

Vp250 Problem Set 10

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Problem 1

- (a) Assume the value of the capacitance is C , the value of the inductance is L . Then the impedance of the capacitor is $-j\frac{1}{\omega C}$, the impedance of the inductor is $j\omega L$. So the output voltage can be evaluated as

$$\tilde{V}_{hi} = V_s \angle 0^\circ \frac{R + j\omega L}{R + j(\omega L - \frac{1}{\omega C})} = V_s \frac{\sqrt{(R^2 + \omega^2 L^2 - \frac{L}{C})^2 + \frac{R^2}{\omega^2 C^2}}}{R^2 + (\omega L - \frac{1}{\omega C})^2} \angle \arctan \frac{\frac{R}{\omega C}}{R^2 + \omega^2 L^2 - \frac{L}{C}}$$

So the ratio is

$$V_{hi}/V_s = \frac{\sqrt{(R^2 + \omega^2 L^2 - \frac{L}{C})^2 + \frac{R^2}{\omega^2 C^2}}}{R^2 + (\omega L - \frac{1}{\omega C})^2}$$

When $\omega \rightarrow 0$,

$$\begin{aligned} V_{hi}/V_s &= \frac{\sqrt{(R^2 + \omega^2 L^2 - \frac{L}{C})^2 + \frac{R^2}{\omega^2 C^2}}}{R^2 + (\omega L - \frac{1}{\omega C})^2} \\ &= \frac{\omega C \sqrt{\omega^2 C^2 (R^2 - \frac{L}{C})^2 + R^2}}{R^2 \omega^2 C^2 + (\omega^2 CL - 1)^2} \\ &\quad \text{Take all } \omega^2 \text{ as } 0 \\ &= \omega C R \end{aligned}$$

So we can see that the ratio is proportional to the ω .

When $\omega \rightarrow \infty$,

$$\begin{aligned} V_{hi}/V_s &= \frac{\sqrt{(R^2 + \omega^2 L^2 - \frac{L}{C})^2 + \frac{R^2}{\omega^2 C^2}}}{R^2 + (\omega L - \frac{1}{\omega C})^2} \\ &= \frac{\sqrt{\frac{1}{\omega^4 L^4} (R^2 + \omega^2 L^2 - \frac{L}{C})^2 + \frac{R^2}{\omega^6 C^2 L^4}}}{\frac{R^2}{\omega^2 L^2} + (1 - \frac{1}{\omega^2 CL})^2} \\ &= \frac{\sqrt{(\frac{R^2}{\omega^2 L^2} + 1 - \frac{1}{\omega^2 CL})^2 + \frac{R^2}{\omega^6 C^2 L^4}}}{\frac{R^2}{\omega^2 L^2} + (1 - \frac{1}{\omega^2 CL})^2} \\ &\quad \text{Take all } \frac{1}{\omega} \text{ as } 0 \\ &= 1 \end{aligned}$$

- (b)

$$\tilde{V}_{lo} = V_s \angle 0^\circ \frac{-j\frac{1}{\omega C}}{R + j(\omega L - \frac{1}{\omega C})} = V_s \frac{\sqrt{(\frac{1}{\omega^2 C^2} - \frac{L}{C})^2 + \frac{R^2}{\omega^2 C^2}}}{R^2 + (\omega L - \frac{1}{\omega C})^2} \angle \arctan \frac{-\frac{R}{\omega C}}{\frac{1}{\omega^2 C^2} - \frac{L}{C}}$$

So the ratio is

$$V_{lo}/V_s = \frac{\sqrt{(\frac{1}{\omega^2 C^2} - \frac{L}{C})^2 + \frac{R^2}{\omega^2 C^2}}}{R^2 + (\omega L - \frac{1}{\omega C})^2}$$

When $\omega \rightarrow \infty$,

$$\begin{aligned}
 V_{lo}/V_s &= \frac{\sqrt{(\frac{1}{\omega^2 C^2} - \frac{L}{C})^2 + \frac{R^2}{\omega^2 C^2}}}{R^2 + (\omega L - \frac{1}{\omega C})^2} \\
 &= \frac{\sqrt{\frac{1}{\omega^4 L^4} (\frac{1}{\omega^2 L^2} - \frac{L}{C})^2 + \frac{R^2}{\omega^6 C^2 L^4}}}{\frac{R^2}{\omega^2 L^2} + (1 - \frac{1}{\omega^2 CL})^2} \\
 &\quad \text{Take all } \frac{1}{\omega^2} \text{ as } 0 \\
 &= \frac{1}{\omega^2 LC}
 \end{aligned}$$

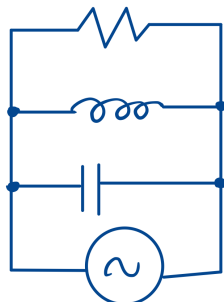
So it is proportional to ω^{-2} .

When $\omega \rightarrow 0$,

$$\begin{aligned}
 V_{lo}/V_s &= \frac{\sqrt{(\frac{1}{\omega^2 C^2} - \frac{L}{C})^2 + \frac{R^2}{\omega^2 C^2}}}{R^2 + (\omega L - \frac{1}{\omega C})^2} \\
 &= \frac{\sqrt{(1 - \omega^2 CL)^2 + R^2 \omega^2 C^2}}{R^2 \omega^2 C^2 + (\omega^2 LC - 1)^2} \\
 &\quad \text{Take all } \omega^2 \text{ as } 0 \\
 &= 1
 \end{aligned}$$

Problem 2

(a) The circuit graph:



For three loops,

$$\begin{cases} v_R - v_L = 0 \\ v_L - v_c = 0 \\ v_c - v = 0 \end{cases} \Rightarrow v_R = v_L = v_C = v$$

$$\begin{cases} v_R = i_R R \\ v_L = i_L Z_L \\ v_C = i_C Z_C \\ v = i(R || Z_L || Z_C) = \end{cases} \Rightarrow i = i_R + i_C + i_L$$

(b) $\tilde{v} = V \angle 0^\circ$.

$$\begin{aligned}
 \tilde{i}_R &= \frac{\tilde{v}}{R} = \frac{V}{R} \angle 0^\circ \\
 \tilde{i}_C &= \frac{\tilde{v}}{\frac{1}{j\omega C}} = V\omega C \angle 90^\circ \\
 \tilde{i}_L &= \frac{\tilde{v}}{j\omega L} = \frac{V}{\omega L} \angle -90^\circ
 \end{aligned}$$

(c)

$$\tilde{i} = \frac{V}{R} \angle 0^\circ + V\omega C \angle 90^\circ + \frac{V}{\omega L} \angle -90^\circ = \frac{V}{R} + j \left(V\omega C - \frac{V}{\omega L} \right)$$

So

$$I = \sqrt{\left(\frac{V}{R}\right)^2 + \left(V\omega C - \frac{V}{\omega L}\right)^2} = \sqrt{I_R^2 + (I_C - I_L)^2} = V \sqrt{\left(\frac{1}{R}\right)^2 + \left(\omega C - \frac{1}{\omega L}\right)^2}$$

(d) When $\omega_0 = \frac{1}{\sqrt{LC}}$,

$$\tilde{i}_L = V \sqrt{\frac{C}{L}} \angle -90^\circ \Rightarrow I_L = V \sqrt{\frac{C}{L}}$$

$$\tilde{i}_C = V \sqrt{\frac{C}{L}} \angle 90^\circ \Rightarrow I_C = V \sqrt{\frac{C}{L}}$$

Hence, $I_C = I_L$.

For I ,

$$I = \frac{V}{R}$$

, which is the minimum of I because $\left(\omega C - \frac{1}{\omega L}\right)^2 \geq 0$.

The power of the resistor is $P = \frac{V^2}{2R}$, which is a constant. So you can say that it is a minimum when $\omega = \omega_0$.

(e) when it is at the resonance,

$$\begin{aligned} \tilde{i} &= \frac{V}{R} + j \left(V\omega C - \frac{V}{\omega L} \right) = \sqrt{\frac{V^2}{R^2} + \left(V\omega C - \frac{V}{\omega L} \right)^2} \angle \arctan \frac{V\omega C - \frac{V}{\omega L}}{\frac{V}{R}} \\ &\Rightarrow \tilde{i} = \sqrt{\frac{V^2}{R^2} + \left(V\omega C - \frac{V}{\omega L} \right)^2} \angle \arctan \frac{RV\omega^2 CL - VR}{V\omega L} \end{aligned}$$

So the phase angle is

$$\phi = \arctan \frac{RV\omega^2 CL - VR}{V\omega L} = 0$$

The phase lag in RLC series circuit is $\tan \phi = \frac{\omega L - \frac{1}{\omega C}}{R}$. When $\omega = \omega_0$, the phase shift is 0, the same as the phase shift as the parallel condition.

Problem 3

For f_1

$$\begin{cases} \frac{\partial^2 f_1}{\partial x^2} = 4Ak^2(x - tv)^2 e^{-k(x-tv)^2} - 2Ake^{-k(x-tv)^2} \\ \frac{1}{v^2} \cdot \frac{\partial^2 f_1}{\partial t^2} = \frac{1}{v^2} (4Ak^2v^2(x - tv)^2 e^{-k(x-tv)^2} - 2Akv^2 e^{-k(x-tv)^2}) \end{cases} \Rightarrow \frac{\partial^2 f_1}{\partial x^2} = \frac{1}{v^2} \cdot \frac{\partial^2 f_1}{\partial t^2}$$

So f_1 satisfies.

For f_2

$$\begin{cases} \frac{\partial^2 f_2}{\partial x^2} = -Ak^2 \sin(k(x - tv)) \\ \frac{1}{v^2} \cdot \frac{\partial^2 f_2}{\partial t^2} = \frac{1}{v^2} (-Ak^2v^2 \sin(k(x - tv))) \end{cases} \Rightarrow \frac{\partial^2 f_2}{\partial x^2} = \frac{1}{v^2} \cdot \frac{\partial^2 f_2}{\partial t^2}$$

So f_2 satisfies.

For f_3

$$\frac{\partial^2 f_3}{\partial x^2} = 16Ak^4x^2 e^{-k(kx^2+tv)^2} (kx^2 + tv)^2 - 8Ak^3x^2 e^{-k(kx^2+tv)^2} - 4Ak^2 e^{-k(kx^2+tv)^2} (kx^2 + tv)$$

$$\frac{1}{v^2} \cdot \frac{\partial^2 f_3}{\partial t^2} = \frac{1}{v^2} (4Ak^2 v^2 e^{-k(kx^2+tv)^2} (kx^2 + tv)^2 - 2Akv^2 e^{-k(kx^2+tv)^2})$$

these two are not equal, so f_3 does not satisfy.

For f_4

$$\frac{\partial^2 f_4}{\partial x^2} = -Ak^2 \sin(kx) \cos^3(ktv)$$

$$\frac{1}{v^2} \cdot \frac{\partial^2 f_4}{\partial t^2} = \frac{1}{v^2} (6Ak^2 v^2 \sin(kx) \sin^2(ktv) \cos(ktv) - 3Ak^2 v^2 \sin(kx) \cos^3(ktv))$$

these two are not equal, so f_4 does not satisfy.

Problem 4

(a)

$$\begin{cases} \frac{\partial^2 \xi}{\partial x^2} = -Ak^2 \sin(kx) \cos(\omega t) \\ \frac{1}{v^2} \cdot \frac{\partial^2 \xi}{\partial t^2} = \frac{k^2}{\omega^2} (-A\omega^2 \sin(kx) \cos(\omega t)) \end{cases} \Rightarrow \frac{\partial^2 \xi}{\partial x^2} = \frac{1}{v^2} \cdot \frac{\partial^2 \xi}{\partial t^2}$$

So it satisfies the wave equation.

(b)

$$\xi(x, t) = A \sin(kx) \cos(\omega t) = \frac{1}{2} \sin(kx + \omega t) + \frac{1}{2} \cos(kx - \omega t)$$

Problem 5

(a) Reflective. By the conservation of momentum, when the sail is reflective, the spaceship can obtain a higher speed opposite to the photons.

(b) Suppose the distance between the spaceship and the sun is d , the mass of sun is M , the mass of the spaceship is m , P is the power, c is the speed of the light and I is the intensity.

$$\begin{cases} I = \frac{P}{4\pi d^2} \\ p = \frac{2I}{c} \\ p \cdot 4\pi d^2 = \frac{GMm}{d^2} \end{cases} \Rightarrow \begin{cases} A = 4\pi d^2 = \frac{2\pi GMmc}{P} \\ = \frac{2\pi \cdot 6.67 \cdot 10^{-11} \cdot 1.989 \cdot 10^{30} \cdot 10 \cdot 10^3 \cdot 3 \cdot 10^8}{3.9 \cdot 10^{26}} \\ = 6.41 \cdot 10^6 m^2 = 6.41 km^2 \end{cases}$$

(c) From (b) we can see that the formula for the area of the sail has nothing to do with the distance.

Problem 6

(a) Assume a unit vector \hat{l} which is parallel to the axis of the cylinder, \hat{t} , tangent to the circle which is concentric with the cylinder.

$$|B| \cdot 2\pi a = \mu_0 I \Rightarrow |B| = \frac{\mu_0 I}{2\pi a} \Rightarrow \bar{B} = \frac{\mu_0 I}{2\pi a} \hat{t}$$

The resistance:

$$R = \rho \frac{dl}{\pi a^2}$$

The infinitesimal potential difference between a dl long distance in the conductor is

$$dU = |E| dl \Rightarrow |E| = \frac{dU}{dl} = \frac{IR}{dl} = \frac{I\rho \frac{dl}{\pi a^2}}{dl} = \frac{I\rho}{\pi a^2} \Rightarrow \bar{E} = \frac{I\rho}{\pi a^2} \hat{l}$$

(b)

$$|S| = \frac{1}{\mu_0} |E| \cdot |B| = \frac{1}{\mu_0} \cdot \frac{\mu_0 I}{2\pi a} \cdot \frac{I\rho}{\pi a^2} = \frac{I^2 \rho}{2\pi^2 a^3} \Rightarrow \bar{S} = -\frac{I^2 \rho}{2\pi^2 a^3} \hat{n}$$

where \hat{n} is the unit vector which normal to the surface of the cylinder and points out of the surface.

(c) Denote the total flow rate of the energy as r .

$$r = \int_{\Sigma} \bar{S} \, d\bar{A} = |S| \cdot 2\pi a l = \frac{I^2 \rho l}{\pi a^2}$$

(d)

$$P = I^2 R = I^2 \rho \frac{l}{\pi a^2} = \frac{I^2 \rho l}{\pi a^2}$$

It is the same as in (c). And since the energy can be generated within this conductor, the direction of S is pointing out the conductor, which is the positive direction as we defined.