

# HIGH-ORDER WAVE PROPAGATION ALGORITHMS FOR GENERAL HYPERBOLIC SYSTEMS

DAVID I. KETCHESON\*, MATTEO PARSANI†, AND RANDALL J. LEVEQUE‡

**Abstract.** We present a finite volume method that is applicable to general hyperbolic PDEs, including non-conservative and spatially varying systems. The method can be extended to arbitrarily high order of accuracy and allows a well-balanced implementation for capturing solutions of balance laws near steady state. This well-balancing is achieved through the  $f$ -wave Riemann solver and a novel wave-slope WENO reconstruction procedure. The spatial discretization, like that of the well-known Clawpack software, is based on solving Riemann problems and calculating fluctuations (not fluxes). Our implementation employs weighted essentially non-oscillatory reconstruction in space and strong stability preserving Runge-Kutta integration in time. We demonstrate the wide applicability and advantageous properties of the method through numerical examples, including problems in non-conservative form, problems with spatially varying fluxes, and problems involving near-equilibrium solutions of balance laws.

**1. Introduction.** Many important physical phenomena are governed by hyperbolic systems of conservation laws. In one space dimension the standard conservation law has the form

$$q_t + f(q)_x = 0, \quad (1.1)$$

where the components of  $q \in \mathbb{R}^m$  are conserved quantities and the components of  $f : \mathbb{R}^m \times \mathbb{R}^m \rightarrow \mathbb{R}^m$  are the corresponding fluxes. Very many numerical methods have been developed for the solution of (1.1); some of the most successful are the high resolution Godunov-type methods based on the use of Riemann solvers and nonlinear limiters. These and other methods are generally based on *flux-differencing* and make explicit use of the flux function  $f$ .

Herein we also consider the more general quasilinear variable-coefficient hyperbolic system

$$\kappa(x)q_t + A(q, x, t)q_x = 0, \quad (1.2)$$

where  $A : \mathbb{R}^m \times \mathbb{R} \times \mathbb{R} \rightarrow \mathbb{R}^{m \times m}$  is diagonalizable with real eigenvalues. Wave-propagation methods of up to second-order accuracy have been developed for such systems in, e.g. [12, 10]. These methods are based on wave-propagation Riemann solvers, which compute *fluctuations*, (i.e. traveling discontinuities) rather than fluxes and thus can be applied to the general system (1.2) just as easily as to the conservation law (1.1).

Second-order methods may often be the best choice in terms of a balance between computational cost and desired resolution, especially for problems with solutions dominated by shocks or other discontinuities with relatively simple structures between these discontinuities. For problems containing complicated smooth solution structures, where the accurate resolution of small scales is required (e.g. simulation of compressible turbulence, computational aeroacoustics (CAA), computational electromagnetism (CEM), turbulent combustion etc.), schemes with higher order accuracy are desirable.

The purpose of this work is to present a numerical method that combines the advantages of wave-propagation solvers with high order accuracy. The basic discretization approach was presented already in [8]; here, we give a more detailed presentation and demonstrate the wide applicability of the method. The new method combines the notions of wave propagation ([12, 14]) and the method of lines, and can in principle be extended to arbitrarily high order accuracy by the use of high order accurate spatial reconstructions and

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\*King Abdullah University of Science and Technology, Box 4700, Thuwal, Saudi Arabia, 23955-6900. (david.ketcheson@kaust.edu.sa)

†King Abdullah University of Science and Technology, Box 4700, Thuwal, Saudi Arabia, 23955-6900. (matteo.parsani@kaust.edu.sa)

‡Department of Applied Mathematics, University of Washington, Box 352420, Seattle, WA 98195-2420. (rjl@uw.edu)

high order accurate ordinary differential equation (ODE) solvers. The implementation presented here is based on the fifth-order accurate weighted essentially non-oscillatory (WENO) reconstruction and a fourth-order strong-stability-preserving Runge-Kutta (RK) scheme, and can be applied to system (1.2) as long as the correct structure of the Riemann solution for the system is understood. We restrict our attention to problems in one or two dimensions, although the method may be extended in a straightforward manner to higher dimensions.

An alternative approach to high order discretization of hyperbolic PDEs (the adaptive high order derivatives, or ADER, method) has been developed by Titarev & Toro [20] and subsequent authors. That approach uses the Cauchy-Kovalevski procedure and has the advantage of leading to one-step time discretization. The method of lines approach used in the present work seems more straightforward and allows manipulation of the method properties by the use of different time integrators, but requires the evaluation of multiple stages per time step.

A similar class of methods, applicable to non-conservative hyperbolic systems, has been developed by Castro, Gallardo, Pares, and their coauthors; see, e.g. [2]. Those methods also use WENO reconstruction and Runge-Kutta time stepping in conjunction with Riemann solvers, and lead to a discretization with a form similar to that presented here and in [8]. Those methods have recently been combined with the ADER approach; see [3]. The present method differs in the approach to reconstruction and the kind of Riemann solvers used. These differences result in some potential advantages: our method also handles system (1.2) with capacity function  $\kappa$  and it can make use of  $f$ -wave Riemann solvers [1] as well as wave-slope reconstruction to ensure conservation or well-balancing and achieve high order convergence even for some problems with discontinuous coefficients. Using our approach, it is not necessary to artificially enlarge a system of balance laws in order to obtain a well-balanced scheme. Finally, there is a freely available implementation of the method that uses a framework familiar to many practitioners of hyperbolic PDEs.

The methods described in this paper are implemented in the software package SharpClaw, which is freely available on the web at <http://www.clawpack.org>.

SharpClaw employs the same interface that is used in Clawpack [14] for problem specification and setup, as well as for the necessary Riemann solvers. This makes it simple to apply SharpClaw to a problem that has been set up in Clawpack.

The paper is organized as follows. In Section 2.2, we present Godunov’s method for linear hyperbolic PDEs in wave propagation form [14]. This method is extended to high order in Section 2.3 by introducing a high order reconstruction based on cell averages. Generalization to nonlinear hyperbolic systems is presented in Section 2.4. Further extensions and details of the method are presented in the remainder of Section 2. Numerical examples, including application to acoustics, elasticity, and shallow water waves, are presented in Section 3.

**2. Semi-discrete wave-propagation.** The wave-propagation algorithm was first introduced by LeVeque [12] in 1997 in the framework of high resolution finite volume methods for solving hyperbolic systems of equations. The scheme is conservative, second-order accurate in smooth regions, and captures shocks without introducing spurious oscillations. In this section, we extend the wave-propagation algorithm to arbitrarily high order of accuracy through use of high order reconstructions and time marching schemes. For simplicity, we focus on the one dimensional (1D) scheme and then briefly describe the extension to two dimensions (2D).

**2.1. Riemann Problems and Notation.** The notation for Riemann solutions used in this paper comes primarily from [14], and is motivated by consideration of the linear hyperbolic system

$$q_t + Aq_x = 0. \tag{2.1}$$

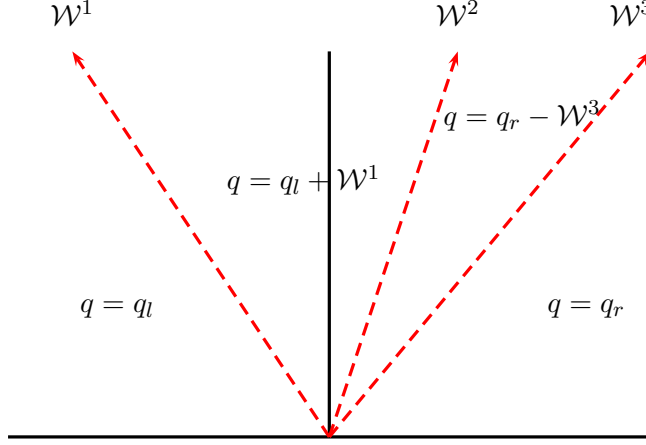


FIG. 2.1. The wave propagation solution of the Riemann problem.

Here  $q \in \mathbb{R}^m$  and  $A \in \mathbb{R}^{m \times m}$ . System (2.1) is said to be hyperbolic if  $A$  is diagonalizable with real eigenvalues; we will henceforth assume this to be the case. Let  $s^p$  and  $r^p$  for  $1 \leq p \leq m$  denote the eigenvalues and the corresponding right eigenvectors of  $A$  with the eigenvalues ordered so that  $s^1 \leq s^2 \leq \dots \leq s^m$ .

Consider the *Riemann problem* consisting of (2.1) together with initial data

$$q(x, 0) = \begin{cases} q_l & x < 0 \\ q_r & x > 0 \end{cases} \quad (2.2)$$

The solution for  $t > 0$  consists of  $m$  discontinuities, the  $p$ th one proportional to  $r^p$  and moving at speed  $s^p$ . They can be obtained by decomposing the difference  $q_r - q_l$  in terms of the eigenvectors  $r^p$ :

$$q_r - q_l = \sum_p \alpha^p r^p = \sum_p \mathcal{W}^p. \quad (2.3)$$

We refer to the vectors  $\mathcal{W}^p$  as waves. Each wave is a jump discontinuity along the ray  $x = s^p t$  in phase space. The solution is pictured in Figure 2.1 for  $m = 3$ . For brevity, we will sometimes refer to the Riemann problem with initial left state  $q_l$  and initial right state  $q_r$  as *the Riemann problem with initial states  $(q_l, q_r)$* .

In a finite volume method, it is useful to define notation for the net effect of all left- or right-going waves:

$$\mathcal{A}^- \Delta q \equiv \sum_{p=1}^m (s^p)^- \mathcal{W}^p \quad (2.4a)$$

$$\mathcal{A}^+ \Delta q \equiv \sum_{p=1}^m (s^p)^+ \mathcal{W}^p. \quad (2.4b)$$

Here and throughout,  $(x)^\pm$  denotes the positive or negative part of  $x$ :

$$(x)^- = \min(x, 0) \quad (x)^+ = \max(x, 0).$$

Note that the symbols  $\mathcal{A}^\pm \Delta q$ , referred to as *fluctuations*, should be interpreted as single entities that represent the net effect of all waves travelling to the right or left. The notation is motivated by the case of a constant coefficient linear system (2.1), in which case  $\mathcal{A}^\pm \Delta q = A^\pm (q_r - q_l)$ , where  $A^-$  (respectively  $A^+$ ) is the matrix obtained by setting all positive (respectively negative) eigenvalues of  $A$  to zero. See [12] or [14] for more details.

The notation for waves and fluctuations defined in (2.3) and (2.4) can also be used to describe numerical solutions of Riemann problems for nonlinear systems if the numerical solver approximates the solution by a series of propagating jump discontinuities, which is very often the case. Because the approximate Riemann solution for a nonlinear system depends not only on the difference  $q_r - q_l$  but on the values of the states, we will sometimes employ for clarity the notation  $\mathcal{W}^p(q_l, q_r)$  to denote the  $p$ th wave in the solution of the Riemann problem with initial states  $(q_l, q_r)$ .

**2.2. First-order Godunov's method.** Consider the constant-coefficient linear system in one dimension (2.1). Taking a finite volume approach, we define the cell averages (i.e. the solution variables)

$$Q_i(t) = \frac{1}{\Delta x} \int_{x_{i-\frac{1}{2}}}^{x_{i+\frac{1}{2}}} q(x, t) dx,$$

where the index  $i$  and the quantity  $\Delta x$  denote the cell index and the cell size, respectively. To solve the linear system (2.1), we initially approximate the solution  $q(x, t)$  by these cell averages; that is, at  $t = t_0$  we define the piecewise-constant function

$$\tilde{q}(x, t_0) = Q_i \text{ for } x \in (x_{i-\frac{1}{2}}, x_{i+\frac{1}{2}}). \quad (2.5)$$

The linear system (2.1) with initial data  $\tilde{q}$  consists locally of a series of Riemann problems, one at each interface  $x_{i-\frac{1}{2}}$ . The Riemann problem at  $x_{i-\frac{1}{2}}$  consists of (2.1) with the piecewise constant initial data

$$q(x, 0) = \begin{cases} Q_{i-1} & x < x_{i-\frac{1}{2}} \\ Q_i & x > x_{i-\frac{1}{2}}. \end{cases}$$

As discussed above, the solution of the Riemann problem is expressed as a set of waves obtained by decomposing the jump in  $Q$  in terms of the eigenvectors of  $A$ :

$$Q_i - Q_{i-1} = \sum_p \alpha_{i-\frac{1}{2}}^p r_{i-\frac{1}{2}}^p = \sum_p \mathcal{W}^p(Q_{i-1}, Q_i). \quad (2.6)$$

Let  $\tilde{q}(x, t_0 + \Delta t)$  denote the exact evolution of  $\tilde{q}$  after a time increment  $\Delta t$ . If we take  $\Delta t$  small enough that the waves from adjacent interfaces do not pass through more than one cell, then we can integrate (2.1) over  $[x_{i-\frac{1}{2}}, x_{i+\frac{1}{2}}] \times [0, \Delta t]$  and divide by  $\Delta x$  to obtain

$$Q_i(t_0 + \Delta t) - Q_i(t_0) = -\frac{1}{\Delta x} \int_{x_{i-\frac{1}{2}}}^{x_{i+\frac{1}{2}}} A \tilde{q}_x(x, t_0 + \Delta t) dx. \quad (2.7)$$

Here  $\tilde{q}_x$  should be understood in the sense of distributions.

We can split the integral above into three parts, representing the Riemann fans from the two interfaces, and the remaining piece:

$$\int_{x_{i-\frac{1}{2}}}^{x_{i+\frac{1}{2}}} A \tilde{q}_x dx = \int_{x_{i-\frac{1}{2}}}^{x_{i-\frac{1}{2}} + s^R \Delta t} A \tilde{q}_x dx + \int_{x_{i+\frac{1}{2}} + s^L \Delta t}^{x_{i+\frac{1}{2}}} A \tilde{q}_x dx + \int_{x_{i-\frac{1}{2}} + s^R \Delta t}^{x_{i+\frac{1}{2}} + s^L \Delta t} A \tilde{q}_x dx. \quad (2.8)$$

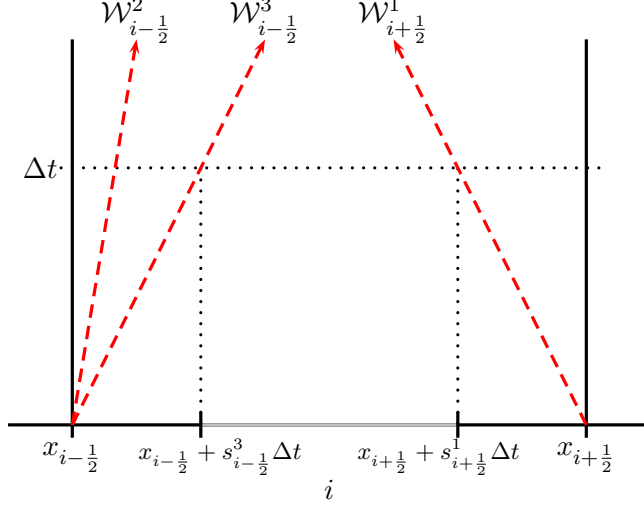


FIG. 2.2. Time evolution of the reconstructed solution  $\tilde{q}$  in cell  $i$ .

The relevant regions are depicted in Figure 2.2. Here we have defined  $s^L = \min(s_{i+\frac{1}{2}}^1, 0)$  and  $s^R = \max(s_{i-\frac{1}{2}}^m, 0)$ . The third integral in (2.8) vanishes because  $\tilde{q}(x, \Delta t)$  is constant outside the Riemann fans, by the definition (2.5). Hence (2.8) reduces to

$$\int_{x_{i-\frac{1}{2}}}^{x_{i+\frac{1}{2}}} A \tilde{q}_x dx = \Delta t \sum_{p=1}^m \left(s_{i-\frac{1}{2}}^p\right)^+ \mathcal{W}_{i-\frac{1}{2}}^p + \Delta t \sum_{p=1}^m \left(s_{i+\frac{1}{2}}^p\right)^- \mathcal{W}_{i+\frac{1}{2}}^p \quad (2.9a)$$

$$= \Delta t \left( \mathcal{A}^+ \Delta Q_{i-\frac{1}{2}} + \mathcal{A}^- \Delta Q_{i+\frac{1}{2}} \right), \quad (2.9b)$$

where the *fluctuations*  $\mathcal{A}^- \Delta Q_{i+\frac{1}{2}}$  and  $\mathcal{A}^+ \Delta Q_{i-\frac{1}{2}}$  are defined by

$$\mathcal{A}^- \Delta Q_{i+\frac{1}{2}} \equiv \sum_{p=1}^m \left(s_{i+\frac{1}{2}}^p\right)^- \mathcal{W}_{i+\frac{1}{2}}^p, \quad \mathcal{W}_{i+\frac{1}{2}}^p \equiv \mathcal{W}^p(Q_i, Q_{i+1}) \quad (2.10a)$$

$$\mathcal{A}^+ \Delta Q_{i-\frac{1}{2}} \equiv \sum_{p=1}^m \left(s_{i-\frac{1}{2}}^p\right)^+ \mathcal{W}_{i-\frac{1}{2}}^p, \quad \mathcal{W}_{i-\frac{1}{2}}^p \equiv \mathcal{W}^p(Q_{i-1}, Q_i). \quad (2.10b)$$

Note again that the fluctuations  $\mathcal{A}^+ \Delta Q_{i-\frac{1}{2}}$  and  $\mathcal{A}^- \Delta Q_{i+\frac{1}{2}}$  are motivated by the idea of a matrix-vector product but should be interpreted as single entities that represent the net effect of all waves travelling to the right or left. The upper-case  $Q$  in the fluctuations is meant to emphasize that they are based on differences of cell averages. For instance, the fluctuation  $\mathcal{A}^+ \Delta Q_{i-\frac{1}{2}}$  corresponds to the effect of right-going waves from the Riemann problem with initial states  $(Q_{i-1}, Q_i)$ .

Substituting (2.9b) into (2.7), we obtain the scheme

$$Q_i^{n+1} - Q_i^n = -\frac{\Delta t}{\Delta x} \left( \mathcal{A}^+ \Delta Q_{i-\frac{1}{2}} + \mathcal{A}^- \Delta Q_{i+\frac{1}{2}} \right).$$

Dividing by  $\Delta t$  and taking the limit as  $\Delta t$  approaches zero, we obtain the semi-discrete wave-propagation form of the (first-order) Godunov's scheme

$$\frac{\partial Q_i}{\partial t} = -\frac{1}{\Delta x} \left( \mathcal{A}^+ \Delta Q_{i-\frac{1}{2}} + \mathcal{A}^- \Delta Q_{i+\frac{1}{2}} \right). \quad (2.11)$$

Equation (2.11) constitutes a linear system of ordinary differential equations (ODEs) that may be integrated, for instance, with a Runge-Kutta method. It is clear from the derivation that this scheme reduces to the corresponding flux-differencing scheme when applied to systems written in conservation form, e.g. system (1.1). The advantage of the proposed scheme over flux-differencing schemes lies in the ability to solve systems which are not in conservation form, e.g. the general quasilinear variable-coefficient hyperbolic system (1.2). Since systems of this form generally cannot be rewritten in terms of a flux function, fluctuations are calculated in terms of the decomposition (2.8).

**2.3. Extension to higher order.** The method of the previous section is only first-order accurate in space. In order to improve the spatial accuracy, we replace the piecewise-constant approximation (2.5) by a piecewise-polynomial approximation that is accurate to order  $p$  in regions where the solution is smooth:

$$\tilde{q}(x, t_0) = \tilde{q}_i(x) \text{ for } x \in (x_{i-\frac{1}{2}}, x_{i+\frac{1}{2}}), \quad (2.12)$$

where

$$\tilde{q}_i(x) = q(x, t_0) + \mathcal{O}(\Delta x^{p+1}).$$

Integration of  $A\tilde{q}_x$  over  $[x_{i-\frac{1}{2}}, x_{i+\frac{1}{2}}]$  again yields (2.8), but now the third integral is non-zero in general, since  $\tilde{q}$  is not constant outside the Riemann fans. Define

$$q_{i-\frac{1}{2}}^R \equiv \lim_{x \rightarrow x_{i-\frac{1}{2}}^+} \tilde{q}_i(x_{i-\frac{1}{2}}) \quad q_{i+\frac{1}{2}}^L \equiv \lim_{x \rightarrow x_{i+\frac{1}{2}}^-} \tilde{q}_i(x_{i+\frac{1}{2}}), \quad (2.13)$$

where superscripts  $L$  and  $R$  refer respectively to the left and the right state of the interface considered. Then in place of (2.9), we now obtain

$$\int_{x_{i-\frac{1}{2}}}^{x_{i+\frac{1}{2}}} A\tilde{q}_x dx = \Delta t \sum_{p=1}^m \left( s_{i-\frac{1}{2}}^p \right)^+ \mathcal{W}_{i-\frac{1}{2}}^p + \Delta t \sum_{p=1}^m \left( s_{i+\frac{1}{2}}^p \right)^- \mathcal{W}_{i+\frac{1}{2}}^p + \int_{x_{i-\frac{1}{2}} + s^R \Delta t}^{x_{i+\frac{1}{2}} + s^L \Delta t} A\tilde{q}_x dx \quad (2.14a)$$

$$= \Delta t \left( \mathcal{A}^+ \Delta q_{i-\frac{1}{2}} + \mathcal{A}^- \Delta q_{i+\frac{1}{2}} \right) + A(q_{i+\frac{1}{2}}^L - q_{i-\frac{1}{2}}^R). \quad (2.14b)$$

The resulting fully-discrete scheme is thus

$$Q_i^{n+1} - Q_i^n = -\frac{\Delta t}{\Delta x} \left( \mathcal{A}^+ \Delta q_{i-\frac{1}{2}} + \mathcal{A}^- \Delta q_{i+\frac{1}{2}} + A(q_{i+\frac{1}{2}}^L - q_{i-\frac{1}{2}}^R) \right).$$

We use the notation  $\mathcal{A}^\pm \Delta q$  instead of  $\mathcal{A}^\pm \Delta Q$  because the states in the Riemann problems are not the cell averages, but rather the reconstructed interface values. In other words, the fluctuations at  $x_{i-\frac{1}{2}}$  are defined by

$$\mathcal{A}^\pm \Delta q_{i-\frac{1}{2}} = \sum_{p=1}^m \left( s^p(q_{i-\frac{1}{2}}^L, q_{i-\frac{1}{2}}^R) \right)^\pm \mathcal{W}^p(q_{i-\frac{1}{2}}^L, q_{i-\frac{1}{2}}^R).$$

For instance, the fluctuation  $\mathcal{A}^+ \Delta q_{i-\frac{1}{2}}$  corresponds to the effect of right-going waves from the Riemann problem with initial states  $(q_{i-\frac{1}{2}}^L, q_{i-\frac{1}{2}}^R)$ . Moreover, we can view the term  $A(q_{i+\frac{1}{2}}^L - q_{i-\frac{1}{2}}^R)$  as the sum of both the left- and right-going fluctuations resulting from a Riemann problem with initial states  $(q_{i-\frac{1}{2}}^R, q_{i+\frac{1}{2}}^L)$ . It is natural to denote this term, which we refer to as a *total fluctuation*, by  $\mathcal{A} \Delta q_i$ :

$$\mathcal{A} \Delta q_i = \sum_{p=1}^m \left( s^p(q_{i-\frac{1}{2}}^R, q_{i+\frac{1}{2}}^L) \right)^\pm \mathcal{W}^p(q_{i-\frac{1}{2}}^R, q_{i+\frac{1}{2}}^L).$$

Dividing by  $\Delta t$  and taking the limit as  $\Delta t$  approaches zero, we obtain the semi-discrete scheme

$$\frac{\partial Q_i}{\partial t} = -\frac{1}{\Delta x} \left( \mathcal{A}^+ \Delta q_{i-\frac{1}{2}} + \mathcal{A}^- \Delta q_{i+\frac{1}{2}} + \mathcal{A} \Delta q_i \right). \quad (2.15)$$

**2.4. Nonlinear systems.** Next we generalize the method to solve one-dimensional nonlinear hyperbolic systems:

$$q_t + A(q, x) q_x = 0. \quad (2.16)$$

We again assume that  $A$  is a constant function of  $x$  within each cell, so we can write  $A(q, x) = A_i(q)$ . In the special case that  $A$  is the Jacobian matrix of some function  $f$ , (2.16) corresponds to the conservation law (1.1). Our method can be applied to the general system (2.16) as long as the physically meaningful solution to the Riemann problem can be approximated. We assume the Riemann problem solution at  $x_{i-\frac{1}{2}}$  is computed or approximated as consisting of discontinuities (waves)  $\mathcal{W}_{i-\frac{1}{2}}^p$  propagating at speeds  $s_{i-\frac{1}{2}}^p$ , as is the case for any linearized Riemann solver, and often for other approximate solvers. Then the scheme is given by

$$\frac{\partial Q_i}{\partial t} = -\frac{1}{\Delta x} \left( \mathcal{A}^+ \Delta q_{i-\frac{1}{2}} + \mathcal{A}^- \Delta q_{i+\frac{1}{2}} + \int_{x_{i-\frac{1}{2}}}^{x_{i+\frac{1}{2}}} A_i(\tilde{q}) \tilde{q}_x dx \right). \quad (2.17)$$

In general, the integral in (2.17) must be evaluated by quadrature; however, for the conservative system (1.1), the integral can be evaluated exactly, and is given by

$$\int_{x_{i-\frac{1}{2}}}^{x_{i+\frac{1}{2}}} A_i(\tilde{q}) \tilde{q}_x dx = f(q_{i+\frac{1}{2}}^L) - f(q_{i-\frac{1}{2}}^R). \quad (2.18)$$

If the fluctuations are computed using a Roe solver or some other conservative wave-propagation Riemann solver, then the flux difference appearing in (2.18) is equal to the sum of fluctuations from a fictitious ‘internal’ Riemann problem for the current cell  $i$ , just as in the linear case above:

$$f(q_{i+\frac{1}{2}}^L) - f(q_{i-\frac{1}{2}}^R) = \mathcal{A}^+ \Delta q_i + \mathcal{A}^- \Delta q_i = \mathcal{A} \Delta q_i. \quad (2.19)$$

Specifically, the fluctuations  $\mathcal{A}^\pm \Delta q_i$  are those resulting from the Riemann problem with initial states  $(q_{i-\frac{1}{2}}^R, q_{i+\frac{1}{2}}^L)$ . Then we can write (2.17) also as

$$\frac{\partial Q_i}{\partial t} = -\frac{1}{\Delta x} \left( \mathcal{A}^- \Delta q_{i+\frac{1}{2}} + \mathcal{A}^+ \Delta q_{i-\frac{1}{2}} + \mathcal{A} \Delta q_i \right). \quad (2.20)$$

Note that, for the conservative system (1.1), if a Roe solver or an  $f$ -wave solver (see Section 2.6) is used, then the fluctuations are equal to the flux differences

$$\mathcal{A}^- \Delta q_{i-\frac{1}{2}} = \hat{f}_{i-\frac{1}{2}} - f(q_{i-\frac{1}{2}}^L) \quad (2.21)$$

$$\mathcal{A}^+ \Delta q_{i-\frac{1}{2}} = f(q_{i-\frac{1}{2}}^R) - \hat{f}_{i-\frac{1}{2}}, \quad (2.22)$$

where  $\hat{f}_{i-\frac{1}{2}}$  is the numerical flux at  $x_{i-\frac{1}{2}}$ . Thus (2.20) is equivalent to the traditional flux-differencing method

$$\frac{\partial Q_i}{\partial t} = -\frac{1}{\Delta x} \left( \hat{f}_{i+\frac{1}{2}} - \hat{f}_{i-\frac{1}{2}} \right). \quad (2.23)$$

In particular, the scheme is conservative in this case.

**2.5. Capacity-form differencing.** In many applications the system of conservation laws takes the form

$$\kappa(x)q_t + f(q)_x = 0, \quad (2.24)$$

in one space dimension, or

$$\kappa(x, y)q_t + f(q)_x + g(q)_y = 0, \quad (2.25)$$

in two dimensions, where  $\kappa$  is a given function of space and is usually indicated as *capacity function* (see [12]). Systems like (2.24) and (2.25) arise naturally in the derivation of a conservation law, where the flux of a quantity is naturally defined in terms of one variable  $q$ , whereas it is a different quantity  $\kappa q$  that is conserved. For instance, for the flow in a porous media,  $\kappa$  would be the porosity. Note that a capacity function can also appear in systems that are not in conservation form, e.g. the quasilinear system (1.2).

Several approaches can be used to reduce such a system to a more familiar conservation law. One natural approach is the capacity-form differencing [12],

$$\frac{\partial Q_i}{\partial t} = -\frac{1}{\kappa_i \Delta x} \left( \mathcal{A}^+ \Delta q_{i-\frac{1}{2}} + \mathcal{A}^- \Delta q_{i+\frac{1}{2}} + \mathcal{A} \Delta q_i \right), \quad (2.26)$$

where  $\kappa_i$  is the capacity of the  $i$ th cell. This is a simple extension of (2.15) or (2.20) which ensures that  $\sum \kappa_i Q_i$  is conserved (except possibly at the boundaries) and yet allows the Riemann solution to be computed based on  $q$  as in the case  $\kappa = 1$ .

**2.6.  $f$ -wave Riemann solvers.** For application to conservation laws, it is desirable to ensure that the wave-propagation discretization is conservative. This can easily be accomplished by using an  $f$ -wave Riemann solver [1]. Use of  $f$ -wave solvers is also useful for problems with spatially varying flux function, as well as problems involving balance laws near steady state.

The idea of the  $f$ -wave splitting for (1.1) is to decompose the flux difference  $f(q_r) - f(q_l)$  into waves rather than the  $q$ -difference used in (2.6), i.e. we decompose the flux difference as a linear combination of the right eigenvectors  $r^p$  of some jacobian:

$$f(q_r) - f(q_l) = \sum_p \beta^p r^p = \sum_p \mathcal{Z}^p(q_l, q_r). \quad (2.27)$$

Note that the  $f$ -waves have the dimensions of a  $q$  increment multiplied by the wave speed.



The fluctuations are then defined as

$$\mathcal{A}^- \Delta q \equiv \sum_{p:s^p < 0} \mathcal{Z}^p(q_l, q_r) \quad \mathcal{A}^+ \Delta q \equiv \sum_{p:s^p > 0} \mathcal{Z}^p(q_l, q_r)$$

Note that the total fluctuation in cell  $i$  is given simply by

$$\mathcal{A} \Delta q_i = f\left(q_{i+\frac{1}{2}}^L\right) - f\left(q_{i-\frac{1}{2}}^R\right).$$

An advantage of particular interest is the possibility to include source terms directly into the  $f$ -wave decomposition. In fact, for balance laws that include source terms,

$$q_t + f(q)_x = \psi(q, x),$$

one can easily extend this algorithm by first discretizing the source term to obtain values  $\Psi_{i-\frac{1}{2}}$  at the cell interfaces and then compute the waves  $\mathcal{Z}_{i-\frac{1}{2}}^p$  by splitting

$$f(q_r) - f(q_l) - \Delta x \Psi(q_l, q_r, x) = \sum_p \beta^p r^p = \sum_p \mathcal{Z}^p(q_l, q_r). \quad (2.28)$$

Here  $\Psi(q_l, q_r, x)$  is some suitable average of  $\psi(q, x)$ , between the neighboring states. In Bale et al. [1], it has been shown that for the second-order FV wave-propagation scheme implemented in Clawpack, the  $f$ -wave approach is very useful for handling source terms, especially in cases where the solution is close to a steady state because it leads to a well-balanced scheme. However, for our high order wave-propagation scheme, application of the  $f$ -wave algorithm with componentwise or characteristic-wise reconstruction (which take no account of the source term) does not lead to a method that is well-balanced, even though the source term is accounted for in the Riemann solves. This is because the reconstruction has already introduced variation in the solution.

In order to get a high-order well-balanced scheme, the  $f$ -wave Riemann solver in combination with a wave-slope reconstruction approach is used. This reconstruction is presented in the next section.

**2.7. Reconstruction.** The reconstruction (2.12) should be performed in a manner that yields high order accuracy but avoids spurious oscillations near discontinuities. For this purpose, we use weighted essentially non-oscillatory (WENO) reconstruction [19]. The spatial accuracy of the method will in general be equal to that of the reconstruction. In the present work we employ fifth-order WENO reconstruction.

For systems of equations, the simplest approach to reconstruction is *component-wise reconstruction*, which consists of simply applying the scalar reconstruction approach to each element of  $q$ . A more sophisticated approach is *characteristic-wise reconstruction*, in which an eigendecomposition of  $q$  is performed, followed by reconstruction of each eigencomponent. For problems with spatially-varying coefficients, even the characteristic-wise reconstruction may not be satisfying, since it involves comparing coefficients of eigenvectors whose direction in state space varies from one cell to the next. In Clawpack, an alternative kind of TVD limiting known as *wave limiting* has been implemented and shown to be effective for such problems.

**2.7.1. Wave-slope reconstruction.** In order to implement a wave-type WENO limiter, we rewrite the WENO reconstruction in terms of ratios of differences in  $Q$ ; i.e. we write

$$\begin{aligned} q_{i-\frac{1}{2}}^R &= Q_i - \phi(\theta_{i-\frac{1}{2}, 2-k}, \dots, \theta_{i-\frac{1}{2}, k-1}) \Delta Q_{i-\frac{1}{2}} \\ q_{i+\frac{1}{2}}^L &= Q_i + \phi(\theta_{i+\frac{1}{2}, 1-k}, \dots, \theta_{i+\frac{1}{2}, k-2}) \Delta Q_{i-\frac{1}{2}}, \end{aligned}$$

where

$$\theta_{i-\frac{1}{2},j} = \frac{\Delta Q_{i-\frac{1}{2}+j}}{\Delta Q_{i-\frac{1}{2}}}$$

and  $\phi$  is a nonlinear function defined implicitly by the WENO reconstruction procedure. The following reconstruction method, which we refer to as *wave-slope reconstruction*, accounts for spatial variation in the coefficients of the hyperbolic system. At each interface  $x_{i-\frac{1}{2}}$ , a Riemann problem is solved using the adjacent cell average values  $Q_{i-1}, Q_i$  as left and right states, just as in the implementation of Godunov's method. This results in a set of waves  $\mathcal{W}_{i-\frac{1}{2}}^p$ . The reconstructed values are given by

$$\begin{aligned} q_{i-\frac{1}{2}}^L &= Q_{i-1} + \sum_p \phi_{i-\frac{1}{2}}^p(\theta_{i+\frac{1}{2},1-k}, \dots, \theta_{i+\frac{1}{2},k-2}) \mathcal{W}_{i-\frac{1}{2}}^p \\ q_{i-\frac{1}{2}}^R &= Q_i - \sum_p \phi_{i-\frac{1}{2}}^p(\theta_{i-\frac{1}{2},2-k}, \dots, \theta_{i-\frac{1}{2},k-1}) \mathcal{W}_{i-\frac{1}{2}}^p, \end{aligned}$$

where

$$\theta_{i-\frac{1}{2}}^p = \frac{\mathcal{W}_{i-\frac{1}{2}}^p \cdot \mathcal{W}_{i-\frac{1}{2}}^p}{\mathcal{W}_{i-\frac{1}{2}}^p \cdot \mathcal{W}_{i-\frac{1}{2}}^p}.$$

**2.7.2.  $f$ -wave-slope reconstruction.** Wave-slope reconstruction can also be performed using an  $f$ -wave Riemann solver. This is useful for computing near-equilibrium solutions of balance laws, since application of (2.28) will lead to a constant reconstructed function in regions where source terms and hyperbolic terms are balanced. We refer to this as  $f$ -wave-slope reconstruction; the algorithm is identical to that outlined above except that, since the  $f$ -waves have the form of a  $q$  increment multiplied by the wave speed, the waves  $\mathcal{W}^p$  are computed as  $\mathcal{W}^p = \mathcal{Z}^p/s^p$ . Particular attention must be given to the special situations of  $s^p = 0$  or  $s^p$  very close to machine zero.

**2.8. Time integration.** The semi-discrete scheme can be integrated in time using any initial-value ODE solver. Herein we use the ten-stage fourth-order strong-stability-preserving Runge-Kutta scheme of [6]. This method has a large stability region and a large SSP coefficient, allowing use of a large CFL number in practical computations. In all numerical examples of the next section, a CFL number of 2.45 is used.

To summarize, the full semi-discrete algorithm used in each Runge-Kutta stage is as follows.

0. (*only if using wave-slope reconstruction*) Solve the Riemann problem at each interface  $x_{i-\frac{1}{2}}$  using the adjacent cell average values  $Q_{i-1}, Q_i$  as left and right states.
1. Compute the reconstructed piecewise function  $\tilde{q}$ , and in particular the states  $q_{i-\frac{1}{2}}^R, q_{i+\frac{1}{2}}^L$  in each cell, using component-wise, characteristic-wise, or wave-slope reconstruction.
2. At each interface  $x_{i-\frac{1}{2}}$ , compute the fluctuations  $\mathcal{A}^+ \Delta q_{i-\frac{1}{2}}$  and  $\mathcal{A}^- \Delta q_{i-\frac{1}{2}}$  by solving the Riemann problem with initial states  $(q_{i-\frac{1}{2}}^L, q_{i-\frac{1}{2}}^R)$ .
3. Over each cell, compute the integral  $\int A(\tilde{q}) \tilde{q}_x dx$ . For conservative systems this is just the total fluctuation  $\mathcal{A} \Delta q_i$ .
4. Compute  $\partial Q / \partial t$  using the semi-discrete scheme (2.17).

Note again that, for conservative systems, the quadrature in step 3 requires nothing more than evaluating and differencing the fluxes.

**2.9. Extension to Two Dimensions.** In this section, we extend the numerical wave propagation method to two dimensions using a simple dimension-by-dimension approach. The method is applicable to systems of the form

$$q_t + A(q, x, y)q_x + B(q, x, y)q_y = 0 \quad (2.29)$$

on uniform Cartesian grids.

The 2D analog of the semi-discrete scheme (2.20) is

$$\begin{aligned} \frac{\partial Q_{ij}}{\partial t} = & -\frac{1}{\Delta x \Delta y} \left( \mathcal{A}^- \Delta q_{i+\frac{1}{2},j} + \mathcal{A}^+ \Delta q_{i-\frac{1}{2},j} + \mathcal{A} \Delta q_{i,j} \right. \\ & \left. + \mathcal{B}^- \Delta q_{i,j+\frac{1}{2}} + \mathcal{B}^+ \Delta q_{i,j-\frac{1}{2}} + \mathcal{B} \Delta q_{i,j} \right). \end{aligned} \quad (2.30)$$

For the method to be high order accurate, the fluctuation terms like  $\mathcal{A}^- \Delta q_{i+\frac{1}{2},j}$  should involve integrals over cell edges, while the total fluctuation terms like  $\mathcal{A} \Delta q_{i,j}$  should involve integrals over cell areas. This can be achieved by forming a genuinely multidimensional reconstruction of  $q$  and using, e.g., Gauss quadrature. An implementation following this approach exists in the SharpClaw software. For nonlinear problems containing shocks, the genuinely multidimensional reconstruction has been found to be inefficient (at least for some simple test problems), as it typically yields only a small improvement in accuracy over the dimension-by-dimension scheme given below, but has a much greater computational cost on the same mesh. Recently, this result has been reported in Zhang et al. [21]. In the latter work, it has been shown that for high precision simulation of smooth flows, a genuinely multidimensional reconstruction could take less CPU time to reach the same error threshold than the dimension-by-dimension scheme. The reason is that they are both high order accurate for linear systems, but the first scheme is only second-order accurate for nonlinear systems, whereas the second one is still high order accurate. A careful comparison of the two approaches is left for future work. Indeed, for problems containing both shocks and rich smooth flow structures (e.g. shocks interactions with turbulent boundary layer or shock interaction with vortices), lower order methods usually are too dissipative and high order stable methods such as WENO could represent an efficient alternative.

We now describe the dimension-by-dimension scheme for a single Runge-Kutta stage. We first reconstruct piecewise-polynomial functions  $\tilde{q}_j(x)$  along each row of the grid and  $\tilde{q}_i(y)$  along each column, by applying a 1D reconstruction procedure to each slice. We thus obtain reconstructed values

$$\tilde{q}_j^R(x_{i-\frac{1}{2}}) \approx q(x_{i-\frac{1}{2}}, y_j) \quad (2.31a)$$

$$\tilde{q}_j^L(x_{i+\frac{1}{2}}) \approx q(x_{i+\frac{1}{2}}, y_j) \quad (2.31b)$$

$$\tilde{q}_i^R(y_{j-\frac{1}{2}}) \approx q(x_i, y_{j-\frac{1}{2}}) \quad (2.31c)$$

$$\tilde{q}_i^L(y_{j+\frac{1}{2}}) \approx q(x_i, y_{j+\frac{1}{2}}) \quad (2.31d)$$

for each cell  $i, j$ . The fluctuation terms in (2.30) are determined by solving Riemann problems between the appropriate reconstructed values; for instance  $\mathcal{B}^- \Delta q_{i,j+\frac{1}{2}}$  is determined by solving a Riemann problem in the  $y$ -direction with initial states  $(q_{i,j+\frac{1}{2}}^L, q_{i,j+\frac{1}{2}}^R)$ . In the case of conservative systems or piecewise-constant coefficients, the total fluctuation terms  $\mathcal{A} \Delta q_{i,j}$  and  $\mathcal{B} \Delta q_{i,j}$  can be similarly determined by summing the left- and right-going fluctuations of an appropriate Riemann problem. Thus, for instance,  $\mathcal{B} \Delta q_{i,j}$  is determined by solving Riemann problem in the  $y$ -direction with initial states  $(q_{i,j-\frac{1}{2}}^R, q_{i,j+\frac{1}{2}}^L)$ .

**3. Numerical applications.** In this section we present results of numerical tests using the wave propagation methods just described. The examples included are chosen to emphasize the advantages of the

wave propagation approach, as reviewed above. We make some comparisons with the well-known second-order wave propagation code Clawpack [15, 14]).

**3.1. Acoustics.** In this section, the high-order wave propagation algorithm is applied to the 1D equations of linear acoustics in piecewise homogeneous materials:

$$p_t + K(x, y)(u_x + v_y) = 0 \quad (3.1a)$$

$$u_t + \frac{1}{\rho(x, y)}p_x = 0 \quad (3.1b)$$

$$v_t + \frac{1}{\rho(x, y)}p_y = 0. \quad (3.1c)$$

Here  $p$  is the pressure and  $u, v$  are the x- and y-velocities, respectively. The coefficients  $\rho$  and  $K$ , which vary in space, are the density and bulk modulus of the medium. We will also refer to the sound speed  $c = \sqrt{K/\rho}$ . Notice that in general since  $\rho$  varies in space, the last two equations above are not in conservation form. This test case demonstrates that the proposed approach is able to solve hyperbolic system of equations written in nonconservative form. Of course, this system can be written in conservative form as follows:

$$\epsilon_t - (u_x + v_y) = 0 \quad (3.2a)$$

$$\rho(x, y)u_t - (K(x, y)\epsilon)_x = 0 \quad (3.2b)$$

$$\rho(x, y)v_t - (K(x, y)\epsilon)_y = 0, \quad (3.2c)$$

Where  $\epsilon = -p/K$  is the strain. As we will see, the latter form may be advantageous in terms of the accuracy that can be obtained.

We assume the material is homogeneous in each computational cell and apply an exact Riemann solver at each interface; for details of this solver see e.g. [5].

**3.1.1. One-dimensional acoustics.** We first consider one-dimensional acoustic waves in a piecewise-constant medium with a single interface. Namely, we solve (3.1) on the interval  $x \in [-10, 10]$  with

$$(\rho, c) = \begin{cases} (\rho_l, c_l) & x < 0 \\ (\rho_r, c_r) & x > 0 \end{cases}$$

We measure the convergence rate of the solution in order to verify the order of accuracy for smooth solutions. The initial condition is a compact, six-times differentiable purely right-moving pulse:

$$p(x, 0) = \frac{((x - x_0) - a)^6((x - x_0) + a)^6}{a^{12}}\xi(x - x_0)$$

$$u(x, 0) = p(x, 0)/Z(x)$$

where

$$\xi(x - x_0) = \begin{cases} 0 & \text{for } |x - x_0| > a \\ 1 & \text{for } |x - x_0| \leq a. \end{cases}$$

with  $x_0 = -4$  and  $a = 1$ . This condition was chosen to be sufficiently smooth to demonstrate the design order of the scheme and to give a solution that is identically zero at the material interface at the initial and final times.

Table 3.1 shows  $L_1$  errors and convergence rates for propagation in a homogeneous medium with  $\rho_l = c_l = \rho_r = c_r = 1$ . Here we use componentwise reconstruction. Specifically, we compute

$$E_{L_1} = \Delta x \sum_i |Q_i - \bar{Q}_i| \quad (3.3)$$

where  $\bar{Q}_i$  is a highly accurate solution cell average computed by characteristics or by using a very fine grid. For the acoustics problems in this section,  $\bar{Q}$  is computed using characteristics and adaptive Gauss quadrature. Table 3.1 indicates that in each case, the order of convergence is approximately equal to the design order of the discretization.

TABLE 3.1  
*Errors for homogeneous acoustics test*

mx	SharpClaw		Clawpack	
	Error	Order	Error	Order
200	3.60e-02		4.10e-02	
400	3.65e-03	3.30	1.30e-02	1.66
800	1.85e-04	4.31	3.61e-03	1.85
1600	7.35e-06	4.65	8.94e-04	2.01

To test the accuracy in the presence of discontinuous coefficients we take

$$\rho_l = c_l = 1 \quad \rho_r = 4 \quad c_r = 1/2,$$

with an impedance ratio of  $Z_r/Z_l = 2$ . As was noted in [1], this system can also be solved in the conservative form (3.2) using the  $f$ -wave approach. We include results of this approach, where we have also performed characteristic-wise rather than component-wise reconstruction. Results are shown in Table 3.2. In this case all schemes exhibit a convergence rate below the formal order, even though the initial and final solutions are smooth. To investigate this further, we repeat the same test with a wider pulse by taking  $a = 4$ . Results are shown in Table 3.3.

For the latter test, we observe a convergence rate of approximately two for SharpClaw, one for Clawpack, and five for SharpClaw using the  $f$ -wave approach and characteristic-wise reconstruction. The last convergence rate is remarkable, considering that the solution is not differentiable when it passes through the material interface. Further investigation of the accuracy of this approach for more complicated problems with discontinuous coefficients is ongoing. In tests not shown here, Clawpack achieves approximately second-order accuracy when used with an  $f$ -wave Riemann solver for this problem.

TABLE 3.2  
*Errors for acoustics interface with narrow pulse*

mx	SharpClaw		SharpClaw $f$ -wave		Clawpack	
	Error	Order	Error	Order	Error	Order
200	2.10e-01		9.50e-02		1.98e-01	
400	5.98e-02	1.81	1.42e-02	2.74	7.26e-02	1.45
800	1.25e-02	2.26	1.42 e-03	3.32	2.21e-02	1.71
1600	1.17e-03	3.42	1.20e-04	3.56	7.86e-03	1.49

TABLE 3.3  
 $L^1$  Errors for acoustics interface problem with wide pulse ( $a=4$ )

mx	SharpClaw		SharpClaw $f$ -wave		Clawpack	
	Error	Order	Error	Order	Error	Order
200	9.67e-03		5.01e-03		5.23e-02	
400	2.01e-03	2.27	4.63e-04	3.44	2.32e-02	1.17
800	4.89e-04	2.04	2.51e-05	4.36	1.09e-02	1.09
1600	1.22e-04	2.00	6.49e-07	5.12	5.26e-03	1.05



FIG. 3.1. Pressure in the sonic crystal for a long wavelength plane wave incident from the left.

**3.1.2. A Two-dimensional sonic crystal.** In this section we model sound propagation in a sonic crystal. A sonic crystal is a periodic structure composed of materials with different sound speeds and impedances. The periodic inhomogeneity can give rise to *bandgaps* – frequency bands that are completely reflected by the crystal. This phenomenon is widely utilized in photonics, but its significance for acoustics has only recently been considered. Photonic crystals can be analyzed quite accurately using analytic techniques, since they are essentially infinite size structures relative to the wavelength of the waves of interest. In contrast, sonic crystals are typically only a few wavelengths in size, so that the effects of their finite size cannot be neglected. For more information on sonic crystals, see for instance the review paper [17].

We consider a square array of square rods in air with a plane wave disturbance incident parallel to one of the axes of symmetry. The array is infinitely wide but only eight periods deep. The lattice spacing is 10 cm and the rods have a cross-sectional side length of 4 cm, so that the filling fraction is 0.16. This crystal is similar to one studied in [18], and it is expected that sound waves in the 1200-1800 Hz range will experience severe attenuation in passing through it, while longer wavelengths will not be significantly attenuated.

A numerical instability very similar to that observed in 1D simulations in [4, 5] was observed when the standard Clawpack method was applied to this problem. The fifth-order WENO method with characteristic-wise limiting showed no such instability.

Figure 3.1 shows the RMS pressure for a plane wave with  $k = 15$  incident from the left. This wave has a frequency of about 800 Hz, well below the partial band gap. As expected, the wave passes through the crystal without significant attenuation. In Figure 3.2, the pressure is plotted along a slice in the  $x$ -direction approximately midway between rows of rods.

Figure 3.3 shows the RMS pressure for an incident plane wave with frequency 1600 Hz, inside the partial bandgap. Notice that the wave is almost entirely reflected, resulting in a standing wave in front of the crystal. Figure 3.4 shows the RMS pressure along a slice in the  $x$ -direction.

**3.2. Nonlinear Elasticity in a Spatially Varying Medium.** In this section we consider a more difficult test involving nonlinear wave propagation and many material interfaces. This problem was considered previously in [10] and studied extensively in [11]. Solitary waves were observed to arise from the interaction of nonlinearity and an effective dispersion due to material interfaces in layered media.

Elastic compression waves in one dimension are governed by the equations

$$\epsilon_t(x, t) - u_x(x, t) = 0 \quad (3.4a)$$

$$(\rho(x)u(x, t))_t - \sigma(\epsilon(x, t), x)_x = 0. \quad (3.4b)$$

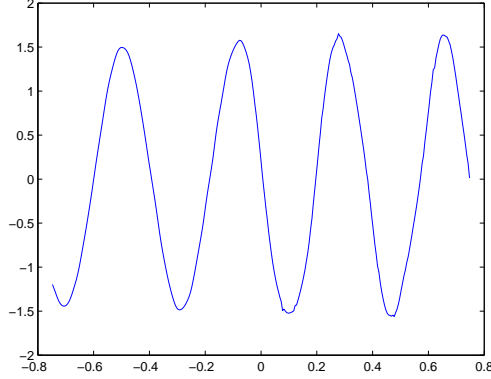


FIG. 3.2. *Pressure in the sonic crystal for a long wavelength plane wave incident from the left.*



FIG. 3.3. *RMS pressure in the sonic crystal for a plane wave incident from the left.*

where  $\epsilon$  is the strain,  $u$  the velocity,  $\rho$  the density, and  $\sigma$  the stress. This is a conservation law of the form (1.1), with

$$q(x, t) = \begin{pmatrix} \epsilon \\ \rho(x)u \end{pmatrix} \quad f(q, x) = \begin{pmatrix} -u \\ -\sigma(\epsilon, x) \end{pmatrix}.$$

Note that the density and the stress-strain relationship vary in  $x$ . The Jacobian of the flux function is

$$f'(q) = \begin{pmatrix} 0 & -1/\rho(x) \\ -\sigma_\epsilon(\epsilon, x) & 0 \end{pmatrix}.$$

In the case of the linear stress-strain relation  $\sigma(x) = K(x)\epsilon(x)$ , (3.4) is equivalent to the one-dimensional form of the acoustics equations considered in the previous section.

We consider the piecewise constant medium studied in [10, 11]:

$$(\rho(x), K(x)) = \begin{cases} (1, 1) & \text{if } j < x < (j + \frac{1}{2}) \text{ for some integer } j \\ (4, 4) & \text{otherwise,} \end{cases} \quad (3.5)$$

with exponential stress-strain relation

$$\sigma(\epsilon, x) = \exp(K(x)\epsilon) - 1. \quad (3.6)$$

The initial condition is uniformly zero, and the boundary condition at the left generates a half-cosine pulse.

We solve this problem using the  $f$ -wave solver developed in [10]. Figure 3.5 shows a comparison of results using Clawpack and SharpClaw on this problem, with 24 cells per layer. The SharpClaw results are significantly more accurate.

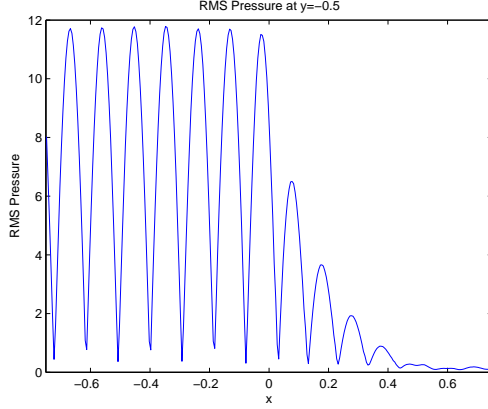


FIG. 3.4. *RMS pressure in the sonic crystal along a slice.*

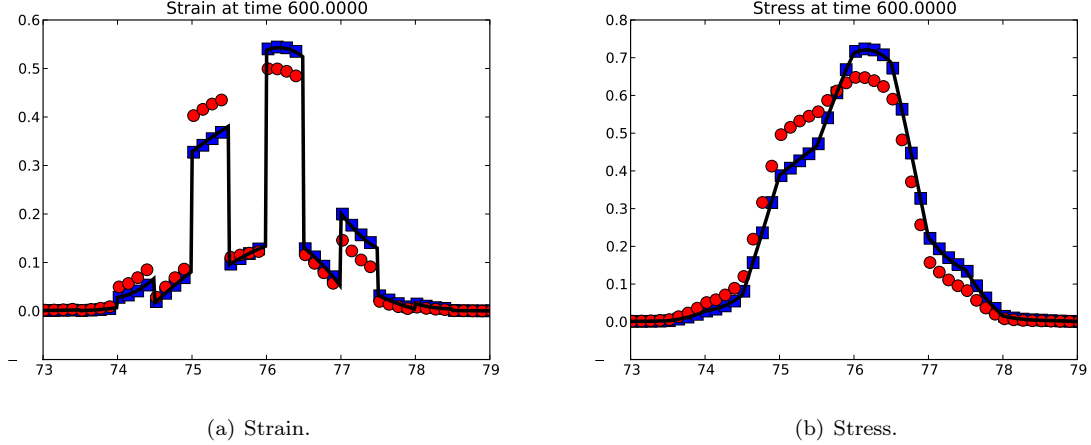


FIG. 3.5. *Comparison of Clawpack (red circles) and SharpClaw (blue squares) solution of the stegoton problem using 24 cells per layer. For clarity, only every third solution point is plotted. The black line represents a very highly resolved solution.*

Solutions of (3.4) are time-reversible in the absence of shocks. As discussed in [7, 9], the effective dispersion induced by material inhomogeneities suppresses the formation of shocks, for small amplitude initial and boundary conditions, rendering the solution time-reversible for very long times. This provides a useful numerical test. We solve the stegoton problem numerically up to time  $T$ , then negate the velocity and continue solving to time  $2T$ . The solution at any time  $2T - t_0$ , with  $t_0 \leq T$ , should be exactly equal to the solution at  $t_0$ . We take  $T = 600$  and  $t_0 = 60$ . Figure 3.6(a) shows the solution obtained using SharpClaw on a grid with 24 cells per layer. The  $t = 1140$  solution (squares) is in excellent agreement with the  $t = 60$  solution (solid line). In fact, the maximum point-wise difference has magnitude less than  $2 \times 10^{-2}$ . Using a grid twice as fine, with 48 cells per layer, reduces the point-wise difference to  $1 \times 10^{-3}$ . The Clawpack solution, computed on the same grid (24 cells per layer), is shown in Figure 3.6(b). Again, the SharpClaw



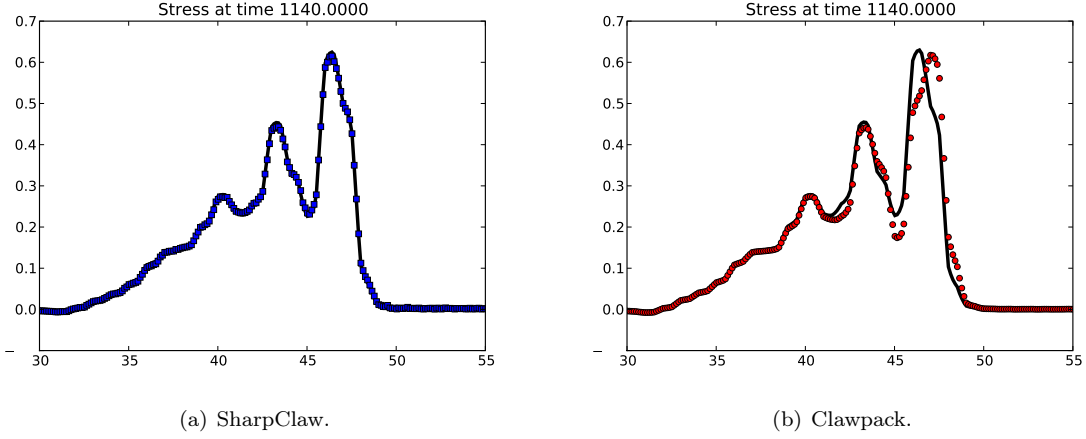


FIG. 3.6. Comparison of forward solution (black line) and time-reversed solution (symbols).

solution is noticeably more accurate. For a more detailed study of this time-reversibility test, we refer to [9].

**3.3. Shallow Water Flow.** In order to show the capabilities of the proposed scheme to deal with nonlinear problems with source terms, the shallow water equations are also considered. The conservative form of the depth-averaged equations of mass and momentum in two space dimensions can be written as follows:

$$h_t + (hu)_x + (hv)_y = 0 \quad (3.7a)$$

$$(hu)_t + \left( \frac{1}{2}hu^2 + \frac{1}{2}gh^2 \right)_x + (huv)_y = -ghb_x \quad (3.7b)$$

$$(hv)_t + (huv)_x + \left( \frac{1}{2}hv^2 + \frac{1}{2}gh^2 \right)_y = -ghb_y, \quad (3.7c)$$

where  $h$ ,  $u$  and  $v$  are the depth of the fluid and the velocity components in  $x$  and  $y$  directions, respectively. The function  $b(x, y)$  is the bottom elevation and  $g$  is constant for gravitational acceleration.

In the following section, two test cases are presented: a radially symmetric dam-break problem over a flat bottom topography ( $b = 0$ ) and a small perturbation of a steady state over a hump.

**3.3.1. Radial dam-break problem.** This problem consists in computing the flow induced by the instantaneous collapse of an idealized circular dam. It is widely used to benchmark various numerical techniques that tend to simulate interfacial flows and impact problems.

The dam, which is an infinitesimally thin circular wall with a radius of 0.5, is located at the center of a square computational domain of  $2.5 \times 2.5$ . The water level is initially  $h = 2.0$  inside the circle and  $h = 1.0$  outside. The initial solution has zero discharge, i.e. both velocity components are zero. The dam is removed at time  $t = 0$ . This tests the ability of the method to compute the 2D propagation of nonlinear waves and the extent to which symmetry is preserved in the numerical solution. In the presence of radial symmetry,

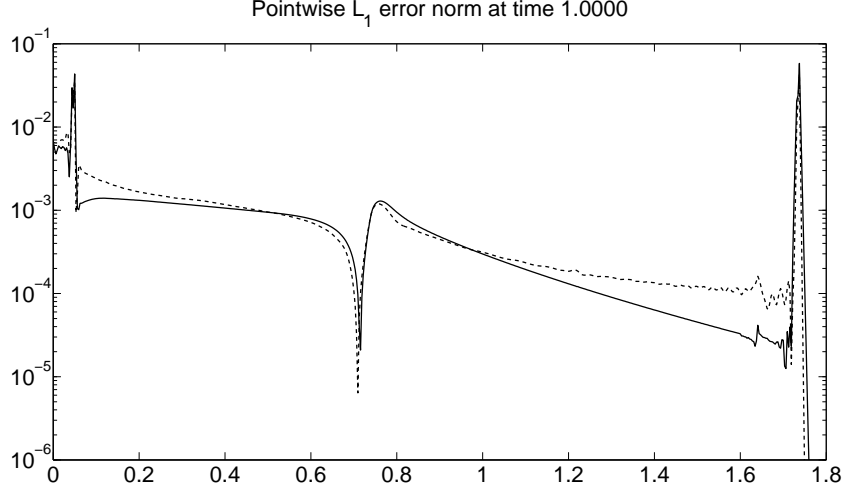


FIG. 3.7. Pointwise absolute error for the water height  $h$  on a grid with 800 cells. SharpClaw solution: continuous line; Clawpack solution: dashed line.

system (3.7) can be recast in the following form:

$$h_t + (hU)_r = -\frac{hU}{r} \quad (3.8a)$$

$$(hU)_t + \left( \frac{1}{2}hU^2 + \frac{1}{2}gh^2 \right)_r = -\frac{hU^2}{r}, \quad (3.8b)$$

where  $h$  is still the depth of the fluid, whereas  $U$  and  $r$  are the radial velocity and the radial position. An important feature of these equations is the presence of a source term, which physically arises from the fact that the fluid is spreading out and it is impossible to have constant depth and constant non-zero radial velocity.

A first comparison between SharpClaw and Clawpack is performed by solving the 1D system (3.8) on the interval  $0 \leq r \leq 2.5$ . A wall boundary condition and non-reflecting boundary condition are imposed at the left and the right boundaries, respectively. The final time for the analysis is taken to be  $t = 1$ . The classical  $q$ -wave Riemann solver based on the Roe linearization is used to solve the Riemann problem at each interface (see for instance [14] for details), where the left and the right states are computed by using the characteristic-wise WENO reconstruction. The gravitational acceleration is set to  $g = 1$ . A highly resolved solution obtained with Clawpack on a grids with 25,600 cells is used as a reference solution. The  $q$ -wave Riemann solver

It is well-known that formal order of accuracy is lost in a shock wave propagating in a coupled system of equation [16] and in general it is reduced to first-order. However, if we plot the difference between the computed solution available at the cell's center and the reference solution conservatively averaged on the same grid, i.e.  $E_i = |Q_i - \bar{Q}_i|$ , then we can visualize where the errors are largest as well as their spatial structure. Figure 3.7 shows this difference, for a grid with 800 cells. The largest errors in both solutions are near the shocks. In the smooth regions, the SharpClaw solution is more accurate than that of the Clawpack code.

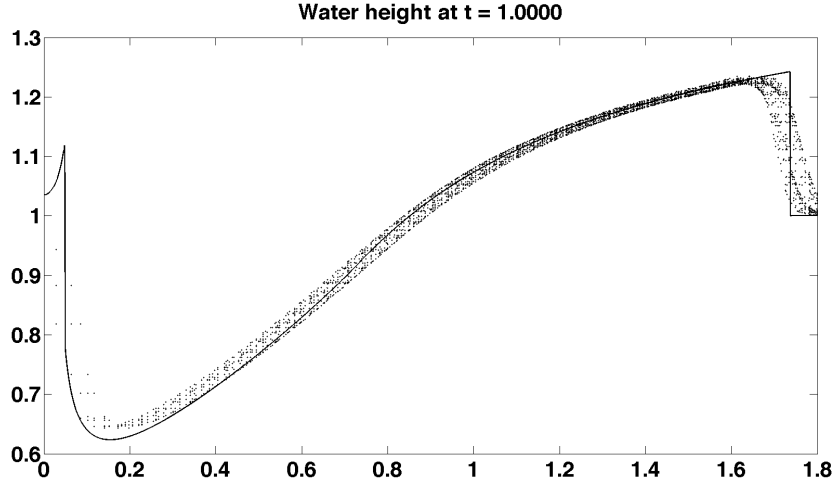


FIG. 3.8. Solution for the 2D radial dam-break problem on a grid with  $125 \times 125$  cells, plotted as a function of radius.

Next we consider the same problem using the full 2D equations (3.7). The SharpClaw and Clawpack codes are tested on two grids with  $125 \times 125$  and  $500 \times 500$  cells. The final time for the analysis is again taken to be  $t = 1$ .

Figure 3.8 shows the water height  $h$  at  $t = 1.0$ . The 1D reference solution used before is also plotted for comparison. Clawpack results (not shown) indicate similar accuracy and similarly good symmetry, show that the solutions are similar and both schemes can preserve a good radial symmetry, though they cannot resolve the shock near the origin. The grid is in fact too coarse.

The solutions obtained on the finer grid ( $500 \times 500$  cells) are shown in Figure 3.9. The effect of the grid refinement is clearly visible. In fact, the solutions gets close to the reference solution. However, the density of the grid near the origin is still coarse to resolve well the shock near the origin.

**3.3.2. Perturbation of a steady state solution.** Conservation laws with source terms often have steady states in which the flux gradient are non-zero but exactly balanced by source terms. A good numerical scheme, should be able to preserve such steady states and calculate accurately small perturbations around these conditions. A classical benchmark test case to investigate these properties is the small perturbation of a 2D steady state water given by LeVeque [13].

System (3.7) is solved in a rectangular domain  $[0, 2] \times [0, 1]$ , with a bottom topography characterized by an isolated elliptical shaped hump:

$$b(x, y) = 0.8 \exp(-5(x - 0.9)^2 - 50(y - 0.5)^2).$$

The surface is initially flat with  $h(x, y, 0) = 1 - b(x, y)$  except for  $0.05 < x < 0.15$ , where  $h$  is perturbed upward by  $\epsilon = 0.01$ . The initial discharge in both direction is zero, i.e.  $hu(x, y, 0) = hv(x, y, 0) = 0$ . Non-reflecting (i.e., zero-extrapolation) conditions are imposed at all boundaries. The gravitational acceleration is set to 9.81.

An effort was made to achieve a well-balanced scheme using the  $f$ -wave approach combined with component-wise or characteristic-wise WENO reconstruction, but this was unsuccessful. This is not surprising, since the algorithm begins by reconstructing a non-constant function. Figure 3.10 shows the contour levels of the solution at  $t = 0.06$  and  $t = 0.12$  on a fine grid with  $600 \times 300$  cells, obtained with the  $f$ -wave

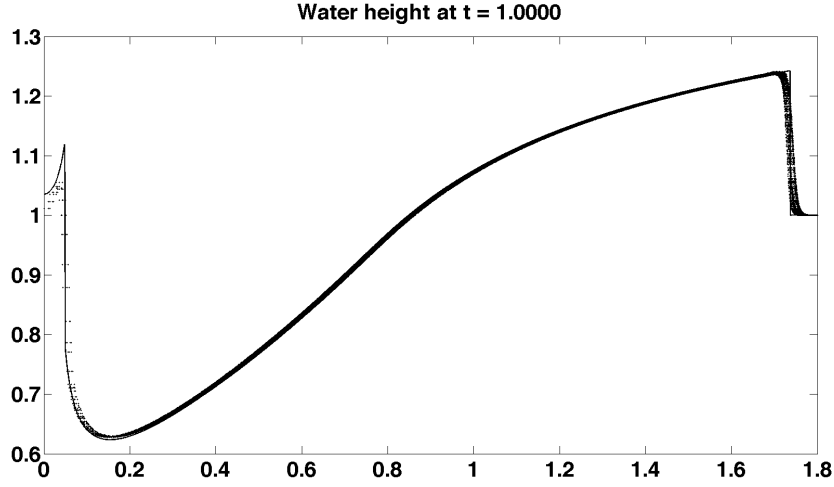


FIG. 3.9. Solution for the 2D radial dam-break problem on a grid with  $500 \times 500$  cells, plotted as a function of radius.

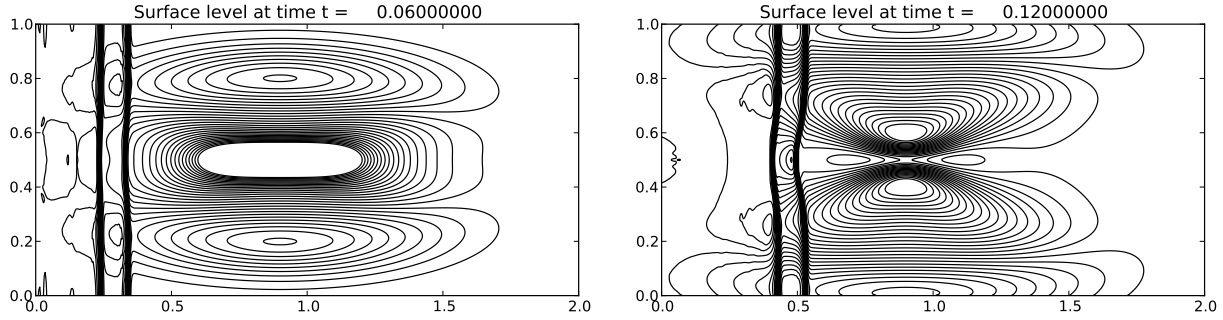


FIG. 3.10. Contour of the surface level  $h + b$  at time  $t = 0.06$  and  $t = 0.12$ . Component-wise reconstruction approach. Contour levels: 0.99942 : 0.000238 : 1.00656.

Riemann solver and the component-wise reconstruction approach as a building block for the WENO scheme. The scheme is not well-balanced and spurious waves are generated around the hump. Similar results are obtained using characteristic-wise reconstruction.

In order to balance the scheme, the  $f$ -wave-slope reconstruction introduced in Section 2.7 is used instead. In this approach, the WENO reconstruction is applied to waves computed by solving Riemann problems with the  $f$ -wave solver. When the source term is included in these Riemann problems, the resulting waves vanish exactly. Figure 3.11 shows the surface level a cross section along  $y = 0.5$  at time  $t = 0.06$  computed with both reconstruction approaches (and the  $f$ -wave Riemann solver) on a uniform mesh with  $600 \times 300$ . It is seen that the  $f$ -wave-slope reconstruction method keeps the surface flat, whereas the component-wise reconstruction introduces spurious waves which have an amplitude of the order of the disturbance that we want to resolve.

Figure 3.12 shows the solution on two uniform meshes with  $200 \times 100$  cells and  $600 \times 300$  cells, computed using the  $f$ -wave-slope reconstruction approach. The results clearly indicate that the detailed structure of

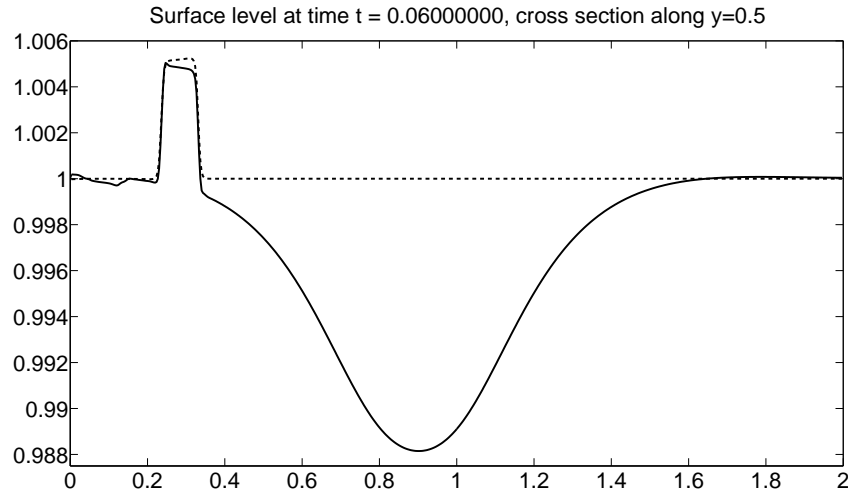


FIG. 3.11. Surface level  $h + b$  along a cross section at  $y = 0.5$  and time  $t = 0.06$ . Solid line:  $f$ -wave Riemann solver and component-wise reconstruction; dashed line:  $f$ -wave Riemann solver and  $f$ -wave-slope reconstruction.

the evolution of such a small perturbation is resolved well even with the relatively coarse mesh. In addition, these results agree with those reported in [13].

**4. Conclusions.** We have presented a general approach to extending the finite volume wave propagation algorithm to arbitrary high order of accuracy in one and two dimensions. The algorithm is based on a method-of-lines approach, wherein the semi-discrete scheme relies on high order reconstruction and computation of fluctuations, including a *total fluctuation* term arising inside each cell. By using WENO reconstruction and strong stability preserving time integration, high order accurate non-oscillatory results are obtained, as demonstrated through a variety of test problems.

This algorithm has several desirable features. Like the second-order wave propagation algorithms in Clawpack [12], it is applicable to general hyperbolic systems (e.g. non-conservative systems or those with spatially varying flux function). It gives significantly better accuracy than Clawpack for smooth problems. It has been shown to achieve high order accuracy even for problems with discontinuous coefficients. Finally, the algorithm can be adapted to give a well-balanced scheme for general balance laws by use of the  $f$ -wave approach and a new *wave-slope reconstruction* technique.

Hyperbolic systems of equations with both smooth and non-smooth solution have been used to test the properties and the capabilities of the proposed method. The schemes have been compared for the one dimensional equations of linear acoustic in different conditions, the one dimensional nonlinear elastic equation in a spatially varying medium and the two dimensional shallow water equations with and without bottom topography. Two types of Riemann solver have been used, i.e the classical ( $q$ -) wave algorithm and the  $f$ -wave approach. The new scheme performed well for all the test cases. For the one dimensional problems the SharpClaw results are significantly more accurate than the Clawpack results, even for non-smooth solutions.

In two dimensions, the presented dimension-by-dimension reconstruction approach is formally only second-order accurate for nonlinear systems of equations (see [21]); however, it gives improved accuracy over the second-order scheme implemented in Clawpack for the test problems considered. Further investigation of different approaches to multidimensional reconstruction for problems containing both shocks and rich smooth flow structures is a topic of future research.

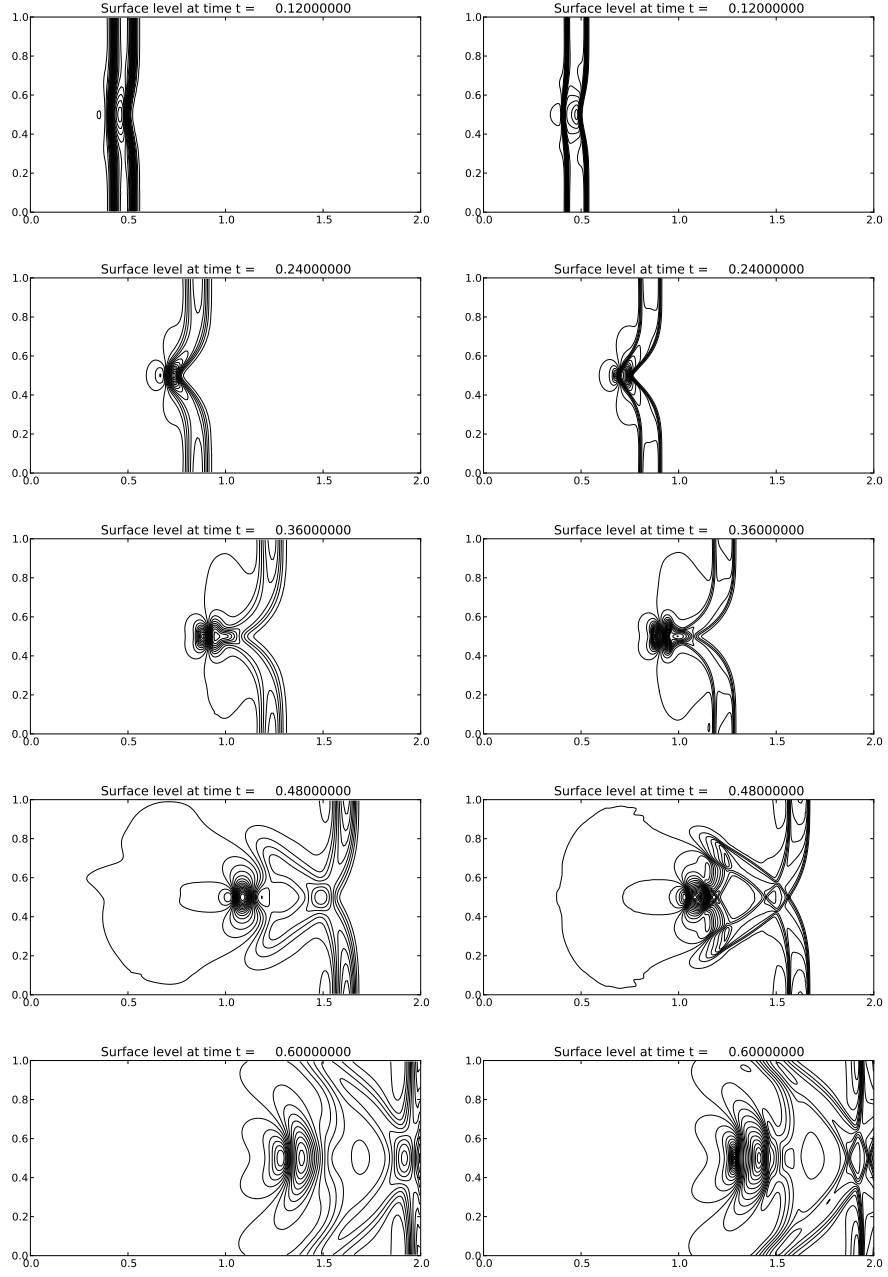


FIG. 3.12. Contour of the surface level  $h + b$ .  $f$ -wave-slope reconstruction. 30 uniformly spaced contour lines.  $t = 0.12$  from 0.99942 to 1.00656;  $t = 0.24$  from 0.99318 to 1.01659;  $t = 0.36$  from 0.98814 to 1.01161;  $t = 0.48$  from 0.99023 to 1.00508;  $t = 0.6$  from 0.995144 to 1.00629. Left: results with a  $200 \times 100$  cells. Right: results with a  $600 \times 300$  cells.

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