975	-.163	-.143	-.126	-.101	-.094	-.091	-.072	-.065	-.057	-.044	-.043	-.039	-.031	-.011	-.010	
	1.000	-.132	-.077	-.070	-.021	-.029	-.007	-.003	-.026	-.025	-.043	-.016	-.021	.047	.073	.049	

a No orifice.

NACA



TABLE 3.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-(3)(10.40) PROPELLER BLADE SECTION ( $x = 0.60$ ) - Continued(r)  $M = 0.60$ .

J	2.465	2.439	2.406	2.366	2.333	2.302	2.274	2.234	2.204	2.168	2.142	2.116	2.092	2.062	2.050	2.010	1.998	1.965
$M_x$	.759	.765	.768	.771	.778	.782	.786	.789	.792	.795	.802	.806	.810	.814	.823	.824	.833	.834
$\alpha$	-1.20	-.90	-.52	-.06	.34	.71	1.05	1.55	1.94	2.40	2.75	3.09	3.42	3.83	4.00	4.56	4.73	5.21
$\Delta\delta$	-.01	.01	.04	.06	.09	.11	.12	.14	.16	.17	.17	.18	.18	.19	.20	.20	.20	.21
$\alpha_1$	0	.03	.07	.21	.25	.32	.39	.52	.56	.64	.72	.80	.87	.93	.96	1.04	1.03	1.07
$c_n$	.0006	.0129	.0290	.0816	.0987	.1277	.1516	.2058	.2213	.2516	.2813	.3142	.3381	.3608	.3735	.4045	.4000	.4129
$c_m$	-.0502	-.0481	-.0424	-.0420	-.0338	-.0324	-.0282	-.0267	-.0218	-.0200	-.0198	-.0198	-.0218	-.0210	-.0216	-.0216	-.0100	-.0064
$c_c$					.0135	.0129	.0128	.0116	.0110	.0121	.0155	.0187	.0213	.0233	.0256	.0280	.0306	.0323
c/b	Pressure coefficient, P																	
Upper surface	0.000	1.174	1.177	1.180	1.181	1.185	1.187	1.190	1.192	1.194	1.195	1.200	1.202	1.205	1.208	1.213	1.215	1.220
	.025	.361	.331	.300	.230	.182	.143	.095	.005	-.036	-.092	-.128	-.175	-.209	-.248	-.271	-.325	-.351
	.050	.092	.067	.040	-.023	-.062	-.096	-.137	-.214	-.247	-.296	-.326	-.369	-.400	-.438	-.462	-.519	-.541
	.100	-.115	-.139	-.161	-.213	-.249	-.276	-.309	-.375	-.404	-.446	-.468	-.493	-.507	-.518	-.516	-.533	-.535
	.200	-.281	-.302	-.318	-.359	-.388	-.410	-.436	-.492	-.520	-.549	-.595	-.609	-.650	-.672	-.681	-.713	-.720
	.300	-.382	-.403	-.415	-.450	-.473	-.492	-.512	-.554	-.581	-.612	-.622	-.642	-.650	-.672	-.696	-.745	-.760
	.400	-.509	-.530	-.543	-.572	-.588	-.604	-.639	-.677	-.687	-.707	-.715	-.725	-.737	-.754	-.756	-.782	-.795
	.500	-.605	-.630	-.639	-.674	-.711	-.725	-.729	-.764	-.794	-.826	-.843	-.859	-.865	-.872	-.873	-.894	-.898
	.600	-.618	-.657	-.678	-.707	-.742	-.783	-.834	-.857	-.886	-.921	-.941	-.964	-.974	-.974	-.958	-.918	-.783
	.700	-.516	-.521	-.485	-.493	-.487	-.469	-.455	-.442	-.392	-.385	-.398	-.372	-.360	-.357	-.358	-.376	-.377
Lower surface	.800	-.297	-.289	-.271	-.246	-.232	-.217	-.200	-.181	-.170	-.174	-.195	-.222	-.254	-.278	-.298	-.335	-.344
	.900	.029	.030	.037	.048	.045	.046	.042	.034	.025	-.008	-.060	-.126	-.176	-.212	-.245	-.293	-.318
	.950	.132	.123	.122	.118	.109	.106	.093	.080	.066	.027	-.032	-.099	-.157	-.195	-.230	-.281	-.311
	.0375	-.789	-.740	-.652	-.506	-.432	-.358	-.290	-.177	-.129	-.070	-.028	.030	.064	.104	.135	.181	.212
	.075	-.529	-.505	-.454	-.369	-.324	-.272	-.226	-.145	-.109	-.067	-.034	.012	.038	.068	.093	.128	.155
	.150	-.399	-.391	-.364	-.314	-.287	-.250	-.217	-.157	-.132	-.102	-.077	-.043	-.024	-.002	.017	.044	.064
	.250	-.370	-.369	-.351	-.313	-.296	-.269	-.245	-.202	-.183	-.159	-.140	-.112	-.096	-.079	-.064	-.043	0
	.350	-.347	-.351	-.338	-.312	-.302	-.280	-.264	-.230	-.216	-.201	-.187	-.161	-.150	-.136	-.122	-.106	-.092
	.450	-.341	-.350	-.343	-.326	-.322	-.307	-.295	-.270	-.262	-.250	-.241	-.221	-.212	-.201	-.192	-.179	-.169
	.550	-.340	-.354	-.354	-.346	-.350	-.341	-.337	-.321	-.321	-.317	-.314	-.303	-.297	-.291	-.285	-.276	-.270
	.650	-.319	-.336	-.340	-.341	-.353	-.348	-.352	-.347	-.357	-.367	-.373	-.375	-.377	-.378	-.378	-.376	-.377
	.750	-.255	-.271	-.278	-.287	-.301	-.301	-.310	-.318	-.333	-.354	-.376	-.403	-.420	-.442	-.464	-.482	-.506
	.850	-.102	-.117	-.122	-.134	-.149	-.149	-.160	-.171	-.185	-.207	-.232	-.263	-.287	-.310	-.335	-.373	-.465
	.925	.033	.023	.017	.004	-.010	-.010	-.022	-.035	-.048	-.073	-.105	-.143	-.176	-.200	-.224	-.263	-.318
	.975	.113	.105	.104	.091	.078	.078	.065	.050	.036	.002	-.039	-.098	-.140	-.174	-.209	-.259	-.311
	1.000	.185	.162	.140	.150	.122	.130	.113	.090	.087	.040	-.010	-.080	-.140	-.180	-.220	-.275	-.350

No orifice

NACA

TABLE 3.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(10.40) PROPELLER BLADE SECTION ( $x = 0.60$ ) - Concluded

(g)  $M = 0.63$ .

$J$	1.981	1.998	2.033	2.053	2.079	2.107	2.132	2.157	2.188	2.210	2.242	2.272	2.306	2.332	2.362	2.391
$M_x$	.875	.872	.866	.858	.853	.849	.842	.838	.833	.826	.822	.817	.816	.809	.802	.799
$\alpha_x$	4.98	4.73	4.24	3.96	3.60	3.22	2.88	2.55	2.15	1.86	1.45	1.08	.66	.35	-.01	-.35
$\Delta\delta$	.17	.16	.14	.12	.11	.10	.08	.07	.06	.05	.05	.04	.03	.03	.03	.02
$\rho_{t1}$	.80	.73	.71	.64	.60	.53	.49	.45	.39	.35	.32	.30	.26	.23	.17	.10
$c_n$	.3084	.2826	.2742	.2503	.2323	.2052	.1916	.1755	.1542	.1387	.1258	.1187	.1013	.0884	.0658	.0406
$c_m$	.0052	.0082	.0098	.0103	.0085	.0057	.0010	-.0020	-.0064	-.0092	-.0151	-.0233	-.0297	-.0364	-.0421	-.0475
$c_c$	.0435	.0419	.0416	.0400	.0379	.0356	.0330	.0308	.0280	.0262	.0253	.0241	.0217	.0203	.0183	.0179
$c/b$	Pressure coefficients, P															
Upper Surface	$\theta$ .000	1.206	1.204	1.201	1.197	1.195	1.193	1.189	1.188	1.185	1.183	1.181	1.178	1.178	1.174	1.170
	.025	-.192	-.162	-.136	-.109	-.083	-.044	-.026	.012	.052	.088	.131	.166	.216	.250	.296
	.050	-.393	-.366	-.337	-.309	-.287	-.250	-.236	-.205	-.171	-.140	-.102	-.073	-.030	-.005	.036
	.100	-.420	-.416	-.411	-.409	-.392	-.368	-.389	-.368	-.341	-.316	-.285	-.260	-.224	-.202	-.167
	.200	-.598	-.586	-.575	-.568	-.562	-.534	-.519	-.480	-.456	-.444	-.419	-.396	-.366	-.350	-.323
	.300	-.645	-.629	-.611	-.594	-.578	-.557	-.560	-.550	-.530	-.518	-.497	-.478	-.454	-.441	-.419
	.400	-.690	-.676	-.669	-.665	-.666	-.651	-.650	-.644	-.604	-.620	-.609	-.602	-.590	-.581	-.548
	.500	-.785	-.781	-.781	-.783	-.783	-.772	-.776	-.772	-.756	-.743	-.726	-.715	-.686	-.672	-.668
	.600	-.893	-.894	-.896	-.902	-.901	-.888	-.890	-.882	-.863	-.852	-.840	-.827	-.809	-.809	-.790
	.700	-.408	-.375	-.381	-.365	-.347	-.325	-.315	-.312	-.315	-.354	-.452	-.590	-.727	-.828	-.751
	.800	-.362	-.335	-.337	-.322	-.305	-.280	-.265	-.246	-.226	-.217	-.214	-.202	-.173	-.181	-.222
	.900	-.335	-.319	-.317	-.301	-.278	-.250	-.231	-.204	-.167	-.136	-.107	-.071	-.010	.029	.041
	.950	-.335	-.312	-.308	-.267	-.267	-.237	-.214	-.183	-.142	-.108	-.069	-.026	.037	.081	.118
Lower Surface	.0375	.200	.166	.141	.100	.050	.003	-.029	-.083	-.129	-.186	-.248	-.314	-.391	-.476	-.575
	.075	.153	.126	.108	.073	.031	-.005	-.032	-.072	-.108	-.149	-.194	-.241	-.294	-.350	-.408
	.150	.070	.049	.036	.009	-.026	-.053	-.074	-.106	-.131	-.162	-.195	-.229	-.266	-.306	-.338
	.250	-.013	-.030	-.041	-.066	-.098	-.121	-.141	-.169	-.188	-.212	-.235	-.261	-.289	-.319	-.343
	.350	-.077	-.090	-.099	-.123	-.153	-.173	-.189	-.211	-.227	-.248	-.265	-.286	-.308	-.333	-.349
	.450	-.146	-.158	-.167	-.191	-.217	-.235	-.250	-.270	-.280	-.296	-.312	-.329	-.343	-.365	-.372
	.550	-.252	-.263	-.271	-.295	-.319	-.334	-.324	-.364	-.371	-.385	-.395	-.406	-.413	-.423	-.416
	.650	-.360	-.371	-.379	-.402	-.425	-.438	-.449	-.462	-.463	-.468	-.469	-.468	-.457	-.449	-.419
	.750	-.496	-.505	-.516	-.537	-.558	-.567	-.572	-.576	-.553	-.520	-.481	-.443	-.400	-.372	-.338
	.850	-.592	-.600	-.606	-.626	-.631	-.595	-.501	-.389	-.314	-.277	-.252	-.229	-.198	-.177	-.145
	.925	-.599	-.591	-.574	-.525	-.388	-.293	-.247	-.213	-.176	-.149	-.121	-.092	-.053	-.024	.016
	.975	-.518	-.458	-.405	-.340	-.294	-.256	-.229	-.195	-.149	-.111	-.075	-.030	.023	.062	.110
	1.000	-.349	-.320	-.276	-.228	-.274	-.232	-.214	-.188	-.137	-.097	-.042	.002	.058	.121	.165

<sup>a</sup>No orifice.

NACA

TABLE 4.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-(3)(09.00) PROPELLER BLADE SECTION ( $x = 0.70$ )

$$[\beta_{0.75R} = 45^\circ; \beta_x = 47.0^\circ; B = 2]$$

(a)  $N = 1140$  rpm.

$J$	1.373	1.520	1.658	1.812	1.973	2.127	2.277	2.423	2.553	2.495	2.362	2.210	2.057	1.908	1.750	1.605	1.447	
$M_x$	.449	.466	.480	.500	.517	.534	.553	.573	.589	.581	.564	.543	.527	.508	.490	.473	.455	
$\alpha_x$	15.02	12.35	9.99	7.51	5.10	2.95	1.00	- .77	-2.26	-1.61	-.05	1.86	3.91	6.06	8.49	10.88	13.66	
$\Delta\theta$	.35	.32	.28	.23	.18	.14	.08	.03	-.02	.01	.05	.11	.16	.21	.25	.30	.34	
$\alpha_1$	3.19	2.68	2.51	2.04	1.54	1.11	.71	.32	.04	.15	.48	.88	1.31	1.74	2.25	2.56	2.83	
$c_H$	1.1097	.9335	.8852	.7252	.5497	.4000	.2548	.1174	.0139	.0555	.1732	.3181	.4723	.6187	.7587	.8994	.9864	
$c_F$	-.0790	-.0134	-.0082	-.0256	-.0320	-.0374	-.0437	-.0483	-.0499	-.0516	-.0469	-.0397	-.0329	-.0293	-.0182	-.0052	-.0406	
$c_o$																		
$a/b$	Pressure coefficient, P																	
Upper surface	0.000	1.052	1.056	1.059	1.064	1.068	1.073	1.078	1.084	1.089	1.087	1.082	1.075	1.071	1.066	1.061	1.057	1.053
	.025	-1.611	-2.114	-2.650	-3.190	-3.714	-4.237	-4.758	-5.276	-5.791	-6.303	-6.812	-7.318	-7.821	-8.321	-8.818	-9.312	-9.804
	.050	-1.567	-2.022	-2.391	-2.753	-3.116	-3.478	-3.839	-4.198	-4.555	-4.910	-5.262	-5.611	-5.958	-6.303	-6.645	-6.984	-7.321
	.100	-1.475	-1.858	-2.130	-2.391	-2.642	-2.892	-3.141	-3.389	-3.636	-3.882	-4.127	-4.371	-4.613	-4.854	-5.093	-5.330	-5.566
	.200	-1.368	-1.645	-1.872	-2.091	-2.309	-2.526	-2.742	-2.957	-3.171	-3.384	-3.596	-3.807	-4.017	-4.226	-4.433	-4.639	-4.844
	.300	-1.241	-1.457	-1.672	-1.886	-2.099	-2.311	-2.522	-2.732	-2.941	-3.149	-3.356	-3.562	-3.767	-3.971	-4.174	-4.376	-4.577
	.400	-1.079	-1.208	-1.336	-1.463	-1.589	-1.714	-1.839	-1.963	-2.086	-2.208	-2.329	-2.449	-2.568	-2.685	-2.801	-2.916	-3.030
	.500	-.906	-1.052	-1.197	-1.341	-1.484	-1.626	-1.767	-1.907	-2.046	-2.184	-2.321	-2.457	-2.592	-2.726	-2.859	-2.991	-3.122
	.600	-.750	-.932	-1.113	-1.293	-1.472	-1.650	-1.827	-1.999	-2.170	-2.340	-2.509	-2.676	-2.841	-2.999	-3.156	-3.311	-3.465
	.700	-.600	-.833	-1.065	-1.296	-1.526	-1.755	-1.982	-2.208	-2.433	-2.657	-2.880	-3.101	-3.320	-3.537	-3.752	-3.965	-4.177
	.800	-.470	-.746	-1.070	-1.392	-1.713	-2.033	-2.352	-2.670	-2.987	-3.303	-3.618	-3.931	-4.242	-4.551	-4.858	-5.163	-5.467
	.900	-.363	-.680	-1.099	-1.517	-1.934	-2.350	-2.765	-3.179	-3.592	-4.004	-4.415	-4.824	-5.231	-5.636	-6.039	-6.440	-6.839
	.950	-.300	-.648	-1.123	-1.600	-2.076	-2.551	-3.025	-3.498	-3.969	-4.438	-4.905	-5.370	-5.833	-6.294	-6.753	-7.210	-7.664
Lower surface	.0375	.890	.847	.790	.660	.444	.206	-.063	-.369	-.626	-.810	-1.028	-1.268	-1.528	-1.794	-2.064	-2.338	-2.616
	.075	.720	.667	.604	.484	.302	.122	-.075	-.384	-.645	-.831	-1.053	-1.299	-1.566	-1.842	-2.117	-2.391	-2.669
	.150	.538	.492	.433	.333	.194	.065	-.065	-.382	-.647	-.834	-1.057	-1.304	-1.571	-1.846	-2.120	-2.393	-2.671
	.250	.390	.350	.303	.219	.110	.009	-.088	-.391	-.653	-.840	-1.063	-1.310	-1.577	-1.851	-2.124	-2.396	-2.678
	.350	.289	.257	.220	.151	.057	-.017	-.096	-.397	-.660	-.847	-1.070	-1.317	-1.584	-1.857	-2.129	-2.401	-2.683
	.450	.191	.172	.145	.087	.011	-.051	-.114	-.415	-.678	-.865	-1.088	-1.335	-1.602	-1.874	-2.145	-2.417	-2.699
	.550	.099	.093	.075	.034	-.030	-.080	-.130	-.431	-.694	-.881	-1.104	-1.351	-1.618	-1.889	-2.160	-2.431	-2.713
	.650	.006	.011	.013	-.018	-.069	-.106	-.145	-.446	-.709	-.896	-1.119	-1.366	-1.633	-1.904	-2.174	-2.445	-2.727
	.750	-.063	-.038	-.018	-.032	-.069	-.093	-.116	-.447	-.710	-.897	-1.120	-1.367	-1.634	-1.905	-2.175	-2.446	-2.728
	.850	-.109	-.066	-.021	-.018	-.033	-.039	-.047	-.448	-.711	-.898	-1.121	-1.368	-1.635	-1.906	-2.176	-2.447	-2.729
	.925	-.132	-.074	.003	.021	.022	.035	.039	-.449	-.712	-.899	-1.122	-1.369	-1.636	-1.907	-2.177	-2.448	-2.730
	.975	-.202	-.126	-.008	.034	.059	.087	.103	-.450	-.713	-.900	-1.123	-1.370	-1.637	-1.908	-2.178	-2.449	-2.731
	1.000	-.250	-.142	0	.066	.128	.189	.169	-.451	-.714	-.901	-1.124	-1.371	-1.638	-1.909	-2.179	-2.450	-2.732

No orifice.



TABLE 4.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(09.00) PROPELLER BLADE SECTION ( $\alpha = 0.70$ ) - Continued

(b)  $N = 1350$  rpm.

$J$	1.488	1.624	1.753	1.893	2.014	2.144	2.285	2.417	2.522	2.472	2.352	2.225	2.089	1.959	1.834	1.695	1.560
$M_x$	.555	.568	.582	.599	.616	.637	.656	.679	.698	.687	.667	.644	.626	.603	.589	.570	.558
$\Delta P$	12.92	10.56	8.44	6.28	4.52	2.73	.90	-.70	-1.91	-1.34	.08	1.67	3.47	5.31	7.17	9.38	11.65
$a_1$	.40	.37	.34	.29	.24	.18	.11	.05	0	.02	.08	.14	.20	.26	.31	.36	.39
$a_n$	2.85	2.68	2.42	2.01	1.56	1.13	.67	.31	.03	.15	.49	.89	1.32	1.75	2.16	2.58	2.75
$c_n$	.9910	.9406	.8581	.7174	.5581	.4065	.2426	.1119	.0113	.0545	.1777	.3213	.4729	.6258	.7671	.9116	.9632
$c_x$	-.0324	-.0033	-.0126	-.0188	-.0290	-.0351	-.0454	-.0486	-.0541	-.0517	-.0455	-.0391	-.0331	-.0251	-.0157	-.0095	-.0115
$c_o$																	
$a/b$	Pressure coefficient, P																
Upper surface	$a$	0.000	1.079	1.083	1.087	1.092	1.098	1.105	1.112	1.121	1.128	1.124	1.116	1.108	1.101	1.094	1.089
	$\theta$	.025	-1.873	-2.554	-2.823	-1.933	-1.217	-.611	-.157	.188	.390	.305	.032	-.348	-.869	-1.495	-2.335
	$\phi$	.050	-1.693	-2.280	-2.688	-1.660	-1.029	-.634	-.314	-.053	.117	.044	-.174	-.453	-.803	-1.235	-2.085
	$\psi$	.100	-1.607	-1.924	-1.214	-1.071	-.892	-.621	-.402	-.211	-.079	-.136	-.299	-.506	-.728	-.959	-1.097
	$\chi$	.200	-1.362	-1.222	-.918	-.821	-.695	-.556	-.424	-.299	-.208	-.249	-.358	-.487	-.619	-.752	-.867
	$\eta$	.300	-1.058	-.861	-.781	-.707	-.623	-.530	-.438	-.350	-.281	-.311	-.390	-.484	-.573	-.661	-.737
	$\xi$	.400	-.813	-.670	-.682	-.633	-.581	-.517	-.452	-.390	-.340	-.362	-.418	-.485	-.546	-.604	-.653
	$\zeta$	.500	-.643	-.547	-.621	-.597	-.567	-.530	-.490	-.451	-.416	-.433	-.469	-.514	-.549	-.581	-.605
	$\eta$	.600	-.514	-.428	-.524	-.523	-.510	-.494	-.473	-.451	-.432	-.441	-.459	-.488	-.502	-.516	-.522
	$\theta$	.700	-.414	-.312	-.410	-.425	-.431	-.436	-.433	-.430	-.423	-.427	-.430	-.440	-.436	-.431	-.416
	$\phi$	.800	-.331	-.189	-.220	-.232	-.251	-.269	-.280	-.286	-.288	-.287	-.280	-.280	-.263	-.248	-.220
Lower surface	$\psi$	.900	-.266	-.089	-.015	.001	-.009	-.029	-.043	-.056	-.063	-.061	-.048	-.042	-.021	-.006	-.001
	$\chi$	.950	-.239	-.060	.063	.083	.098	.105	.106	.104	.104	.103	.106	.100	.102	.093	.070
	$\eta$	.0375	.862	.824	.728	.580	.397	.164	-.103	-.412	-.664	-.554	-.253	.015	.273	.482	.643
	$\theta$	.075	.688	.645	.549	.419	.271	.090	-.103	-.313	-.475	-.406	-.205	-.021	.173	.336	.474
	$\phi$	.150	.509	.475	.391	.318	.176	.046	-.085	-.223	-.327	-.282	-.149	-.034	.104	.224	.329
	$\psi$	.250	.367	.337	.270	.184	.093	-.007	-.107	-.208	-.282	-.249	-.156	-.069	.036	.134	.218
	$\chi$	.350	.268	.250	.194	.123	.046	-.035	-.114	-.192	-.246	-.222	-.153	-.085	.002	.079	.149
	$\eta$	.450	.174	.169	.123	.063	-.002	-.068	-.136	-.194	-.236	-.219	-.165	-.111	-.042	.024	.085
	$\theta$	.550	.085	.093	.059	.009	-.044	-.098	-.150	-.197	-.227	-.215	-.173	-.132	-.075	-.022	.027
	$\phi$	.650	-.002	.021	.002	-.038	-.080	-.126	-.164	-.197	-.215	-.211	-.180	-.152	-.106	-.065	-.025
	$\psi$	.750	-.061	-.020	-.021	-.049	-.078	-.108	-.132	-.150	-.159	-.157	-.142	-.126	-.096	-.067	-.040
	$\chi$	.850	-.106	-.036	-.009	-.024	-.037	-.048	-.057	-.060	-.056	-.050	-.057	-.058	-.045	-.031	-.021
	$\eta$	.925	-.127	-.028	.028	.029	.031	.032	.037	.047	.056	.052	.043	.029	.029	.022	.022
	$\theta$	.975	-.198	-.058	.042	.052	.069	.088	.106	.122	.136	.128	.116	.092	.077	.063	.038
	$a$	1.000	-.215	-.058	.112	.205	.140	.179	.169	.191	.189	.167	.187	.171	.208	.146	.090

No orifice.

NACA

TABLE 4.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(09.00) PROPELLER BLADE SECTION ( $\alpha = 0.70$ ) - Continued

(a)  $N = 1500$  rpm.

J	1.643	1.762	1.890	2.019	2.105	2.237	2.343	2.474	2.533	2.418	2.283	2.175	2.065	1.966	1.837	1.694
$M_{\infty}$	.615	.630	.651	.668	.683	.707	.724	.747	.759	.735	.711	.692	.673	.659	.640	.619
$\alpha_1$	10.24	8.30	6.32	4.45	3.25	1.51	.18	-1.37	-2.04	-.71	.93	2.32	3.80	5.19	7.13	9.39
$\Delta\theta$	.37	.31	.26	.20	.17	.11	.06	-.01	-.05	.02	.10	.14	.18	.22	.28	.35
$c_l$	2.85	2.45	2.07	1.58	1.31	.92	.58	.22	.05	.36	.72	1.10	1.42	1.75	2.25	2.71
$c_{l1}$	1.0045	.8697	.7348	.5684	.4697	.3294	.2116	.0800	.0184	.1316	.2619	.3955	.5110	.6277	.8039	.9658
$c_{l2}$	.0031	-.0066	-.0156	-.0247	-.0313	-.0408	-.0556	-.0627	-.0661	-.0574	-.0483	-.0366	-.0292	-.0241	-.0075	-.0003
$c_o$																
$c/b$	Pressure coefficient, P															
Upper surface	0.000	1.098	1.102	1.110	1.117	1.123	1.132	1.138	1.148	1.153	1.143	1.134	1.126	1.119	1.113	1.106
	.025	-2.847	-2.395	-1.805	-1.177	-.785	-.279	.043	.324	.434	.213	-.130	-.520	-.947	-1.395	-2.122
	.050	-2.759	-2.356	-1.868	-1.168	-.809	-.430	-.180	.053	.152	-.042	-.312	-.610	-.931	-1.503	-2.122
	.100	-2.500	-2.082	-1.491	-.880	-.737	-.492	-.310	-.126	-.046	-.201	-.405	-.612	-.801	-.904	-1.829
	.200	-1.196	-.799	-.851	-.754	-.657	-.515	-.400	-.257	-.211	-.322	-.462	-.584	-.697	-.803	-.839
	.300	-.742	-.755	-.744	-.673	-.614	-.519	-.443	-.347	-.305	-.385	-.481	-.565	-.641	-.705	-.758
	.400	-.663	-.679	-.667	-.624	-.587	-.529	-.480	-.415	-.386	-.441	-.503	-.558	-.605	-.641	-.675
	.500	-.604	-.627	-.628	-.605	-.591	-.562	-.543	-.506	-.491	-.521	-.553	-.577	-.602	-.616	-.631
	.600	-.498	-.525	-.541	-.537	-.537	-.531	-.532	-.526	-.528	-.524	-.528	-.531	-.540	-.539	-.535
	.700	-.383	-.407	-.430	-.445	-.456	-.470	-.489	-.502	-.512	-.490	-.474	-.462	-.454	-.439	-.417
	.800	-.208	-.208	-.220	-.242	-.261	-.282	-.304	-.319	-.328	-.307	-.290	-.274	-.258	-.235	-.211
Lower surface	.900	-.027	-.001	.016	.007	.002	-.016	-.030	-.035	-.049	-.036	-.026	-.011	-.001	.009	.006
	.950	.038	.058	.083	.096	.110	.121	.123	.129	.123	.126	.122	.114	.102	.089	.064
	.0375	.806	.711	.583	.395	.248	-.004	-.253	-.588	-.782	-.435	-.113	.127	.307	.475	.642
	.075	.630	.541	.426	.270	.156	-.031	-.208	-.446	-.680	-.334	-.113	.062	.198	.334	.480
	.150	.462	.387	.293	.172	.090	-.041	-.157	-.286	-.362	-.227	-.093	.024	.122	.224	.337
	.250	.331	.266	.189	.089	.024	-.076	-.162	-.257	-.318	-.217	-.114	-.026	.047	.130	.224
	.350	.245	.190	.125	.039	-.012	-.092	-.160	-.230	-.274	-.201	-.123	-.052	.005	.075	.153
	.450	.164	.119	.061	-.010	-.051	-.119	-.176	-.226	-.263	-.205	-.145	-.086	-.038	.020	.087
	.550	.092	.055	.006	-.053	-.088	-.145	-.186	-.221	-.248	-.208	-.164	-.117	-.077	-.029	.027
	.650	.031	.001	-.045	-.094	-.120	-.164	-.191	-.210	-.230	-.205	-.178	-.145	-.113	-.074	-.025
	.750	-.004	-.028	-.057	-.095	-.111	-.135	-.147	-.149	-.160	-.152	-.144	-.126	-.110	-.080	-.045
	.850	.001	-.014	-.031	-.055	-.054	-.057	-.053	-.038	-.040	-.048	-.059	-.058	-.058	-.042	-.025
No orifice.	.925	.034	.026	.023	.016	.027	.039	.053	.077	.080	.062	.044	.030	.019	.020	.021
	.975	.059	.035	.047	.053	.075	.105	.121	.144	.153	.133	.111	.085	.060	.048	.032
	1.000	.076	.059	.106	.144	.167	.207	.215	.213	.213	.224	.174	.176	.148	.141	.106

No orifice.

NACA

TABLE 4.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(09.00) PROPELLER BLADE SECTION ( $\alpha = 0.70$ ) - Continued

(d)  $N = 1600$  rpm.

$\frac{C_p}{C_{p,0}}$	2.454 .803	2.357 .789	2.295 .777	2.211 .760	2.137 .746	2.062 .731	1.971 .716	1.887 .702	1.916 .709	2.010 .723	2.103 .741	2.174 .752	2.258 .770	2.336 .783	2.393 .797
$\frac{C_{p,0}}{C_{p,0}}$	-1.13 .04	.05 .04	.78 .09	1.85 .15	2.82 .21	3.84 .28	5.13 .37	6.37 .43	5.94 .41	4.57 .33	3.28 .24	2.33 .18	1.24 .12	.27 .06	-.42 .02
$\frac{C_{p,0}}{C_{p,0}}$	.12 .0452	.44 .1581	.65 .2368	1.00 .3616	1.25 .4494	1.52 .5458	1.84 .6581	2.22 .7916	2.09 .7471	1.71 .6142	1.39 .5006	1.14 .4110	.81 .2942	.54 .1945	.34 .1229
$\frac{C_{p,0}}{C_{p,0}}$	-.0653 .0180	-.0549 .	-.0491 .	-.0408 .	-.0354 .	-.0297 .	-.0225 .	-.0202 .	-.0205 .	-.0265 .	-.0321 .	-.0387 .	-.0446 .	-.0506 .	-.0641 .
$c/b$	Pressure coefficient, $P$														
Upper surface	.000	1.172	1.165	1.160	1.153	1.147	1.142	1.135	1.130	1.133	1.138	1.146	1.150	1.158	1.163
.025	.365	.168	.009	-.256	-.497	-.795	-1.065	-1.445	-1.327	-.947	-.668	-.399	-.109	.099	.298
.050	.090	-.084	-.205	-.440	-.656	-1.039	-1.315	-1.577	-1.488	-1.206	-.858	-.568	-.318	-.141	-.006
.100	-.103	-.246	-.351	-.526	-.680	-.817	-1.243	-1.497	-1.423	-1.085	-.769	-.620	-.433	-.292	-.183
.200	-.261	-.374	-.451	-.575	-.683	-.866	-.997	-1.464	-1.384	-.943	-.792	-.641	-.512	-.407	-.325
.300	-.353	-.440	-.499	-.588	-.662	-.730	-.763	-.761	-.761	-.754	-.702	-.637	-.544	-.465	-.403
.400	-.453	-.527	-.577	-.634	-.682	-.716	-.722	-.675	-.675	-.673	-.705	-.666	-.604	-.543	-.493
.500	-.577	-.638	-.665	-.694	-.698	-.684	-.673	-.622	-.622	-.623	-.694	-.685	-.607	-.548	-.511
.600	-.669	-.704	-.671	-.620	-.599	-.584	-.579	-.569	-.576	-.585	-.588	-.607	-.650	-.690	-.691
.700	-.775	-.743	-.699	-.640	-.616	-.582	-.557	-.535	-.539	-.563	-.565	-.579	-.589	-.505	-.646
.800	-.276	-.267	-.263	-.252	-.251	-.238	-.234	-.240	-.239	-.236	-.238	-.251	-.258	-.262	-.274
.900	-.004	.013	.016	.018	.016	.013	.015	.012	.012	.015	.019	.019	.016	.016	.001
.950	.127	.121	.120	.115	.106	.091	.090	.098	.093	.088	.102	.112	.116	.126	.130
Lower surface	.0375	-.585	-.371	-.196	.013	.144	.286	.428	.548	.511	.371	.236	.097	-.090	-.274
.075	-.707	-.307	-.177	-.023	.073	.184	.298	.401	.369	.251	.142	.037	-.102	-.235	-.413
.150	-.324	-.219	-.139	-.036	.030	.110	.196	.278	.232	.158	.079	.004	-.091	-.175	-.270
.250	-.332	-.226	-.160	-.078	-.027	.036	.106	.176	.154	.074	.012	-.047	-.122	-.190	-.266
.350	-.304	-.224	-.169	-.101	-.059	-.004	.053	.111	.092	.027	-.025	-.076	-.137	-.191	-.251
.450	-.307	-.241	-.195	-.137	-.101	-.055	-.003	.049	.030	-.028	-.072	-.115	-.168	-.213	-.261
.550	-.305	-.253	-.215	-.166	-.137	-.098	-.054	-.007	-.022	-.075	-.112	-.146	-.192	-.228	-.267
.650	-.292	-.256	-.227	-.188	-.167	-.136	-.098	-.054	-.071	-.118	-.147	-.175	-.210	-.236	-.264
.750	-.210	-.199	-.182	-.159	-.147	-.129	-.100	-.063	-.078	-.115	-.134	-.152	-.173	-.186	-.198
.850	-.075	-.085	-.081	-.075	-.076	-.072	-.072	-.068	-.038	-.064	-.071	-.076	-.081	-.079	-.075
.925	.054	.033	.029	.023	.014	.007	.013	.033	.025	.008	.014	.019	.023	.034	.048
.975	.130	.102	.096	.083	.065	.047	.046	.064	.055	.047	.039	.074	.088	.105	.124
1.000	.228	.210	.205	.162	.163	.134	.136	.142	.132	.120	.156	.159	.190	.210	.228

\*No orifices.

NACA

TABLE 4.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(09.00) PROPELLER BLADE SECTION ( $x = 0.70$ ) - Continued

(e)  $M = 0.56$ .

	2.518	2.464	2.406	2.366	2.327	2.283	2.236	2.196	2.161	2.128	2.083	2.055	2.019	1.987	1.958
$J$	.750	.758	.763	.768	.777	.785	.789	.795	.802	.811	.816	.825	.833	.839	.845
$M_x$	-1.87	-1.25	-.57	-.09	.38	.93	1.52	2.04	2.50	2.94	3.35	3.94	4.45	4.90	5.32
$\Delta\delta$	-.03	.01	.05	.07	.09	.11	.14	.16	.18	.21	.24	.26	.28	.31	.32
$\alpha_1$	.04	.16	.33	.43	.56	.68	.81	.94	1.03	1.14	1.27	1.35	1.43	1.52	1.60
$C_{D1}$	.0155	.0574	.1203	.2071	.2842	.3465	.3929	.4381	.4729	.5090	.5487	.5839	.6135	.6439	.6723
$C_{D2}$	-.0660	-.0651	-.0617	-.0596	-.0576	-.0529	-.0460	-.0441	-.0397	-.0398	-.0431	-.0439	-.0470	-.0436	-.0439
$C_c$									.0050	.0057	.0076	.0108	.0140	.0171	.0173
$c/b$	Pressure coefficient, P														
Upper surface	0.000	1.149	1.153	1.155	1.157	1.160	1.164	1.166	1.168	1.171	1.173	1.178	1.182	1.186	1.191
	.025	.421	.353	.244	.174	.085	.008	-.079	-.164	-.218	-.281	-.340	-.374	-.439	-.464
	.050	.142	.078	-.017	-.076	-.151	-.218	-.295	-.373	-.424	-.490	-.581	-.649	-.702	-.719
	.100	-.058	-.110	-.188	-.237	-.299	-.355	-.419	-.479	-.515	-.539	-.550	-.539	-.641	-.678
	.200	-.213	-.258	-.320	-.360	-.408	-.454	-.511	-.577	-.623	-.643	-.678	-.695	-.709	-.779
	.300	-.302	-.340	-.392	-.426	-.466	-.501	-.544	-.584	-.618	-.665	-.711	-.732	-.753	-.789
	.400	-.381	-.419	-.466	-.500	-.543	-.573	-.610	-.635	-.641	-.674	-.720	-.752	-.785	-.823
	.500	-.476	-.514	-.558	-.591	-.637	-.681	-.726	-.765	-.785	-.795	-.816	-.839	-.879	-.912
	.600	-.506	-.541	-.579	-.613	-.657	-.727	-.790	-.832	-.853	-.876	-.905	-.924	-.951	-.926
	.700	-.492	-.507	-.519	-.519	-.509	-.493	-.489	-.487	-.516	-.511	-.446	-.405	-.403	-.396
	.800	-.321	-.317	-.310	-.298	-.274	-.247	-.225	-.203	-.186	-.182	-.218	-.273	-.319	-.348
Lower surface	.900	-.058	-.043	-.030	-.017	.009	.030	.032	.029	.018	-.016	-.082	-.160	-.240	-.317
	.950	.119	.127	.128	.128	.127	.074	.110	.094	.074	.033	-.031	-.113	-.205	-.304
	.0375	-.748	-.647	-.487	-.388	-.272	-.173	-.095	-.013	.042	.112	.172	.229	.282	.314
	.075	-.539	-.492	-.377	-.310	-.231	-.161	-.105	-.045	-.001	.052	.098	.145	.188	.214
	.150	-.357	-.317	-.256	-.219	-.171	-.127	-.093	-.053	-.023	.007	.051	.087	.119	.140
	.250	-.311	-.283	-.242	-.219	-.183	-.151	-.129	-.101	-.076	-.045	-.018	.012	.037	.053
	.350	-.270	-.253	-.225	-.210	-.185	-.161	-.147	-.125	-.108	-.083	-.062	-.036	-.003	.021
	.450	-.259	-.248	-.229	-.219	-.205	-.191	-.185	-.170	-.158	-.139	-.122	-.102	-.087	-.057
	.550	-.248	-.241	-.231	-.227	-.219	-.212	-.214	-.206	-.204	-.190	-.181	-.168	-.160	-.140
	.650	-.229	-.230	-.227	-.227	-.226	-.226	-.236	-.237	-.239	-.239	-.240	-.239	-.242	-.238
	.750	-.162	-.163	-.167	-.171	-.175	-.181	-.196	-.203	-.212	-.223	-.236	-.247	-.270	-.293
	.850	-.043	-.047	-.055	-.062	-.070	-.078	-.097	-.108	-.120	-.137	-.160	-.182	-.223	-.260
	.925	.076	.070	.061	.050	.041	.033	.012	-.001	-.015	-.037	-.064	-.099	-.152	-.198
	.975	.148	.142	.133	.122	.106	.099	.078	.063	.045	.014	-.026	-.074	-.129	-.176
	1.000	.191	.176	.167	.158	.142	.144	.150	.130	.080	.047	-.010	-.070	-.161	-.248

\*No orifice.

NACA

TABLE 4.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(09.00) PROPELLER BLADE SECTION ( $x = 0.70$ ) - Continued

( $t$ )  $M = 0.60$ .

$J$	2.453	2.414	2.363	2.326	2.290	2.251	2.212	2.173	2.140	2.106	2.080	2.049	2.020	1.983
$M_x$	.810	.818	.824	.830	.839	.846	.849	.856	.866	.870	.882	.889	.896	.896
$\alpha_x$	-1.12	-.67	-.06	.39	.84	1.33	1.83	2.34	2.78	3.24	3.59	4.02	4.43	4.96
$\Delta\delta$	-.01	.03	.08	.11	.14	.16	.19	.20	.22	.23	.24	.24	.25	.26
$\alpha_1$	.14	.22	.31	.40	.51	.61	.71	.76	.77	.85	.94	1.02	1.11	1.26
$c_n$	.0510	.0806	.1135	.1445	.1832	.2213	.2568	.2748	.2781	.3065	.3355	.3639	.3987	.4516
$c_m$	-.0678	-.0647	-.0567	-.0513	-.0534	-.0469	-.0365	-.0302	-.0195	-.0161	-.0180	-.0180	-.0246	-.0300
$c_c$	.0182	.0185	.0201	.0223	.0244	.0260	.0263	.0284	.0290	.0301	.0310	.0327	.0337	.0335
$c/b$	Pressure coefficient, $P$													
Upper surface	0.000	1.175	1.179	1.181	1.184	1.188	1.191	1.193	1.196	1.201	1.203	1.209	1.213	1.217
	.025	.379	.337	.276	.219	.166	.113	.034	-.019	-.062	-.103	-.129	-.166	-.197
	.050	.106	.070	.017	-.031	-.079	-.125	-.194	-.243	-.287	-.331	-.375	-.440	-.472
	.100	-.086	-.115	-.160	-.200	-.239	-.277	-.331	-.366	-.385	-.387	-.379	-.375	-.409
	.200	-.247	-.269	-.305	-.338	-.372	-.406	-.470	-.495	-.505	-.521	-.534	-.549	-.586
	.300	-.341	-.357	-.384	-.408	-.431	-.456	-.493	-.533	-.554	-.576	-.578	-.594	-.603
	.400	-.441	-.452	-.471	-.488	-.503	-.513	-.540	-.568	-.587	-.600	-.615	-.638	-.649
	.500	-.562	-.583	-.609	-.628	-.646	-.659	-.678	-.685	-.702	-.711	-.709	-.733	-.743
	.600	-.660	-.677	-.705	-.724	-.736	-.751	-.776	-.782	-.791	-.800	-.800	-.810	-.819
	.700	-.774	-.825	-.842	-.869	-.870	-.807	-.723	-.687	-.538	-.544	-.502	-.523	-.561
	.800	-.864	-.834	-.810	-.798	-.817	-.838	-.865	-.883	-.876	-.889	-.897	-.930	-.954
Lower surface	.900	.010	.026	.012	-.048	-.125	-.140	-.176	-.222	-.242	-.263	-.274	-.311	-.337
	.950	.124	.108	.078	.006	-.046	-.085	-.128	-.193	-.235	-.258	-.273	-.314	-.338
	.0375	-.592	-.520	-.443	-.352	-.259	-.179	-.087	-.018	.052	.107	.160	.213	.260
	.075	-.718	-.585	-.436	-.323	-.234	-.169	-.101	-.046	.010	.054	.098	.141	.180
	.150	-.305	-.292	-.259	-.214	-.169	-.130	-.087	-.051	-.008	.025	.061	.092	.123
	.250	-.337	-.310	-.275	-.240	-.202	-.169	-.134	-.107	-.071	-.042	-.012	.014	.040
	.350	-.310	-.291	-.266	-.242	-.213	-.189	-.162	-.141	-.112	-.085	-.059	-.037	.010
	.450	-.313	-.305	-.289	-.277	-.257	-.238	-.216	-.202	-.175	-.152	-.127	-.108	-.088
	.550	-.309	-.310	-.308	-.310	-.301	-.291	-.278	-.270	-.248	-.228	-.204	-.188	-.169
	.650	-.294	-.305	-.318	-.340	-.352	-.357	-.357	-.361	-.347	-.330	-.307	-.294	-.276
	.750	-.212	-.224	-.247	-.275	-.304	-.332	-.363	-.428	-.440	-.430	-.414	-.408	-.390
	.850	-.076	-.091	-.116	-.146	-.174	-.204	-.240	-.324	-.412	-.448	-.461	-.470	-.457
No orifice.	.925	.049	.032	.003	-.033	-.063	-.094	-.199	-.197	-.262	-.316	-.391	-.474	-.469
	.975	.120	.099	.065	.013	-.026	-.059	-.104	-.176	-.246	-.284	-.324	-.441	-.484
	1.000	.175	.140	.085	.025	0	-.046	-.030	-.170	-.240	-.278	-.276	-.330	-.410

No orifice.





TABLE 4.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(09.00) PROPELLER BLADE SECTION ( $x = 0.70$ ) - Continued

(g)  $M = 0.64$

	$J$	$M_x$	$\alpha_x'$	$\Delta\delta$	$\alpha_1$	$c_n$	$c_m$	$c_c$												
	1.997	2.017	2.038	2.058	2.075	2.097	2.114	2.138	2.154	2.178	2.201	2.223	2.242	2.267	2.290	2.313	2.332	2.360	2.378	
	.957	.953	.947	.943	.934	.930	.926	.921	.915	.907	.905	.902	.895	.890	.886	.882	.875	.871	.868	
	4.76	4.47	4.18	3.90	3.66	3.36	3.13	2.81	2.59	2.28	1.97	1.69	1.45	1.13	.84	.55	.32	-.02	-.24	
	.19	.17	.15	.13	.12	.10	.09	.08	.07	.06	.05	.04	.02	.01	0	-.01	-.01	-.02	-.03	
	1.21	1.14	1.07	.96	.93	.86	.76	.64	.54	.47	.36	.30	.25	.21	.13	.09	.03	-.04	-.07	
	.4323	.4090	.3819	.3432	.3329	.3077	.2748	.2264	.1935	.1684	.1284	.1071	.0910	.0755	.0458	.0316	.0110	-.0142	-.0239	
	-.0703	-.0670	-.0577	-.0506	-.0503	-.0464	-.0346	-.0231	-.0102	-.0066	.0010	.0008	-.0011	-.0097	-.0157	-.0193	-.0208	-.0229	-.0269	
	.0538	.0534	.0520	.0516	.0526	.0535	.0517	.0506	.0488	.0476	.0464	.0448	.0437	.0426	.0415	.0400	.0387	.0363	.0337	
	Pressure coefficient, $P$																			
$c/b$																				
Upper surface	0.000	1.250	1.248	1.244	1.242	1.237	1.235	1.233	1.230	1.227	1.223	1.222	1.220	1.217	1.214	1.211	1.209	1.206	1.203	
	.025	-.057	-.038	-.021	.015	.030	.065	.078	.097	.123	.131	.163	.186	.211	.244	.273	.290	.317	.368	
	.050	-.322	-.305	-.280	-.228	-.199	-.165	-.152	-.132	-.107	-.099	-.069	-.050	-.027	0	.025	.040	.063	.108	
	.100	-.273	-.243	-.244	-.240	-.244	-.236	-.240	-.242	-.232	-.232	-.212	-.197	-.182	-.158	-.139	-.128	-.111	-.088	
	.200	-.423	-.419	-.419	-.402	-.396	-.379	-.377	-.376	-.369	-.373	-.360	-.350	-.333	-.304	-.268	-.278	-.263	-.243	
	.300	-.478	-.471	-.465	-.446	-.446	-.435	-.437	-.430	-.417	-.419	-.403	-.390	-.370	-.358	-.351	-.344	-.332	-.319	
	.400	-.527	-.517	-.511	-.494	-.490	-.475	-.472	-.468	-.463	-.465	-.451	-.439	-.430	-.418	-.414	-.411	-.408	-.399	
	.500	-.619	-.612	-.609	-.591	-.589	-.581	-.586	-.587	-.585	-.587	-.576	-.549	-.569	-.566	-.564	-.563	-.558	-.547	
	.600	-.687	-.681	-.680	-.668	-.674	-.668	-.673	-.672	-.671	-.676	-.669	-.665	-.665	-.659	-.656	-.657	-.654	-.645	
	.700	-.800	-.798	-.800	-.791	-.796	-.791	-.796	-.798	-.802	-.809	-.806	-.804	-.803	-.800	-.801	-.802	-.800	-.797	
	.800	-.806	-.792	-.694	-.618	-.652	-.654	-.552	-.474	-.404	-.373	-.326	-.312	-.298	-.310	-.312	-.300	-.282	-.244	
	.900	-.431	-.419	-.404	-.388	-.391	-.382	-.364	-.348	-.324	-.313	-.283	-.264	-.252	-.251	-.247	-.238	-.222	-.188	
	.950	-.430	-.415	-.400	-.383	-.387	-.376	-.359	-.345	-.321	-.310	-.278	-.248	-.232	-.215	-.207	-.196	-.179	-.114	
Lower surface	.0375	.277	.257	.224	.187	.152	.124	.095	.038	.007	-.038	-.087	-.126	-.174	-.225	-.261	-.291	-.336	-.378	
	.075	.199	.185	.157	.128	.098	.075	.048	-.001	-.028	-.064	-.108	-.144	-.196	-.271	-.341	-.404	-.516	-.595	
	.150	.150	.139	.117	.096	.073	.057	.033	-.006	-.026	-.055	-.083	-.106	-.136	-.166	-.188	-.204	-.219	-.245	
	.250	.071	.062	.043	.026	.005	-.011	-.033	-.069	-.085	-.112	-.137	-.157	-.182	-.208	-.229	-.249	-.285	-.311	
	.350	.024	.015	-.001	-.017	-.035	-.050	-.067	-.100	-.114	-.137	-.158	-.173	-.193	-.212	-.228	-.242	-.275	-.306	
	.450	-.049	-.056	-.072	-.086	-.104	-.116	-.136	-.167	-.179	-.202	-.218	-.232	-.248	-.264	-.278	-.291	-.314	-.329	
	.550	-.124	-.131	-.146	-.157	-.173	-.185	-.204	-.233	-.245	-.266	-.283	-.297	-.311	-.326	-.340	-.353	-.376	-.391	
	.650	-.218	-.224	-.238	-.249	-.267	-.277	-.295	-.323	-.334	-.356	-.372	-.383	-.398	-.410	-.424	-.437	-.462	-.475	
	.750	-.335	-.339	-.353	-.364	-.381	-.392	-.409	-.434	-.447	-.467	-.481	-.492	-.505	-.514	-.526	-.537	-.557	-.562	
	.850	-.414	-.419	-.435	-.443	-.460	-.473	-.490	-.514	-.526	-.543	-.556	-.565	-.576	-.579	-.578	-.574	-.573	-.567	
	.925	-.442	-.448	-.463	-.471	-.488	-.499	-.515	-.540	-.550	-.567	-.578	-.578	-.578	-.578	-.578	-.578	-.578	-.578	
	.975	-.456	-.461	-.476	-.483	-.499	-.506	-.521	-.540	-.539	-.539	-.539	-.539	-.539	-.539	-.539	-.539	-.539	-.539	
	1.000	-.445	-.454	-.462	-.462	-.435	-.482	-.477	-.485	-.480	-.481	-.480	-.480	-.480	-.480	-.480	-.480	-.480	-.480	

\*No orifice.

NACA

TABLE 5.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-(3)(08.20) PROPELLER BLADE SECTION ( $x = 0.78$ )

$$\beta_{0.75R} = 45^\circ; \beta_x = 43.85^\circ; B = 2$$

(a)  $N = 1140$  rpm.

$J$	1.405	1.553	1.707	1.870	2.031	2.172	2.336	2.481	2.584	2.542	2.417	2.250	2.103	1.942	1.770	1.611	1.458
$M_x$	.487	.506	.523	.541	.555	.573	.591	.609	.620	.615	.601	.581	.562	.546	.528	.508	.495
$c_{x'}$	14.02	11.49	8.99	6.50	4.20	2.30	.22	-1.51	-2.67	-2.20	-.76	1.29	3.21	5.45	8.01	10.53	13.10
$\Delta\theta$	.36	.32	.27	.22	.17	.12	.06	0	-.05	-.03	.03	.10	.14	.20	.25	.29	.35
$c_d$	2.97	2.80	2.65	2.13	1.60	1.13	.62	.24	0	.09	.43	.87	1.35	1.83	2.47	2.74	2.95
$c_n$	.9310	.8826	.8355	.6768	.5097	.3629	.2000	.0765	.0010	.0287	.1371	.2803	.4323	.5832	.7813	.8619	.9258
$c_m$	-.0595	-.0054	-.0146	-.0262	-.0352	-.0461	-.0564	-.0635	-.0651	-.0647	-.0596	-.0537	-.0385	-.0292	-.0226	-.0041	-.0262
$c_o$																	
$c/b$	Pressure coefficient, P																
Upper surface	$x=0.000$	1.061	1.065	1.070	1.075	1.079	1.084	1.090	1.096	1.099	1.097	1.093	1.087	1.081	1.076	1.072	1.066
	.025	-1.307	-2.041	-3.384	-1.980	-1.083	-.510	-.003	.322	.499	.431	.183	-.249	-.783	-1.493	-2.868	-2.564
	.050	-1.277	-1.921	-1.718	-1.284	-.895	-.590	-.213	.031	.174	.118	-.076	-.383	-.720	-1.149	-1.501	-2.189
	.100	-1.251	-1.714	-1.183	-.935	-.675	-.478	-.264	-.098	.008	-.032	-.169	-.375	-.579	-.808	-1.079	-1.619
	.200	-1.141	-1.171	-.865	-.733	-.575	-.459	-.321	-.209	-.137	-.165	-.257	-.396	-.518	-.664	-.826	-1.007
	.300	-1.003	-.836	-.722	-.632	-.525	-.445	-.349	-.267	-.211	-.232	-.301	-.402	-.485	-.587	-.701	-.760
	.400	-.858	-.641	-.638	-.584	-.507	-.455	-.383	-.320	-.281	-.295	-.347	-.425	-.481	-.552	-.632	-.624
	.500	-.705	-.504	-.564	-.536	-.484	-.451	-.405	-.363	-.335	-.345	-.382	-.435	-.473	-.518	-.571	-.523
	.600	-.582	-.397	-.481	-.474	-.442	-.431	-.403	-.374	-.357	-.362	-.386	-.424	-.440	-.466	-.496	-.420
	.700	-.475	-.302	-.376	-.398	-.384	-.393	-.383	-.371	-.362	-.369	-.375	-.394	-.391	-.400	-.407	-.317
	.800	-.391	-.222	-.230	-.264	-.270	-.294	-.306	-.308	-.307	-.306	-.305	-.313	-.287	-.273	-.268	-.202
Lower surface	.900	-.317	-.154	-.045	-.047	-.057	-.101	-.117	-.127	-.135	-.130	-.120	-.119	-.080	-.056	-.056	-.097
	.950	-.281	-.125	.027	.070	.082	.062	.050	.046	.039	.042	.049	.046	.073	.070	.037	-.056
	.0375	.817	.783	.720	.566	.346	.110	-.185	-.459	-.661	-.566	-.329	-.035	.228	.455	.657	.762
	.075	.669	.630	.565	.430	.252	.076	-.132	-.319	-.451	-.390	-.232	-.030	.165	.339	.504	.606
	.150	.493	.455	.395	.289	.159	.032	-.108	-.231	-.319	-.281	-.171	-.039	.093	.219	.347	.432
	.250	.360	.328	.279	.197	.094	-.002	-.100	-.184	-.244	-.218	-.140	-.055	.044	.139	.240	.310
	.350	.263	.238	.203	.133	.051	-.025	-.102	-.166	-.210	-.190	-.136	-.070	.007	.085	.167	.224
	.450	.179	.163	.138	.083	.011	-.049	-.110	-.155	-.189	-.176	-.135	-.084	-.023	.040	.108	.152
	.550	.092	.087	.076	.030	-.035	-.075	-.121	-.154	-.177	-.165	-.138	-.101	-.054	-.005	.051	.082
	.650	.015	.026	.032	0	-.047	-.085	-.119	-.139	-.154	-.148	-.129	-.105	-.072	-.033	.012	.027
	.750	-.059	-.032	-.003	-.025	-.057	-.085	-.099	-.109	-.116	-.111	-.103	-.097	-.072	-.050	-.017	-.018
	.850	-.097	-.047	.011	.002	-.014	-.023	-.023	-.021	-.018	-.019	-.021	-.028	-.023	-.013	.003	-.021
	.925	-.120	-.047	.038	.043	.036	.060	.069	.078	.082	.081	.074	.064	.050	.032	.040	-.009
	.975	-.186	-.076	.052	.074	.090	.120	.137	.144	.148	.148	.139	.132	.103	.075	.058	-.016
	1.000	-.248	-.092	.085	.190	.127	.158	.175	.178	.183	.177	.170	.165	.170	.110	.063	-.025

<sup>a</sup>No orifice.

NACA



TABLE 5.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(08,20) PROPELLER BLADE SECTION ( $\alpha = 0.78$ ) - Continued

(a)  $N = 1500$  rpm.

J	1.716	1.829	1.968	2.092	2.214	2.326	2.451	2.513	2.476	2.389	2.264	2.137	2.033	1.910	1.801
$M_x$	.687	.704	.720	.738	.758	.777	.799	.809	.802	.787	.763	.744	.727	.708	.692
$\alpha_1$	8.85	7.11	5.08	3.36	1.75	.34	-1.16	-1.87	-1.45	-.42	1.11	2.76	4.17	5.92	7.54
$\Delta\delta$	.45	.38	.30	.23	.15	.07	-.03	-.07	-.04	.02	.12	.20	.26	.34	.40
$c_l$	3.04	2.50	1.95	1.52	1.12	.67	.36	.08	.22	.51	.91	1.34	1.72	2.21	2.63
$c_m$	.9664	.7923	.6213	.4845	.3587	.2161	.1161	.0271	.0700	.1623	.2919	.4306	.5497	.7052	.8329
$c_c$	-.0133	-.0177	-.0283	-.0411	-.0515	-.0633	-.0769	-.0842	-.0787	-.0728	-.0572	-.0466	-.0329	-.0262	-.0169
c/b	Pressure coefficient, P														
Upper surface	$\theta$ , 0.000	1.125	1.131	1.137	1.145	1.152	1.160	1.170	1.174	1.172	1.165	1.154	1.147	1.140	1.132
	.025	-1.956	-1.553	-1.085	-.641	-.194	.143	.392	.503	.442	.286	-.039	-.452	-.870	-1.305
	.050	-2.024	-1.673	-1.303	-.858	-.422	-.143	.073	.178	.122	-.021	-.293	-.643	-1.116	-1.477
	.100	-1.933	-1.588	-1.247	-.685	-.410	-.242	-.078	.007	-.041	-.150	-.348	-.582	-.914	-1.436
	.200	-1.801	-1.479	-.724	-.647	-.497	-.359	-.236	-.165	-.204	-.289	-.437	-.587	-.680	-1.160
	.300	-1.337	-.565	-.635	-.603	-.513	-.419	-.325	-.268	-.301	-.366	-.475	-.571	-.635	-.596
	.400	-.549	-.569	-.637	-.619	-.567	-.514	-.441	-.393	-.419	-.473	-.554	-.604	-.632	-.619
	.500	-.566	-.561	-.593	-.585	-.571	-.550	-.510	-.477	-.496	-.529	-.568	-.585	-.590	-.587
	.600	-.519	-.500	-.525	-.533	-.543	-.564	-.592	-.575	-.585	-.582	-.557	-.541	-.527	-.520
	.700	-.435	-.406	-.426	-.441	-.459	-.481	-.500	-.526	-.585	-.511	-.474	-.457	-.428	-.425
	.800	-.290	-.244	-.256	-.276	-.298	-.313	-.326	-.326	-.306	-.327	-.311	-.296	-.259	-.249
	.900	-.078	-.009	-.006	-.021	-.032	-.044	-.049	-.042	-.053	-.053	-.047	-.034	-.006	-.012
	.950	.042	.106	.102	.114	.119	.118	.123	.127	.120	.119	.109	.100	.106	.103
Lower surface	.0375	.639	.578	.415	.232	.007	-.257	-.570	-.867	-.708	-.423	-.116	.135	.324	.491
	.075	.501	.452	.316	.172	.005	-.188	-.466	-.793	-.595	-.307	-.089	.097	.244	.378
	.150	.348	.317	.209	.097	-.016	-.144	-.274	-.298	-.306	-.211	-.081	.045	.150	.259
	.250	.241	.223	.131	.051	-.042	-.134	-.226	-.271	-.251	-.183	-.090	.004	.089	.174
	.350	.162	.153	.077	.007	-.067	-.142	-.209	-.246	-.229	-.178	-.107	-.030	.039	.112
	.450	.095	.097	.028	-.029	-.088	-.150	-.200	-.226	-.214	-.178	-.123	-.061	-.003	.059
	.550	.033	.038	-.020	-.070	-.116	-.165	-.199	-.217	-.209	-.183	-.146	-.095	-.048	.007
	.650	-.014	-.001	-.053	-.092	-.125	-.162	-.181	-.228	-.187	-.170	-.150	-.112	-.076	-.028
	.750	-.047	-.026	-.070	-.095	-.115	-.132	-.134	-.134	-.136	-.131	-.131	-.110	-.087	-.046
	.850	-.023	.006	-.023	-.032	-.032	-.035	-.018	-.013	-.019	-.022	-.043	-.039	-.034	-.007
	.925	.028	.062	.047	.054	.068	.074	.098	.105	.100	.090	.062	.056	.041	.057
	.975	.059	.098	.084	.106	.129	.142	.165	.171	.165	.156	.125	.112	.080	.097
	1.000	.083	.120	.118	.125	.153	.192	.216	.230	.194	.192	.184	.188	.143	.129

\*No orifice.

NACA

TABLE 5.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(08.20) PROPELLER BLADE SECTION ( $x = 0.78$ ) - Continued

(a)  $N = 1600$  rpm.

$J$	1.871	1.958	2.030	2.113	2.202	2.290	2.366	2.456	2.405	2.332	2.253	2.167	2.080	2.017	1.920
$M_x$	.750	.766	.777	.792	.806	.825	.838	.855	.844	.831	.816	.799	.783	.776	.757
$\alpha_x$	6.49	5.22	4.21	3.08	1.91	.79	-.15	-1.22	-.61	.27	1.28	2.36	3.52	4.39	5.77
$\Delta\theta$	.56	.48	.40	.30	.20	.10	.02	-.09	-.03	.06	.14	.24	.35	.42	.52
$\alpha_1$	2.60	2.15	1.86	1.52	1.09	.79	.40	-.06	.18	.59	.91	1.25	1.58	1.89	2.31
$c_n$	.8252	.6858	.5935	.4877	.3503	.2542	.1290	-.0181	.0574	.1903	.2968	.4019	.5065	.6032	.7355
$c_m$	-.0342	-.0390	-.0423	-.0539	-.0567	-.0654	-.0652	-.0642	-.0623	-.0646	-.0583	-.0526	-.0441	-.0416	-.0387
$c_c$						-.0140	-.0182	-.0221	-.0205	-.0160					
$c/b$	Pressure coefficient, $P$														
Upper surface	$a_0$ .000	1.149	1.156	1.160	1.167	1.173	1.182	1.188	1.196	1.190	1.186	1.178	1.170	1.163	1.152
	.025	-1.155	-.873	-.668	-.405	-.114	.131	.318	.473	.398	.233	.016	-.227	-.502	-.706
	.050	-1.340	-1.118	-.944	-.682	-.379	-.159	.007	.155	.085	-.066	-.259	-.491	-.782	-.969
	.100	-1.331	-1.118	-.925	-.593	-.417	-.259	-.127	-.004	-.066	-.184	-.335	-.491	-.701	-.958
	.200	-1.284	-1.064	-.860	-.685	-.500	-.379	-.272	-.169	-.221	-.316	-.434	-.577	-.717	-.903
	.300	-1.257	-1.047	-.846	-.694	-.560	-.433	-.347	-.262	-.306	-.380	-.489	-.609	-.742	-.863
	.400	-1.244	-.942	-.786	-.724	-.618	-.550	-.480	-.400	-.440	-.506	-.581	-.661	-.739	-.765
	.500	-.510	-.569	-.826	-.815	-.732	-.667	-.597	-.522	-.561	-.621	-.700	-.763	-.828	-.773
	.600	-.433	-.493	-.499	-.758	-.781	-.734	-.674	-.602	-.639	-.692	-.757	-.797	-.547	-.501
	.700	-.374	-.407	-.405	-.383	-.412	-.801	-.794	-.735	-.768	-.800	-.572	-.397	-.401	-.408
	.800	-.236	-.239	-.236	-.222	-.218	-.209	-.211	-.221	-.221	-.207	-.214	-.229	-.234	-.235
Lower surface	.900	-.010	.007	.009	.018	.018	.016	.011	-.040	-.003	.022	.017	.013	.011	.003
	.950	.122	.120	.111	.119	.119	.102	.079	.025	.062	.104	.114	.115	.114	.126
	.0375	.522	.409	.309	.185	.003	-.212	-.424	-.630	-.503	-.322	-.104	.067	.223	.334
	.075	.409	.315	.234	.139	0	-.159	-.368	-.669	-.587	-.240	-.079	.047	.170	.255
	.150	.286	.208	.142	.071	-.023	-.135	-.239	-.540	-.292	-.181	-.076	.008	.094	.159
	.250	.199	.140	.086	.028	-.047	-.138	-.213	-.292	-.259	-.172	-.092	-.023	.046	.100
	.350	.135	.080	.032	-.017	-.080	-.159	-.218	-.303	-.255	-.184	-.121	-.061	-.002	.044
	.450	.079	.030	-.017	-.056	-.109	-.178	-.225	-.289	-.253	-.196	-.144	-.086	-.045	-.002
	.550	.025	-.020	-.060	-.096	-.141	-.204	-.246	-.292	-.268	-.219	-.173	-.128	-.085	-.049
	.650	-.015	-.056	-.091	-.121	-.158	-.212	-.246	-.283	-.266	-.221	-.185	-.150	-.110	-.079
	.750	-.035	-.068	-.098	-.121	-.145	-.184	-.209	-.233	-.220	-.188	-.166	-.140	-.113	-.090
	.850	.009	-.016	-.037	-.047	-.057	-.079	-.092	-.106	-.097	-.078	-.069	-.059	-.045	-.031
	.925	.087	.064	.047	.046	.044	.032	.021	.002	.015	.035	.040	.042	.045	.052
	.975	.135	.108	.095	.100	.103	.093	.077	.048	.068	.094	.100	.099	.095	.097
	$a_1$ .000	.236	.164	.167	.151	.173	.140	.118	.072	.093	.125	.170	.165	.164	.158

\*No orifice.

NACA

TABLE 5.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(08.20) PROPELLER BLADE SECTION ( $\alpha = 0.78$ ) - Continued

(a)  $M = 0.56$ .

$J$	1.954	1.985	2.015	2.066	2.090	2.128	2.177	2.210	2.263	2.307	2.349	2.387	2.446	2.504
$M_x$	.901	.890	.883	.870	.866	.857	.849	.841	.837	.829	.826	.807	.800	.787
$\alpha_x'$	5.28	4.84	4.42	3.71	3.38	2.87	2.23	1.79	1.12	.57	.05	-.40	-1.10	-1.78
$\Delta B$	.39	.36	.34	.29	.27	.24	.20	.17	.13	.09	.06	.03	-.02	-.06
$c_l$	1.56	1.46	1.40	1.34	1.25	1.18	1.08	.95	.80	.66	.58	.45	.27	.06
$c_{lH}$	.4961	.4652	.4477	.4290	.4000	.3774	.3465	.3058	.2581	.2135	.1852	.1452	.0865	.0181
$c_{mH}$	-.0428	-.0410	-.0423	-.0511	-.0539	-.0574	-.0603	-.0636	-.0623	-.0695	-.0714	-.0754	-.0759	-.0791
$c_o$	.0265	.0236	.0219	.0214	.0204	.0200	.0186	.0165	.0156	.0151				
$a/b$	Pressure coefficient, P													
Upper surface	.0000	1.220	1.214	1.210	1.203	1.201	1.197	1.193	1.189	1.187	1.184	1.178	1.174	1.165
	.025	-.237	-.226	-.207	-.157	-.104	-.064	-.003	.050	.137	.202	.267	.335	.505
	.050	-.522	-.515	-.496	-.445	-.392	-.350	-.283	-.232	-.152	-.095	-.038	.025	.103
	.100	-.555	-.544	-.521	-.437	-.373	-.369	-.335	-.304	-.249	-.206	-.163	-.116	-.053
	.200	-.600	-.586	-.553	-.527	-.505	-.494	-.460	-.418	-.372	-.337	-.302	-.264	-.213
	.300	-.654	-.642	-.619	-.606	-.574	-.557	-.515	-.495	-.442	-.396	-.372	-.346	-.302
	.400	-.688	-.680	-.667	-.651	-.626	-.614	-.585	-.553	-.528	-.515	-.496	-.472	-.422
	.500	-.781	-.781	-.765	-.759	-.735	-.725	-.691	-.673	-.658	-.628	-.597	-.558	-.491
	.600	-.846	-.848	-.839	-.832	-.804	-.792	-.768	-.752	-.729	-.698	-.648	-.616	-.570
	.700	-.497	-.452	-.453	-.531	-.524	-.564	-.699	-.835	-.844	-.795	-.733	-.625	-.530
	.800	-.361	-.338	-.322	-.319	-.296	-.294	-.250	-.210	-.208	-.216	-.257	-.298	-.321
	.900	-.330	-.293	-.262	-.231	-.200	-.198	-.131	-.042	.004	.015	-.001	-.025	-.046
	.950	-.323	-.276	-.232	-.177	-.132	-.120	-.057	.027	.083	.120	.129	.128	.116
Lower surface	.0375	.318	.282	.248	.182	.147	.058	-.010	-.082	-.188	-.274	-.375	-.480	-.629
	.075	.259	.227	.199	.146	.119	.046	-.007	-.062	-.141	-.205	-.279	-.371	-.519
	.150	.172	.146	.124	.083	.066	.009	-.027	-.063	-.117	-.153	-.194	-.237	-.287
	.250	.104	.084	.066	.031	.020	-.030	-.058	-.086	-.129	-.149	-.176	-.202	-.231
	.350	.036	.018	.004	-.028	-.034	-.077	-.096	-.119	-.150	-.163	-.182	-.195	-.213
	.450	-.029	-.044	-.056	-.083	-.086	-.122	-.135	-.149	-.171	-.176	-.184	-.191	-.200
	.550	-.117	-.128	-.136	-.158	-.154	-.184	-.186	-.192	-.204	-.199	-.198	-.195	-.198
	.650	-.205	-.214	-.216	-.231	-.221	-.238	-.226	-.217	-.218	-.201	-.192	-.184	-.179
	.750	-.318	-.320	-.311	-.301	-.266	-.277	-.223	-.203	-.190	-.165	-.151	-.138	-.130
	.850	-.368	-.344	-.294	-.238	-.181	-.163	-.126	-.100	-.084	-.057	-.042	-.026	-.015
	.925	-.314	-.252	-.197	-.137	-.086	-.069	-.030	.002	.026	.056	.071	.085	.098
	.975	-.298	-.258	-.210	-.133	-.075	-.051	-.006	.042	.082	.119	.137	.151	.164
	1.000	-.268	-.260	-.180	-.137	-.079	-.051	-.001	.060	.126	.141	.170	.209	.211

No orifice.

NACA

TABLE 5.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-(3)(08.20) PROPELLER BLADE SECTION ( $x = 0.78$ ) - Continued $(r) M = 0.60.$ 

$\frac{r}{M}$	2.464	2.430	2.386	2.347	2.306	2.232	2.182	2.151	2.121	2.080	2.051	2.012	1.981	2.301
$\frac{r}{M}$	.850	.859	.868	.875	.883	.898	.905	.916	.923	.929	.939	.947	.955	.881
$\frac{r}{M}$	-1.31	-.91	-.39	.09	.59	1.52	2.17	2.57	2.97	3.52	3.92	4.46	4.90	.65
$\frac{r}{M}$	-.07	-.03	.02	.06	.10	.17	.20	.22	.24	.26	.27	.28	.29	.11
$\frac{r}{M}$	.02	.05	.12	.24	.31	.50	.67	.77	.89	1.04	1.16	1.33	1.50	.31
$\frac{r}{M}$	.0064	.0161	.0387	.0781	.0987	.1606	.2155	.2477	.2845	.3335	.3690	.4245	.4768	.0987
$\frac{r}{M}$	-.0897	-.0737	-.0649	-.0582	-.0493	-.0346	-.0305	-.0285	-.0341	-.0403	-.0508	-.0624	-.0793	-.0508
$\frac{r}{M}$	.0230	.0248	.0270	.0294	.0304	.0328	.0358	.0398	.0405	.0407	.0424	.0439	.0458	.0311
$c/b$	Pressure coefficient, P													
Upper surface	.000	1.194	1.198	1.202	1.206	1.210	1.218	1.221	1.227	1.231	1.234	1.240	1.244	1.209
	.025	.500	.464	.420	.372	.323	.220	.179	.121	.088	.049	.022	-.017	.327
	.050	.186	.151	.110	.066	.022	-.070	-.128	-.164	-.201	-.239	-.264	-.304	.025
	.100	.023	-.002	-.034	-.064	-.097	-.163	-.201	-.197	-.228	-.239	-.284	-.346	-.099
	.200	-.152	-.170	-.195	-.219	-.243	-.304	-.343	-.357	-.365	-.380	-.384	-.406	-.245
	.300	-.250	-.259	-.278	-.300	-.335	-.384	-.416	-.433	-.443	-.459	-.469	-.485	-.335
	.400	-.389	-.393	-.404	-.409	-.420	-.459	-.488	-.497	-.502	-.513	-.522	-.540	-.423
	.500	-.503	-.516	-.530	-.543	-.553	-.571	-.599	-.610	-.612	-.621	-.622	-.636	-.558
	.600	-.588	-.603	-.615	-.621	-.633	-.654	-.673	-.680	-.683	-.694	-.697	-.706	-.639
	.700	-.715	-.732	-.746	-.750	-.753	-.767	-.787	-.786	-.784	-.792	-.792	-.799	-.760
Lower surface	.800	-.467	-.273	-.232	-.231	-.243	-.285	-.351	-.405	-.416	-.410	-.514	-.613	-.238
	.900	-.048	-.102	-.150	-.183	-.195	-.203	-.245	-.290	-.317	-.335	-.368	-.406	-.198
	.950	.065	-.023	-.084	-.120	-.139	-.154	-.190	-.251	-.292	-.314	-.343	-.390	-.145
	.0375	-.713	-.553	-.441	-.367	-.305	-.146	-.067	.007	.077	.144	.187	.241	-.319
	.075	-.729	-.620	-.556	-.433	-.303	-.111	-.050	.013	.070	.124	.158	.240	-.329
	.150	-.620	-.472	-.324	-.208	-.174	-.088	-.051	-.007	.038	.080	.103	.136	-.187
	.250	-.293	-.261	-.247	-.217	-.180	-.108	-.079	-.044	-.003	.035	.054	.082	-.110
	.350	-.296	-.280	-.265	-.234	-.206	-.145	-.122	-.090	-.054	-.020	-.001	.021	-.218
	.450	-.280	-.271	-.266	-.249	-.230	-.182	-.164	-.136	-.104	-.075	-.058	-.038	-.238
	.550	-.273	-.280	-.291	-.285	-.275	-.238	-.225	-.201	-.173	-.146	-.129	-.112	-.283

<sup>a</sup>No airfoils.

NACA

TABLE 5.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(08.20) PROPELLER BLADE SECTION ( $x = 0.78$ ) - Concluded

(a)  $M = 0.65$ .

	J	2.382	2.343	2.312	2.285	2.272	2.234	2.198	2.171	2.141	2.114	2.091	2.060	2.035	2.022	1.987
$M_x$		.937	.945	.951	.957	.968	.974	.976	.983	.991	.998	1.004	1.009	1.016	1.028	1.032
$\alpha$		-.34	.14	.52	.85	1.01	1.50	1.96	2.31	2.71	3.07	3.38	3.80	4.14	4.32	4.81
$\alpha_i$		-.30	-.19	-.04	-.12	.28	.47	.62	.77	.88	.96	1.07	1.17	1.26	1.34	1.43
$c_n$		-.0968	-.0394	-.0116	.0387	.0903	.1516	.1981	.2452	.2826	.3058	.3432	.3748	.4026	.4284	.4568
$c_m$		-.0146	-.0196	-.0247	-.0374	-.0487	-.0623	-.0710	-.0803	-.0897	-.0890	-.0911	-.0975	-.1026	-.1042	-.1106
$c_c$		.0509	.0512	.0523	.0542	.0578	.0608	.0636	.0636	.0636	.0627	.0619	.0610	.0603	.0599	.0597
c/b	Pressure coefficient, P															
Upper surface	0.000	1.238	1.243	1.247	1.250	1.256	1.259	1.261	1.265	1.269	1.273	1.277	1.280	1.284	1.293	1.295
	.025	.505	.477	.435	.411	.398	.366	.340	.297	.268	.268	.231	.194	.164	.148	.130
	.050	.804	.178	.140	.117	.105	.076	.052	.011	-.003	-.021	-.063	-.097	-.122	-.138	-.157
	.100	.060	.040	.011	-.005	-.009	-.029	-.046	-.072	-.077	-.079	-.096	-.120	-.168	-.194	-.216
	.200	-.097	-.110	-.133	-.147	-.157	-.178	-.189	-.208	-.210	-.211	-.231	-.247	-.255	-.263	-.283
	.300	-.186	-.206	-.233	-.246	-.242	-.254	-.267	-.287	-.289	-.292	-.311	-.328	-.342	-.343	-.356
	.400	-.293	-.298	-.315	-.326	-.328	-.342	-.350	-.359	-.358	-.356	-.373	-.390	-.404	-.407	-.417
	.500	-.422	-.424	-.435	-.441	-.438	-.447	-.455	-.470	-.467	-.462	-.472	-.481	-.491	-.493	-.505
	.600	-.503	-.506	-.520	-.527	-.522	-.527	-.529	-.541	-.540	-.535	-.545	-.555	-.563	-.559	-.569
	.700	-.623	-.621	-.632	-.636	-.631	-.635	-.637	-.643	-.639	-.632	-.640	-.647	-.655	-.649	-.656
Lower surface	.800	-.736	-.738	-.742	-.744	-.737	-.740	-.739	-.744	-.737	-.728	-.735	-.741	-.744	-.738	-.742
	.900	-.847	-.864	-.869	-.884	-.899	-.925	-.921	-.947	-.954	-.944	-.941	-.949	-.956	-.950	-.953
	.950	-.926	-.943	-.955	-.965	-.973	-.982	-.986	-.995	-.996	-.993	-.990	-.994	-.997	-.996	-.999
	.0375	-.345	-.279	-.235	-.201	-.156	-.115	-.077	-.013	.034	.087	.136	.190	.231	.272	.299
	.075	-.443	-.408	-.371	-.332	-.274	-.195	-.116	-.015	.037	.086	.127	.171	.206	.240	.260
	.150	-.617	-.575	-.510	-.438	-.353	-.255	-.166	-.069	.038	.075	.101	.132	.158	.184	.199
	.250	-.775	-.689	-.593	-.493	-.382	-.269	-.169	-.090	.002	.035	.058	.086	.108	.131	.142
	.350	-.872	-.729	-.607	-.487	-.353	-.215	-.105	-.075	-.047	-.015	.004	.028	.049	.069	.080
	.450	-.981	-.768	-.625	-.481	-.325	-.174	-.134	-.123	-.093	-.062	-.044	-.024	-.005	.015	.023
	.550	-.930	-.631	-.494	-.345	-.245	-.222	-.202	-.171	-.140	-.110	-.093	-.072	-.054	-.036	-.028
	.650	-.891	-.571	-.437	-.341	-.235	-.292	-.273	-.244	-.217	-.190	-.177	-.159	-.144	-.126	-.119
	.750	-.888	-.470	-.357	-.341	-.313	-.297	-.280	-.254	-.229	-.205	-.193	-.176	-.160	-.141	-.134
	.850	-.843	-.526	-.416	-.350	-.347	-.338	-.315	-.293	-.268	-.245	-.235	-.210	-.194	-.174	-.168
	.925	-.565	-.548	-.539	-.524	-.498	-.479	-.464	-.442	-.419	-.394	-.382	-.366	-.349	-.330	-.324
	.975	-.417	-.447	-.491	-.515	-.500	-.487	-.473	-.453	-.431	-.407	-.394	-.380	-.363	-.343	-.337
	1.000	-.220	-.240	-.280	-.310	-.305	-.350	-.380	-.415	-.405	-.400	-.384	-.360	-.363	-.346	-.326

\*No crifice.

NACA



TABLE 6.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-(3)(07.50) PROPELLER BLADE SECTION ( $x = 0.85$ )

$$[\beta_{0.75R} = 45^\circ; \beta_x = 41.3^\circ; B = 2]$$

(a)  $N = 1140$  rpm.

	1.368	1.512	1.660	1.798	1.982	2.132	2.234	2.373	2.538	2.625	2.468	2.312	2.183	2.079	1.900	1.765	1.607	1.440
$M_x$	.506	.523	.536	.547	.564	.582	.592	.607	.627	.639	.616	.600	.582	.571	.554	.543	.527	.511
$q_{x'}$	14.17	11.78	9.43	7.35	4.72	2.71	1.38	-.33	-2.24	-3.21	-1.44	.41	2.04	3.40	5.87	7.85	10.26	12.96
$\Delta p$	.37	.33	.28	.24	.17	.11	.07	.01	-.06	-.09	-.02	.04	.09	.14	.21	.25	.30	.35
$C_L$	2.59	3.03	2.97	2.54	1.87	1.38	1.01	.63	.17	-.03	.32	.77	1.18	1.54	2.11	2.72	3.05	3.15
$C_D$	.6806	.8000	.7903	.6768	.5019	.3719	.2732	.1716	.0468	-.0084	.0868	.2087	.3194	.4129	.5645	.7245	.8110	.8316
$C_M$	-.0647	-.0177	-.0133	-.0308	-.0349	-.0429	-.0537	-.0625	-.0686	-.0794	-.0681	-.0605	-.0504	-.0397	-.0323	-.0256	-.0079	-.0251
$C_o$																		
$c/b$	Pressure coefficient, P																	
Upper surface	$\theta$	1.065	1.070	1.073	1.077	1.082	1.087	1.090	1.095	1.102	1.106	1.098	1.093	1.087	1.084	1.079	1.076	1.071
	.000	1.065	1.070	1.073	1.077	1.082	1.087	1.090	1.095	1.102	1.106	1.098	1.093	1.087	1.084	1.079	1.076	1.071
	.025	-.746	-1.427	-2.149	-2.865	-3.564	-4.247	-4.915	-5.568	-6.206	-6.829	-7.437	-8.030	-8.608	-9.171	-9.719	-10.252	-10.770
	.050	-.724	-1.402	-2.120	-2.832	-3.529	-4.210	-4.872	-5.523	-6.164	-6.795	-7.416	-8.027	-8.628	-9.219	-9.799	-10.368	-10.926
	.100	-.696	-1.397	-2.113	-2.822	-3.517	-4.196	-4.856	-5.505	-6.144	-6.773	-7.392	-8.001	-8.599	-9.186	-9.761	-10.325	-10.878
	.200	-.629	-1.167	-1.892	-2.611	-3.324	-4.030	-4.728	-5.418	-6.100	-6.773	-7.437	-8.091	-8.734	-9.366	-9.987	-10.597	-11.196
	.300	-.579	-.899	-1.638	-2.371	-3.097	-3.815	-4.524	-5.224	-5.915	-6.597	-7.270	-7.933	-8.586	-9.229	-9.861	-10.482	-11.092
	.400	-.538	-.618	-.549	-.451	-.344	-.228	-.103	.031	.156	.271	.377	.473	.560	.637	.704	.761	.808
	.500	-.517	-.461	-.401	-.336	-.265	-.188	-.105	.014	.129	.235	.331	.417	.493	.559	.615	.661	.697
	.600	-.498	-.358	-.215	-.069	.081	.216	.335	.438	.524	.592	.642	.675	.699	.714	.720	.717	.704
Lower surface	$\theta$	-.481	-.277	-.131	.044	.239	.444	.650	.856	1.062	1.268	1.473	1.678	1.882	2.085	2.286	2.485	2.682
	.000	-.481	-.277	-.131	.044	.239	.444	.650	.856	1.062	1.268	1.473	1.678	1.882	2.085	2.286	2.485	2.682
	.025	-.462	-.211	-.022	.168	.363	.568	.773	.978	1.182	1.386	1.589	1.791	1.992	2.192	2.390	2.587	2.782
	.050	-.443	-.155	.073	.268	.463	.668	.872	1.076	1.279	1.481	1.682	1.882	2.081	2.278	2.474	2.669	2.862
	.100	-.419	-.128	-.007	.200	.395	.590	.784	.978	1.171	1.363	1.554	1.744	1.932	2.118	2.303	2.487	2.669
	.200	-.373	-.073	.149	.344	.539	.733	.926	1.118	1.309	1.499	1.688	1.875	2.060	2.243	2.424	2.603	2.780
	.300	-.330	-.030	.188	.383	.578	.771	.963	1.154	1.344	1.533	1.721	1.907	2.091	2.272	2.451	2.628	2.803
	.400	-.290	-.010	.208	.403	.598	.791	.982	1.172	1.361	1.549	1.736	1.921	2.104	2.285	2.464	2.641	2.816
	.500	-.252	.010	.258	.453	.648	.841	1.032	1.222	1.411	1.599	1.786	1.971	2.154	2.335	2.514	2.691	2.866
	.600	-.217	.044	.290	.485	.680	.873	1.064	1.254	1.443	1.631	1.818	2.003	2.186	2.367	2.546	2.723	2.898

No orifice.

NACA

TABLE 6.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(07.50) PROPELLER BLADE SECTION ( $x = 0.85$ ) - Continued

(b)  $N = 1350$  rpm.

$\frac{r}{R}$	1.468 .618	1.600 .634	1.744 .648	1.880 .665	2.013 .682	2.142 .695	2.276 .714	2.410 .734	2.543 .756	2.488 .747	2.364 .724	2.208 .703	2.087 .687	1.933 .671	1.809 .658	1.676 .640	1.536 .628
$\frac{c_l}{c_d}$	12.50	10.37	8.15	6.15	4.30	2.57	.86	-.77	-2.30	-1.67	-.22	1.71	3.29	5.12	7.19	9.19	11.39
$\frac{c_m}{c_d}$	.57	.54	.49	.41	.33	.24	.14	.04	-.07	-.02	.07	.19	.28	.37	.45	.52	.56
$\frac{c_{m'}}{c_d}$	3.10	3.24	3.06	2.37	1.07	1.39	.90	.47	.05	.28	.68	1.17	1.60	2.05	2.68	3.24	3.12
$\frac{c_{m''}}{c_d}$	.8200	.8639	.8174	.6335	.5032	.3761	.2432	.1284	.0142	.0761	.1839	.3165	.4303	.5490	.7168	.8626	.8271
$\frac{c_{m'''}}{c_d}$	-.0254	.0013	-.0115	-.0323	-.0549	-.0441	-.0572	-.0653	-.0726	-.0676	-.0623	-.0486	-.0416	-.0321	-.0236	-.0123	-.0077
$\frac{o}{b}$	Pressure coefficient, $P$																
Upper surface	$\frac{r}{R}$	1.098	1.104	1.109	1.115	1.122	1.127	1.135	1.143	1.152	1.147	1.139	1.131	1.124	1.118	1.113	1.107
	$\frac{c_l}{c_d}$	1.098	1.104	1.109	1.115	1.122	1.127	1.135	1.143	1.152	1.147	1.139	1.131	1.124	1.118	1.113	1.107
	$\frac{c_m}{c_d}$	-.1.410	-.2.572	-.2.020	-.1.275	-.991	-.438	.001	.340	.560	.468	.200	-.204	-.688	-.1.166	-.1.772	-.2.332
	$\frac{c_{m'}}{c_d}$	-.1.389	-.2.538	-.2.147	-.1.761	-.1.005	-.596	-.281	-.081	.174	.087	-.134	-.430	-.773	-.1.316	-.1.857	-.2.364
	$\frac{c_{m''}}{c_d}$	-.1.293	-.2.153	-.1.921	-.1.849	-.1.677	-.1.495	-.1.302	-.1.22	.023	-.042	-.201	-.398	-.592	-.726	-.1.407	-.2.156
	$\frac{c_{m'''}}{c_d}$	-.1.115	-.901	-.676	-.710	-.610	-.490	-.377	-.299	-.159	-.205	-.314	-.437	-.546	-.651	-.708	-.759
	$\frac{c_{m''''}}{c_d}$	-.882	-.634	-.611	-.607	-.529	-.448	-.374	-.292	-.220	-.253	-.332	-.414	-.487	-.558	-.613	-.664
	$\frac{c_{m'''''}}{c_d}$	-.682	-.564	-.588	-.534	-.483	-.438	-.384	-.334	-.356	-.409	-.465	-.510	-.549	-.586	-.607	-.626
	$\frac{c_{m''''''}}{c_d}$	-.534	-.488	-.513	-.520	-.487	-.451	-.423	-.389	-.359	-.374	-.408	-.443	-.472	-.495	-.517	-.534
	$\frac{c_{m'''''''}}{c_d}$	-.419	-.422	-.463	-.481	-.463	-.450	-.440	-.426	-.415	-.419	-.436	-.452	-.460	-.464	-.472	-.459
	$\frac{c_{m''''''''}}{c_d}$	-.334	-.332	-.383	-.409	-.405	-.409	-.418	-.419	-.425	-.422	-.422	-.420	-.410	-.401	-.395	-.374
Lower surface	$\frac{r}{R}$	1.098	1.104	1.109	1.115	1.122	1.127	1.135	1.143	1.152	1.147	1.139	1.131	1.124	1.118	1.113	1.107
	$\frac{c_l}{c_d}$	1.098	1.104	1.109	1.115	1.122	1.127	1.135	1.143	1.152	1.147	1.139	1.131	1.124	1.118	1.113	1.107
	$\frac{c_m}{c_d}$	-.266	-.202	-.232	-.256	-.259	-.277	-.295	-.307	-.320	-.315	-.308	-.296	-.275	-.254	-.231	-.201
	$\frac{c_{m'}}{c_d}$	-.217	-.062	-.038	-.043	-.047	-.066	-.088	-.100	-.113	-.107	-.106	-.089	-.060	-.043	-.046	-.053
	$\frac{c_{m''}}{c_d}$	-.193	-.007	.061	.070	.080	.080	.069	.065	.059	.060	.060	.070	.078	.075	.057	.042
	$\frac{c_{m'''}}{c_d}$	.0375	.747	.715	.631	.507	.335	.133	-.097	-.359	-.648	-.846	-.944	-.011	.222	.402	.569
	$\frac{c_{m''''}}{c_d}$	.075	.605	.572	.491	.381	.238	.076	-.097	-.292	-.515	-.695	-.835	-.014	.149	.294	.436
	$\frac{c_{m'''''}}{c_d}$	.150	.452	.420	.359	.268	.162	.050	-.065	-.192	-.301	-.395	-.477	-.014	.097	.201	.312
	$\frac{c_{m''''''}}{c_d}$	.250	.325	.302	.253	.178	.096	.011	-.074	-.158	-.237	-.282	-.324	-.038	.045	.126	.214
	$\frac{c_{m'''''''}}{c_d}$	.350	.232	.218	.180	.115	.049	-.018	-.087	-.147	-.204	-.248	-.284	-.056	.009	.073	.147
	$\frac{c_{m''''''''}}{c_d}$	.450	.159	.155	.128	.070	.017	-.037	-.091	-.137	-.180	-.211	-.231	-.070	-.018	.036	.098
	$\frac{c_{m'''''''''}}{c_d}$	.550	.084	.093	.074	.018	-.024	-.068	-.104	-.136	-.167	-.194	-.215	-.092	-.052	-.009	.044
	$\frac{c_{m''''''''''}}{c_d}$	.650	.011	.034	.027	-.012	-.045	-.076	-.109	-.129	-.148	-.161	-.172	-.096	-.066	-.032	.010
	$\frac{c_{m'''''''''''}}{c_d}$	.750	-.057	-.068	-.004	-.030	-.053	-.074	-.097	-.103	-.110	-.107	-.102	-.095	-.069	-.046	.014
	$\frac{c_{m''''''''''''}}{c_d}$	.850	-.086	-.008	.014	.004	-.010	-.022	-.023	-.014	-.012	-.015	-.019	-.031	-.019	-.007	.018
	$\frac{c_{m'''''''''''''}}{c_d}$	.925	-.083	.030	.064	.037	.076	.069	.086	.091	.087	.078	.061	.048	.036	.060	.076
	$\frac{c_{m''''''''''''''}}{c_d}$	.975	-.161	.012	.058	.073	.088	.114	.139	.146	.141	.128	.096	.079	.069	.071	.087
	$\frac{c_{m'''''''''''''''}}{c_d}$	1.000	-.185	-.005	.037	.089	.091	.105	.136	.165	.171	.152	.107	.135	.160	.140	.085

<sup>a</sup>No orifice.<sup>b</sup>Lower surface only.

NACA

TABLE 6.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(07.50) PROPELLER BLADE SECTION ( $x = 0.85$ ) - Continued

(a)  $N = 1500$  rpm.

$J$	2.561	2.455	2.312	2.197	2.083	1.957	1.850	1.709	1.779	1.904	2.009	2.140	2.254	2.382	2.507
$M_I$	.828	.808	.784	.766	.751	.734	.718	.701	.712	.725	.742	.763	.778	.801	.820
$a_1'$	-2.50	-1.29	.41	1.86	3.35	5.07	6.59	8.68	7.63	5.81	4.35	2.59	1.13	-.43	-1.89
$\Delta\theta$	-.18	-.07	.07	.18	.29	.39	.47	.56	.52	.43	.35	.24	.13	.01	-.12
$a_1$	.03	.45	.89	1.34	1.67	2.13	2.66	3.34	3.00	2.45	1.94	1.54	1.19	.69	.26
$c_l$	.0071	.1219	.2419	.3639	.4497	.5723	.7123	.8935	.8006	.6587	.5213	.4168	.3226	.1877	.0697
$c_m$	-.0993	-.0887	-.0710	-.0556	-.0398	-.0341	-.0275	-.0198	-.0225	-.0288	-.0352	-.0497	-.0598	-.0760	-.0919
$c_o$															
$\alpha/b$	Pressure coefficient, P														
Upper surface	00.000	1.183	1.174	1.163	1.156	1.150	1.142	1.136	1.130	1.134	1.139	1.146	1.153	1.161	1.171
	00.025	.609	.462	.164	-.164	-.347	-.570	-.870	-.1.030	-.1.786	-.2.983	-.4.764	-.6.370	-.8.316	-.1.179
	00.050	.225	.081	-.178	-.449	-.817	-1.207	-1.496	-1.670	-1.659	-1.412	-1.081	-.647	-.327	-.092
	00.100	.068	-.051	-.242	-.427	-.631	-1.137	-1.460	-1.752	-1.625	-1.354	-.960	-.542	-.348	-.151
	00.200	-.138	-.234	-.372	-.492	-.606	-.612	-1.336	-1.726	-1.589	-1.163	-.614	-.361	-.144	-.003
	00.300	-.217	-.291	-.388	-.465	-.522	-.561	-.501	-.889	-.654	-.499	-.365	-.200	-.137	-.020
	00.400	-.310	-.335	-.367	-.401	-.430	-.462	-.480	-.508	-.513	-.548	-.524	-.550	-.514	-.463
	00.500	-.419	-.460	-.493	-.509	-.518	-.535	-.518	-.445	-.485	-.528	-.527	-.513	-.506	-.482
	00.600	-.527	-.544	-.533	-.522	-.504	-.507	-.494	-.442	-.472	-.501	-.502	-.510	-.527	-.542
	00.700	-.635	-.587	-.501	-.473	-.439	-.430	-.419	-.377	-.403	-.428	-.427	-.451	-.484	-.524
	00.800	-.738	-.594	-.328	-.304	-.270	-.263	-.258	-.242	-.256	-.265	-.260	-.284	-.312	-.336
	00.900	-.856	-.669	-.063	-.054	-.034	-.033	-.040	-.059	-.054	-.039	-.030	-.042	-.057	-.062
	00.950	-.111	-.099	-.097	-.099	-.098	-.088	-.081	-.091	-.066	-.085	-.090	-.099	-.097	-.105
Lower surface	00.0375	-.941	-.652	-.180	.037	.224	.381	.512	.651	.590	.464	.331	.153	-.043	-.838
	00.075	-.950	-.385	-.159	.003	.150	.275	.390	.516	.459	.345	.231	.089	-.062	-.776
	00.150	-.631	-.248	-.101	.002	.101	.191	.278	.381	.332	.242	.157	.061	-.041	-.729
	00.250	-.197	-.202	-.106	-.026	.046	.114	.185	.269	.230	.156	.088	.015	-.060	-.621
	00.350	-.181	-.176	-.107	-.047	.009	.062	.123	.196	.161	.099	.042	.001	-.073	-.591
	00.450	-.171	-.162	-.110	-.064	-.022	.022	.073	.138	.106	.053	.004	-.037	-.084	-.574
	00.550	-.166	-.158	-.122	-.091	-.059	-.025	.021	.076	.049	.003	-.039	-.070	-.104	-.568
	00.650	-.142	-.139	-.119	-.093	-.073	-.050	-.009	.036	.013	-.025	-.059	-.079	-.106	-.544
	00.750	-.093	-.097	-.095	-.081	-.073	-.061	-.029	.009	-.010	-.042	-.069	-.080	-.092	-.598
	00.850	.016	.005	-.008	-.021	-.022	-.015	.010	.036	.023	.001	-.021	-.027	-.014	-.007
	00.925	.121	.107	.092	.089	.058	.027	.054	.080	.066	.043	.031	.072	.085	.111
	00.975	.159	.145	.127	.097	.082	.074	.085	.094	.089	.084	.073	.090	.113	.148
	01.000	.215	.185	.220	.160	.180	.177	.130	.150	.136	.145	.125	.115	.135	.095

No orifice.

NACA

TABLE 6.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(07.50) PROPELLER BLADE SECTION ( $\alpha = 0.85$ ) - Continued

(4)  $N = 1600$  rpm.

	$J$	$M_x$	$C_{x1}$	$\Delta B$	$C_{d1}$	$C_{d2}$	$C_{d3}$	$C_{d4}$	$C_{d5}$	$C_{d6}$	$C_{d7}$	$C_{d8}$	$C_{d9}$	$C_{d10}$	$C_{d11}$	$C_{d12}$	$C_{d13}$	$C_{d14}$	$C_{d15}$	$C_{d16}$	$C_{d17}$	$C_{d18}$
	1.791	1.869	1.961	2.062	2.141	2.248	2.326	2.412	2.519	2.464	2.361	2.280	2.195	2.095	2.023	1.931	1.827					
	.763	.780	.788	.803	.817	.831	.844	.858	.879	.869	.850	.835	.819	.804	.793	.778	.762					
	7.45	6.31	5.01	3.62	2.58	1.21	.25	-.79	-2.03	-1.40	-.18	.81	1.88	3.19	4.15	5.43	6.92					
	.67	.64	.55	.44	.33	.17	.05	-.08	-.24	-.16	0	.12	.25	.39	.48	.58	.66					
	3.00	2.64	2.26	1.87	1.60	1.25	.86	.39	-.18	.12	.64	1.03	1.42	1.72	2.05	2.39	2.84					
	.8045	.7071	.6071	.5045	.4316	.3381	.2323	.1052	-.0484	.0335	.1742	.2800	.3832	.4665	.5510	.6420	.7606					
	-.0269	-.0279	-.0328	-.0423	-.0572	-.0675	-.0800	-.0824	-.0846	-.0819	-.0783	-.0747	-.0605	-.0477	-.0420	-.0333	-.0257					
								.0207	.0235	.0221	.0182											
$c/b$	Pressure coefficient, P																					
Upper surface	0.000	1.155	1.162	1.165	1.172	1.178	1.185	1.191	1.198	1.208	1.204	1.194	1.186	1.179	1.172	1.167	1.161	1.154				
	.025	-.967	-.775	-.638	-.431	-.192	.078	.287	.471	.598	.536	.376	.170	-.062	-.333	-.538	-.716	-.847				
	.050	-1.332	-1.171	-.978	-.741	-.523	-.264	-.075	.092	.224	.157	.001	-.181	-.393	-.647	-.853	-1.068	-1.291				
	.100	-1.319	-1.159	-.969	-.729	-.472	-.239	-.167	-.034	.075	.021	-.107	-.246	-.391	-.581	-.846	-1.059	-1.288				
	.200	-1.332	-1.171	-.968	-.707	-.448	-.238	-.130	-.228	-.130	-.178	-.286	-.406	-.566	-.720	-.897	-1.085	-1.288				
	.300	-1.287	-1.128	-.963	-.743	-.589	-.434	-.362	-.280	-.199	-.240	-.324	-.409	-.512	-.674	-.838	-1.035	-1.237				
	.400	-.998	-.823	-.680	-.599	-.463	-.340	-.256	-.199	-.130	-.151	-.240	-.302	-.444	-.598	-.683	-.690	-.839				
	.500	-.573	-.411	-.380	-.449	-.632	-.613	-.575	-.516	-.445	-.480	-.546	-.604	-.618	-.520	-.457	-.387	-.439				
	.600	-.359	-.359	-.460	-.557	-.592	-.677	-.649	-.597	-.541	-.571	-.624	-.670	-.657	-.576	-.534	-.456	-.370				
	.700	-.285	-.358	-.427	-.453	-.507	-.715	-.745	-.710	-.672	-.695	-.727	-.734	-.548	-.469	-.445	-.419	-.354				
	.800	-.183	-.227	-.251	-.251	-.255	-.234	-.245	-.280	-.256	-.251	-.268	-.239	-.255	-.259	-.255	-.254	-.229				
	.900	-.014	-.020	-.017	-.007	-.003	.008	.013	-.033	-.106	-.073	.004	.006	-.002	-.010	-.013	-.023	-.028				
	.950	.088	.105	.113	.118	.123	.117	.093	.028	-.060	-.020	.080	.109	.115	.114	.113	.105	.091				
Lower surface	.0375	.558	.463	.370	.254	.119	-.054	-.242	-.595	-.748	-.700	-.364	-.140	.029	.184	.304	.402	.508				
	.075	.434	.353	.273	.175	.070	-.067	-.216	-.573	-.768	-.711	-.322	-.134	-.001	.118	.219	.299	.391				
	.150	.317	.256	.194	.123	.049	-.043	-.134	-.225	-.748	-.538	-.190	-.084	-.001	.081	.153	.213	.283				
	.250	.220	.170	.117	.062	.006	-.067	-.136	-.211	-.604	-.229	-.172	-.102	-.034	.030	.085	.134	.191				
	.350	.150	.109	.067	.020	-.025	-.083	-.135	-.189	-.289	-.196	-.161	-.108	-.056	-.007	.039	.079	.126				
	.450	.095	.061	.025	-.015	-.051	-.097	-.139	-.182	-.172	-.185	-.160	-.119	-.076	-.038	.001	.036	.076				
	.550	.038	.010	-.024	-.056	-.084	-.120	-.155	-.193	-.185	-.201	-.172	-.138	-.105	-.078	-.045	-.015	.020				
	.650	.004	-.017	-.070	-.074	-.097	-.123	-.149	-.179	-.187	-.191	-.161	-.138	-.111	-.092	-.066	-.041	-.012				
	.750	-.020	-.032	-.056	-.075	-.088	-.101	-.117	-.141	-.161	-.152	-.124	-.112	-.094	-.087	-.070	-.051	-.029				
	.850	.017	.013	-.003	-.017	-.014	-.009	-.018	-.035	-.064	-.047	-.021	-.016	-.025	-.027	-.014	0	.012				
	.925	.063	.059	.063	.089	.092	.082	.058	.024	.024	.044	.078	.087	.089	.091	.064	.051	.027				
	.975	.095	.115	.107	.096	.114	.123	.108	.067	.019	.039	.098	.113	.096	.081	.052	.100	.101				
	1.000	.135	.157	.117	.155	.160	.187	.124	.068	0	.036	.112	.135	.135	.115	.148	.142	.150				

No orifice.

NACA

TABLE 6.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-(3)(07.50) PROPELLER BLADE SECTION ( $x = 0.85$ ) - Continued(e)  $M = 0.56$ .

$J$	2.534	2.482	2.440	2.397	2.354	2.328	2.286	2.254	2.222	2.184	2.151	2.124	2.092	2.066	2.030	2.007	1.982	1.954	1.931	
$M_\infty$	.823	.830	.838	.846	.852	.860	.866	.876	.883	.888	.899	.911	.914	.921	.928	.937	.948	.952	.961	
$c_{x'}$	-2.20	-1.61	-1.12	-.61	-.22	.22	.74	1.13	1.54	2.02	2.45	2.80	3.23	3.57	4.06	4.37	4.72	5.11	5.15	
$\Delta\theta$	-.12	-.08	-.04	.01	.04	.07	.11	.14	.18	.21	.24	.27	.30	.33	.36	.38	.41	.43	.44	
$c_l$	0	.15	.28	.41	.53	.63	.75	.84	.94	1.04	1.11	1.17	1.27	1.34	1.47	1.55	1.70	1.84	1.88	
$c_n$	0	.0400	.0768	.1119	.1445	.1710	.2039	.2284	.2535	.2800	.2994	.3148	.3394	.3594	.3948	.4155	.4561	.4948	.5045	
$c_m$	-0.039	-0.0811	-0.0778	-0.0715	-0.0700	-0.0672	-0.0629	-0.0547	-0.0533	-0.0500	-0.0439	-0.0377	-0.0364	-0.0328	-0.0374	-0.0420	-0.0531	-0.0660	-0.0718	
$c_o$					.0164	.0173	.0189	.0222	.0224	.0234	.0244	.0245	.0248	.0262	.0274	.0282	.0300	.0318	.0331	
$c/b$	Pressure coefficient, P																			
Upper surface	$a_{0.000}$	1.181	1.184	1.188	1.192	1.195	1.199	1.201	1.207	1.210	1.213	1.219	1.225	1.227	1.230	1.234	1.236	1.245	1.248	1.253
	.025	.585	.537	.483	.444	.392	.339	.289	.242	.206	.164	.121	.124	.041	.012	-.018	-.029	-.044	-.063	-.096
	.050	.202	.156	.105	.066	.021	-.025	-.071	-.114	-.147	-.186	-.227	-.221	-.295	-.311	-.332	-.339	-.349	-.367	-.398
	.100	.053	.015	-.026	-.064	-.086	-.123	-.152	-.181	-.200	-.221	-.249	-.223	-.287	-.325	-.366	-.382	-.395	-.417	-.409
	.200	-.147	-.179	-.213	-.240	-.267	-.302	-.329	-.371	-.406	-.423	-.442	-.408	-.471	-.481	-.493	-.502	-.511	-.528	-.519
	.300	-.224	-.252	-.281	-.295	-.312	-.335	-.360	-.393	-.405	-.424	-.450	-.423	-.491	-.505	-.521	-.525	-.529	-.543	-.536
	.400	-.368	-.403	-.446	-.463	-.476	-.489	-.495	-.519	-.534	-.542	-.556	-.518	-.581	-.589	-.605	-.611	-.613	-.623	-.614
	.500	-.412	-.438	-.472	-.506	-.532	-.558	-.571	-.585	-.598	-.608	-.627	-.590	-.647	-.649	-.658	-.666	-.671	-.682	-.674
	.600	-.507	-.537	-.555	-.578	-.606	-.634	-.652	-.670	-.678	-.686	-.698	-.665	-.727	-.735	-.738	-.739	-.739	-.752	-.743
	.700	-.583	-.626	-.670	-.679	-.706	-.739	-.757	-.773	-.763	-.744	-.713	-.580	-.531	-.538	-.617	-.661	-.758	-.826	-.820
	.800	-.288	-.271	-.242	-.218	-.200	-.194	-.177	-.196	-.201	-.207	-.225	-.186	-.243	-.261	-.285	-.297	-.332	-.321	-.313
	.900	-.045	-.033	-.012	.013	.022	0	-.045	-.114	-.128	-.147	-.180	-.151	-.215	-.239	-.263	-.274	-.306	-.354	-.376
	.950	.110	.110	.112	.118	.110	.064	.007	-.073	-.095	-.123	-.163	-.138	-.211	-.234	-.257	-.266	-.299	-.345	-.370
Lower surface	.0375	-.926	-.851	-.718	-.549	-.395	-.317	-.226	-.162	-.108	-.035	.009	.118	.129	.175	.222	.258	.295	.329	.338
	.075	-.930	-.842	-.655	-.489	-.365	-.292	-.208	-.154	-.112	-.053	-.018	.079	.081	.122	.160	.192	.225	.254	.263
	.150	-.377	-.299	-.248	-.231	-.204	-.181	-.136	-.106	-.079	-.034	-.012	.073	.062	.092	.122	.148	.173	.196	.204
	.250	-.210	-.220	-.216	-.197	-.177	-.167	-.137	-.123	-.104	-.070	-.054	.023	.007	.033	.059	.082	.102	.120	.130
	.350	-.194	-.200	-.197	-.184	-.171	-.169	-.150	-.142	-.129	-.104	-.094	-.022	-.045	-.021	-.001	.021	.039	.055	.064
	.450	-.181	-.188	-.187	-.177	-.171	-.175	-.162	-.163	-.155	-.134	-.128	-.060	-.087	-.059	-.050	-.032	-.016	-.002	.006
	.550	-.178	-.186	-.189	-.184	-.183	-.196	-.195	-.207	-.204	-.190	-.190	-.125	-.158	-.144	-.127	-.111	-.096	-.086	-.078
	.650	-.160	-.171	-.177	-.177	-.181	-.201	-.211	-.238	-.245	-.241	-.246	-.185	-.157	-.208	-.195	-.178	-.166	-.157	-.149
	.750	-.117	-.128	-.136	-.140	-.147	-.173	-.193	-.238	-.270	-.295	-.317	-.264	-.306	-.299	-.289	-.274	-.265	-.258	-.252
	.850	-.010	-.023	-.032	-.034	-.043	-.071	-.093	-.135	-.158	-.186	-.249	-.272	-.369	-.378	-.374	-.362	-.353	-.347	-.340
	.925	.095	.083	.073	.072	.062	.029	.002	-.046	-.066	-.089	-.127	-.107	-.191	-.265	-.322	-.333	-.335	-.336	-.332
	.975	.143	.129	.118	.113	.100	.059	.014	-.052	-.080	-.111	-.160	-.148	-.227	-.247	-.285	-.311	-.318	-.323	-.319
	1.000	.211	.182	.160	.145	.132	.089	.044	-.061	-.095	-.132	-.180	-.160	-.270	-.248	-.274	-.303	-.300	-.321	-.302

<sup>a</sup>No orifice.<sup>b</sup>Lower surface only.

NACA

TABLE 6.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(07.50) PROPELLER BLADE SECTION ( $x = 0.85$ ) - Continued

(F)  $M = 0.60$ .

$J$	1.958	1.977	2.019	2.045	2.073	2.095	2.129	2.146	2.198	2.240	2.257	2.290	2.336	2.363	2.403	2.436	2.460
$M_x$	1.018	1.008	1.000	.993	.984	.972	.966	.953	.951	.946	.934	.926	.919	.910	.904	.895	.890
$\alpha_x$	5.05	4.78	4.21	3.85	3.48	3.18	2.73	2.52	1.84	1.32	1.09	.68	.12	-.21	-.68	-1.07	-1.35
$\Delta\theta$	.33	.31	.28	.26	.24	.23	.20	.18	.14	.11	.09	.06	.02	-.01	-.06	-.10	-.13
$\alpha_1$	1.85	1.76	1.52	1.39	1.32	1.17	1.01	.85	.61	.40	.31	.20	.07	-.02	-.10	-.16	-.22
$\alpha_n$	.4968	.4716	.4071	.3723	.3335	.3148	.2726	.2297	.1645	.1084	.0842	.0542	.0187	-.0058	-.0271	-.0439	-.0587
$\alpha_m$	-.1147	-.1091	-.0873	-.0793	-.0741	-.0708	-.0589	-.0494	-.0348	-.0246	-.0235	-.0274	-.0324	-.0368	-.0503	-.0598	-.0641
$\alpha_o$	.0511	.0500	.0453	.0442	.0444	.0439	.0420	.0386	.0390	.0376	.0355	.0338	.0320	.0301	.0284	.0261	.0256
$o/b$	Pressure coefficient, P																
Upper surface	0.000	1.286	1.280	1.275	1.271	1.265	1.258	1.255	1.248	1.247	1.244	1.237	1.233	1.229	1.224	1.222	1.217
	.025	.099	.108	.142	.167	.192	.209	.224	.243	.311	.360	.386	.397	.457	.482	.523	.551
	.050	-.202	-.204	-.176	-.161	-.149	-.139	-.128	-.111	-.046	.005	.028	.029	.093	.116	.155	.182
	.100	-.259	-.258	-.223	-.189	-.156	-.147	-.150	-.146	-.098	-.065	-.054	-.063	-.011	.001	.031	.051
	.200	-.321	-.305	-.358	-.350	-.341	-.337	-.338	-.338	-.307	-.278	-.259	-.255	-.204	-.196	-.167	-.149
	.300	-.406	-.414	-.393	-.382	-.369	-.364	-.359	-.359	-.323	-.291	-.284	-.299	-.249	-.240	-.219	-.211
	.400	-.488	-.499	-.478	-.468	-.460	-.462	-.462	-.440	-.423	-.419	-.433	-.391	-.394	-.381	-.380	-.375
	.500	-.546	-.559	-.536	-.530	-.524	-.527	-.534	-.539	-.515	-.493	-.488	-.506	-.468	-.474	-.460	-.454
	.600	-.615	-.630	-.612	-.612	-.610	-.613	-.618	-.618	-.593	-.576	-.575	-.594	-.562	-.567	-.554	-.549
	.700	-.690	-.711	-.697	-.696	-.696	-.702	-.706	-.707	-.693	-.683	-.684	-.707	-.678	-.686	-.675	-.674
	.800	-.753	-.781	-.777	-.786	-.789	-.790	-.682	-.477	-.452	-.374	-.300	-.281	-.230	-.225	-.220	-.214
	.900	-.826	-.761	-.478	-.392	-.368	-.356	-.329	-.295	-.271	-.244	-.222	-.226	-.176	-.163	-.141	-.122
	.950	-.586	-.497	-.416	-.374	-.357	-.345	-.320	-.282	-.255	-.225	-.204	-.205	-.156	-.141	-.113	-.082
Lower surface	.0375	.333	.294	.258	.205	.177	.136	.071	.024	-.062	-.138	-.188	-.255	-.319	-.451	-.538	-.612
	.075	.263	.227	.197	.149	.127	.091	.032	-.012	-.089	-.151	-.231	-.383	-.411	-.479	-.563	-.640
	.150	.216	.186	.164	.126	.111	.083	.036	.005	-.044	-.092	-.124	-.178	-.204	-.286	-.448	-.503
	.250	.146	.118	.100	.067	.107	.030	-.013	-.039	-.080	-.120	-.150	-.201	-.203	-.252	-.351	-.448
	.350	.083	.056	.043	.013	.005	-.017	-.057	-.080	-.112	-.143	-.168	-.216	-.222	-.256	-.371	-.486
	.450	.032	.008	-.002	-.029	-.036	-.057	-.091	-.112	-.131	-.152	-.170	-.210	-.208	-.235	-.237	-.222
	.550	-.043	-.066	-.075	-.098	-.107	-.126	-.160	-.179	-.197	-.216	-.230	-.266	-.247	-.256	-.245	-.233
	.650	-.123	-.148	-.155	-.178	-.184	-.204	-.237	-.254	-.268	-.282	-.293	-.326	-.299	-.300	-.276	-.258
	.750	-.219	-.244	-.250	-.269	-.277	-.296	-.326	-.342	-.355	-.366	-.374	-.403	-.370	-.367	-.335	-.270
	.850	-.305	-.329	-.334	-.352	-.358	-.378	-.404	-.418	-.428	-.436	-.442	-.462	-.395	-.294	-.191	-.136
	.925	-.368	-.331	-.333	-.348	-.353	-.371	-.396	-.406	-.414	-.418	-.434	-.267	-.149	-.115	-.078	-.041
	.975	-.297	-.320	-.323	-.340	-.346	-.364	-.387	-.393	-.392	-.368	-.263	-.210	-.152	-.135	-.096	-.051
	1.000	-.290	-.306	-.320	-.331	-.333	-.341	-.354	-.323	-.322	-.262	-.198	-.190	-.157	-.151	-.109	-.060

No orifice.

NACA

TABLE 6.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-(3)(07.50) PROPELLER BLADE SECTION ( $\alpha = 0.85$ ) - Concluded(g)  $M = 0.64$ .

$\frac{y}{c}$	2.386	2.377	2.323	2.308	2.270	2.231	2.208	2.186	2.157	2.131	2.098	2.079	2.049	2.031	2.002	1.983
$\frac{y}{c}$	.962	.969	.976	.988	.993	1.000	1.007	1.018	1.026	1.034	1.039	1.048	1.058	1.064	1.072	1.082
$\frac{y}{c}$	-.14	-.13	.28	.46	.93	1.42	1.71	1.99	2.37	2.71	3.14	3.40	3.80	4.04	4.44	4.70
$\frac{y}{c}$	-.32	-.12	-.09	-.08	-.04	-.01	.01	.03	.06	.09	.12	.14	.17	.19	.23	.25
$\frac{y}{c}$	-.0871	-.0439	.0090	.0394	.0884	.1484	.1942	.2303	.2574	.2871	.3103	.3329	.3658	.3897	.4084	.4361
$\frac{y}{c}$	-.0305	-.0403	-.0465	-.0480	-.0605	-.0759	-.0900	-.0980	-.1018	-.1024	-.1068	-.1096	-.1127	-.1132	-.1167	-.1196
$\frac{y}{c}$	.0473	.0490	.0498	.0497	.0521	.0560	.0590	.0590	.0582	.0580	.0575	.0569	.0563	.0555	.0550	.0545
$\frac{y}{c}$	Pressure coefficient, $P$															
$\frac{y}{c}$	Pressure coefficient, $P$															
Upper surface	1.253	1.257	1.260	1.268	1.270	1.275	1.278	1.286	1.291	1.296	1.299	1.305	1.312	1.315	1.321	1.326
.000	.025	.038	.058	.082	.102	.121	.132	.150	.169	.186	.201	.217	.232	.248	.263	.278
.050	.081	.070	.059	.053	.031	.007	-.006	-.023	-.033	-.043	-.044	-.043	-.032	-.013	-.009	-.009
.100	-.113	-.122	-.131	-.143	-.174	-.195	-.201	-.211	-.217	-.223	-.223	-.220	-.228	-.235	-.242	-.250
.200	-.158	-.169	-.174	-.174	-.189	-.213	-.221	-.232	-.240	-.246	-.248	-.245	-.258	-.267	-.273	-.285
.300	-.304	-.309	-.311	-.311	-.322	-.336	-.337	-.343	-.345	-.350	-.350	-.344	-.349	-.354	-.361	-.373
.400	-.378	-.381	-.382	-.380	-.391	-.408	-.410	-.413	-.414	-.413	-.410	-.403	-.408	-.412	-.417	-.428
.500	-.475	-.474	-.472	-.468	-.474	-.488	-.491	-.498	-.498	-.497	-.495	-.486	-.487	-.486	-.488	-.498
.600	-.586	-.585	-.580	-.572	-.576	-.584	-.582	-.585	-.586	-.584	-.581	-.571	-.571	-.571	-.571	-.574
.700	-.711	-.709	-.702	-.691	-.690	-.699	-.694	-.690	-.686	-.683	-.679	-.668	-.666	-.663	-.661	-.663
.800	-.306	-.398	-.421	-.428	-.428	-.587	-.779	-.801	-.799	-.794	-.782	-.776	-.764	-.761	-.752	-.747
.900	-.265	-.318	-.328	-.330	-.372	-.507	-.751	-.820	-.818	-.807	-.801	-.788	-.783	-.779	-.776	-.773
.950																
Lower surface	.0375	-.396	-.332	-.255	-.171	-.113	-.080	-.041	.011	.049	.101	.145	.192	.241	.285	.351
.075	-.428	-.365	-.315	-.281	-.247	-.209	-.156	-.070	-.009	.053	.098	.144	.189	.229	.249	.285
.150	-.346	-.308	-.269	-.222	-.152	-.074	-.018	.011	.034	.069	.102	.138	.170	.202	.217	.245
.250	-.361	-.318	-.244	-.170	-.105	-.038	-.067	-.032	-.008	.025	.055	.090	.116	.143	.157	.181
.350	-.351	-.285	-.212	-.154	-.105	-.136	-.110	-.074	-.051	-.021	.004	.035	.058	.084	.100	.118
.450	-.309	-.248	-.208	-.185	-.169	-.150	-.126	-.093	-.074	-.047	-.020	.012	.032	.055	.066	.084
.550	-.309	-.279	-.251	-.225	-.210	-.193	-.172	-.140	-.123	-.101	-.081	-.055	-.037	-.016	-.005	.014
.650	-.347	-.330	-.305	-.279	-.268	-.256	-.238	-.214	-.199	-.177	-.158	-.132	-.114	-.094	-.083	-.066
.750	-.421	-.407	-.384	-.360	-.350	-.343	-.325	-.303	-.289	-.269	-.248	-.225	-.208	-.190	-.178	-.162
.850	-.480	-.472	-.450	-.427	-.421	-.416	-.398	-.379	-.366	-.347	-.329	-.306	-.290	-.272	-.261	-.245
.925	-.465	-.462	-.440	-.417	-.414	-.411	-.398	-.382	-.371	-.353	-.336	-.313	-.296	-.279	-.269	-.253
.975	-.405	-.428	-.413	-.393	-.389	-.387	-.376	-.360	-.349	-.332	-.317	-.296	-.281	-.263	-.252	-.236
1.000	-.256	-.300	-.284	-.296	-.320	-.280	-.360	-.342	-.325	-.314	-.298	-.270	-.285	-.258	-.243	-.215

No orifice.

NACA

TABLE 7.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-(3)(07.00) PROPELLER BLADE SECTION ( $x = 0.90$ )

$$\left[ \beta_{0.75R} = 45^\circ; \beta_x = 39.63^\circ; B = 2 \right]$$

(a)  $N = 1140$  rpm.

$\frac{r}{R}$	2.552	2.485	2.406	2.332	2.248	2.179	2.072	2.000	1.926	1.848	1.774	1.685	1.616	1.543	1.461
$\frac{c}{b}$	2.552	2.485	2.406	2.332	2.248	2.179	2.072	2.000	1.926	1.848	1.774	1.685	1.616	1.543	1.461
$\frac{c}{b}$	.663	.648	.637	.630	.623	.614	.604	.594	.586	.583	.574	.565	.562	.553	.545
$\frac{c}{b}$	-.08	-.05	-.02	.02	.05	.08	.12	.16	.19	.22	.25	.28	.30	.32	.35
$\frac{c}{b}$	.09	.28	.55	.78	1.12	1.39	1.71	2.04	2.29	2.59	2.92	3.21	3.42	3.47	3.47
$\frac{c}{b}$	.0197	.0632	.1226	.1739	.2487	.3084	.3797	.4516	.5077	.5723	.6445	.7071	.7555	.7665	.7639
$\frac{c}{b}$	-.0623	-.0615	-.0580	-.0579	-.0510	-.0474	-.0415	-.0347	-.0328	-.0300	-.0270	-.0218	-.0141	-.0070	-.0149
$\frac{c}{b}$	Pressure coefficient, $P$														
Upper surface	.0000	1.115	1.109	1.105	1.102	1.100	1.097	1.094	1.091	1.088	1.087	1.085	1.082	1.081	1.078
	.025	.353	.437	.481	.516	.549	.581	.616	.651	.684	.716	.748	.782	.812	.848
	.050	.198	.104	-.017	-.125	-.226	-.319	-.408	-.491	-.568	-.640	-.706	-.766	-.821	-.871
	.100	.022	-.049	-.136	-.203	-.263	-.317	-.367	-.411	-.450	-.484	-.513	-.538	-.559	-.576
	.200	-.108	-.155	-.220	-.283	-.340	-.394	-.443	-.487	-.525	-.557	-.582	-.601	-.616	-.628
	.300	-.231	-.265	-.316	-.362	-.402	-.435	-.463	-.487	-.507	-.522	-.533	-.540	-.544	-.548
	.400	-.275	-.273	-.325	-.365	-.398	-.424	-.443	-.458	-.469	-.476	-.480	-.482	-.483	-.483
	.500	-.287	-.308	-.341	-.369	-.390	-.404	-.413	-.418	-.421	-.422	-.422	-.422	-.422	-.422
	.600	-.307	-.322	-.351	-.374	-.391	-.401	-.406	-.408	-.408	-.408	-.408	-.408	-.408	-.408
	.700	-.297	-.306	-.331	-.351	-.365	-.374	-.379	-.381	-.381	-.381	-.381	-.381	-.381	-.381
	.800	-.272	-.275	-.294	-.307	-.315	-.318	-.321	-.321	-.321	-.321	-.321	-.321	-.321	-.321
	.900	-.122	-.120	-.137	-.142	-.144	-.144	-.144	-.144	-.144	-.144	-.144	-.144	-.144	-.144
	.950	.022	.028	.038	.042	.043	.044	.044	.044	.044	.044	.044	.044	.044	.044
Lower surface	.0375	-.546	-.445	-.342	-.249	-.161	-.064	.039	.144	.248	.353	.458	.562	.664	.765
	.075	-.401	-.308	-.247	-.187	-.125	-.064	.034	.136	.237	.341	.444	.546	.646	.745
	.150	-.247	-.193	-.159	-.125	-.086	-.040	.002	.082	.177	.274	.371	.466	.559	.650
	.250	-.183	-.147	-.133	-.107	-.074	-.034	.000	.040	.078	.118	.156	.191	.222	.250
	.350	-.158	-.131	-.128	-.096	-.051	-.002	.008	.038	.069	.098	.124	.148	.168	.184
	.450	-.142	-.121	-.124	-.081	-.021	.001	.004	.030	.052	.071	.088	.103	.116	.126
	.550	-.130	-.115	-.121	-.066	-.003	.005	.009	.021	.039	.054	.068	.080	.090	.098
	.650	-.115	-.107	-.118	-.056	-.008	.006	.009	.014	.027	.042	.056	.068	.078	.086
	.750	-.084	-.078	-.095	-.049	.000	.006	.009	.015	.027	.042	.056	.068	.078	.086
	.850	0	.003	-.015	.006	.006	.008	.009	.015	.027	.042	.056	.068	.078	.086
	.925	.073	.074	.053	.070	.067	.064	.047	.045	.041	.042	.042	.042	.042	.042
	.975	.137	.139	.115	.131	.125	.121	.098	.087	.081	.073	.070	.070	.070	.070
	1.000	.179	.173	.152	.169	.161	.158	.125	.125	.138	.120	.110	.089	.060	.030

No orifice.

NACA



TABLE 7.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-(3)(07.00) PROPELLER BLADE SECTION ( $x = 0.90$ ) - Continued(b)  $N = 1350$  rpm.

	2.575	2.501	2.445	2.381	2.312	2.246	2.181	2.111	2.033	1.970	1.894	1.834	1.779	1.696	1.618	1.552	1.511
$M_x$	.781	.768	.760	.750	.743	.732	.725	.714	.706	.698	.688	.684	.678	.667	.660	.651	.653
$\alpha_x$	-2.69	-1.86	-1.22	-.47	.36	1.17	1.98	2.88	3.91	4.76	5.81	6.66	7.74	8.67	9.85	10.87	11.51
$\Delta\theta$	-.14	-.06	-.01	.04	.10	.17	.22	.28	.34	.39	.44	.48	.52	.55	.58	.59	.60
$c_d$	-.01	.29	.51	.74	.94	1.24	1.45	1.72	2.06	2.24	2.52	2.91	3.29	3.41	3.70	3.66	3.58
$c_n$	-.0026	.0632	.1148	.1661	.2094	.2765	.3242	.3829	.4581	.4974	.5600	.6452	.7277	.7548	.8174	.8090	.7916
$c_m$	-.0850	-.0765	-.0710	-.0668	-.0605	-.0511	-.0465	-.0433	-.0395	-.0339	-.0295	-.0272	-.0193	-.0146	-.0098	-.0025	-.0043
$c_c$																	
$c/b$	Pressure coefficient, P																
Upper surface	$\theta_0$ .000	1.162	1.157	1.153	1.149	1.147	1.142	1.139	1.135	1.131	1.129	1.125	1.123	1.121	1.115	1.113	1.111
	.005	.611	.580	.423	.288	.132	-.048	-.265	-.535	-.876	-1.100	-1.308	-1.451	-1.765	-2.029	-2.263	-2.398
	.050	.246	.162	.080	-.025	-.138	-.267	-.414	-.589	-.798	-1.021	-1.443	-1.646	-1.825	-2.004	-2.202	-2.229
	.100	.053	-.016	-.077	-.152	-.233	-.317	-.410	-.512	-.619	-.662	-.686	-1.214	-1.668	-1.834	-2.027	-1.834
	.200	-.109	-.156	-.197	-.246	-.296	-.346	-.396	-.450	-.501	-.549	-.594	-.602	-.576	-.567	-.690	-.829
	.300	-.220	-.297	-.283	-.315	-.346	-.379	-.410	-.441	-.480	-.510	-.544	-.559	-.568	-.563	-.547	-.598
	.400	-.296	-.316	-.335	-.355	-.378	-.397	-.416	-.442	-.505	-.488	-.516	-.522	-.534	-.527	-.580	-.542
	.500	-.349	-.361	-.372	-.384	-.396	-.409	-.418	-.433	-.449	-.462	-.479	-.485	-.493	-.493	-.481	-.447
	.600	-.385	-.387	-.390	-.394	-.397	-.404	-.404	-.413	-.420	-.427	-.436	-.440	-.439	-.438	-.423	-.375
	.700	-.382	-.374	-.372	-.370	-.367	-.365	-.360	-.360	-.359	-.364	-.367	-.367	-.363	-.360	-.341	-.285
	.800	-.329	-.321	-.314	-.308	-.297	-.289	-.272	-.272	-.265	-.261	-.261	-.260	-.254	-.251	-.238	-.201
	.900	-.119	-.115	-.108	-.101	-.090	-.083	-.073	-.067	-.061	-.055	-.058	-.062	-.064	-.071	-.070	-.082
	.950	.054	.054	.058	.061	.066	.070	.073	.072	.072	.068	.058	.053	.044	.033	.022	-.015
Lower surface	.0375	-1.089	-.846	-.516	-.302	-.172	-.053	.066	.174	.281	.357	.440	.511	.587	.633	.685	.713
.075	-.911	-.312	-.268	-.217	-.133	-.050	.034	.115	.199	.256	.324	.384	.451	.491	.540	.566	.587
.150	-.215	-.226	-.182	-.127	-.083	-.034	.019	.072	.127	.168	.215	.260	.312	.344	.385	.404	.422
.250	-.191	-.172	-.142	-.105	-.075	-.044	-.006	.031	.070	.100	.136	.172	.213	.240	.271	.285	.298
.350	-.170	-.151	-.129	-.105	-.079	-.055	-.028	.001	.031	.053	.079	.110	.144	.165	.192	.202	.213
.450	-.152	-.140	-.124	-.105	-.087	-.070	-.049	-.030	-.005	.012	.034	.059	.090	.107	.129	.133	.138
.550	-.140	-.129	-.116	-.105	-.093	-.081	-.065	-.050	-.031	-.017	.001	.023	.047	.062	.079	.078	.079
.650	-.122	-.116	-.109	-.102	-.097	-.089	-.079	-.067	-.053	-.044	-.028	-.011	.010	.021	.035	.028	.022
.750	-.081	-.080	-.078	-.075	-.077	-.075	-.070	-.065	-.057	-.053	-.040	-.026	-.009	-.001	.008	-.007	-.024
.850	.018	.016	.015	.014	.007	.003	.002	.002	.002	.002	.004	.008	.019	.024	.028	.002	-.028
.925	.098	.095	.093	.086	.074	.067	.062	.055	.049	.044	.028	.038	.050	.054	.057	.022	-.032
.975	.161	.158	.153	.148	.134	.125	.119	.111	.098	.090	.078	.080	.078	.079	.081	.046	-.028
1.000	.192	.188	.183	.182	.160	.155	.150	.147	.135	.171	.119	.153	.144	.137	.095	.052	-.003

No orifice.

NACA

TABLE 7.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(07.00) PROPELLER BLADE SECTION ( $x = 0.90$ ) - Continued

(a)  $N = 1500$  rpm.

$\frac{J}{M_\infty}$ $\Delta \theta$ $\frac{C_p}{C_{p0}}$ $\frac{C_{p0}}{C_{p00}}$	2.553 .876 -2.47 -.22 -.08 -.0168 -.1036 .0217	2.510 .853 -1.97 -.16 .14 .0316 -.1018	2.449 .822 -1.27 -.09 .37 .0819 -.0819	2.410 .846 -.81 -.04 .53 .1197 -.0784	2.364 .837 -.27 .01 .76 .1713 -.0744	2.318 .830 .28 .06 .95 .2132 -.0683	2.256 .821 1.04 .14 .14 .2539 -.0635	2.210 .810 1.62 .19 .134 .2981 -.0570	2.153 .802 2.34 .25 1.62 .3610 -.0477	2.112 .797 2.87 .30 1.73 .3855 -.0453	2.041 .784 3.51 .37 2.03 .4503 -.0379	1.988 .779 4.22 .42 2.31 .5142 -.0352	1.930 .770 5.31 .48 2.54 .5665 -.0310	1.883 .765 5.97 .52 2.82 .6271 -.0280	1.822 .757 6.83 .57 3.10 .6871 -.0262	1.760 .751 7.73 .61 3.37 .7432 -.0234	1.715 .746 8.39 .63 3.69 .8168 -.0218	
$\frac{o}{b}$	Pressure coefficient, P																	
Upper surface	.000 .025 .050 .100 .200 .300 .400 .500 .600 .700 .800 .900 .950	1.207 .638 .281 .085 -.098 -.232 -.336 -.409 -.457 -.535 -.622 -.005 .107	1.200 .585 .230 .040 -.132 -.256 -.345 -.410 -.471 -.551 -.623 -.007 .117	1.195 .505 .156 -.022 -.183 -.293 -.370 -.435 -.485 -.563 -.631 -.027 .111	1.192 .443 .098 -.071 -.220 -.321 -.400 -.451 -.490 -.564 -.629 -.036 .107	1.187 .375 .028 -.126 -.261 -.348 -.430 -.465 -.489 -.550 -.629 -.040 .106	1.184 .256 -.053 -.190 -.307 -.379 -.457 -.489 -.498 -.550 -.629 -.045 .101	1.180 .104 -.175 -.283 -.370 -.418 -.457 -.489 -.498 -.550 -.629 -.045 .101	1.175 -.033 -.290 -.367 -.424 -.446 -.476 -.492 -.498 -.550 -.629 -.045 .102	1.171 -.222 -.440 -.535 -.553 -.606 -.647 -.691 -.700 -.702 -.727 -.035 .102	1.169 -.356 -.571 -.704 -.759 -.806 -.847 -.891 -.900 -.902 -.927 -.035 .095	1.163 -.571 -.732 -.852 -.884 -.926 -.947 -.982 -.993 -.994 -1.001 -.035 .094	1.161 -.732 -.859 -1.016 -1.039 -1.018 -.983 -.960 -.999 -1.004 -1.007 -1.031 -.035 .088	1.158 -.859 -.968 -1.160 -1.039 -1.141 -.983 -.960 -.999 -1.004 -1.007 -1.031 -.035 .083	1.155 -.968 -1.160 -1.291 -1.243 -1.141 -.983 -.960 -.999 -1.004 -1.007 -1.031 -.035 .080	1.152 -1.088 -1.281 -1.291 -1.243 -1.141 -.983 -.960 -.999 -1.004 -1.007 -1.031 -.035 .078	1.150 -1.217 -1.411 -1.392 -1.356 -1.286 -1.428 -1.416 -1.421 -1.361 -1.251 -1.049 -.067	1.148 -1.389 -1.515 -1.494 -1.459 -1.390 -1.407 -1.353 -1.254 -1.063 -.056
Lower surface	.0375 .075 .150 .250 .350 .450 .550 .650 .750 .850 .925 .975 1.000	-.815 -.780 -.723 -.542 -.079 -.094 -.124 -.135 -.099 -.012 .089 .141 .163	-.813 -.777 -.680 -.105 -.118 -.140 -.144 -.141 -.097 .016 .101 .155 .200	-.760 -.675 -.149 -.150 -.149 -.149 -.146 -.138 -.097 .012 .096 .132 .197	-.638 -.461 -.175 -.150 -.142 -.126 -.126 -.126 -.094 .011 .089 .147 .170	-.395 -.250 -.145 -.124 -.123 -.126 -.126 -.120 -.094 .006 .088 .147 .180	-.251 -.190 -.112 -.098 -.076 -.093 -.103 -.112 -.093 .003 .076 .132 .171	-.115 -.097 -.062 -.034 -.054 -.075 -.090 -.103 -.090 -.005 .054 .122 .159	-.013 -.022 -.016 .001 -.024 -.054 -.075 -.092 -.084 -.005 .054 .122 .164	.098 .059 .036 .022 -.012 -.045 -.067 -.089 -.084 -.010 .054 .122 .160	.293 .177 .114 .060 .018 -.020 -.047 -.074 -.076 -.006 .052 .102 .146	.326 .236 .156 .092 .042 -.020 -.030 -.059 -.066 -.001 .052 .102 .175	.392 .289 .196 .120 .068 .021 -.013 -.044 -.059 -.066 -.008 .057 .109 .158	.456 .343 .235 .153 .095 .045 -.007 -.028 -.053 -.018 .063 .111 .150	.513 .392 .273 .183 .119 .065 .025 -.012 -.040 .022 .065 .105 .140	.575 .444 .313 .215 .144 .088 .045 -.007 -.013 .028 .063 .103 .125	.616 .482 .341 .237 .164 .103 .057 .015 -.006 .026 .059 .102 .141	

No orifice.

NACA

TABLE 7.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(07.00) PROPELLER BLADE SECTION ( $\alpha = 0.90$ ) - Continued

(d)  $N = 1600$  rpm.

$J$ $M_x$ $\Delta h$ $c_{f, \Delta}$ $c_{p, \Delta}$ $c_c$	1.842 .804 6.54 .69 3.06 .6800 -.0300	1.913 .815 5.54 .64 2.73 .6071 -.0311	1.990 .830 4.49 .56 2.36 .5226 -.0331	2.075 .840 3.35 .46 1.97 .4387 -.0452	2.157 .856 2.29 .34 1.64 .3645 -.0524	2.244 .870 1.19 .20 1.20 .2671 -.0618	2.310 .877 .38 .08 .81 .1813 -.0642 .0170	2.396 .895 -.65 -.07 .37 .0832 -.0726 .0208	2.277 .871 .78 .14 .99 .2226 -.0647	2.207 .860 1.65 .26 1.35 .2997 -.0604	2.117 .846 2.81 .40 1.80 .4006 -.0494	2.039 .834 3.83 .50 2.06 .4574 -.0393	1.941 .816 5.16 .62 2.51 .5587 -.0328	1.890 .810 5.86 .66 2.78 .6168 -.0302	
$c/b$	Pressure coefficient, $P$														
Upper surface	.00.000	1.172	1.177	1.184	1.188	1.197	1.204	1.207	1.217	1.204	1.198	1.192	1.186	1.178	1.175
	.025	-.822	-.707	-.542	-.302	-.065	.160	.316	.515	.257	.093	-.178	-.405	-.643	-.749
	.050	-1.014	-.866	-.681	-.474	-.316	-.131	.001	.183	-.048	-.188	-.367	-.563	-.784	-.922
	.100	-1.052	-.923	-.751	-.580	-.403	-.252	-.149	.009	-.188	-.295	-.479	-.693	-.851	-.967
	.200	-1.084	-.954	-.820	-.641	-.525	-.412	-.311	-.157	-.344	-.446	-.558	-.720	-.896	-.988
	.300	-1.034	-.966	-.832	-.676	-.569	-.445	-.359	-.238	-.371	-.454	-.592	-.714	-.890	-.985
	.400	-.828	-.748	-.626	-.579	-.561	-.495	-.440	-.368	-.451	-.484	-.572	-.487	-.605	-.624
	.500	-.435	-.407	-.373	-.499	-.530	-.527	-.517	-.451	-.527	-.533	-.536	-.393	-.351	-.369
	.600	-.323	-.350	-.418	-.468	-.547	-.569	-.569	-.491	-.573	-.559	-.520	-.465	-.350	-.355
	.700	-.317	-.354	-.400	-.487	-.602	-.628	-.616	-.542	-.622	-.632	-.513	-.471	-.376	-.350
	.800	-.229	-.248	-.245	-.230	-.200	-.224	-.235	-.268	-.244	-.207	-.224	-.244	-.251	-.246
	.900	-.028	-.030	-.019	-.002	.011	.013	-.018	-.005	.009	.002	.004	-.011	-.026	-.032
	.950	.096	.096	.103	.110	.110	.075	.029	.032	.066	.104	.113	.106	.102	.097
Lower surface	.0375	.486	.402	.314	.201	.068	-.100	-.304	-.520	-.208	-.046	.135	.247	.372	.433
	.075	.372	.302	.226	.137	.032	-.091	-.224	-.475	-.166	-.050	.089	.175	.277	.327
	.150	.262	.209	.153	.090	.018	-.057	-.125	-.289	-.094	-.030	.058	.116	.191	.228
	.250	.178	.131	.088	.041	-.013	-.068	-.120	-.097	-.094	-.045	.019	.062	.121	.150
	.350	.110	.071	.034	-.004	-.048	-.091	-.133	-.106	-.111	-.075	-.024	.010	.060	.085
	.450	.058	.024	-.008	-.041	-.076	-.111	-.147	-.127	-.126	-.096	-.056	-.028	.015	.038
	.550	.015	-.015	-.042	-.069	-.100	-.127	-.159	-.142	-.139	-.114	-.081	-.060	-.021	-.002
	.650	-.020	-.047	-.072	-.092	-.120	-.143	-.174	-.163	-.152	-.127	-.102	-.086	-.052	-.034
	.750	-.034	-.055	-.073	-.087	-.106	-.120	-.148	-.131	-.128	-.108	-.095	-.086	-.059	-.045
	.850	.026	.012	0	-.006	-.013	-.021	-.045	-.015	-.022	-.009	-.007	-.005	.012	.019
	.925	.080	.071	.064	.062	.059	.049	.021	.054	.046	.063	.063	.060	.071	.075
	.975	.134	.131	.125	.124	.121	.099	.061	.086	.085	.111	.119	.116	.125	.129
	1.000	.230	.185	.155	.199	.183	.135	.078	.095	.103	.168	.167	.184	.178	.168

\*No orifice.

NACA

(e)  $M = 0.56$ .

<sup>a</sup>No orifice.

TABLE 7.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(07.00) PROPELLER BLADE SECTION ( $x = 0.90$ ) - Continued

( $t$ )  $M = 0.62$

$\gamma$	1.998	2.023	2.054	2.080	2.111	2.131	2.165	2.208	2.229	2.267	2.293	2.325	2.369	2.403	2.440	
$M_x$	1.068	1.099	1.048	1.041	1.031	1.020	1.010	1.003	.992	.988	.976	.968	.963	.954	.946	
$\alpha\delta'$	4.38	4.05	3.63	3.29	2.88	2.63	2.19	1.64	1.38	.91	.59	.20	-.33	-.73	-1.21	
$\alpha_1$	.30	.27	.23	.20	.17	.15	.12	.08	.06	.02	0	-.04	-.08	-.12	-.16	
$\alpha_2$	1.82	1.79	1.64	1.57	1.44	1.30	1.13	.96	.74	.49	.29	.15	-.04	-.20	-.30	
$c_m$	.4039	.3974	.3642	.3484	.3210	.2897	.2513	.2135	.1648	.1084	.0645	.0335	-.0081	-.0448	-.0665	
$c_m$	-.1047	-.1051	-.1068	-.1053	-.0986	-.0965	-.0892	-.0804	-.0667	-.0564	-.0468	-.0376	-.0507	-.0574	-.0664	
$c_c$	.0480	.0493	.0501	.0501	.0499	.0498	.0494	.0486	.0432	.0403	.0389	.0376	.0369	.0347	.0331	
c/b	Pressure coefficient, P															
Upper surface	a0.000	1.318	1.312	1.305	1.301	1.294	1.287	1.281	1.277	1.270	1.268	1.261	1.256	1.253	1.248	1.244
	.025	.202	.222	.254	.272	.291	.326	.355	.383	.399	.440	.468	.490	.508	.557	.587
	.050	-.001	.004	.016	.019	.025	.049	.069	.090	.101	.136	.158	.176	.209	.234	.255
	.100	-.138	-.136	-.116	-.104	-.093	-.072	-.056	-.042	-.035	-.009	.006	.018	.041	.060	.076
	.200	-.253	-.255	-.238	-.232	-.225	-.206	-.199	-.199	-.201	-.185	-.174	-.160	-.137	-.115	-.097
	.300	-.288	-.305	-.302	-.304	-.305	-.290	-.283	-.278	-.276	-.255	-.237	-.222	-.209	-.195	-.184
	.400	-.374	-.367	-.374	-.395	-.381	-.366	-.363	-.362	-.357	-.343	-.333	-.313	-.306	-.296	-.298
	.500	-.449	-.462	-.458	-.459	-.455	-.440	-.437	-.437	-.437	-.427	-.425	-.419	-.413	-.408	-.410
	.600	-.508	-.521	-.514	-.516	-.519	-.508	-.507	-.508	-.513	-.505	-.505	-.502	-.500	-.496	-.497
	.700	-.564	-.580	-.576	-.581	-.584	-.572	-.572	-.576	-.582	-.575	-.572	-.565	-.557	-.551	-.550
	.800	-.617	-.641	-.642	-.645	-.644	-.632	-.635	-.646	-.654	-.654	-.659	-.661	-.658	-.638	-.616
	.900	-.663	-.697	-.706	-.722	-.734	-.738	-.746	-.702	-.458	-.313	-.233	-.195	-.179	-.155	-.143
	.950	-.685	-.717	-.725	-.734	-.694	-.627	-.509	-.358	-.294	-.248	-.201	-.171	-.160	-.138	-.123
Lower surface	.0375	.307	.263	.218	.179	.135	.081	.023	-.051	-.110	-.208	-.288	-.350	-.411	-.472	-.532
	.075	.252	.213	.174	.140	.099	.054	.003	-.053	-.099	-.171	-.246	-.315	-.386	-.451	-.514
	.150	.212	.181	.154	.128	.098	.069	.035	-.010	-.048	-.125	-.189	-.250	-.322	-.404	-.469
	.250	.149	.121	.097	.076	.051	.032	.006	-.035	-.068	-.103	-.149	-.212	-.290	-.351	-.415
	.350	.099	.076	.057	.038	.017	.001	-.022	-.054	-.078	-.115	-.138	-.159	-.244	-.332	-.395
	.450	.023	-.002	-.020	-.038	-.057	-.069	-.091	-.120	-.138	-.161	-.176	-.187	-.214	-.273	-.350
	.550	-.028	-.051	-.067	-.083	-.099	-.108	-.127	-.150	-.164	-.182	-.191	-.195	-.206	-.204	-.208
	.650	-.098	-.109	-.133	-.147	-.161	-.166	-.184	-.204	-.215	-.224	-.227	-.225	-.231	-.218	-.192
	.750	-.172	-.191	-.204	-.217	-.228	-.233	-.250	-.268	-.282	-.289	-.296	-.299	-.300	-.290	-.255
	.850	-.215	-.237	-.249	-.262	-.272	-.281	-.297	-.316	-.329	-.336	-.344	-.347	-.346	-.327	-.282
	.925	-.260	-.283	-.294	-.307	-.318	-.326	-.342	-.360	-.373	-.379	-.388	-.389	-.375	-.309	-.281
	.975	-.207	-.229	-.240	-.254	-.266	-.273	-.288	-.305	-.315	-.315	-.310	-.293	-.220	-.098	-.052
	a1.000	-.183	-.176	-.190	-.212	-.230	-.230	-.194	-.224	-.253	-.209	-.163	-.200	-.163	-.150	-.089

\*No orifice.

NACA

TABLE 7.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(07.00) PROPELLER BLADE SECTION ( $x = 0.90$ ) - Continued

(g)  $M = 0.65$ .

J	2.002	2.035	2.066	2.092	2.118	2.129	2.161	2.195	2.223	2.244	2.274	2.309	2.341	2.363	2.392
$M_{x_1}$	1.133	1.119	1.112	1.105	1.092	1.081	1.070	1.063	1.053	1.042	1.034	1.025	1.016	1.011	1.000
$c_{x_1}$	4.33	3.89	3.47	3.13	2.79	2.65	2.24	1.81	1.45	1.19	.82	.39	.01	-.26	-.60
$c_{y_1}$	.25	.21	.17	.14	.11	.09	.06	.02	0	-.02	-.05	-.08	-.10	-.12	-.15
$c_{y_2}$	1.69	1.61	1.50	1.35	1.26	1.12	1.02	.90	.78	.62	.52	.32	.14	.01	-.23
$c_{y_3}$	.3768	.3561	.3329	.2994	.2794	.2487	.2274	.2010	.1729	.1381	.1148	.0706	.0303	.0029	-.0516
$c_{y_4}$	-.1059	-.1034	-.0981	-.0987	-.0971	-.0964	-.0942	-.0923	-.0895	-.0898	-.0864	-.0844	-.0809	-.0733	-.0566
$c_{y_5}$	.0498	.0501	.0508	.0508	.0509	.0525	.0526	.0534	.0536	.0537	.0543	.0537	.0536	.0529	.0507
c/b	Pressure coefficient, P														
Upper surface	0.000	1.362	1.352	1.346	1.342	1.334	1.327	1.324	1.315	1.309	1.301	1.296	1.290	1.282	1.274
	.025	.308	.326	.348	.371	.387	.408	.423	.451	.471	.492	.511	.543	.566	.596
	.050	.102	.106	.116	.127	.133	.141	.149	.173	.188	.205	.220	.248	.262	.286
	.100	-.042	-.039	-.021	.003	.013	.018	.020	.037	.047	.060	.070	.090	.100	.110
	.200	-.159	-.158	-.140	-.124	-.120	-.118	-.118	-.109	-.108	-.106	-.101	-.084	-.073	-.060
	.300	-.211	-.195	-.177	-.165	-.165	-.165	-.156	-.156	-.150	-.144	-.133	-.111	-.094	-.092
	.400	-.225	-.228	-.235	-.239	-.250	-.278	-.256	-.259	-.243	-.254	-.250	-.224	-.197	-.233
	.500	-.358	-.369	-.359	-.354	-.355	-.358	-.360	-.355	-.354	-.353	-.350	-.341	-.337	-.343
	.600	-.415	-.430	-.418	-.410	-.413	-.423	-.429	-.424	-.425	-.428	-.426	-.419	-.417	-.426
	.700	-.471	-.486	-.477	-.475	-.481	-.492	-.500	-.498	-.500	-.503	-.502	-.495	-.494	-.503
	.800	-.548	-.567	-.562	-.561	-.565	-.580	-.590	-.589	-.593	-.595	-.593	-.584	-.584	-.598
Lower surface	.900	-.592	-.618	-.622	-.629	-.641	-.661	-.673	-.678	-.687	-.696	-.697	-.695	-.697	-.702
	.950	-.608	-.633	-.635	-.640	-.653	-.672	-.685	-.690	-.700	-.711	-.719	-.717	-.664	-.335
	.0375	.341	.300	.275	.227	.178	.116	.074	.020	-.043	-.109	-.174	-.232	-.283	-.372
	.075	.286	.251	.232	.191	.144	.093	.057	.014	-.033	-.079	-.137	-.203	-.257	-.353
	.150	.252	.227	.215	.184	.132	.109	.072	.020	-.032	-.075	-.118	-.171	-.226	-.328
	.250	.196	.173	.164	.137	.111	.069	.036	.009	-.031	-.085	-.141	-.179	-.210	-.293
	.350	.149	.127	.118	.093	.069	.031	.002	-.024	-.053	-.080	-.126	-.179	-.220	-.298
	.450	.071	.050	.042	.019	-.002	-.036	-.059	-.080	-.106	-.125	-.145	-.187	-.232	-.325
	.550	.023	.004	-.004	-.025	-.045	-.078	-.101	-.118	-.142	-.160	-.174	-.185	-.213	-.313
	.650	-.044	-.061	-.070	-.089	-.107	-.139	-.160	-.175	-.193	-.209	-.222	-.223	-.233	-.312
	.750	-.117	-.135	-.144	-.160	-.175	-.204	-.223	-.237	-.254	-.266	-.277	-.278	-.283	-.337
	.850	-.158	-.176	-.185	-.199	-.213	-.242	-.259	-.269	-.284	-.297	-.306	-.307	-.314	-.341
	.925	-.198	-.219	-.228	-.240	-.256	-.285	-.300	-.312	-.327	-.339	-.348	-.355	-.369	-.373
	.975	-.149	-.171	-.179	-.191	-.207	-.233	-.249	-.260	-.275	-.289	-.298	-.298	-.304	-.321
	1.000	-.088	-.116	-.113	-.143	-.155	-.205	-.175	-.208	-.220	-.241	-.256	-.255	-.280	-.225

\*No orifice.

NACA

TABLE 8.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-(3)(06.50) PROPELLER BLADE SECTION ( $\tau = 0.95$ )

$$[\beta_{0.75R} = 45^\circ; \beta_x = 38.33^\circ; B = 2]$$

(a)  $N = 1140$  rpm.

J	2.578	2.500	2.422	2.346	2.257	2.184	2.107	2.019	1.950	1.868	1.776	1.709	1.639	1.570	1.488	1.396	1.338
$M_x$	.678	.673	.663	.659	.647	.637	.628	.623	.614	.605	.598	.596	.588	.578	.578	.564	.565
$C_{p,x}$	-2.49	-1.62	-.73	.16	1.23	2.13	3.11	4.25	5.17	6.29	7.57	8.53	9.56	10.58	11.83	13.26	14.18
$\Delta B$	-.12	-.08	-.05	-.02	.03	.06	.10	.14	.18	.21	.25	.27	.29	.32	.34	.35	.38
$\alpha_1$	.03	.26	.52	.78	1.07	1.35	1.68	2.05	2.34	2.76	3.17	3.48	3.82	3.93	4.02	4.08	4.30
$\alpha_n$	.0045	.0416	.0845	.1255	.1723	.2171	.2690	.3297	.3774	.4413	.5077	.5581	.6084	.6400	.6884	.6990	.6858
$\alpha_m$	-.0472	-.0475	-.0433	-.0410	-.0388	-.0350	-.0329	-.0280	-.0249	-.0232	-.0244	-.0226	-.0179	-.0136	-.0046	-.0128	-.0129
$\alpha_c$																	
Pressure coefficient, P																	
$r/b$	0.000	1.120	1.119	1.115	1.113	1.109	1.105	1.102	1.100	1.097	1.094	1.092	1.091	1.089	1.086	1.086	1.082
Upper surface	.025	.519	.405	.276	.128	-.047	-.234	-.469	-.734	-.1030	-.1386	-.1874	-.2301	-.2632	-.2661	-.1.802	-.1.821
	.050	.188	.098	.009	-.090	-.197	-.305	-.436	-.581	-.715	-.856	-.1.009	-.1.087	-.1.343	-.1.737	-.1.765	-.1.634
	.100	-.003	-.067	-.129	-.193	-.261	-.325	-.399	-.480	-.553	-.639	-.726	-.779	-.836	-.1.297	-.1.245	-.1.060
	.200	-.112	-.151	-.189	-.225	-.263	-.298	-.336	-.376	-.423	-.469	-.521	-.591	-.578	-.678	-.677	-.692
	.300	-.170	-.198	-.221	-.244	-.268	-.292	-.316	-.345	-.377	-.411	-.449	-.466	-.498	-.493	-.541	-.599
	.400	-.203	-.217	-.237	-.250	-.267	-.285	-.301	-.327	-.351	-.376	-.411	-.414	-.441	-.437	-.454	-.505
	.500	-.227	-.241	-.252	-.269	-.276	-.287	-.299	-.317	-.338	-.359	-.385	-.390	-.411	-.399	-.390	-.438
	.600	-.266	-.273	-.280	-.289	-.296	-.303	-.314	-.324	-.342	-.359	-.381	-.383	-.398	-.379	-.351	-.370
	.700	-.266	-.272	-.274	-.280	-.284	-.288	-.294	-.301	-.315	-.329	-.347	-.344	-.356	-.335	-.298	-.310
	.800	-.232	-.235	-.233	-.235	-.237	-.239	-.239	-.244	-.254	-.262	-.275	-.267	-.279	-.260	-.224	-.250
Lower surface	.900	-.111	-.108	-.106	-.105	-.104	-.105	-.104	-.100	-.106	-.110	-.117	-.109	-.128	-.125	-.120	-.135
	.950	.027	.027	.028	.027	.027	.026	.025	.030	.023	.017	.009	.010	-.012	-.022	-.056	-.1.163
	.0375	-.574	-.451	-.359	-.248	-.132	-.027	.083	.193	.273	.367	.446	.526	.564	.606	.631	.651
	.075	-.365	-.286	-.209	-.142	-.070	0	.076	.152	.208	.277	.337	.405	.432	.471	.490	.509
	.150	-.210	-.167	-.126	-.086	-.042	-.002	.046	.098	.134	.182	.224	.275	.294	.325	.340	.356
	.250	-.161	-.133	-.109	-.084	-.053	-.027	.007	.044	.067	.100	.132	.172	.184	.205	.218	.230
	.350	-.144	-.125	-.107	-.090	-.071	-.052	.025	.001	.018	.046	.066	.102	.108	.127	.132	.140
	.450	-.127	-.113	-.099	-.087	-.073	-.059	-.037	-.017	-.023	.017	.033	.063	.067	.082	.085	.089
	.550	-.124	-.114	-.106	-.097	-.086	-.075	-.059	-.043	-.035	-.019	-.007	.020	.020	.030	.031	.029
	.650	-.124	-.119	-.114	-.107	-.099	-.094	-.080	-.069	-.065	-.053	-.042	-.019	-.024	-.016	-.020	-.029
	.750	-.086	-.082	-.081	-.078	-.073	-.070	-.061	-.051	-.051	-.040	-.035	-.018	-.024	-.020	-.032	-.047
	.850	-.021	-.026	-.022	-.023	-.022	-.022	-.017	-.015	-.018	-.013	-.015	-.001	-.011	-.012	-.032	-.067
	.925	.036	.034	.028	.025	.024	.020	.019	.016	.007	.005	-.002	.007	-.005	-.010	-.046	-.1.107
	.975	.068	.092	.089	.083	.080	.075	.071	.061	.046	.039	.024	.025	.018	.007	-.050	-.1.147
	1.000	.077	.131	.122	.125	.121	.118	.115	.196	.168	.157	.160	.145	.120	.095	.005	-.1.144

No orifice.

NACA

TABLE 8.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(06.50) PROPELLER BLADE SECTION ( $x = 0.95$ ) - Continued

(b)  $N = 1350$  rpm.

$J$	2.254	2.503	2.440	2.376	2.322	2.253	2.205	2.126	2.052	1.988	1.930	1.858	1.804	1.733	1.657	1.604	1.541	1.475
$M_x$	.812	.804	.793	.782	.773	.764	.757	.750	.743	.732	.725	.717	.713	.705	.694	.693	.691	.682
$\alpha_x^b$	-2.23	-1.66	-.94	-.19	.45	1.28	1.87	2.87	3.82	4.66	5.44	6.43	7.18	8.19	9.29	10.07	11.02	12.03
$\Delta\delta$	-.14	-.09	-.02	.04	.10	.16	.21	.28	.34	.39	.44	.49	.52	.56	.58	.60	.62	.62
$\alpha_1$	-.15	.10	.38	.60	.78	1.05	1.32	1.61	1.99	2.30	2.60	2.91	3.29	3.86	4.11	4.45	4.28	4.23
$c_n$	-.0243	.0168	.0610	.0974	.1258	.1684	.2123	.2584	.3200	.3684	.4181	.4658	.5271	.6168	.6606	.7123	.6839	.6735
$c_m$	-.0569	-.0521	-.0479	-.0442	-.0430	-.0403	-.0362	-.0348	-.0293	-.0259	-.0249	-.0226	-.0215	-.0147	-.0161	-.0102	-.0079	.0005
$c_d$																		
$o/b$	Pressure coefficient, P																	
Upper surface	$\theta$	1.176	1.172	1.167	1.162	1.159	1.155	1.152	1.149	1.146	1.142	1.139	1.136	1.134	1.131	1.127	1.127	1.126
	.025	.532	.470	.379	.273	.144	.003	-.151	-.343	-.603	-.814	-1.029	-1.220	-1.410	-1.637	-1.853	-2.003	-2.132
	.050	.201	.146	.072	-.009	-.101	-.203	-.305	-.431	-.594	-.759	-1.021	-1.244	-1.419	-1.631	-1.788	-1.909	-2.002
	.100	-.006	-.047	-.105	-.162	-.224	-.291	-.351	-.424	-.508	-.564	-.570	-.650	-.703	-.763	-.823	-.888	-1.335
	.200	-.136	-.163	-.193	-.226	-.261	-.297	-.325	-.364	-.403	-.432	-.464	-.486	-.493	-.501	-.530	-.581	-.620
	.300	-.202	-.219	-.238	-.257	-.279	-.302	-.319	-.343	-.369	-.393	-.415	-.437	-.447	-.461	-.472	-.476	-.477
	.400	-.231	-.242	-.253	-.267	-.280	-.297	-.307	-.324	-.343	-.361	-.376	-.394	-.407	-.422	-.433	-.428	-.422
	.500	-.271	-.278	-.282	-.292	-.301	-.312	-.319	-.332	-.347	-.361	-.375	-.392	-.401	-.418	-.428	-.424	-.413
	.600	-.323	-.325	-.324	-.327	-.333	-.341	-.343	-.355	-.364	-.372	-.382	-.396	-.404	-.419	-.425	-.418	-.400
	.700	-.319	-.316	-.312	-.315	-.317	-.322	-.326	-.332	-.338	-.342	-.349	-.361	-.368	-.380	-.387	-.379	-.354
	.800	-.270	-.266	-.260	-.259	-.261	-.263	-.261	-.268	-.271	-.273	-.275	-.281	-.287	-.300	-.306	-.297	-.276
	.900	-.092	-.092	-.088	-.089	-.091	-.095	-.093	-.099	-.099	-.097	-.097	-.100	-.110	-.125	-.136	-.131	-.130
	.950	.062	.058	.059	.056	.052	.048	.048	.044	.041	.037	.034	.027	.019	.007	-.007	-.011	-.040
Lower surface	$\theta$	-.863	-.749	-.519	-.383	-.260	-.154	-.055	.038	.143	.216	.296	.363	.422	.479	.544	.583	.614
	.025	-.901	-.326	-.269	-.210	-.145	-.082	-.019	.041	.113	.165	.225	.276	.319	.367	.420	.453	.479
	.050	-.171	-.187	-.158	-.125	-.088	-.053	-.013	.022	.068	.103	.145	.181	.213	.247	.288	.315	.333
	.100	-.163	-.158	-.133	-.114	-.090	-.069	-.041	-.018	.015	.038	.070	.095	.120	.148	.179	.200	.214
	.200	-.156	-.148	-.130	-.118	-.103	-.087	-.067	-.051	-.029	-.011	.014	.034	.053	.075	.099	.118	.127
	.300	-.140	-.132	-.118	-.109	-.100	-.087	-.072	-.060	-.043	-.029	-.009	.007	.023	.041	.060	.074	.079
	.400	-.139	-.133	-.123	-.118	-.109	-.102	-.089	-.082	-.068	-.059	-.044	-.033	-.018	-.006	.012	.023	.025
	.500	-.144	-.141	-.133	-.131	-.124	-.120	-.112	-.104	-.098	-.092	-.080	-.069	-.057	-.046	-.032	-.022	-.024
	.600	-.098	-.099	-.094	-.095	-.092	-.091	-.084	-.082	-.076	-.071	-.064	-.057	-.048	-.039	-.030	-.023	-.030
	.700	-.023	-.025	-.024	-.028	-.031	-.032	-.030	-.031	-.033	-.032	-.028	-.027	-.023	-.017	-.013	-.008	-.019
	.800	.045	.041	.037	.031	.027	.022	.019	.013	.008	.001	-.003	-.004	-.004	-.003	-.002	-.001	-.014
	.900	.112	.106	.103	.097	.089	.082	.078	.070	.058	.045	.036	.028	.027	.028	.021	.023	.008
	1.000	.373	.388	.300	.271	.267	.224	.214	.190	.155	.109	.074	.057	.059	.060	.056	.061	.032

<sup>a</sup>No orifices.<sup>b</sup>Lower surface only.

NACA



TABLE 8.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(06.50) PROPELLER BLADE SECTION ( $x = 0.95$ ) - Continued

(c)  $N = 1500$  rpm.

	$J$	$M_x$	$\alpha_x$	$\Delta\delta$	$\alpha_1$	$c_n$	$c_m$	$c_c$							
	2.529	2.485	2.437	2.375	2.316	2.252	2.180	2.134	2.072	2.022	1.960	1.896	1.840	1.762	
	.895	.888	.879	.871	.861	.850	.839	.832	.822	.815	.804	.792	.789	.775	
	-1.95	-1.45	-.90	-.18	.52	1.29	2.18	2.76	3.56	4.21	5.04	5.90	6.68	7.77	
	-.24	-.17	-.09	-.01	.07	.14	.23	.27	.36	.41	.48	.55	.60	.65	
	-.06	.07	.34	.57	.84	1.12	1.49	1.72	1.99	2.25	2.69	3.16	3.51	4.01	
	-.0103	.0116	.0548	.0923	.1352	.1803	.2394	.2761	.3187	.3600	.4310	.5071	.5652	.6426	
	-.0695	-.0616	-.0497	-.0492	-.0456	-.0436	-.0383	-.0369	-.0336	-.0295	-.0293	-.0254	-.0251	-.0231	
	.0178														
c/b	Pressure coefficient, P														
Upper surface	$a_{0.000}$	1.217	1.212	1.208	1.204	1.199	1.194	1.188	1.185	1.180	1.177	1.172	1.167	1.165	1.160
	.025	.547	.495	.436	.341	.239	.098	-.064	-.203	-.360	-.503	-.664	-.804	-.942	-1.162
	.050	.222	.176	.121	.038	-.046	-.157	-.283	-.385	-.504	-.689	-.810	-.921	-1.019	-1.244
	.100	.005	-.035	-.079	-.147	-.211	-.293	-.379	-.450	-.648	-.737	-.892	-1.011	-1.145	-1.303
	.200	-.154	-.176	-.205	-.247	-.284	-.322	-.360	-.390	-.405	-.413	-.637	-.946	-1.088	-1.224
	.300	-.240	-.242	-.259	-.286	-.306	-.329	-.354	-.366	-.384	-.384	-.378	-.385	-.414	-.474
	.400	-.272	-.284	-.288	-.308	-.317	-.329	-.350	-.353	-.370	-.366	-.368	-.350	-.350	-.380
	.500	-.308	-.319	-.326	-.341	-.350	-.357	-.370	-.374	-.383	-.389	-.396	-.397	-.399	-.398
	.600	-.380	-.389	-.393	-.401	-.409	-.414	-.421	-.419	-.419	-.421	-.428	-.433	-.437	-.432
	.700	-.476	-.479	-.480	-.448	-.388	-.371	-.373	-.371	-.374	-.377	-.388	-.398	-.406	-.406
	.800	-.398	-.284	-.262	-.269	-.271	-.274	-.281	-.281	-.284	-.287	-.299	-.312	-.326	-.330
Lower surface	.900	-.001	-.014	-.028	-.041	-.046	-.051	-.061	-.064	-.068	-.073	-.084	-.099	-.115	-.125
	.950	.110	.109	.102	.093	.090	.086	.075	.075	.068	.064	.055	.048	.038	.031
	.0375	-.608	-.579	-.524	-.427	-.335	-.180	-.065	.027	.111	.187	.263	.337	.395	.478
	.075	-.766	-.759	-.710	-.590	-.467	-.090	-.020	.042	.099	.153	.210	.264	.309	.375
	.150	-.604	-.454	-.124	-.130	-.102	-.056	-.014	.025	.061	.099	.138	.177	.208	.259
	.250	-.243	-.085	-.129	-.130	-.106	-.074	-.047	-.019	.006	.034	.063	.091	.114	.156
	.350	-.071	-.124	-.144	-.135	-.117	-.095	-.078	-.056	-.038	-.017	.005	.027	.046	.081
	.450	-.107	-.136	-.138	-.129	-.115	-.097	-.085	-.068	-.054	-.036	-.021	0	.013	.041
	.550	-.143	-.152	-.148	-.140	-.129	-.115	-.107	-.092	-.083	-.068	-.055	-.043	-.030	-.004
	.650	-.175	-.171	-.165	-.160	-.152	-.139	-.134	-.120	-.113	-.104	-.093	-.078	-.068	-.045
	.750	-.124	-.121	-.117	-.118	-.113	-.105	-.103	-.096	-.092	-.084	-.075	-.064	-.058	-.039
	.850	-.030	-.030	-.030	-.036	-.036	-.035	-.040	-.037	-.037	-.034	-.030	-.024	-.020	-.009
No orifice.	.925	.042	.044	.042	.034	.030	.027	.016	.015	.010	.007	.008	.010	.011	.017
	.975	.101	.104	.103	.098	.092	.088	.075	.071	.060	.053	.049	.051	.051	.055
	1.000	.175	.161	.161	.152	.157	.144	.128	.120	.115	.126	.120	.100	.111	.109

No orifice.

NACA

TABLE 8.—PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(06.50) PROPELLER BLADE SECTION ( $x = 0.95$ ) — Continued

(a)  $N = 1600$  rpm.

$\frac{y}{M}$	1.913	2.002	2.076	2.140	2.226	2.329	2.395	2.470	2.501	2.453	2.365	2.268	2.195	2.113	2.006	1.973
$M_x$	.852	.867	.879	.887	.903	.918	.930	.943	.947	.939	.923	.904	.893	.879	.862	.858
$\alpha_x^1$	5.67	4.48	3.51	2.69	1.61	.36	-.42	-1.28	-1.63	-1.09	-.07	1.10	2.00	3.03	4.42	4.86
$\Delta\delta$	.66	.56	.48	.38	.24	.04	-.09	-.24	-.29	-.20	-.05	.16	.50	.82	.56	.60
$\alpha_1$	3.00	2.59	2.16	1.76	1.32	.77	.44	.02	-.26	.01	.50	1.01	1.41	1.93	2.50	2.77
$\alpha_n$	.4819	.4168	.3468	.2823	.2132	.1245	.0716	.0026	-.0416	.0023	.0797	.1619	.2277	.3094	.4013	.4452
$\alpha_m$	-.0303	-.0303	-.0324	-.0323	-.0386	-.0491	-.0541	-.0638	-.0637	-.0628	-.0589	-.0496	-.0389	-.0342	-.0328	-.0305
$\alpha_o$					.0126	.0181	.0213	.0226	.0248	.0224	.0192	.0141	.0111			
$a/b$	Pressure coefficient, P															
Upper surface	$a$ .000	1.195	1.202	1.207	1.212	1.221	1.229	1.235	1.242	1.245	1.240	1.231	1.221	1.216	1.208	1.200
	.025	-.519	-.338	-.162	-.012	.162	.341	.461	.599	.734	.890	.964	.192	.064	-.119	-.352
	.050	-.692	-.485	-.339	-.235	-.123	.013	.079	.198	.299	.394	.492	-.053	-.155	-.271	-.494
	.100	-.752	-.684	-.618	-.511	-.276	-.152	-.053	.014	.045	0	.094	-.209	-.268	-.459	-.635
	.200	-.814	-.700	-.569	-.473	-.396	-.299	-.239	-.165	-.133	-.175	-.258	-.420	-.497	-.670	-.735
	.300	-.661	-.617	-.543	-.459	-.402	-.335	-.304	-.260	-.235	-.262	-.313	-.363	-.412	-.454	-.571
	.400	-.572	-.484	-.425	-.413	-.366	-.328	-.324	-.324	-.309	-.335	-.326	-.350	-.382	-.424	-.475
	.500	-.521	-.480	-.451	-.426	-.379	-.350	-.325	-.342	-.330	-.352	-.348	-.363	-.381	-.430	-.450
	.600	-.397	-.465	-.496	-.459	-.428	-.414	-.396	-.409	-.404	-.413	-.416	-.429	-.430	-.458	-.417
	.700	-.357	-.357	-.451	-.513	-.524	-.509	-.495	-.495	-.498	-.498	-.512	-.532	-.533	-.500	-.426
	.800	-.270	-.257	-.229	-.206	-.228	-.401	-.474	-.507	-.527	-.511	-.482	-.369	-.276	-.235	-.278
	.900	-.046	-.030	-.019	.002	.005	-.032	-.055	-.043	-.055	-.039	-.019	.002	.002	-.020	-.048
	.950	.058	.063	.072	.076	.065	.031	.020	.010	-.012	.004	.028	.065	.082	.083	.072
Lower surface	.0375	.280	.182	.078	-.017	-.159	-.332	-.439	-.491	-.524	-.585	-.637	-.442	-.271	-.016	.175
	.075	.228	.151	.074	.007	-.085	-.381	-.458	-.560	-.583	-.574	-.507	-.153	-.033	.051	.145
	.150	.149	.091	.040	-.003	-.060	-.086	-.363	-.453	-.497	-.474	-.212	-.089	-.041	.023	.088
	.250	.068	.027	-.014	-.042	-.080	-.112	-.047	-.380	-.446	-.408	-.132	-.095	-.059	.016	.028
	.350	.007	-.027	-.055	-.074	-.103	-.075	-.002	-.242	-.339	-.194	-.099	-.080	-.057	.025	.009
	.450	-.031	-.058	-.078	-.093	-.110	-.060	-.151	-.119	-.270	-.127	-.140	-.122	-.103	-.074	-.044
	.550	-.056	-.081	-.117	-.132	-.157	-.210	-.208	-.129	-.183	-.157	-.176	-.154	-.132	-.105	-.079
	.650	-.079	-.102	-.125	-.139	-.161	-.185	-.201	-.179	-.147	-.194	-.207	-.168	-.145	-.118	-.095
	.750	-.082	-.102	-.119	-.130	-.148	-.182	-.205	-.234	-.195	-.238	-.205	-.160	-.139	-.124	-.119
	.850	-.031	-.040	-.049	-.052	-.064	-.121	-.129	-.131	-.136	-.129	-.105	-.081	-.076	-.071	-.063
	.925	.003	.001	.003	.005	-.001	-.076	-.071	-.055	-.068	-.054	-.036	-.027	-.030	-.029	-.023
	.975	.037	.042	.052	.056	.051	-.012	-.011	-.009	-.028	-.015	.009	.022	.027	.029	.028
	1.000	.168	.160	.140	.140	.103	.058	.077	.041	.008	.026	.053	.109	.127	.123	.136

<sup>a</sup>No orifice.

NACA

TABLE 8.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(06.50) PROPELLER BLADE SECTION ( $x = 0.95$ ) - Continued

(e)  $M = 0.56$ .

$J$	1.967	2.000	2.037	2.073	2.098	2.129	2.161	2.188	2.234	2.253	2.309	2.346	2.384	2.416	2.460	2.494	2.536	2.550
$M_x$	1.014	1.004	.995	.987	.977	.968	.958	.947	.940	.931	.923	.914	.905	.895	.885	.878	.869	.864
$\alpha_x$	4.94	4.50	4.02	3.55	3.22	2.83	2.42	2.08	1.51	1.28	.60	.16	-.29	-.63	-1.17	-1.55	-2.02	-2.18
$\Delta\delta$	.51	.47	.42	.38	.35	.31	.27	.24	.18	.16	.09	.05	0	-.04	-.09	-.14	-.19	-.20
$\alpha_1$	2.24	2.08	1.90	1.68	1.49	1.39	1.27	1.20	1.04	.95	.81	.65	.55	.37	.14	.04	-.12	-.21
$c_n$	.3597	.3348	.3061	.2722	.2401	.2225	.2045	.1919	.1669	.1542	.1300	.1042	.0890	.0590	.0223	.0058	-.0200	-.0342
$c_m$	-.0592	-.0535	-.0472	-.0412	-.0380	-.0354	-.0406	-.0435	-.0478	-.0515	-.0588	-.0610	-.0610	-.0624	-.0633	-.0662	-.0701	-.0683
$c_o$	.0287	.0282	.0273	.0259	.0254	.0246	.0227	.0217	.0205	.0196	.0189	.0180	.0174	.0159				
$c/b$	Pressure coefficient, P																	
Upper surface	$a_{0.000}$	1.283	1.277	1.272	1.267	1.261	1.256	1.251	1.244	1.241	1.235	1.231	1.226	1.222	1.217	1.211	1.208	1.201
	.025	.020	.044	.089	.105	.131	.132	.179	.198	.246	.272	.329	.370	.444	.436	.474	.503	.532
	.050	-.190	-.152	-.107	-.105	-.096	-.090	-.078	-.072	-.045	-.022	.020	.056	.080	.112	.145	.169	.217
	.100	-.327	-.319	-.291	-.288	-.273	-.255	-.216	-.199	-.184	-.176	-.145	-.120	-.101	-.076	-.048	-.028	.011
	.200	-.412	-.405	-.380	-.370	-.340	-.335	-.339	-.349	-.339	-.329	-.301	-.281	-.263	-.219	-.190	-.174	-.140
	.300	-.435	-.434	-.414	-.417	-.411	-.409	-.405	-.406	-.396	-.381	-.356	-.316	-.312	-.301	-.281	-.270	-.236
	.400	-.444	-.434	-.414	-.414	-.409	-.406	-.403	-.409	-.380	-.361	-.311	-.316	-.315	-.300	-.275	-.274	-.251
	.500	-.424	-.412	-.392	-.401	-.402	-.402	-.398	-.400	-.386	-.366	-.352	-.338	-.326	-.323	-.297	-.299	-.285
	.600	-.452	-.448	-.434	-.446	-.448	-.450	-.445	-.444	-.425	-.410	-.406	-.403	-.407	-.388	-.379	-.366	-.368
	.700	-.523	-.522	-.514	-.526	-.527	-.527	-.522	-.521	-.512	-.508	-.510	-.512	-.509	-.494	-.472	-.468	-.380
	.800	-.555	-.556	-.546	-.558	-.557	-.559	-.551	-.541	-.537	-.527	-.525	-.502	-.472	-.360	-.282	-.281	-.291
Lower surface	.900	-.438	-.388	-.292	-.210	-.167	-.128	-.086	-.064	-.048	-.028	-.009	.014	.016	-.006	-.029	-.046	-.067
	.950	-.225	-.212	-.181	-.155	-.127	-.098	-.063	-.040	-.020	.006	.034	.077	.101	.113	.111	.104	.093
	.0375	.224	.185	.149	.082	.026	-.019	-.071	-.122	-.183	-.227	-.324	-.405	-.481	-.568	-.634	-.682	-.762
	.075	.210	.180	.154	.095	.050	.017	-.027	-.077	-.190	-.282	-.395	-.492	-.566	-.658	-.733	-.784	-.855
	.150	.156	.132	.118	.071	.039	.017	-.009	-.037	-.063	-.078	-.089	-.096	-.132	-.189	-.278	-.408	-.556
	.250	.073	.055	.042	.001	-.029	-.046	-.066	-.088	-.109	-.121	-.134	-.129	-.123	-.113	-.100	-.089	-.083
	.350	-.002	-.015	-.022	-.056	-.075	-.087	-.098	-.115	-.126	-.133	-.141	-.141	-.143	-.138	-.132	-.130	-.123
	.450	-.066	-.078	-.079	-.106	-.118	-.126	-.135	-.149	-.154	-.155	-.158	-.155	-.157	-.150	-.145	-.146	-.142
	.550	-.066	-.077	-.078	-.106	-.118	-.128	-.138	-.151	-.160	-.165	-.171	-.166	-.164	-.156	-.150	-.150	-.146
	.650	-.123	-.134	-.134	-.161	-.173	-.182	-.193	-.205	-.212	-.212	-.211	-.193	-.183	-.164	-.151	-.149	-.141
	.750	-.195	-.205	-.206	-.231	-.244	-.254	-.261	-.272	-.275	-.251	-.212	-.175	-.157	-.133	-.119	-.112	-.109
	.850	-.236	-.246	-.247	-.270	-.281	-.288	-.293	-.274	-.185	-.132	-.105	-.073	-.054	-.034	-.024	-.023	-.018
	.925	-.250	-.258	-.260	-.281	-.289	-.290	-.241	-.137	-.098	-.068	-.039	-.002	.019	.041	.050	.051	.055
	.975	-.275	-.286	-.287	-.303	-.300	-.271	-.157	-.100	-.066	-.032	.003	.047	.075	.102	.114	.114	.120
	$a_{1.000}$	-.245	-.260	-.244	-.263	-.255	-.205	-.056	-.065	-.013	.009	.040	.094	.117	.150	.162	.180	.180

<sup>a</sup>No orifice.

<sup>b</sup>Lower surface only.

NACA

TABLE 8.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(06.50) PROPELLER BLADE SECTION ( $\alpha = 0.95$ ) - Continued

(f)  $M = 0.60$ .

$J$	2.536	2.481	2.445	2.399	2.357	2.309	2.274	2.236	2.187	2.159	2.119	2.091	2.056	2.019	1.993
$M_x$	.934	.943	.955	.966	.976	.986	.998	1.009	1.019	1.036	1.043	1.052	1.063	1.076	1.086
$\alpha_x$	-2.03	-1.41	-1.00	-.46	.03	.60	1.03	1.49	2.10	2.45	2.96	3.31	3.77	4.25	4.60
$\Delta\theta$	-.29	-.24	-.22	-.17	-.13	-.08	-.05	-.01	.05	.09	.14	.18	.22	.27	.30
$\alpha_1$	-.35	-.31	-.19	-.12	.03	.21	.48	.76	1.04	1.24	1.45	1.65	1.76	1.92	1.96
$c_n$	-.0571	-.0500	-.0300	-.0187	.0042	.0339	.0777	.1216	.1677	.1997	.2326	.2658	.2832	.3065	.3139
$c_m$	-.0770	-.0632	-.0524	-.0447	-.0330	-.0323	-.0456	-.0512	-.0578	-.0678	-.0741	-.0760	-.0764	-.0772	-.0779
$c_c$	.0228	.0245	.0258	.0270	.0287	.0295	.0337	.0374	.0366	.0379	.0389	.0388	.0396	.0402	.0403
$c/b$	Pressure coefficient, $P$														
Upper surface	0.000	1.237	1.242	1.249	1.255	1.261	1.267	1.274	1.280	1.286	1.297	1.302	1.307	1.314	1.324
	.025	.589	.553	.524	.502	.464	.437	.409	.382	-.010	-.053	-.051	.260	.305	.270
	.050	.267	.237	.213	.198	.167	.145	.126	.117	.122	.120	.082	.045	.042	.038
	.100	.062	.040	.023	.013	-.010	-.026	-.028	-.046	-.073	-.060	-.116	-.127	-.134	-.101
	.200	-.119	-.149	-.170	-.172	-.183	-.199	-.203	-.226	-.223	-.199	-.229	-.240	-.257	-.296
	.300	-.224	-.234	-.234	-.231	-.248	-.259	-.262	-.272	-.291	-.269	-.294	-.290	-.296	-.300
	.400	-.309	-.326	-.327	-.325	-.332	-.340	-.337	-.339	-.346	-.319	-.341	-.329	-.335	-.354
	.500	-.319	-.327	-.324	-.319	-.326	-.329	-.324	-.328	-.339	-.314	-.336	-.324	-.324	-.343
	.600	-.398	-.402	-.394	-.383	-.380	-.378	-.365	-.365	-.377	-.353	-.375	-.362	-.356	-.367
	.700	-.499	-.501	-.490	-.476	-.466	-.459	-.446	-.444	-.452	-.429	-.452	-.438	-.431	-.436
	.800	-.507	-.521	-.519	-.509	-.503	-.495	-.486	-.483	-.486	-.460	-.482	-.469	-.463	-.471
	.900	-.014	-.044	-.056	-.074	-.120	-.177	-.397	-.571	-.604	-.584	-.605	-.590	-.581	-.582
	.950	.023	-.018	-.029	-.049	-.076	-.098	-.151	-.211	-.273	-.472	-.612	-.623	-.612	-.605
Lower surface	.0375	-.543	-.481	-.419	-.364	-.290	-.239	-.168	-.095	-.200	-.175	-.158	.107	.175	.214
	.075	-.654	-.614	-.558	-.510	-.446	-.392	-.315	-.177	-.173	-.058	-.004	.090	.157	.188
	.150	-.571	-.515	-.443	-.382	-.316	-.259	-.171	-.084	.008	.072	.081	.110	.131	.154
	.250	-.502	-.442	-.377	-.326	-.251	-.194	-.115	-.088	-.035	.010	.011	.042	.063	.082
	.350	-.442	-.400	-.342	-.285	-.196	-.153	-.117	-.111	-.083	-.042	-.042	-.011	.005	.017
	.450	-.208	-.195	-.162	-.136	-.117	-.131	-.129	-.136	-.126	-.089	-.095	-.067	-.052	-.045
	.550	-.075	-.092	-.096	-.099	-.118	-.136	-.133	-.141	-.124	-.089	-.100	-.073	-.060	-.063
	.650	-.143	-.168	-.176	-.183	-.194	-.200	-.191	-.190	-.175	-.139	-.149	-.124	-.110	-.108
	.750	-.163	-.221	-.244	-.250	-.260	-.258	-.249	-.242	-.232	-.197	-.208	-.182	-.169	-.167
	.850	-.070	-.123	-.244	-.286	-.307	-.303	-.294	-.285	-.276	-.242	-.255	-.192	-.215	-.215
	.925	-.015	-.051	-.091	-.227	-.314	-.319	-.311	-.308	-.294	-.262	-.276	-.239	-.238	-.227
	.975	.008	-.034	-.056	-.100	-.245	-.288	-.306	-.315	-.306	-.276	-.293	-.272	-.251	-.242
	1.000	.055	-.027	-.042	-.045	-.072	-.100	-.279	-.285	-.280	-.292	-.319	-.280	-.255	-.247

<sup>a</sup>No orifice.<sup>b</sup>Lower surface only.

NACA

TABLE 8.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
 MACA 16-(3)(06.50) PROPELLER BLADE SECTION ( $\alpha = 0.95$ ) - Concluded

( $R$ )  $M = 0.65$ .

$J$	2.014	2.043	2.074	2.113	2.132	2.156	2.179	2.213	2.243	2.270	2.302	2.333	2.356	2.383
$M_x$	1.164	1.154	1.143	1.134	1.122	1.110	1.097	1.093	1.083	1.073	1.066	1.052	1.046	1.035
$\Delta\theta$	4.32	3.94	3.53	3.03	2.79	2.49	2.20	1.77	1.40	1.07	.69	.32	.04	-.28
$\alpha_1$	1.93	1.82	1.61	1.44	1.32	1.20	1.05	.92	.79	.70	.46	.30	.18	-.02
$c_n$	.3097	.2919	.2581	.2313	.2116	.1926	.1684	.1468	.1268	.1132	.0742	.0484	.0285	-.0039
$c_m$	-.0715	-.0694	-.0670	-.0653	-.0643	-.0635	-.0648	-.0633	-.0635	-.0627	-.0643	-.0626	-.0597	-.0564
$c_c$	.0395	.0402	.0411	.0411	.0420	.0433	.0434	.0439	.0442	.0431	.0444	.0446	.0456	.0457
$a/b$	Pressure coefficient, $P$													
Upper surface	$\alpha = 0.000$	1.384	1.377	1.369	1.363	1.354	1.346	1.337	1.335	1.328	1.323	1.317	1.308	1.297
	.025	.316	.329	.360	.372	.390	.401	.414	.436	.447	.408	.476	.510	.533
	.050	.097	.114	.138	.150	.154	.155	.160	.176	.185	.209	.200	.234	.251
	.100	-.061	-.058	-.040	-.006	.040	.056	.067	.081	.086	.087	.112	.115	.111
	.200	-.173	-.169	-.149	-.121	-.146	-.135	-.122	-.105	-.104	-.110	-.115	-.118	-.106
	.300	-.202	-.204	-.193	-.189	-.193	-.204	-.213	-.217	-.215	-.189	-.177	-.164	-.166
	.400	-.260	-.261	-.255	-.259	-.272	-.295	-.306	-.302	-.304	-.276	-.268	-.263	-.270
	.500	-.262	-.264	-.262	-.266	-.283	-.294	-.297	-.294	-.300	-.292	-.286	-.280	-.285
	.600	-.275	-.284	-.288	-.292	-.309	-.319	-.324	-.323	-.329	-.327	-.323	-.325	-.341
	.700	-.340	-.352	-.356	-.358	-.371	-.391	-.391	-.373	-.399	-.400	-.398	-.404	-.423
	.800	-.370	-.383	-.386	-.390	-.395	-.402	-.411	-.425	-.423	-.434	-.438	-.445	-.470
Lower surface	.900	-.473	-.489	-.493	-.494	-.508	-.525	-.539	-.544	-.554	-.555	-.558	-.567	-.592
	.950	-.510	-.527	-.534	-.534	-.545	-.561	-.576	-.581	-.592	-.599	-.601	-.608	-.597
	.0375	.309	.280	.228	.165	.132	.093	.057	.029	-.005	-.096	-.114	-.137	-.199
	.075	.303	.263	.132	.055	.021	-.019	-.075	-.127	-.168	-.211	-.266	-.303	-.379
	.150	.266	.244	.207	.168	.135	.085	.015	-.015	-.042	-.030	-.035	-.080	-.171
	.250	.177	.159	.126	.092	.068	.039	-.003	-.034	-.080	-.095	-.134	-.185	-.244
	.350	.104	.089	.059	.029	.006	-.022	-.044	-.067	-.099	-.128	-.150	-.173	-.246
	.450	.047	.029	0	-.025	-.047	-.072	-.091	-.103	-.119	-.154	-.177	-.198	-.247
	.550	.017	-.003	-.026	-.046	-.067	-.090	-.106	-.117	-.127	-.139	-.157	-.187	-.236
	.650	-.016	-.035	-.057	-.076	-.096	-.117	-.134	-.145	-.155	-.159	-.164	-.192	-.259
	.750	-.084	-.101	-.120	-.137	-.156	-.180	-.196	-.206	-.218	-.222	-.221	-.234	-.298
	.850	-.136	-.155	-.171	-.188	-.207	-.229	-.245	-.255	-.266	-.271	-.271	-.272	-.322
a1.000	.925	-.161	-.180	-.197	-.210	-.229	-.250	-.265	-.276	-.288	-.292	-.290	-.290	-.329
	.975	-.172	-.191	-.208	-.226	-.246	-.264	-.282	-.294	-.306	-.311	-.313	-.317	-.344
a1.000		-.176	-.198	-.215	-.236	-.259	-.272	-.295	-.306	-.312	-.328	-.330	-.336	-.363

\*No orifice.

NACA

TABLE 9.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-(2)(05.34) PROPELLER BLADE SECTION ( $\pi = 0.975$ )

$$[\beta_{0.75R} = 45^\circ; \beta_x = 37.65^\circ; B = 2]$$

(a)  $N = 1140$  rpm.

$J$ $M_x$ $\alpha_{0.75R}$ $\beta_x$ $C_L$ $C_D$	1.352 .570 13.84 .38 5.28 -.0690 -.0261	1.434 .576 12.26 .35 5.31 -.0381 -.0321	1.617 .591 9.82 .30 4.87 -.0444 -.0444	1.778 .606 7.32 .25 4.04 -.0428 -.0428	1.922 .621 5.75 .18 3.00 -.0361 -.0361	2.077 .636 3.91 .11 2.07 -.0322 -.0322	2.236 .653 2.52 .04 1.33 -.0317 -.0317	2.404 .669 1.48 -.04 .79 -.0377 -.0377	2.573 .684 -2.15 -.11 .10 -.0423 -.0423	2.620 .692 -2.89 -.14 -.15 -.0447 -.0447	2.481 .679 -1.35 -.08 .32 -.0407 -.0407	2.326 .658 2.32 -.01 .87 -.0332 -.0332	2.171 .643 4.52 .06 1.62 -.0330 -.0330	1.999 .628 6.23 .15 2.30 -.0379 -.0379	1.871 .616 8.82 .21 3.33 -.0401 -.0401	1.686 .599 11.06 .28 4.49 -.0434 -.0434	1.533 .583 13.04 .32 5.11 -.0444 -.0444	1.403 .571 13.36 .36 5.37 -.0293 -.0293	
$c/b$	Pressure coefficient, $P$																		
Upper surface	0.000	1.083	1.085	1.090	1.094	1.099	1.105	1.111	1.117	1.123	1.126	1.121	1.113	1.107	1.102	1.097	1.092	1.087	1.084
	.025	-1.919	-2.007	-2.396	-1.882	-1.232	-.728	-.349	-.004	-.264	-.348	-.139	-.154	-.493	-.950	-1.404	-1.965	-2.208	-2.171
	.050	-1.463	-1.541	-1.122	-.790	-.610	-.407	-.243	-.073	-.047	-.124	-.002	-.152	-.317	-.523	-.671	-.867	-1.423	-1.560
	.100	-1.023	-.974	-.714	-.615	-.488	-.325	-.271	-.164	-.075	-.042	-.121	-.211	-.314	-.430	-.528	-.660	-.839	-.980
	.200	-.561	-.533	-.466	-.399	-.314	-.224	-.189	-.161	-.122	-.106	-.145	-.179	-.213	-.281	-.338	-.426	-.478	-.552
	.300	-.435	-.438	-.427	-.366	-.300	-.228	-.209	-.183	-.158	-.145	-.174	-.197	-.224	-.274	-.319	-.394	-.443	-.463
	.400	-.403	-.423	-.400	-.348	-.285	-.221	-.207	-.188	-.174	-.163	-.186	-.200	-.221	-.264	-.302	-.370	-.415	-.424
	.500	-.395	-.411	-.402	-.352	-.293	-.228	-.215	-.195	-.186	-.182	-.195	-.207	-.228	-.271	-.308	-.374	-.409	-.412
	.600	-.391	-.411	-.417	-.374	-.314	-.251	-.241	-.222	-.216	-.212	-.223	-.232	-.254	-.295	-.333	-.392	-.420	-.408
	.700	-.351	-.361	-.370	-.333	-.279	-.217	-.205	-.186	-.180	-.175	-.187	-.199	-.221	-.260	-.294	-.349	-.374	-.353
	.800	-.327	-.351	-.378	-.348	-.293	-.236	-.228	-.211	-.207	-.207	-.212	-.223	-.241	-.277	-.310	-.361	-.374	-.329
Lower surface	.900	-.279	-.274	-.312	-.283	-.237	-.180	-.170	-.151	-.160	-.163	-.160	-.162	-.183	-.219	-.251	-.296	-.309	-.258
	.950	-.223	-.173	-.164	-.134	-.097	-.046	-.042	-.024	-.032	-.038	-.032	-.034	-.052	-.084	-.109	-.145	-.168	-.175
	.0375	.593	.560	.491	.386	.235	.091	-.096	-.286	-.490	-.571	-.401	-.208	-.032	.146	.290	.440	.529	.590
	.075	.417	.382	.321	.228	.107	.008	-.129	-.249	-.359	-.403	-.312	-.200	-.085	.044	.151	.274	.357	.412
	.150	.283	.255	.211	.158	.086	.037	-.047	-.112	-.180	-.203	-.151	-.088	-.023	.048	.116	.187	.234	.278
	.250	.133	.115	.083	.025	-.044	-.070	-.127	-.164	-.201	-.216	-.189	-.149	-.113	-.072	-.023	.065	.102	.132
	.350	.101	.087	.064	.039	.002	-.011	-.059	-.084	-.110	-.124	-.102	-.079	-.052	-.021	.018	.053	.077	.101
	.450	.053	.046	.034	.017	-.033	-.044	-.082	-.098	-.116	-.127	-.111	-.095	-.075	-.060	-.005	.027	.043	.057
	.550	.063	.021	.011	-.001	-.026	-.031	-.064	-.078	-.092	-.100	-.089	-.076	-.058	-.046	-.012	.007	.020	.030
	.650	-.007	-.005	-.008	-.018	-.040	-.042	-.068	-.081	-.092	-.097	-.089	-.079	-.065	-.058	-.027	-.010	-.003	.002
	.750	-.061	-.048	-.045	-.044	-.058	-.048	-.072	-.079	-.086	-.089	-.086	-.082	-.071	-.070	-.041	-.041	-.047	-.047
	.850	-.087	-.034	-.023	-.023	-.026	-.009	-.029	-.029	-.029	-.029	-.034	-.060	-.030	-.034	-.023	-.021	-.022	-.043
	.925	-.069	-.013	.011	.021	.023	.047	.031	.034	.041	.042	.034	.027	.022	.022	.027	.018	.010	-.034
	.975	-.163	-.059	-.011	.006	.019	.057	.049	.060	.077	.081	.066	.050	.043	.024	.016	-.002	-.018	-.105
	1.000	-.207	-.086	-.031	-.010	.015	.061	.055	.069	.092	.100	.078	.059	.048	.012	.001	-.049	-.040	-.150

\*No orifice.



TABLE 9.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-(2)(05.34) PROPELLER BLADE SECTION ( $x = 0.975$ ) - Continued.(b)  $N = 1350$  rpm.

$J$ $M_\infty$ $\Delta P$ $\alpha_1$ $\alpha_n$ $\alpha_o$	1.475 .696 11.94 5.42 .6290 -.0388	1.586 .702 10.28 5.42 .6290 -.0434	1.689 .712 8.83 4.64 .5394 -.0485	1.779 .725 7.90 4.05 .4710 -.0431	1.877 .733 6.15 3.78 .4123 -.0393	2.000 .743 4.51 2.71 .3129 -.0375	2.129 .757 2.85 1.98 .2290 -.0341	2.282 .819 2.48 1.17 -.0197 -.0504	2.534 .813 1.95 0.01 -.0016 -.0462	2.478 .801 1.32 0.30 -.0348 -.0442	2.407 .793 0.51 0.54 -.0632 -.0421	2.350 .785 0.15 0.76 -.0881 -.0401	2.283 .775 0.95 1.00 -.1171 -.0405	2.221 .767 1.70 1.43 -.1668 -.0347	2.153 .757 2.55 1.84 -.2142 -.0339	2.076 .750 3.52 2.20 -.2542 -.0365	2.011 .740 4.36 2.54 -.2935 -.0377	1.933 .733 5.40 3.04 -.3515 -.0398	1.845 .725 6.59 3.68 -.4239 -.0403	1.751 .713 7.90 4.21 -.4871 -.0447	1.648 .705 9.37 4.89 -.5684 -.0482	1.550 .693 10.81 5.42 -.6290 -.0447
$\alpha/b$	Pressure coefficient, P																					
Upper surface	0.000 .025 .050 .100 .200 .300 .400 .500 .600 .700 .800 .900 .950	1.128 -2.204 -1.928 -1.082 -1.457 -1.460 -1.437 -1.434 -1.439 -1.392 -1.389 -1.304 -1.195	1.130 -2.067 -1.783 -1.190 -1.453 -1.452 -1.428 -1.430 -1.444 -1.403 -1.410 -1.326 -1.158	1.134 -1.827 -1.611 -1.067 -1.432 -1.436 -1.401 -1.409 -1.429 -1.393 -1.403 -1.322 -1.149	1.139 -1.661 -1.446 -1.023 -1.403 -1.406 -1.364 -1.371 -1.395 -1.360 -1.373 -1.294 -1.129	1.142 -1.486 -1.191 -1.028 -1.361 -1.340 -1.329 -1.333 -1.358 -1.325 -1.342 -1.266 -1.108	1.147 -1.094 -1.486 -1.475 -1.309 -1.296 -1.282 -1.293 -1.319 -1.288 -1.307 -1.232 -1.079	1.152 -1.629 -1.388 -1.121 -1.257 -1.261 -1.253 -1.263 -1.290 -1.258 -1.279 -1.200 -1.051	1.176 -1.268 -1.083 -1.088 -1.127 -1.163 -1.179 -1.187 -1.195 -1.221 -1.244 -1.245 -1.218 -1.005	1.172 -1.189 -1.031 -1.042 -1.198 -1.203 -1.204 -1.205 -1.220 -1.221 -1.236 -1.218 -1.005	1.167 -1.060 -1.042 -1.209 -1.252 -1.211 -1.216 -1.230 -1.230 -1.252 -1.236 -1.009	1.164 -1.046 -1.102 -1.254 -1.293 -1.219 -1.220 -1.216 -1.230 -1.230 -1.259 -1.236 -1.018	1.159 -1.185 -1.273 -1.254 -1.303 -1.219 -1.220 -1.216 -1.230 -1.230 -1.259 -1.236 -1.018	1.156 -1.346 -1.254 -1.303 -1.219 -1.220 -1.216 -1.230 -1.230 -1.259 -1.236 -1.018	1.152 -1.545 -1.354 -1.354 -1.406 -1.249 -1.220 -1.216 -1.230 -1.230 -1.259 -1.236 -1.018	1.149 -1.749 -1.494 -1.406 -1.268 -1.220 -1.216 -1.230 -1.230 -1.259 -1.236 -1.018	1.145 -1.982 -1.494 -1.406 -1.268 -1.220 -1.216 -1.230 -1.230 -1.259 -1.236 -1.018	1.142 -1.275 -1.577 -1.513 -1.337 -1.303 -1.270 -1.268 -1.314 -1.308 -1.333 -1.275 -1.097	1.139 -1.528 -1.210 -1.339 -1.327 -1.343 -1.305 -1.288 -1.315 -1.308 -1.333 -1.275 -1.097	1.134 -1.705 -1.484 -1.327 -1.407 -1.363 -1.366 -1.373 -1.367 -1.333 -1.308 -1.275 -1.097	1.131 -1.884 -1.666 -1.779 -1.442 -1.426 -1.408 -1.414 -1.395 -1.360 -1.333 -1.275 -1.097	1.127 -2.117 -1.833 -1.017 -1.454 -1.453 -1.429 -1.442 -1.442 -1.408 -1.395 -1.324 -1.158
Lower surface	0.0375 .075 .150 .250 .350 .450 .550 .650 .750 .850 .950 1.000	.564 .380 .297 .085 .082 .035 .016 -.011 -.042 -.033 -.005 -.040 -.073	.521 .342 .233 .067 .070 .023 .011 -.011 -.048 -.020 -.009 -.016 -.041	.439 .265 .184 .028 .042 .001 -.007 -.028 -.051 -.029 -.013 0	.367 .204 .145 .002 .002 -.015 -.018 -.037 -.044 -.030 -.013 0	.268 .140 .107 -.024 -.003 -.009 -.028 -.044 -.060 -.030 -.020 -.043 -.025	.164 .041 .047 -.065 -.003 -.049 -.043 -.057 -.069 -.036 -.044 -.091 -.073	-.703 -.662 -.201 -.112 -.134 -.133 -.110 -.109 -.103 -.096 -.034 -.044 -.088 -.116	-.554 -.377 -.194 -.213 -.123 -.122 -.102 -.102 -.103 -.098 -.034 -.044 -.088 -.110	-.481 -.362 -.178 -.204 -.119 -.103 -.100 -.090 -.100 -.091 -.036 -.037 -.089	-.267 -.254 -.117 -.163 -.092 -.097 -.086 -.087 -.081 -.086 -.036 -.036 -.075	-.181 -.199 -.087 -.150 -.079 -.088 -.074 -.081 -.079 -.086 -.036 -.036 -.071	-.100 -.147 -.061 -.137 -.070 -.082 -.071 -.081 -.070 -.086 -.036 -.036 -.059	-.009 -.083 -.025 -.113 -.054 -.069 -.061 -.066 -.066 -.066 -.035 -.035 -.059	.065 -.031 -.036 -.074 -.029 -.042 -.048 -.066 -.062 -.073 -.035 -.035 -.040	.139 .078 .065 -.057 -.018 -.046 -.044 -.062 -.042 -.073 -.035 -.035 -.040	.208 .078 .065 -.057 -.018 -.046 -.044 -.062 -.042 -.073 -.035 -.035 -.040	.303 .153 .112 -.022 .006 .031 .026 -.042 -.032 -.039 -.014 -.018 -.010	.366 .221 .156 .012 .031 .011 .002 -.017 -.030 -.027 -.014 -.005 -.086	.467 .293 .200 .043 .053 .011 .002 -.017 -.042 -.023 -.011 -.013 -.086	.530 .354 .239 .069 .074 .025 .011 -.008 -.038 -.022 -.007 -.026 -.052	

No crifice.

NACA

TABLE 9.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(2)(05.34) PROPELLER BLADE SECTION ( $x = 0.975$ ) - Continued

(a)  $N = 1500$  rpm.

$\beta$	1.683	1.740	1.811	1.899	1.960	2.044	2.150	2.275	2.380	2.502	2.622	2.773	2.458	2.325	2.213	2.106	2.012	1.873	1.784
$M_\infty$	.792	.798	.806	.816	.824	.836	.851	.867	.883	.901	.920	.913	.892	.870	.852	.837	.825	.807	.795
$\alpha$	8.86	8.05	7.06	5.85	5.04	4.94	2.58	1.05	-.20	-1.59	-2.91	-2.58	-1.10	.45	1.80	3.14	4.35	6.21	7.43
$\Delta h$	.74	.71	.65	.56	.49	.40	.27	.12	-.02	-.21	-.41	-.32	-.14	.05	.19	.32	.44	.58	.67
$\alpha_1$	5.33	4.79	4.30	3.55	3.03	2.64	1.97	1.28	.76	.28	-.42	-.13	.52	1.00	1.58	2.17	2.69	3.74	4.44
$\alpha_n$	.6206	.5555	.4974	.4084	.3484	.3032	.2277	.1494	.0684	.0323	-.0490	-.0155	.0609	.1171	.1845	.2510	.3090	.4316	.5103
$\alpha_m$	-.0546	-.0509	-.0479	-.0428	-.0413	-.0385	-.0433	-.0389	-.0469	-.0585	-.0631	-.0600	-.0516	-.0457	-.0414	-.0396	-.0401	-.0433	-.0495
$\alpha_o$																			
$a/b$	Pressure coefficient, $P$																		
Upper surface	0.000	1.166	1.170	1.173	1.177	1.181	1.187	1.194	1.202	1.210	1.220	1.230	1.226	1.215	1.203	1.195	1.187	1.182	1.174
	.025	-1.382	-1.311	-1.198	-1.066	-.967	-.846	-.743	-.668	-.605	-.550	-.501	-.441	-.395	-.341	-.294	-.264	-.224	-.184
	.050	-1.282	-1.205	-1.100	-.939	-.799	-.673	-.567	-.484	-.411	-.350	-.291	-.231	-.185	-.141	-.099	-.062	-.024	.014
	.100	-1.223	-1.148	-1.034	-.862	-.716	-.585	-.473	-.382	-.308	-.240	-.180	-.120	-.073	-.029	.011	.048	.084	.117
	.200	-.730	-.588	-.480	-.411	-.346	-.310	-.277	-.229	-.200	-.193	-.161	-.133	-.106	-.081	-.051	-.029	.001	.029
	.300	-.488	-.429	-.378	-.336	-.319	-.300	-.277	-.255	-.240	-.221	-.201	-.183	-.166	-.151	-.129	-.108	-.084	-.059
	.400	-.395	-.367	-.335	-.321	-.304	-.285	-.264	-.244	-.231	-.210	-.199	-.182	-.166	-.151	-.129	-.108	-.084	-.059
	.500	-.430	-.404	-.377	-.350	-.334	-.314	-.296	-.278	-.265	-.250	-.230	-.218	-.202	-.187	-.166	-.144	-.121	-.096
	.600	-.477	-.453	-.428	-.401	-.384	-.363	-.349	-.336	-.323	-.301	-.289	-.276	-.260	-.244	-.229	-.208	-.184	-.159
	.700	-.434	-.409	-.381	-.353	-.335	-.314	-.300	-.291	-.273	-.256	-.237	-.224	-.208	-.193	-.177	-.156	-.132	-.107
	.800	-.462	-.441	-.416	-.387	-.366	-.343	-.328	-.309	-.295	-.277	-.257	-.243	-.227	-.211	-.195	-.174	-.150	-.125
	.900	-.371	-.340	-.314	-.280	-.257	-.227	-.198	-.161	-.133	-.118	-.087	-.078	-.062	-.047	-.032	-.016	.001	.016
	.950	-.157	-.137	-.114	-.089	-.071	-.047	-.022	.009	.032	.047	.067	.058	.041	.017	-.007	-.033	-.059	-.089
Lower surface	.0375	.447	.400	.336	.243	.186	.115	-.005	-.177	-.317	-.475	-.563	-.538	-.401	-.273	-.117	.039	.131	.268
	.075	.281	.236	.185	.108	.062	.007	-.082	-.204	-.316	-.466	-.573	-.538	-.401	-.263	-.158	-.047	.020	.129
	.150	.197	.171	.135	.086	.059	.027	-.023	-.131	-.239	-.377	-.473	-.427	-.295	-.185	-.066	-.005	.034	.100
	.250	.049	.020	-.024	-.063	-.081	-.101	-.106	-.167	-.253	-.369	-.458	-.399	-.263	-.153	-.033	-.095	-.048	-.023
	.350	.047	.037	.020	-.009	-.024	-.036	-.055	-.085	-.105	-.109	-.120	-.108	-.098	-.077	-.051	-.036	-.003	.019
	.450	-.006	-.007	-.010	-.050	-.071	-.082	-.092	-.111	-.125	-.137	-.109	-.109	-.126	-.119	-.104	-.087	-.078	-.053
	.550	-.015	-.021	-.029	-.046	-.059	-.070	-.078	-.094	-.106	-.122	-.104	-.114	-.110	-.101	-.090	-.074	-.068	-.045
	.650	-.030	-.037	-.049	-.068	-.077	-.082	-.088	-.104	-.116	-.132	-.121	-.135	-.118	-.110	-.099	-.087	-.083	-.064
	.750	-.048	-.052	-.063	-.080	-.088	-.091	-.096	-.106	-.113	-.124	-.127	-.129	-.110	-.104	-.096	-.095	-.077	-.066
	.850	-.020	-.022	-.029	-.038	-.041	-.043	-.042	-.046	-.044	-.040	-.040	-.040	-.035	-.047	-.046	-.044	-.037	-.033
	.925	.014	.018	.020	.018	.018	.023	.028	.031	.039	.051	.061	.057	.051	.033	.027	.022	.018	.015
	.975	-.008	.003	.016	.025	.033	.044	.056	.064	.077	.095	.113	.105	.094	.064	.052	.043	.030	.015
	1.000	-.024	-.003	.002	.025	.045	.050	.062	.112	.096	.113	.136	.120	.100	.075	.058	.044	.012	-.005

\*No crifice.

NACA



TABLE 9.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(2)(05.34) PROPELLER BLADE SECTION ( $x = 0.975$ ) - Continued

(d)  $N = 1600$  rpm.

$J$	1.922	2.046	2.125	2.190	2.291	2.368	2.458	2.469	2.427	2.344	2.262	2.168	2.108	2.010	1.956
$M_x$	.877	.896	.907	.915	.932	.943	.960	.961	.952	.938	.921	.909	.901	.884	.875
$\Delta \delta$	5.54	3.91	2.90	2.09	.86	-.06	-1.10	-1.22	-.74	.23	1.20	2.36	3.11	4.38	5.09
$\alpha_1$	.69	.51	.41	.30	.12	-.04	-.20	-.23	-.15	.01	.18	.34	.43	.56	.61
$\alpha_2$	3.68	2.72	2.13	1.56	.91	.41	-.15	-.34	.06	.54	1.11	1.80	2.27	2.91	3.24
$c_{m1}$	.4239	.3129	.2471	.1797	.1065	.0477	-.0171	-.0397	.0061	.0639	.1290	.2074	.2632	.3348	.3732
$c_{m2}$	-.0505	-.0453	-.0466	-.0401	-.0356	-.0323	-.0388	-.0377	-.0377	-.0398	-.0388	-.0436	-.0451	-.0456	-.0494
$c$					.0131	.0141	.0168	.0181	.0158	.0146					
$a/b$	Pressure coefficient, P														
Upper surface	0.000	1.207	1.217	1.223	1.227	1.236	1.242	1.252	1.252	1.248	1.239	1.230	1.224	1.220	1.206
	.025	-.760	-.569	-.407	-.218	-.019	.136	.268	.297	.225	.087	-.079	-.293	-.454	-.706
	.050	-.672	-.380	-.259	-.178	-.063	.039	.131	.149	.100	.006	-.097	-.217	-.284	-.609
	.100	-.685	-.473	-.396	-.306	-.233	-.161	-.081	-.066	-.107	-.186	-.297	-.327	-.421	-.617
	.200	-.522	-.472	-.398	-.337	-.294	-.248	-.189	-.173	-.211	-.265	-.299	-.349	-.407	-.487
	.300	-.461	-.367	-.302	-.286	-.262	-.260	-.257	-.253	-.260	-.221	-.250	-.293	-.302	-.382
	.400	-.463	-.362	-.326	-.303	-.272	-.259	-.287	-.284	-.290	-.265	-.277	-.310	-.327	-.409
	.500	-.450	-.379	-.347	-.320	-.292	-.269	-.294	-.289	-.274	-.275	-.291	-.330	-.349	-.413
	.600	-.443	-.437	-.405	-.365	-.338	-.315	-.321	-.337	-.305	-.323	-.338	-.369	-.404	-.412
	.700	-.436	-.459	-.427	-.394	-.379	-.362	-.352	-.370	-.347	-.367	-.376	-.389	-.406	-.357
	.800	-.403	-.309	-.396	-.440	-.431	-.409	-.384	-.390	-.389	-.415	-.430	-.432	-.344	-.372
	.900	-.259	-.202	-.148	-.095	-.075	-.095	-.152	-.165	-.114	-.075	-.073	-.119	-.171	-.222
	.950	-.073	-.005	.007	.032	.040	.031	.013	.005	.030	.043	.047	.080	-.004	-.060
Lower surface	.0375	.214	.092	-.007	-.112	-.208	-.261	-.309	-.325	-.306	-.252	-.191	-.082	.011	.166
	.075	.115	.020	-.055	-.127	-.241	-.345	-.445	-.470	-.436	-.380	-.384	-.306	-.039	.073
	.150	.077	.015	-.090	-.076	-.115	-.301	-.382	-.409	-.369	-.345	-.302	-.060	-.019	.022
	.250	-.072	-.117	-.146	-.177	-.209	-.166	-.391	-.421	-.381	-.399	-.388	-.162	-.135	-.088
	.350	-.036	-.087	-.086	-.108	-.127	-.123	-.265	-.308	-.328	-.328	-.314	-.099	-.079	-.048
	.450	-.081	-.104	-.120	-.138	-.153	-.157	-.170	-.282	-.317	-.315	-.341	-.130	-.114	-.089
	.550	-.067	-.087	-.109	-.121	-.137	-.142	-.099	-.137	-.121	-.138	-.124	-.112	-.096	-.073
	.650	-.063	-.106	-.122	-.145	-.171	-.183	-.154	-.138	-.173	-.176	-.148	-.131	-.114	-.088
	.750	-.094	-.117	-.133	-.157	-.190	-.236	-.233	-.216	-.244	-.207	-.163	-.139	-.123	-.098
	.850	-.045	-.054	-.064	-.089	-.114	-.136	-.212	-.210	-.177	-.122	-.091	-.071	-.057	-.046
	.925	.010	.013	.012	-.007	-.027	-.042	-.064	-.076	-.040	-.030	-.006	.007	.016	.010
	.975	.036	.053	.056	.038	.017	.004	-.012	-.020	0	.012	.035	.050	.054	.037
	1.000	.075	.073	.084	.087	.086	.096	.096	.080	.091	.090	.100	.094	.069	.101

\*No orifice.

<sup>b</sup>Lower surface only.



TABLE 9.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(2)(05.34) PROPELLER BLADE SECTION ( $x = 0.975$ ) - Continued

(a)  $M = 0.56$ .

	1.968	1.998	2.046	2.065	2.093	2.135	2.155	2.189	2.228	2.266	2.298	2.342	2.377	2.437	2.488	2.537	2.574
$J$	1.038	1.023	1.014	1.004	.996	.986	.973	.963	.957	.947	.938	.927	.915	.904	.893	.883	.875
$M_x$	4.93	4.53	3.91	3.66	3.31	2.77	2.52	2.10	1.62	1.16	.77	.25	-.16	-.86	-1.44	-1.98	-2.39
$\Delta h$	.52	.48	.42	.40	.36	.31	.28	.24	.19	.14	.10	.05	0	-.07	-.14	-.20	-.25
$\alpha$	2.69	2.55	2.35	2.14	1.92	1.70	1.44	1.20	.95	.65	.78	.65	.62	.50	.28	.06	-.10
$c_{m,n}$	.3094	.2932	.2704	.2465	.2213	.1955	.1665	.1394	.1100	.0994	.0919	.0765	.0723	.0581	.0326	.0071	-.0116
$c$	-.0670	-.0671	-.0662	-.0531	-.0483	-.0427	-.0302	-.0267	-.0283	-.0288	-.0325	-.0410	-.0495	-.0551	-.0594	-.0569	-.0580
$c$	.0268	.0272	.0275	.0263	.0255	.0244	.0215	.0186	.0165	.0150	.0144	.0136					
$a/b$	Pressure coefficient, $P$																
Upper surface	$a$ .000	1.295	1.289	1.283	1.277	1.273	1.267	1.259	1.254	1.251	1.243	1.239	1.233	1.227	1.221	1.215	1.210
	.025	-.311	-.317	-.298	-.279	-.243	-.190	-.146	-.106	-.047	-.008	.032	.081	.124	.190	.249	.307
	.050	-.193	-.179	-.136	-.135	-.130	-.126	-.125	-.112	-.084	-.066	-.046	-.021	.001	.040	.077	.113
	.100	-.293	-.289	-.283	-.276	-.268	-.242	-.236	-.211	-.203	-.206	-.203	-.191	-.174	-.142	-.110	-.083
	.200	-.313	-.315	-.305	-.312	-.304	-.290	-.286	-.267	-.280	-.278	-.266	-.257	-.223	-.186	-.164	-.149
	.300	-.322	-.327	-.313	-.310	-.295	-.288	-.291	-.289	-.280	-.279	-.259	-.229	-.244	-.237	-.217	-.207
	.400	-.296	-.299	-.288	-.292	-.288	-.285	-.288	-.288	-.280	-.270	-.265	-.248	-.225	-.225	-.217	-.212
	.500	-.313	-.319	-.307	-.311	-.303	-.300	-.301	-.299	-.288	-.279	-.275	-.263	-.269	-.268	-.256	-.246
	.600	-.354	-.362	-.352	-.357	-.356	-.356	-.357	-.358	-.345	-.332	-.329	-.330	-.337	-.331	-.313	-.307
	.700	-.400	-.411	-.402	-.410	-.407	-.405	-.406	-.403	-.385	-.378	-.366	-.372	-.367	-.343	-.304	-.264
	.800	-.424	-.434	-.428	-.436	-.435	-.433	-.427	-.417	-.416	-.415	-.415	-.416	-.403	-.349	-.296	-.269
Lower surface	.900	-.587	-.609	-.608	-.619	-.617	-.593	-.414	-.241	-.166	-.108	-.087	-.064	-.078	-.118	-.135	-.149
	.950	-.630	-.653	-.633	-.580	-.245	-.175	-.112	-.059	-.025	.012	.038	.062	.059	.035	.026	.010
	.0375	.208	.176	.144	.104	.063	.020	-.026	-.060	-.108	-.143	-.183	-.231	-.287	-.377	-.470	-.572
	.075	.097	.066	.037	0	-.035	-.063	-.096	-.144	-.210	-.247	-.274	-.286	-.282	-.263	-.229	-.177
	.150	.105	.083	.064	.036	.010	-.013	-.043	-.063	-.084	-.093	-.099	-.108	-.119	-.120	-.115	-.140
	.250	-.075	-.095	-.110	-.135	-.154	-.169	-.189	-.203	-.218	-.228	-.227	-.219	-.219	-.257	-.241	-.253
	.350	-.028	-.042	-.048	-.065	-.074	-.081	-.096	-.105	-.112	-.118	-.119	-.121	-.121	-.141	-.137	-.143
	.450	-.067	-.079	-.083	-.099	-.105	-.110	-.124	-.129	-.134	-.137	-.137	-.139	-.136	-.140	-.137	-.141
	.550	-.043	-.057	-.060	-.075	-.084	-.093	-.107	-.116	-.125	-.130	-.131	-.129	-.128	-.122	-.115	-.111
	.650	-.101	-.116	-.119	-.134	-.141	-.148	-.160	-.165	-.170	-.172	-.171	-.162	-.149	-.131	-.118	-.115
	.750	-.172	-.187	-.192	-.205	-.211	-.219	-.228	-.237	-.242	-.233	-.205	-.179	-.154	-.121	-.106	-.102
	.850	-.193	-.211	-.214	-.229	-.237	-.245	-.256	-.259	-.234	-.163	-.133	-.102	-.072	-.042	-.027	-.024
	.925	-.174	-.191	-.197	-.211	-.216	-.225	-.230	-.188	-.116	-.075	-.041	-.008	.024	.059	.061	.062
	.975	-.255	-.276	-.284	-.299	-.307	-.310	-.278	-.174	-.094	-.041	-.004	.040	.069	.093	.105	.108
	1.000	-.305	-.324	-.333	-.322	-.315	-.328	-.283	-.160	-.072	-.020	.009	.072	.112	.109	.125	.120

<sup>a</sup>No orifice.<sup>b</sup>Lower surface only.

NACA

TABLE 9.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(2)(05.34) PROPELLER BLADE SECTION ( $x = 0.975$ ) - Continued

( $r$ )  $M = 0.60$ .

$J$	2.004	2.043	2.063	2.092	2.126	2.151	2.177	2.201	2.235	2.271	2.299	2.335	2.363	2.410	2.439	2.481	2.536
$M_x$	1.101	1.087	1.076	1.067	1.056	1.048	1.039	1.032	1.023	1.013	1.004	.995	.979	.975	.965	.955	.949
$a_{x1}$	4.46	3.95	3.69	3.32	2.89	2.57	2.25	1.95	1.54	1.10	.76	.33	0	-.55	-.88	-1.35	-1.97
$\Delta B$	.29	.24	.21	.17	.13	.10	.06	.04	-.01	-.04	-.07	-.11	-.14	-.18	-.21	-.24	-.30
$\alpha_1$	2.25	2.19	2.05	1.95	1.68	1.55	1.46	1.31	1.15	.90	.69	.52	.33	.14	-.01	-.21	-.44
$\alpha_H$	.2587	.2523	.2368	.2245	.1932	.1794	.1687	.1526	.1332	.1052	.0800	.0610	.0390	.0165	-.0013	-.0245	-.0519
$\alpha_m$	-.0583	-.0516	-.0569	-.0570	-.0574	-.0555	-.0544	-.0543	-.0527	-.0468	-.0399	-.0382	-.0356	-.0391	-.0376	-.0450	-.0519
$\alpha_o$	.0284	.0291	.0292	.0299	.0302	.0306	.0304	.0304	.0301	.0296	.0276	.0268	.0251	.0224	.0190	.0164	.0146
$c/b$	Pressure coefficient, $P$																
Upper surface	$a_{0.000}$	1.341	1.331	1.324	1.318	1.310	1.305	1.296	1.292	1.289	1.283	1.277	1.272	1.263	1.260	1.254	1.249
	$a_{0.025}$	-.096	-.087	-.069	-.029	.004	.023	.049	.082	.132	.174	.208	.242	.265	.283	.313	.339
	$a_{0.050}$	.017	.033	.044	.015	.053	.051	.050	.058	.080	.103	.100	.138	.146	.175	.188	.212
	$a_{0.100}$	-.120	-.116	-.105	-.094	-.077	-.072	-.068	-.051	-.028	-.027	-.029	-.024	-.025	-.004	.002	.019
	$a_{0.200}$	-.159	-.159	-.157	-.164	-.140	-.140	-.141	-.139	-.131	-.127	-.135	-.119	-.123	-.109	-.110	-.093
	$a_{0.300}$	-.195	-.193	-.181	-.174	-.175	-.179	-.184	-.186	-.185	-.189	-.196	-.194	-.195	-.176	-.181	-.186
	$a_{0.400}$	-.163	-.161	-.152	-.155	-.164	-.165	-.169	-.164	-.160	-.160	-.172	-.174	-.187	-.188	-.199	-.200
	$a_{0.500}$	-.172	-.172	-.164	-.171	-.179	-.183	-.187	-.184	-.177	-.156	-.182	-.182	-.197	-.202	-.211	-.218
	$a_{0.600}$	-.221	-.220	-.215	-.222	-.232	-.236	-.238	-.237	-.231	-.229	-.227	-.228	-.237	-.237	-.246	-.259
	$a_{0.700}$	-.265	-.267	-.266	-.272	-.282	-.284	-.286	-.283	-.276	-.268	-.269	-.268	-.275	-.269	-.277	-.281
	$a_{0.800}$	-.288	-.286	-.288	-.296	-.299	-.302	-.303	-.298	-.289	-.288	-.291	-.292	-.303	-.298	-.308	-.306
	$a_{0.900}$	-.437	-.447	-.453	-.462	-.465	-.469	-.469	-.466	-.461	-.461	-.466	-.469	-.447	-.298	-.171	-.090
	$a_{0.950}$	-.480	-.488	-.495	-.503	-.507	-.510	-.513	-.509	-.490	-.387	-.184	-.092	-.024	-.035	.068	.100
Lower surface	$a_{0.0375}$	.285	.262	.242	.220	.164	.140	.111	.087	.058	.028	.002	-.033	-.081	-.134	-.192	-.268
	$a_{0.075}$	.179	.151	.125	.077	-.041	-.103	-.156	-.195	-.232	-.269	-.303	-.333	-.375	-.410	-.459	-.504
	$a_{0.150}$	.194	.174	.158	.140	.099	.086	.073	.056	.006	-.055	-.121	-.164	-.202	-.240	-.290	-.328
	$a_{0.250}$	.040	.023	.011	-.002	-.040	-.055	-.068	-.074	-.072	-.099	-.150	-.191	-.230	-.264	-.244	-.344
	$a_{0.350}$	.067	.055	.048	.030	-.001	-.014	-.025	-.029	-.027	-.026	-.031	-.045	-.077	-.139	-.175	-.230
	$a_{0.450}$	.011	.006	.005	-.014	-.029	-.038	-.046	-.051	-.051	-.052	-.054	-.039	-.032	-.028	-.044	-.102
	$a_{0.550}$	.027	.023	.021	.003	-.013	-.021	-.032	-.034	-.037	-.042	-.045	-.035	-.036	-.019	-.020	-.013
	$a_{0.650}$	-.014	-.017	-.021	-.039	-.053	-.063	-.071	-.074	-.075	-.083	-.088	-.086	-.092	-.081	-.080	-.069
	$a_{0.750}$	.077	-.081	-.085	-.099	-.117	-.126	-.133	-.138	-.141	-.149	-.158	-.160	-.170	-.163	-.165	-.146
	$a_{0.850}$	-.099	-.104	-.110	-.123	-.144	-.152	-.159	-.164	-.167	-.177	-.184	-.190	-.200	-.189	-.181	-.104
	$a_{0.925}$	-.088	-.093	-.101	-.114	-.135	-.143	-.152	-.157	-.161	-.169	-.178	-.184	-.189	-.194	-.042	.025
	$a_{0.975}$	-.158	-.169	-.181	-.196	-.216	-.225	-.236	-.242	-.246	-.252	-.252	-.236	-.190	-.054	.024	.069
	$a_{1.000}$	-.220	-.230	-.232	-.270	-.297	-.303	-.307	-.315	-.323	-.312	-.210	-.175	-.010	.025	.120	.150

<sup>a</sup>No orifice.

NACA

TABLE 9.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(2)(05.34) PROPELLER BLADE SECTION ( $x = 0.975$ ) - Continued

(g)  $M = 0.64$

$\gamma$	1.969	2.024	2.043	2.074	2.098	2.128	2.148	2.177	2.206	2.235	2.263	2.296	2.326	2.359	2.387	2.428
$\alpha_x$	1.184	1.172	1.160	1.149	1.141	1.130	1.118	1.108	1.099	1.091	1.082	1.072	1.063	1.054	1.043	1.032
$\Delta S$	4.65	4.19	3.95	3.93	3.84	2.86	2.61	2.25	1.89	1.53	1.19	.80	.44	.05	-.28	-.75
$\alpha_1$	2.14	2.08	1.93	1.76	1.60	1.48	1.33	1.20	1.08	.92	.77	.61	.44	.32	.12	-.10
$\alpha_2$	.2462	.2387	.2213	.2035	.1842	.1703	.1532	.1387	.1252	.1061	.0894	.0713	.0516	.0368	.0139	-.0216
$\alpha_m$	-.0515	-.0531	-.0530	-.0533	-.0517	-.0506	-.0498	-.0486	-.0487	-.0467	-.0468	-.0497	-.0475	-.0480	-.0453	-.0396
$\alpha_0$	.0278	.0282	.0283	.0281	.0288	.0289	.0288	.0293	.0295	.0291	.0290	.0292	.0293	.0299	.0305	.0312
$a/b$	Pressure coefficient, $P$															
Upper surface	$\alpha = 0.000$	1.400	1.390	1.382	1.373	1.368	1.360	1.351	1.345	1.339	1.333	1.327	1.320	1.315	1.309	1.295
	.025	-.044	-.048	-.059	-.063	-.067	-.073	-.079	-.083	-.087	-.091	-.095	-.099	-.103	-.107	-.111
	.050	-.059	-.072	-.085	-.101	-.106	-.106	-.108	-.110	-.113	-.120	-.134	-.155	-.165	-.169	-.181
	.100	-.078	-.076	-.075	-.062	-.053	-.047	-.033	-.023	-.014	-.008	.011	.021	.018	.013	.003
	.200	-.127	-.130	-.132	-.124	-.121	-.123	-.121	-.121	-.123	-.124	-.117	-.108	-.112	-.119	-.108
	.300	-.162	-.168	-.170	-.160	-.163	-.170	-.174	-.179	-.182	-.185	-.182	-.174	-.182	-.191	-.185
	.400	-.133	-.138	-.140	-.136	-.142	-.150	-.155	-.161	-.166	-.170	-.170	-.168	-.178	-.191	-.193
	.500	-.142	-.150	-.153	-.149	-.156	-.164	-.168	-.174	-.179	-.184	-.183	-.182	-.194	-.206	-.213
	.600	-.168	-.199	-.200	-.197	-.206	-.215	-.220	-.225	-.231	-.236	-.235	-.248	-.260	-.268	-.272
	.700	-.232	-.244	-.246	-.244	-.253	-.260	-.264	-.266	-.270	-.273	-.271	-.270	-.284	-.298	-.308
Lower surface	.800	-.253	-.261	-.264	-.264	-.271	-.278	-.280	-.284	-.284	-.284	-.278	-.280	-.296	-.307	-.316
	.900	-.355	-.413	-.419	-.421	-.431	-.439	-.441	-.445	-.447	-.445	-.445	-.464	-.478	-.490	-.500
	.950	-.432	-.453	-.459	-.461	-.471	-.479	-.481	-.485	-.488	-.490	-.489	-.493	-.509	-.522	-.533
	.0375	.317	.293	.263	.239	.210	.182	.155	.129	.104	.077	.051	.027	-.002	-.034	-.078
	.075	.214	.197	.146	.075	.004	-.050	-.089	-.123	-.153	-.183	-.213	-.244	-.275	-.307	-.344
	.150	.226	.212	.192	.182	.167	.145	.096	.048	.013	-.020	-.061	-.096	-.128	-.163	-.205
	.250	.066	.052	.032	.020	-.004	-.023	-.041	-.066	-.089	-.109	-.131	-.154	-.185	-.219	-.252
	.350	.080	.064	.047	.038	.016	-.005	-.021	-.034	-.049	-.067	-.082	-.094	-.122	-.151	-.181
	.450	.028	.014	.002	-.002	-.021	-.038	-.051	-.062	-.070	-.084	-.099	-.112	-.131	-.158	-.189
	.550	.043	.029	.017	.015	-.002	-.019	-.030	-.042	-.049	-.054	-.059	-.075	-.104	-.131	-.150
No orifice.	.650	.002	-.013	-.021	-.023	-.043	-.059	-.071	-.082	-.091	-.098	-.095	-.096	-.127	-.158	-.185
	.750	-.060	-.074	-.082	-.085	-.104	-.121	-.133	-.144	-.153	-.161	-.162	-.158	-.172	-.202	-.240
	.850	-.085	-.100	-.106	-.112	-.130	-.147	-.159	-.170	-.179	-.189	-.192	-.192	-.203	-.224	-.245
	.925	-.072	-.086	-.094	-.100	-.119	-.135	-.147	-.158	-.168	-.177	-.180	-.185	-.199	-.221	-.249
	.975	-.138	-.157	-.166	-.173	-.194	-.209	-.223	-.236	-.248	-.260	-.267	-.273	-.287	-.290	-.311
	1.000	-.310	-.348	-.316	-.335	-.365	-.340	-.357	-.392	-.400	-.407	-.351	-.375	-.382	-.414	-.466

No orifice.



TABLE 10.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(07.50) PROPELLER BLADE SECTION ( $x = 0.85$ )

$$[\beta_{0.75R} = 45^\circ; \beta_x = 41.5^\circ; B = 1]$$

(a) One-blade propeller;  $N = 1500$  rpm.

$J$	2.053	2.003	1.935	1.890	1.850	1.786	1.728	1.691	1.627	1.680	
$M_T$	.751	.742	.728	.722	.721	.709	.699	.697	.690	.696	
$a_{T1}$	3.75	4.43	5.37	6.01	6.59	7.52	8.39	8.96	9.95	9.13	
$\Delta\delta$	.31	.36	.41	.44	.48	.52	.55	.57	.59	.57	
$a_1$	1.49	1.64	1.89	2.10	2.23	2.48	2.56	2.61	2.52	2.57	
$c_n$	.4794	.5297	.6135	.6813	.7245	.7994	.8316	.8439	.8174	.8290	
$c_m$	-.0257	-.0247	-.0198	-.0144	-.0111	-.0057	-.0011	.0041	-.0088	.0033	
$c_o$											
$c/b$	Pressure coefficient, P										
Upper surface	$a_{0.000}$	1.150	1.146	1.140	1.138	1.137	1.132	1.128	1.128	1.125	1.127
	.025	-.696	-.940	-1.304	-1.463	-1.566	-1.747	-1.893	-1.989	-1.954	-1.962
	.050	-.722	-.923	-1.207	-1.406	-1.542	-1.773	-1.897	-1.971	-1.608	-1.772
	.100	-.476	-.501	-.789	-1.198	-1.334	-1.571	-1.702	-1.818	-1.249	-1.865
	$a_{.200}$	-.396	-.421	-.460	-.539	-.631	-.902	-.914	-.876	-.795	-.790
	.300	-.340	-.366	-.390	-.406	-.410	-.402	-.383	-.391	-.358	-.392
	.400	-.313	-.329	-.340	-.350	-.350	-.348	-.325	-.322	-.374	-.310
	.500	-.279	-.288	-.288	-.293	-.290	-.282	-.256	-.248	-.242	-.228
	.600	-.233	-.236	-.230	-.229	-.220	-.207	-.179	-.165	-.137	-.143
	.700	-.148	-.147	-.134	-.129	-.117	-.101	-.074	-.058	-.052	-.035
Lower surface	.800	.012	.012	.027	.032	.042	.049	.070	.078	.015	.093
	.900	.225	.220	.219	.206	.207	.204	.217	.205	.071	.199
	.950	.313	.293	.283	.256	.255	.253	.267	.243	.098	.230
	.0375	.552	.618	.701	.735	.770	.823	.870	.886	.901	.900
	.075	.466	.520	.589	.618	.650	.700	.743	.760	.777	.773
	.150	.371	.414	.470	.493	.521	.564	.604	.619	.631	.630
	.250	.297	.334	.381	.398	.422	.459	.496	.507	.517	.518
	.350	.255	.291	.328	.340	.360	.393	.429	.438	.444	.450
	.450	.213	.256	.284	.290	.307	.319	.354	.363	.372	.409
	.550	.177	.202	.231	.241	.256	.280	.309	.312	.304	.319
.650	.140	.165	.190	.198	.211	.230	.257	.257	.238	.263	
.750	.151	.166	.187	.189	.200	.215	.239	.234	.202	.236	
.850	.188	.195	.212	.210	.217	.227	.247	.234	.181	.233	
$a_{.925}$	.249	.246	.260	.259	.260	.261	.275	.264	.175	.250	
$a_{.975}$	.308	.309	.310	.304	.301	.305	.300	.268	.171	.273	
$a_{1.000}$	.344	.359	.344	.335	.330	.330	.330	.319	.299	.175	.290

No orifice.

NACA

TABLE 10. -PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-(3)(07.50) PROPELLER BLADE SECTION ( $x = 0.85$ ) - Continued(b) One-blade propeller;  $M = 0.57$ .

$\frac{J}{M}$ $\frac{C_L}{C_D}$ $\frac{C_M}{C_D}$ $\frac{C_{M^2}}{C_D}$ $\frac{C_{M^3}}{C_D}$	2.456 .846 -1.30 -.05 .24 .0768 -.0649	2.349 .868 -.04 .05 .73 .1729 -.0593 .0185	2.286 .877 .74 .11 .70 .2271 -.0585 .0206	2.239 .892 1.32 .16 .77 .2503 -.0511 .0220	2.190 .902 1.94 .21 .85 .2748 -.0408 .0236	2.159 .910 2.34 .24 .90 .2929 -.0398 .0234	2.136 .916 2.64 .26 .97 .3129 -.0408 .0246	2.106 .919 3.04 .29 1.07 .3439 -.0449 .0253	2.081 .924 3.37 .31 1.15 .3710 -.0534 .0263	2.063 .929 3.61 .33 1.27 .4090 -.0641 .0265	2.042 .940 3.89 .35 1.36 .4394 -.0714 .0301	2.017 .942 4.24 .37 1.46 .4697 -.0793 .0310	2.000 .952 4.47 .41 1.53 .4955 -.0878 .0326	1.978 .958 4.77 .43 1.61 .5219 -.0932 .0332	1.958 .964 5.05 .43 1.67 .5390 -.1012 .0334	1.938 .971 5.33 .46 1.76 .5710 -.1102 .0349	1.921 .976 5.57 .47 1.83 .5942 -.1206 .0359	1.900 .983 5.87 .49 1.87 .6071 -.1224 .0375	
c/b	Pressure coefficient, P																		
Upper surface	.0000 .025 .050 .075 .100 .125 .150 .175 .200 .225 .250 .275 .300 .325 .350 .375 .400 .425 .450 .475 .500 .525 .550 .575 .600 .625 .650 .675 .700 .725 .750 .775 .800 .825 .850 .875 .900 .925 .950 .975 1.000	1.191 .325 .149 -.028 -.170 -.277 -.418 -.474 -.533 -.632 -.717 -.836 -.939 1.039 1.139	1.203 .383 .031 -.113 -.235 -.343 -.451 -.551 -.607 -.717 -.816 -.920 1.020 1.120	1.206 .310 -.030 -.161 -.285 -.391 -.484 -.581 -.640 -.712 -.810 -.910 1.010 1.110	1.215 .259 -.079 -.190 -.310 -.417 -.513 -.621 -.692 -.771 -.863 -.963 1.063 1.163	1.220 .213 -.134 -.266 -.390 -.486 -.569 -.644 -.711 -.809 -.909 1.009 1.109	1.224 .172 -.173 -.266 -.390 -.486 -.569 -.644 -.711 -.809 -.909 1.009 1.109	1.228 .143 -.163 -.284 -.406 -.493 -.569 -.644 -.711 -.809 -.909 1.009 1.109	1.229 .126 -.144 -.314 -.410 -.500 -.582 -.657 -.719 -.815 -.915 1.015 1.115	1.232 .108 -.144 -.336 -.420 -.503 -.587 -.661 -.720 -.815 -.915 1.015 1.115	1.234 .110 -.104 -.358 -.425 -.500 -.582 -.661 -.717 -.815 -.915 1.015 1.115	1.241 .110 -.104 -.358 -.425 -.500 -.582 -.663 -.722 -.817 -.917 1.017 1.117	1.242 .109 -.086 -.373 -.440 -.508 -.582 -.663 -.722 -.817 -.917 1.017 1.117	1.247 .112 -.067 -.382 -.455 -.522 -.595 -.663 -.722 -.817 -.917 1.017 1.117	1.250 .115 -.052 -.392 -.474 -.532 -.594 -.663 -.722 -.817 -.917 1.017 1.117	1.254 .122 -.036 -.401 -.473 -.532 -.594 -.663 -.722 -.817 -.917 1.017 1.117	1.258 .129 -.020 -.411 -.480 -.539 -.594 -.663 -.722 -.817 -.917 1.017 1.117	1.261 .136 -.005 -.414 -.480 -.539 -.594 -.663 -.722 -.817 -.917 1.017 1.117	1.265 .148 .011 -.418 -.484 -.541 -.599 -.666 -.723 -.818 -.918 1.018 1.118
	Lower surface	.0375 .075 .110 .150 .190 .230 .270 .310 .350 .390 .430 .470 .510 .550 .590 .630 .670 .710 .750 .790 .830 .870 .910 .950 .990 1.030 1.070 1.110 1.150 1.190 1.230 1.270 1.310 1.350 1.390 1.430 1.470 1.510 1.550 1.590 1.630 1.670 1.710 1.750 1.790 1.830 1.870 1.910 1.950 1.990 2.030 2.070 2.110 2.150 2.190 2.230 2.270 2.310 2.350 2.390 2.430 2.470 2.510 2.550 2.590 2.630 2.670 2.710 2.750 2.790 2.830 2.870 2.910 2.950 2.990 3.030 3.070 3.110 3.150 3.190 3.230 3.270 3.310 3.350 3.390 3.430 3.470 3.510 3.550 3.590 3.630 3.670 3.710 3.750 3.790 3.830 3.870 3.910 3.950 3.990 4.030 4.070 4.110 4.150 4.190 4.230 4.270 4.310 4.350 4.390 4.430 4.470 4.510 4.550 4.590 4.630 4.670 4.710 4.750 4.790 4.830 4.870 4.910 4.950 4.990 5.030 5.070 5.110 5.150 5.190 5.230 5.270 5.310 5.350 5.390 5.430 5.470 5.510 5.550 5.590 5.630 5.670 5.710 5.750 5.790 5.830 5.870 5.910 5.950 5.990 6.030 6.070 6.110 6.150 6.190 6.230 6.270 6.310 6.350 6.390 6.430 6.470 6.510 6.550 6.590 6.630 6.670 6.710 6.750 6.790 6.830 6.870 6.910 6.950 6.990 7.030 7.070 7.110 7.150 7.190 7.230 7.270 7.310 7.350 7.390 7.430 7.470 7.510 7.550 7.590 7.630 7.670 7.710 7.750 7.790 7.830 7.870 7.910 7.950 7.990 8.030 8.070 8.110 8.150 8.190 8.230 8.270 8.310 8.350 8.390 8.430 8.470 8.510 8.550 8.590 8.630 8.670 8.710 8.750 8.790 8.830 8.870 8.910 8.950 8.990 9.030 9.070 9.110 9.150 9.190 9.230 9.270 9.310 9.350 9.390 9.430 9.470 9.510 9.550 9.590 9.630 9.670 9.710 9.750 9.790 9.830 9.870 9.910 9.950 9.990 10.030 10.070 10.110 10.150 10.190 10.230 10.270 10.310 10.350 10.390 10.430 10.470 10.510 10.550 10.590 10.630 10.670 10.710 10.750 10.790 10.830 10.870 10.910 10.950 10.990 11.030 11.070 11.110 11.150 11.190 11.230 11.270 11.310 11.350 11.390 11.430 11.470 11.510 11.550 11.590 11.630 11.670 11.710 11.750 11.790 11.830 11.870 11.910 11.950 11.990 12.030 12.070 12.110 12.150 12.190 12.230 12.270 12.310 12.350 12.390 12.430 12.470 12.510 12.550 12.590 12.630 12.670 12.710 12.750 12.790 12.830 12.870 12.910 12.950 12.990 13.030 13.070 13.110 13.150 13.190 13.230 13.270 13.310 13.350 13.390 13.430 13.470 13.510 13.550 13.590 13.630 13.670 13.710 13.750 13.790 13.830 13.870 13.910 13.950 13.990 14.030 14.070 14.110 14.150 14.190 14.230 14.270 14.310 14.350 14.390 14.430 14.470 14.510 14.550 14.590 14.630 14.670 14.710 14.750 14.790 14.830 14.870 14.910 14.950 14.990 15.030 15.070 15.110 15.150 15.190 15.230 15.270 15.310 15.350 15.390 15.430 15.470 15.510 15.550 15.590 15.630 15.670 15.710 15.750 15.790 15.830 15.870 15.910 15.950 15.990 16.030 16.070 16.110 16.150 16.190 16.230 16.270 16.310 16.350 16.390 16.430 16.470 16.510 16.550 16.590 16.630 16.670 16.710 16.750 16.790 16.830 16.870 16.910 16.950 16.990 17.030 17.070 17.110 17.150 17.190 17.230 17.270 17.310 17.350 17.390 17.430 17.470 17.510 17.550 17.590 17.630 17.670 17.710 17.750 17.790 17.830 17.870 17.910 17.950 17.990 18.030 18.070 18.110 18.150 18.190 18.230 18.270 18.310 18.350 18.390 18.430 18.470 18.510 18.550 18.590 18.630 18.670 18.710 18.750 18.790 18.830 18.870 18.910 18.950 18.990 19.030 19.070 19.110 19.150 19.190 19.230 19.270 19.310 19.350 19.390 19.430 19.470 19.510 19.550 19.590 19.630 19.670 19.710 19.750 19.790 19.830 19.870 19.910 19.950 19.990 20.030 20.070 20.110 20.150 20.190 20.230 20.270 20.310 20.350 20.390 20.430 20.470 20.510 20.550 20.590 20.630 20.670 20.710 20.750 20.790 20.830 20.870 20.910 20.950 20.990 21.030 21.070 21.110 21.150 21.190 21.230 21.270 21.310 21.350 21.390 21.430 21.470 21.510 21.550 21.590 21.630 21.670 21.710 21.750 21.790 21.830 21.870 21.910 21.950 21.990 22.030 22.070 22.110 22.150 22.190 22.230 22.270 22.310 22.350 22.390 22.430 22.470 22.510 22.550 22.590 22.630 22.670 22.710 22.750 22.790 22.830 22.870 22.910 22.950 22.990 23.030 23.070 23.110 23.150 23.190 23.230 23.270 23.310 23.350 23.390 23.430 23.470 23.510 23.550 23.590 23.630 23.670 23.710 23.750 23.790 23.830 23.870 23.910 23.950 23.990 24.030 24.070 24.110 24.150 24.190 24.230 24.270 24.310 24.350 24.390 24.430 24.470 24.510 24.550 24.590 24.630 24.670 24.710 24.750 24.790 24.830 24.870 24.910 24.950 24.990 25.030 25.070 25.110 25.150 25.190 25.230 25.270 25.310 25.350 25.390 25.430 25.470 25.510 25.550 25.590 25.630 25.670 25.710 25.750 25.790 25.830 25.870 25.910 25.950 25.990 26.030 26.070 26.110 26.150 26.190 26.230 26.270 26.310 26.350 26.390 26.430 26.470 26.510 26.550 26.590 26.630 26.670 26.710 26.750 26.790 26.830 26.870 26.910 26.950 26.990 27.030 27.070 27.110 27.150 27.190 27.230 27.270 27.310 27.350 27.390 27.430 27.470 27.510 27.550 27.590 27.630 27.670 27.710 27.750 27.790 27.830 27.870 27.910 27.950 27.990 28.030 28.070 28.110 28.150 28.190 28.230 28.270 28.310 28.350 28.390 28.430 28.470 28.510 28.550 28.590 28.630 28.670 28.710 28.750 28.790 28.830 28.870 28.910 28.950 28.990 29.030 29.070 29.110 29.150 29.190 29.230 29.270 29.310 29.350 29.390 29.430 29.470 29.510 29.550 29.590 29.630 29.670 29.710 29.750 29.790 29.830 29.870 29.910 29.950 29.990 30.030 30.070 30.110 30.150 30.190 30.230 30.270 30.310 30.350 30.390 30.430 30.470 30.510 30.550 30.590 30.630 30.670 30.710 30.750 30.790 30.830 30.870 30.910 30.950 30.990 31.030 31.070 31.110 31.150 31.190 31.230 31.270 31.310 31.350 31.390 31.430 31.470 31.510 31.550 31.590 31.630 31.670 31.710 31.750 31.790 31.830 31.870 31.910 31.950 31.990 32.030 32.070 32.110 32.150 32.190 32.230 32.270 32.310 32.350 32.390 32.430 32.470 32.510 32.550 32.590 32.630 32.670 32.710 32.750 32.790 32.830 32.870 32.910 32.950 32.990 33.030 33.070 33.110 33.150 33.190 33.230 33.270 33.310 33.350 33.390 33.430 33.470 33.510 33.550 33.590 33.630 33.670 33.710 33.750 33.790 33.830 33.870 33.910 33.950 33.990 34.030 34.070 34.110 34.150 34.190 34.230 34.270 34.310 34.350 34.390 34.430 34.470 34.510 34.550 34.590 34.630 34.670 34.710 34.750 34.790 34.830 34.870 34.910 34.950 34.990 35.030 35.070 35.110 35.150 35.190 35.230 35.270 35.310 35.350 35.390 35.430 35.470 35.510 35.550 35.590 35.630 35.670 35.710 35.750 35.790 35.830 35.870 35.910 35.950 35.990 36.030 36.070 36.110 36.150 36.190 36.230 36.270 36.310 36.350 36.390 36.430 36.470 36.510 36.550 36.590 36.630 36.670 36.710 36.750 36.790 36.830 36.870 36.910 36.950 36.990 37.030 37.070 37.110 37.150 37.190 37.230 37.270 37.310 37.350 37.390 37.430 37.470 37.510 37.550 37.590 37.630 37.670 37.710 37.750 37.790 37.830 37.870 37.910 37.950 37.990 38.030 38.070 38.110 38.150 38.190 38.230 38.270 38.310 38.350 38.390 38.430 38.470 38.510 38.550 38.590 38.630 38.670 38.710 38.750 38.790 38.830 38.870 38.910 38.950 38.990 39.030 39.070 39.110 39.150 39.190 39.230 39.270 39.310 39.350 39.390 39.430 39.470 39.510 39.550 39.590 39.630 39.670 39.710 39.750 39.790 39.830 39.870 39.910 39.950 39.990 40.030 40.070 40.110 40.150 40.190 40.230 40.270 40.310 40.350 40.390 40.430 40.470 40.510 40.550 40.590 40.630 40.670 40.710 40.750 40.790 40.830 40.870 40.910 40.950 40.990 41.030 41.070 41.110 41.150 41.190 41.230 41.270 41.310 41.350 41.390 41.430 41.470 41.510 41.550 41.590 41.630 41.670 41.710 41.750 41.790 41.830 41.870 41.910 41.950 41.990 42.030 42.070 42.110 42.150 42.190 42.230 42.270 42.310 42.350 42.390 42.430 42.470 42.510 42.550 42.590 42.630 42.670 42.710 42.750 42.790 42.830 42.870 42.910 42.950 42.990 43.030 43.070 43.110 43.150 43.190 43.230 43.270 43.310 43.350 43.390 43.430 43.470 43.510 43.550 43.590 43.630 43.670 43.710 43.750 43.790 43.830 43.870 43																	

TABLE 10.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(07.50) PROPELLER BLADE SECTION ( $\alpha = 0.85$ ) - Continued

(c) One-blade propeller;  $M = 0.59$ .

J	2.479	2.403	2.333	2.275	2.202	2.143	2.075	2.061	2.037	2.002	1.978	1.960	1.946	1.929	1.906
$M_{\infty}$	.872	.887	.901	.919	.931	.946	.964	.973	.975	.981	.988	.994	.998	1.008	1.015
$\alpha_{\infty}$	-1.57	0	.16	.07	1.79	2.55	3.45	3.64	3.96	4.44	4.77	5.02	5.22	5.46	5.78
$\Delta\theta$	-.07	.35	.07	.12	.20	.25	.32	.33	.35	.39	.41	.43	.44	.46	.49
$\alpha_1$	.22	.35	.50	.65	.88	1.08	1.29	1.40	1.52	1.62	1.71	1.76	1.84	1.89	1.98
$c_m$	.0716	.1150	.1613	.2110	.2658	.3490	.4174	.4523	.4890	.5213	.5503	.5700	.5950	.6130	.6410
$c_{m,c}$	-.0734	-.0744	-.0670	-.0662	-.0705	-.0782	-.0949	-.1039	-.1241	-.1257	-.1331	-.1468	-.1549	-.1605	-.1729
$c_c$	.0147	.0191	.0242	.0285	.0305	.0338	.0383	.0404	.0429	.0444	.0454	.0461	.0480	.0485	.0484
c/b	Pressure coefficient, P														
Upper surface	a <sub>0</sub> .000	1.204	1.212	1.220	1.229	1.235	1.244	1.254	1.259	1.260	1.264	1.268	1.272	1.274	1.280
	.025	.516	.532	.547	.554	.568	.580	.606	.615	.624	.632	.638	.647	.661	.684
	.050	-.200	-.165	-.127	-.091	-.055	-.022	.022	.037	.052	.068	.081	.095	.110	.143
	.100	.028	-.024	-.060	-.101	-.143	-.193	-.242	-.253	-.256	-.286	-.305	-.313	-.318	-.332
	b <sub>0</sub> .200	-.091	-.127	-.180	-.199	-.262	-.320	-.331	-.330	-.350	-.360	-.410	-.414	-.415	-.440
	.300	-.235	-.271	-.302	-.336	-.381	-.410	-.416	-.417	-.414	-.435	-.458	-.461	-.462	-.463
	.400	-.375	-.394	-.400	-.441	-.465	-.488	-.508	-.505	-.506	-.509	-.504	-.494	-.481	-.445
	.500	-.459	-.490	-.499	-.514	-.551	-.560	-.571	-.575	-.580	-.587	-.593	-.593	-.591	-.588
	.600	-.537	-.566	-.580	-.590	-.615	-.637	-.636	-.633	-.636	-.651	-.659	-.658	-.656	-.648
	.700	-.697	-.690	-.699	-.707	-.719	-.730	-.739	-.736	-.733	-.738	-.738	-.734	-.732	-.722
	.800	-.162	-.153	-.167	-.201	-.220	-.269	-.366	-.464	-.648	-.701	-.718	-.715	-.703	-.687
Lower surface	.900	.032	-.047	-.099	-.157	-.210	-.240	-.305	-.332	-.357	-.371	-.410	-.479	-.579	-.764
	.950	.092	-.004	-.073	-.143	-.185	-.238	-.302	-.328	-.351	-.363	-.392	-.434	-.463	-.494
	a <sub>0</sub> .0375	-.630	-.456	-.266	-.103	.046	.145	.251	.283	.309	.357	.380	.403	.432	.489
	.075	-.598	-.400	-.230	-.091	.030	.110	.201	.229	.252	.294	.312	.334	.359	.410
	.150	-.365	-.162	-.121	-.052	.027	.087	.157	.179	.199	.229	.245	.264	.283	.322
	.250	-.178	-.170	-.129	-.085	-.023	.025	.084	.104	.121	.152	.161	.178	.198	.239
	b <sub>0</sub> .350	-.100	-.106	-.110	-.079	-.050	0	.070	.061	.095	.118	.130	.132	.190	.210
	.450	-.089	-.072	-.070	-.050	-.031	.011	.060	.063	.090	.100	.128	.126	.179	.300
	.550	-.110	-.096	-.069	-.041	-.010	.018	.060	.070	.085	.097	.107	.118	.132	.161
	.650	-.151	-.165	-.154	-.134	-.107	-.078	-.037	-.025	-.013	-.001	.010	.022	.034	.064
	.750	-.148	-.207	-.284	-.306	-.299	-.272	-.239	-.229	-.218	-.197	-.190	-.181	-.165	-.133
	.850	-.004	-.036	-.058	-.096	-.120	-.161	-.098	-.093	-.087	-.079	-.069	-.056	-.043	-.011
a <sub>1</sub> .000	b <sub>0</sub> .925	.102	.030	-.040	-.102	-.100	-.140	-.112	-.140	-.116	-.129	-.105	-.072	-.081	.050
	b <sub>0</sub> .975	.140	.050	-.050	-.123	-.100	-.151	-.166	-.200	-.169	-.210	-.205	-.119	-.141	.085
	a <sub>1</sub> .000	.146	.057	-.060	-.140	-.101	-.160	-.201	-.250	-.200	-.270	-.291	-.150	-.180	.010

\*No orifice.

<sup>b</sup>Paired value.

NACA

TABLE 10.-PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(07.50) PROPELLER BLADE SECTION ( $x = 0.85$ ) - Continued

(d) One-blade propeller;  $M = 0.61$ .

$J$	2.360	2.295	2.234	2.177	2.118	2.132	2.108	2.089	2.062	2.037	2.018	1.998	1.974	1.952	1.936	1.921
$M_x$	.926	.941	.955	.969	.976	.981	.987	.993	1.003	1.008	1.014	1.022	1.026	1.033	1.039	1.044
$c_{x'}$	-.17	.62	1.38	2.11	2.49	2.70	3.01	3.26	3.63	3.96	4.22	4.50	4.83	5.13	5.36	5.57
$\Delta\theta$	-.01	.06	.11	.16	.18	.20	.22	.23	.25	.27	.29	.30	.32	.33	.34	.35
$c_{y'}$	.09	.24	.55	.79	.92	1.04	1.14	1.22	1.31	1.39	1.48	1.59	1.63	1.74	1.78	1.83
$c_{y'}$	.0284	.0774	.1800	.2574	.2981	.3381	.3684	.3948	.4245	.4503	.4794	.5142	.5303	.5639	.5761	.5961
$c_m$	-.0205	-.0282	-.0442	-.0660	-.0790	-.0890	-.0965	-.1065	-.1123	-.1188	-.1252	-.1339	-.1390	-.1468	-.1540	-.1575
$c_o$	.0305	.0313	.0332	.0356	.0373	.0390	.0394	.0399	.0415	.0420	.0430	.0460	.0465	.0494	.0501	.0501
$c/b$	Pressure coefficient, $P$															
Upper surface	.0000	1.233	1.241	1.249	1.257	1.261	1.264	1.267	1.271	1.277	1.280	1.283	1.288	1.291	1.296	1.299
	.025	.503	.457	.374	.341	.325	.307	.301	.295	.304	.303	.308	.319	.327	.339	.348
	.050	.154	.128	.058	.012	-.005	-.025	-.018	-.005	.017	.028	.043	.060	.071	.086	.099
	.100	-.010	-.027	-.067	-.096	-.112	-.132	-.139	-.161	-.169	-.190	-.205	-.220	-.233	-.250	-.253
	.200	-.153	-.158	-.210	-.228	-.244	-.258	-.271	-.282	-.273	-.311	-.306	-.326	-.339	-.348	-.353
	.300	-.257	-.267	-.310	-.336	-.343	-.351	-.351	-.359	-.354	-.358	-.365	-.379	-.390	-.397	-.400
	.400	-.354	-.374	-.400	-.416	-.424	-.437	-.437	-.447	-.444	-.449	-.454	-.453	-.454	-.453	-.452
	.500	-.457	-.450	-.507	-.492	-.495	-.502	-.503	-.516	-.510	-.516	-.518	-.521	-.525	-.525	-.527
	.600	-.535	-.528	-.551	-.573	-.575	-.580	-.577	-.578	-.569	-.578	-.584	-.585	-.587	-.591	-.588
	.700	-.658	-.647	-.661	-.665	-.668	-.677	-.675	-.683	-.672	-.672	-.671	-.666	-.667	-.672	-.671
	.800	-.177	-.205	-.310	-.465	-.597	-.786	-.751	-.767	-.760	-.760	-.758	-.752	-.744	-.725	-.696
Lower surface	.900	-.125	-.152	-.222	-.273	-.300	-.335	-.349	-.380	-.440	-.464	-.519	-.624	-.640	-.608	-.628
	.950	-.114	-.149	-.217	-.270	-.295	-.327	-.340	-.368	-.412	-.422	-.443	-.469	-.480	-.541	-.607
	.0375	-.313	-.179	-.020	.093	.129	.168	.200	.233	.280	.317	.345	.380	.403	.433	.451
	.075	-.309	-.179	-.027	.071	.099	.132	.161	.188	.229	.261	.286	.318	.337	.362	.385
	.150	-.166	-.085	-.006	.064	.084	.109	.131	.151	.184	.206	.227	.247	.263	.281	.295
	.250	-.155	-.110	-.048	.008	.026	.044	.065	.081	.111	.135	.152	.176	.189	.207	.221
	.350	-.158	-.110	-.069	-.028	-.011	.003	.036	.040	.092	.070	.092	.123	.131	.145	.159
	.450	-.169	-.132	-.103	-.065	-.057	-.040	-.023	-.011	.001	.032	.032	.060	.068	.082	.093
	.550	-.209	-.186	-.158	-.123	-.112	-.100	-.085	-.073	-.052	-.040	-.026	-.010	0	.015	.027
	.650	-.266	-.250	-.230	-.198	-.185	-.173	-.159	-.148	-.126	-.114	-.100	-.083	-.072	-.058	-.047
	.750	-.326	-.315	-.300	-.271	-.260	-.251	-.236	-.228	-.207	-.192	-.180	-.163	-.152	-.141	-.131
	.850	-.345	-.309	-.277	-.242	-.223	-.201	-.186	-.163	-.150	-.135	-.118	-.106	-.090	-.078	-.064
	.925	-.268	-.240	-.247	-.218	-.206	-.215	-.162	-.134	-.119	-.095	-.078	-.047	-.045	-.025	-.003
	.975	-.168	-.173	-.224	-.203	-.192	-.200	-.136	-.100	-.090	-.054	-.039	-.003	-.002	.004	.037
	1.000	-.106	-.135	-.210	-.200	-.185	-.193	-.121	-.084	-.075	-.034	-.020	.029	.021	.019	.058

No orifice.

NACA



TABLE 10.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN  
NACA 16-(3)(07.50) PROPELLER BLADE SECTION ( $\alpha = 0.85$ ) - Concluded

(e) One-blade propeller;  $M = 0.65$ .

$J$	2.224	2.212	2.189	2.171	2.148	2.121	2.106	2.087	2.066	2.047	2.030	2.000	1.979
$M_{\infty}$	1.005	1.014	1.018	1.023	1.032	1.037	1.044	1.050	1.056	1.062	1.068	1.073	1.080
$\alpha$	1.51	1.61	1.96	2.19	2.49	2.84	3.04	3.29	3.57	3.83	4.06	4.47	4.76
$\Delta b$	0	0	.03	.04	.07	.10	.11	.13	.15	.17	.19	.23	.26
$c_L$	.73	.77	.80	.85	.94	1.01	1.06	1.12	1.19	1.24	1.27	1.34	1.40
$c_D$	.2348	.2515	.2613	.2761	.3026	.3271	.3420	.3613	.3819	.3975	.4090	.4329	.4561
$c_m$	-.1110	-.1146	-.1150	-.1150	-.1164	-.1204	-.1224	-.1229	-.1263	-.1308	-.1316	-.1337	-.1360
$c_c$	.0562	.0560	.0576	.0578	.0583	.0584	.0585	.0586	.0578	.0576	.0577	.0577	.0572
$c/b$	Pressure coefficient, P												
Upper surface	0.000	1.278	1.284	1.286	1.289	1.295	1.298	1.303	1.306	1.310	1.315	1.319	1.326
	.025	.474	.484	.491	.488	.501	.510	.521	.529	.543	.551	.559	.582
	.050	.153	.166	.177	.180	.196	.208	.221	.232	.247	.258	.270	.295
	.100	.022	.020	.012	-.006	-.022	-.035	-.046	-.071	-.084	-.090	-.094	-.128
	.200	-.119	-.113	-.130	-.139	-.146	-.150	-.155	-.169	-.174	-.174	-.180	-.220
	.300	-.227	-.228	-.235	-.247	-.253	-.257	-.258	-.260	-.261	-.262	-.284	-.299
	.400	-.317	-.316	-.320	-.332	-.339	-.344	-.347	-.348	-.350	-.351	-.352	-.348
	.500	-.402	-.404	-.405	-.408	-.406	-.412	-.417	-.421	-.421	-.422	-.420	-.431
	.600	-.483	-.480	-.480	-.482	-.483	-.484	-.478	-.480	-.484	-.489	-.486	-.499
	.700	-.571	-.567	-.569	-.574	-.578	-.581	-.578	-.578	-.576	-.573	-.566	-.576
Lower surface	.800	-.665	-.665	-.664	-.662	-.657	-.657	-.652	-.646	-.634	-.619	-.603	-.577
	.900	-.727	-.742	-.741	-.741	-.735	-.732	-.730	-.730	-.728	-.723	-.718	-.716
	.950	-.674	-.727	-.761	-.771	-.769	-.767	-.764	-.761	-.759	-.754	-.748	-.746
	.0375	.003	.033	.071	.097	.145	.183	.225	.264	.297	.324	.349	.421
	.075	-.020	.010	.047	.071	.116	.149	.187	.220	.249	.270	.295	.354
	.150	-.030	.048	.069	.081	.111	.135	.165	.190	.212	.230	.248	.285
	.250	-.026	-.009	.009	.019	.047	.070	.098	.121	.140	.154	.170	.214
	.350	-.023	-.049	-.039	-.029	0	.020	.045	.061	.080	.097	.110	.148
	.450	-.086	-.082	-.074	-.065	-.040	-.025	-.004	.010	.025	.041	.059	.086
	.550	-.128	-.114	-.100	-.095	-.078	-.066	-.050	-.039	-.024	-.010	.002	.026
Lower surface	.650	-.191	-.178	-.167	-.161	-.143	-.132	-.118	-.107	-.092	-.079	-.066	-.042
	.750	-.271	-.260	-.250	-.243	-.228	-.216	-.198	-.183	-.173	-.159	-.147	-.120
	.850	-.215	-.228	-.230	-.231	-.222	-.214	-.202	-.191	-.176	-.162	-.148	-.121
	.925	-.160	-.173	-.210	-.226	-.220	-.205	-.200	-.191	-.177	-.169	-.150	-.119
	.975	-.115	-.132	-.200	-.221	-.217	-.195	-.200	-.190	-.177	-.163	-.145	-.110
	1.000	-.091	-.110	-.195	-.220	-.217	-.187	-.199	-.189	-.179	-.160	-.140	-.105

\*Paired value.

<sup>b</sup>No orifice.

NACA

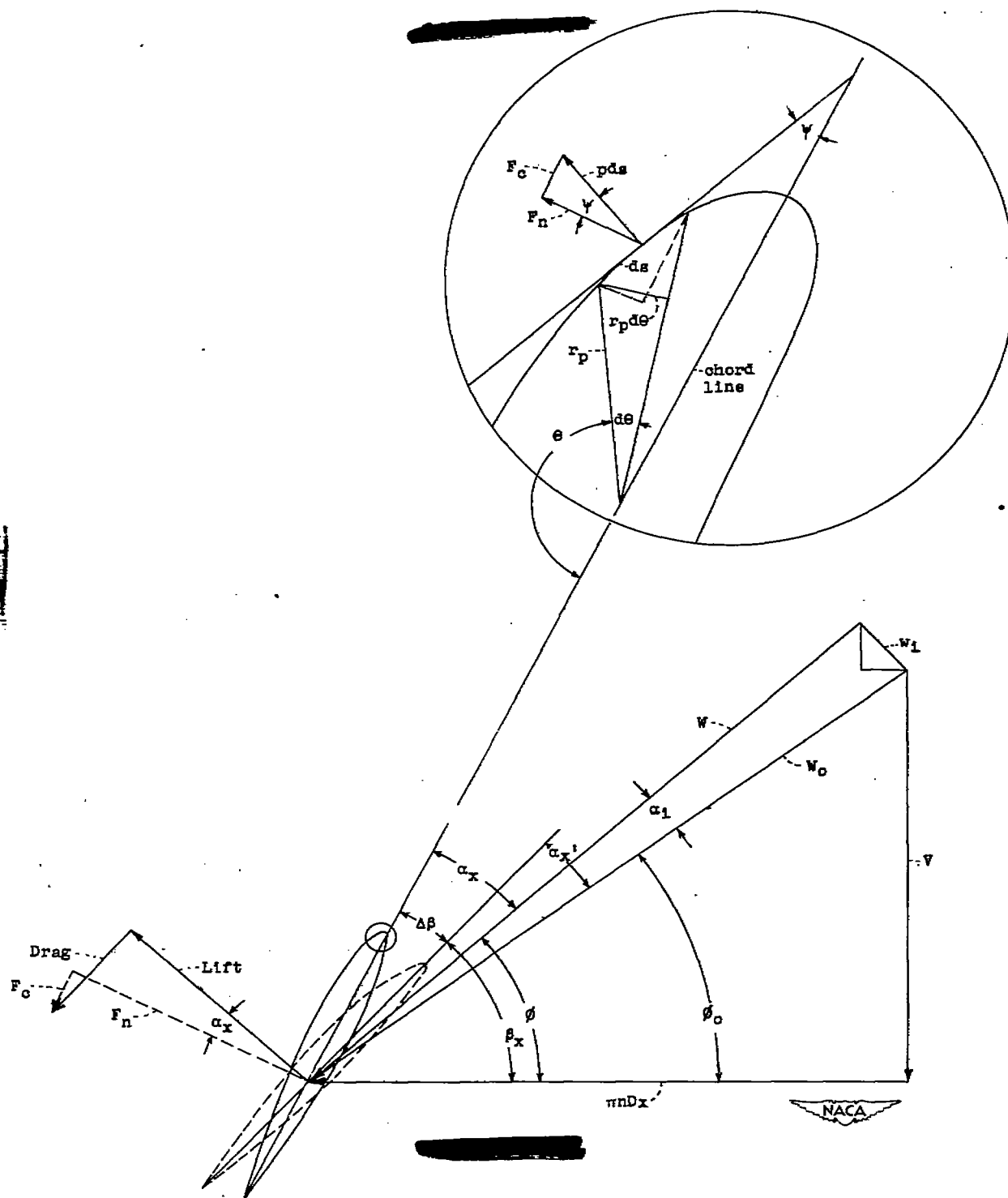


Figure 1.- Vector diagram of the velocities and forces acting on a blade section.

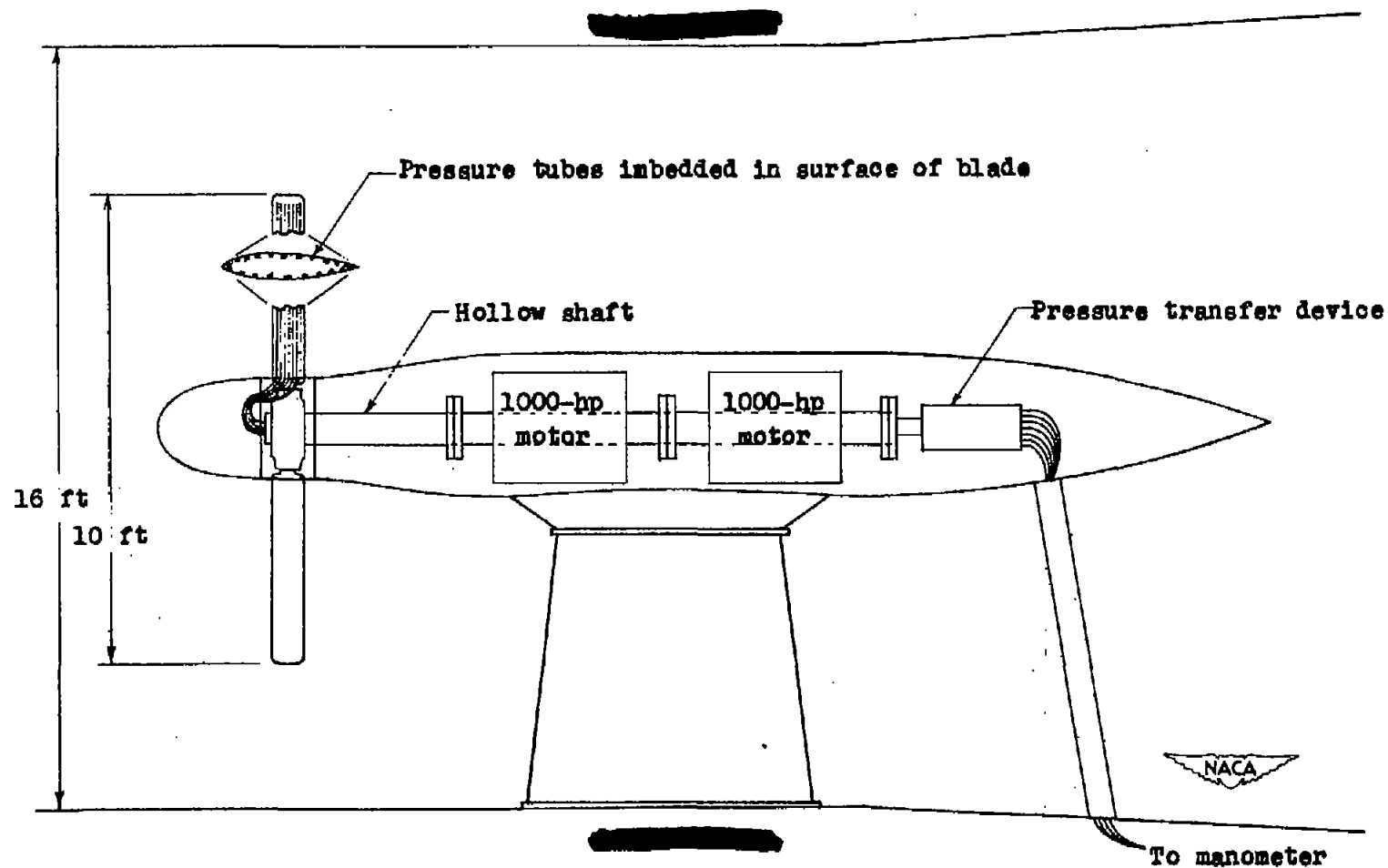


Figure 2.- Diagram of the apparatus used to obtain pressure distributions on the sections of operating propellers.

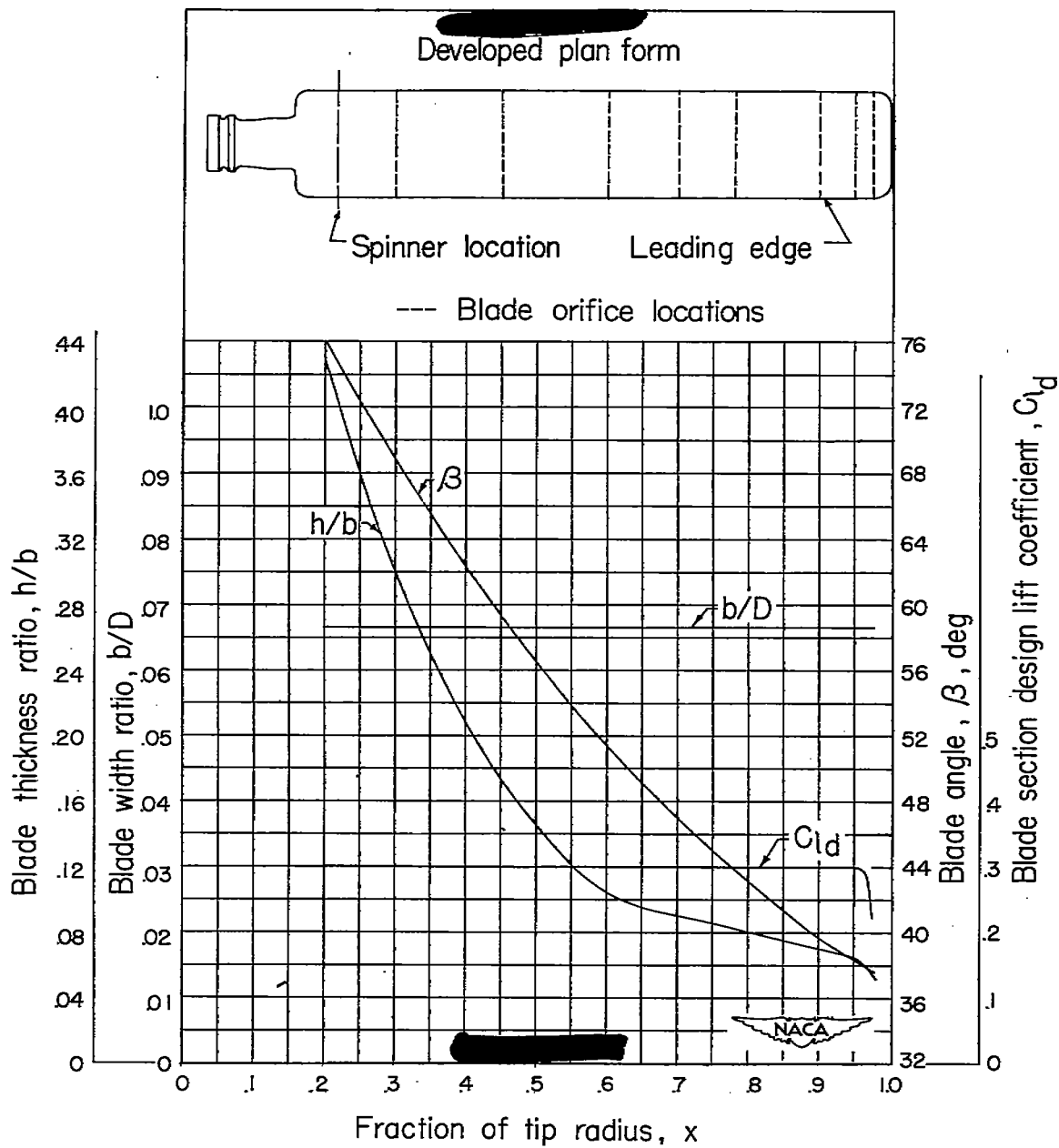


Figure 3.- Blade-form curves for NACA 10-(3)(090)-03 propeller.

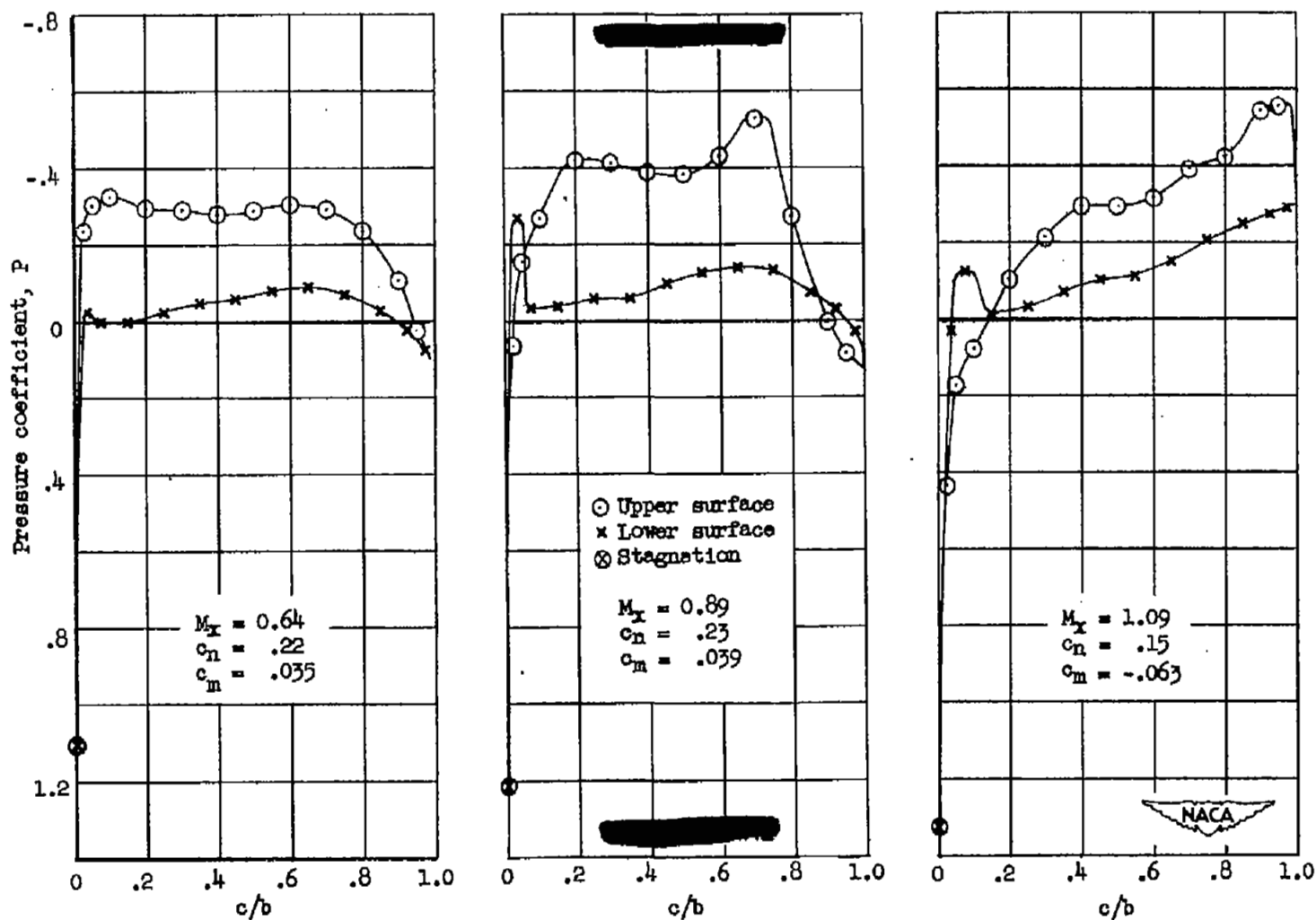


Figure 4.- Typical pressure distributions along the chord of the NACA 16-306.50 blade section located at the  $x = 0.95$  radius;  $\alpha_x = 0.8$  (approx.).

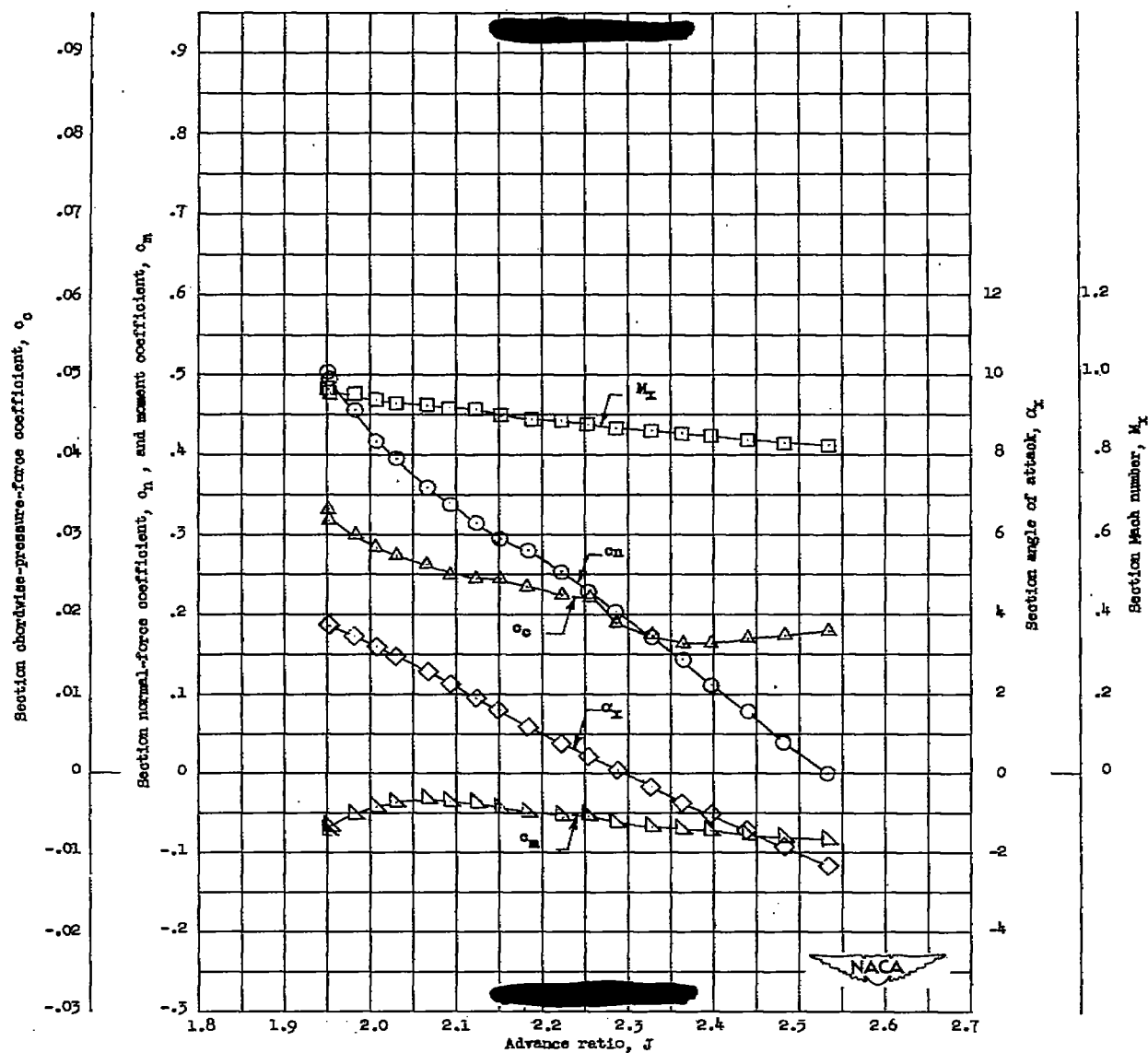


Figure 5.- Variation of section normal-force coefficient, moment coefficient, chordwise-pressure-force coefficient, angle of attack, and Mach number with advance ratio for the blade section at the  $x = 0.85$  radius (from table 6(e)).

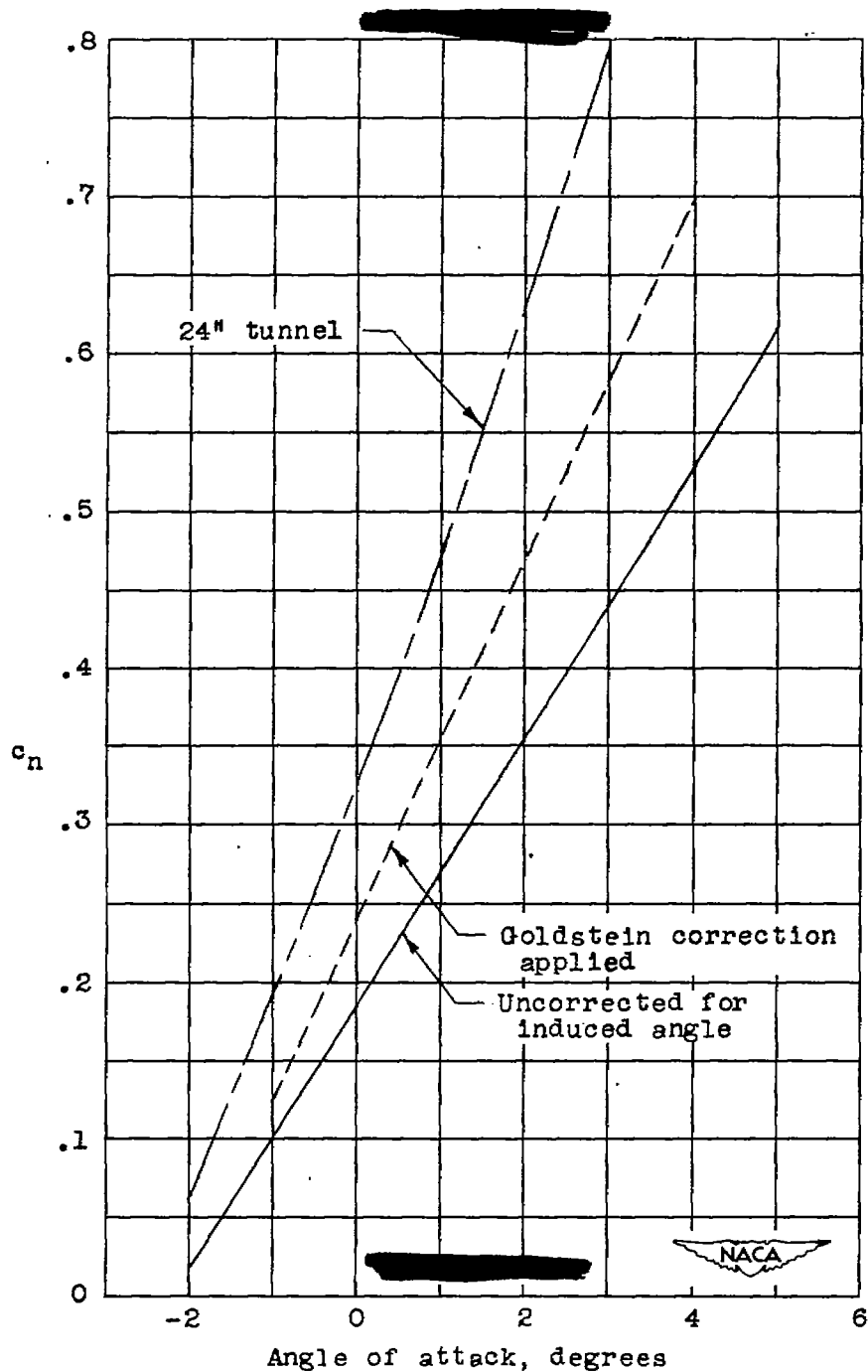


Figure 6.- Effect of induced-angle correction on the slope of the normal-force-coefficient curve of a NACA 16-309 blade section operating at  $x = 0.7$ ;  $M_x = 0.70$ .

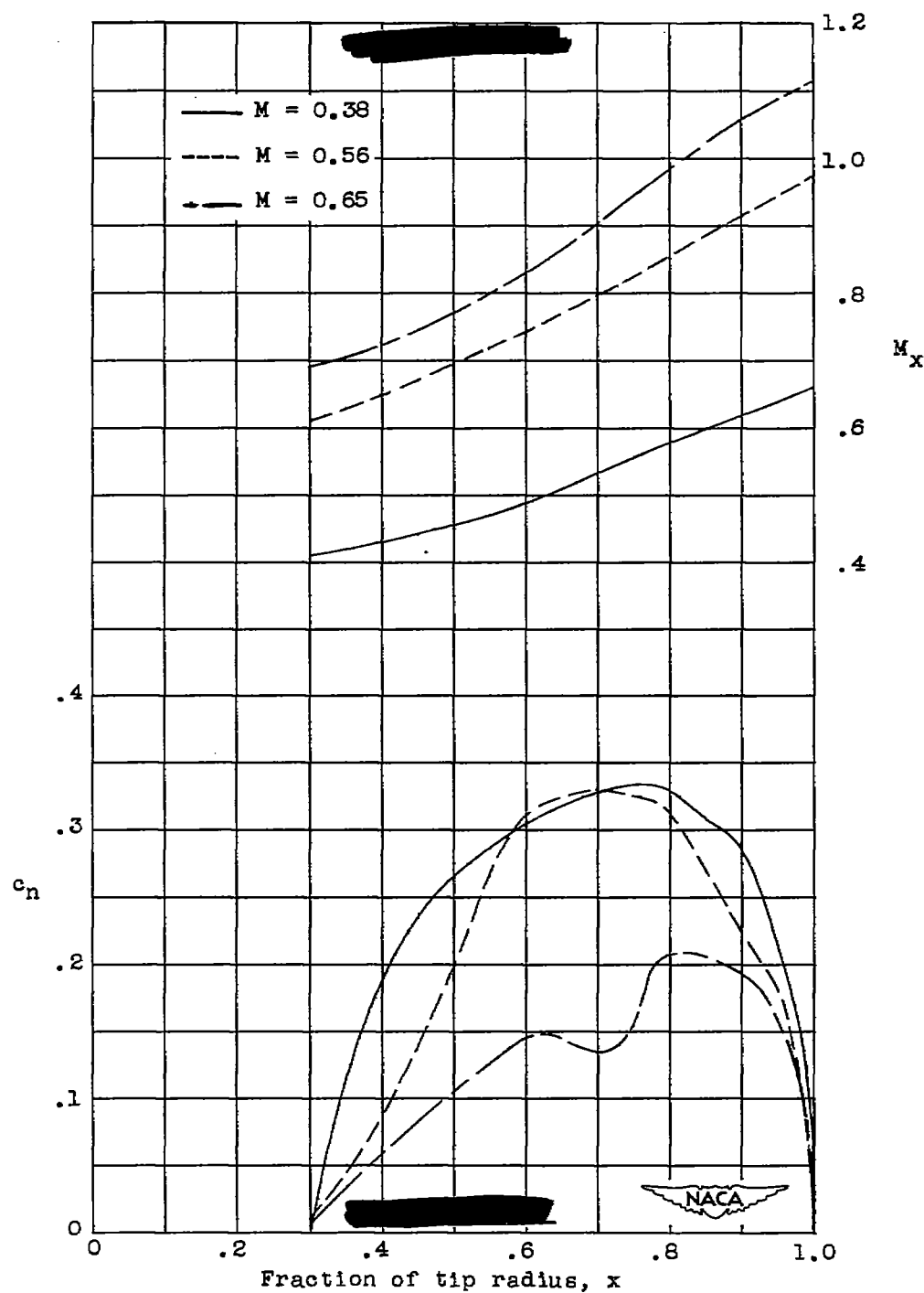


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( $x = 0.85$ ). [ $\beta_{0.75R} = 45^\circ$ ;  $\beta_x = 41.3^\circ$ ;  $B = 2$ ]

(a) $N = 1140$ rpm	48
(b) $N = 1350$ rpm	49
(c) $N = 1500$ rpm	50
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(e) $M = 0.56$	52
(f) $M = 0.60$	53
(g) $M = 0.64$	54

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( $x = 0.90$ ). [ $\beta_{0.75R} = 45^\circ$ ;  $\beta_x = 39.63^\circ$ ;  $B = 2$ ]

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(a) N = 1140 rpm . . . . .	62
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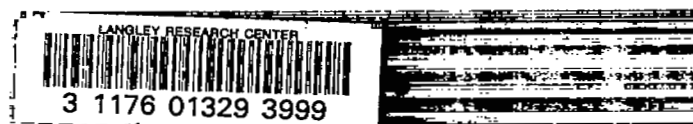
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