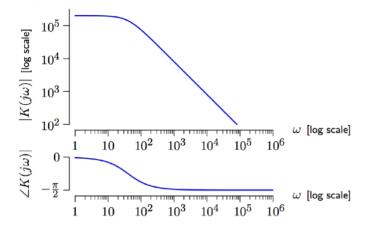
VE216 Lecture 12

CT Feedback and Control

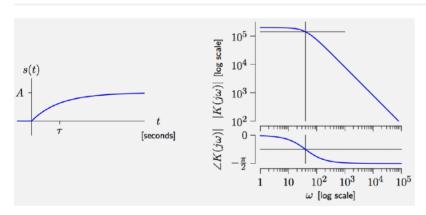
Op-Amp Data Introduction

The gain of an op-amp depends on frequency.



The **low-gain** at **high frequencies** limits applications.

Time Constant and System Function Control



In an increasing system, the time constant au is the time for the step response to reach $1-\frac{1}{e}$ of the final value.

System Bode Plot to Frequency Response

We can see the plot of the frequency response looks like the bode plot of $\frac{1}{s+\alpha}$.

Then we do some improvements to make it real: $K(s) = \frac{\alpha K_0}{s+\alpha}$.

With inverse Laplace transform, we get $h(t) = \alpha K_0 e^{-\alpha t} u(t)$ as impulse response.

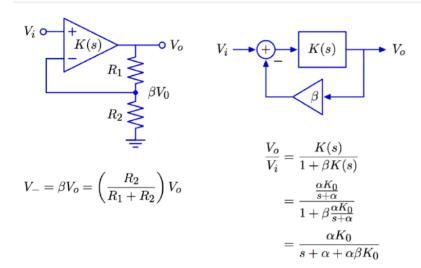
Then integrate from $-\infty$ to t, we get $s(t)=\int_{-\infty}^t h(\tau)d\tau=\int_0^t h(\tau)d\tau=K_0(1-e^{-\alpha t})u(t)$.

With the parameter $K_0=2\times 10^5$ and lpha=40, we get the result that $au=rac{1}{lpha}=rac{1}{40}s$.

Op Amp Disadvantages

- Frequency Response: the high gain is only in low frequencies.
- Step Response: slow by electronic standards ($au = rac{1}{40} s$).

Performance Improvement by Feedback

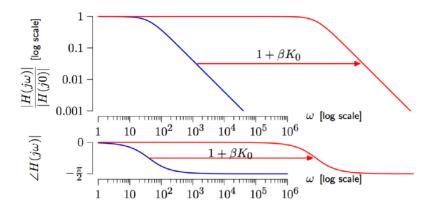


So the origin pole is $s = -\alpha$.

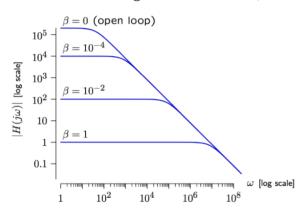
The new pole is $s=-\alpha(1+\beta K_0)$, even negative then 0.

So consider au will be smaller, the response is faster.

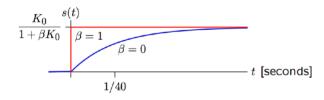
Detailed Performance Improvement

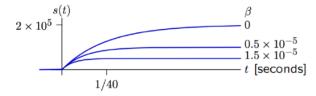


• Feedback trades gain for band width (the width of frequency to maintain the gain unchanged):



ullet Step response: $s(t)=rac{K_0}{1+eta K_0}(1-e^{-lpha(1+eta K_0)t})u(t)$





with the same $\left. rac{d}{dt} s(t)
ight|_{t=0^+}$

Motor Controller

We build a robot arm with input v(t) and output as $\theta(t)$.

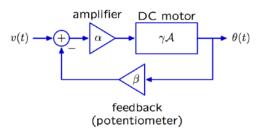
$$v(t) \longrightarrow \text{DC motor} \longrightarrow \theta(t)$$

The **rotational speed** is proportional to the **input voltage**.

So the angle is the **integral** of rotation speed.

$$V \longrightarrow \gamma A \longrightarrow \Theta$$

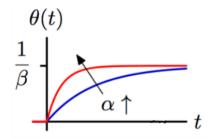
So we apply the proportional **feedback** to control the angle of the motor's shift.



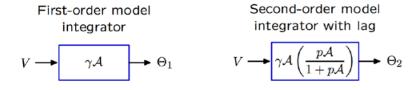
the feedback function is $\frac{\Theta}{V}=\frac{\alpha\gamma A}{1+\alpha\beta\gamma A}=\frac{\alpha\gamma}{s+\alpha\beta\gamma}$ (substitute A with $\frac{1}{s}$) with single pole $-\alpha\beta\gamma$.

Then the impulse response: $h(t) = \alpha \gamma e^{-\alpha \beta \gamma t} u(t)$.

Then the step response: $s(t)=rac{1}{eta}(1-e^{-lphaeta\gamma t})u(t)$.



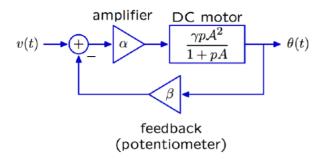
In real life, the motor integrator has lag, so we change it:



with the step response:

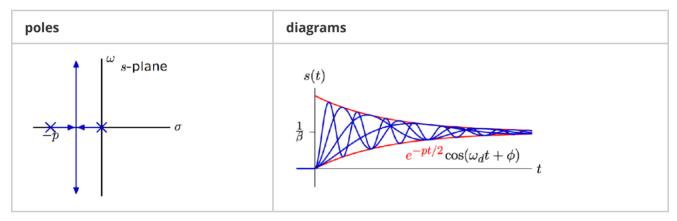
$$\begin{array}{c|c} v(t) & \theta(t) \\ 1 & \theta_1(t) = \gamma t u(t) \\ \vdots & \theta_2(t) = \left(\gamma t - \frac{\gamma}{p}(1 - e^{-pt})\right) u(t) \end{array}$$

So the second-order model is:



with feedback frequency response:
$$\frac{\frac{\alpha\gamma pA^2}{1+pA}}{1+\frac{\alpha\beta\gamma pA^2}{1+pA}} = \frac{\alpha\beta pA^2}{1+pA+\alpha\beta\gamma pA^2} = \frac{\alpha\gamma p}{s^2+ps+\alpha\beta\gamma p}$$
 thus the poles are $s=-\frac{p}{2}\pm\sqrt{(\frac{p}{2})^2-\alpha\beta\gamma p}$

When we increase the $oldsymbol{eta}$, then we get the two poles collide from $oldsymbol{0}$ and $-oldsymbol{p}$ to imaginary part.



Summary

CT feedback is useful to

- Increase speed and bandwidth
- Control position instead of speed