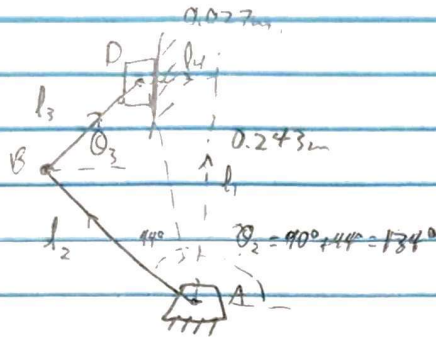


H/W3

problem 1 a)



$$\begin{aligned} l_2 &= 0.105 \text{ m} & \theta_2 &= 136^\circ \\ l_3 &= 0.172 \text{ m} & \theta_3 &= 73.6^\circ \\ l_1 &= 0.243 \text{ m} & l_{\text{arm}} &= 0.301 \text{ m} \\ l_4 &= 0.027 \text{ m} \end{aligned}$$

Initial position isn't possible,  
assuming  $l_1$  is wrong:

$$\begin{aligned} \text{Re: } l_2 \cdot \cos(136) + l_3 \cdot \cos \theta_3 + l_4 &= 0, \quad \theta_3 = \cos^{-1} \left( \frac{-l_4 - l_2 \cos \theta_2}{l_3} \right) = 74.5^\circ \\ \text{Im: } l_1 &= l_2 \cdot \sin(136) + l_3 \cdot \sin \theta_3 = 0.2413 \text{ m} \end{aligned}$$

$$\begin{aligned} \frac{d}{dt} (\bar{R}_2 + \bar{R}_3 - \bar{R}_1 + \bar{R}_4) &= 0 & \text{solve for } l \text{ in terms of } \omega_2, \\ l_2 j \omega_2 e^{j\theta_2} + l_3 j \omega_3 e^{j\theta_3} - l_1 j &= 0 \\ -l_2 \omega_2 \sin \theta_2 - l_3 \omega_3 \sin \theta_3 &= 0, \quad \omega_3 = -\frac{\omega_2 l_2 \sin \theta_2}{l_3 \sin \theta_3} \\ -l_1 j + l_2 j \omega_2 \cos \theta_2 + l_3 j \omega_3 \cos \theta_3 &= 0 \end{aligned}$$

$$\begin{aligned} \dot{l}_1 &= l_2 \cdot \omega_2 \cdot \cos \theta_2 + l_3 \cdot \left( -\frac{\omega_2 l_2 \sin \theta_2 \cdot \cos \theta_3}{l_3 \sin \theta_3} \right) & \text{mechanical advantage} &= \frac{F_{\text{out}}}{F_{\text{in}}} \\ & & F_{\text{in}} \cdot l_{\text{arm}} \cdot \omega_2 &= F_{\text{out}} \cdot \dot{l}_1 \\ & & \frac{l_{\text{arm}} \cdot \omega_2 \cdot F_{\text{out}}}{\dot{l}_1} &= F_{\text{in}} \end{aligned}$$

$$\text{mechanical advantage} = \frac{l_{\text{arm}}}{l_2 \cdot \cos \theta_2 - l_2 \cdot \frac{\sin \theta_2 \cdot \cos \theta_3}{\sin \theta_3} - \frac{l_4 - l_2 \cos \theta_2}{l_3}}$$

$$\text{mechanical advantage}(134^\circ) = 3.211$$

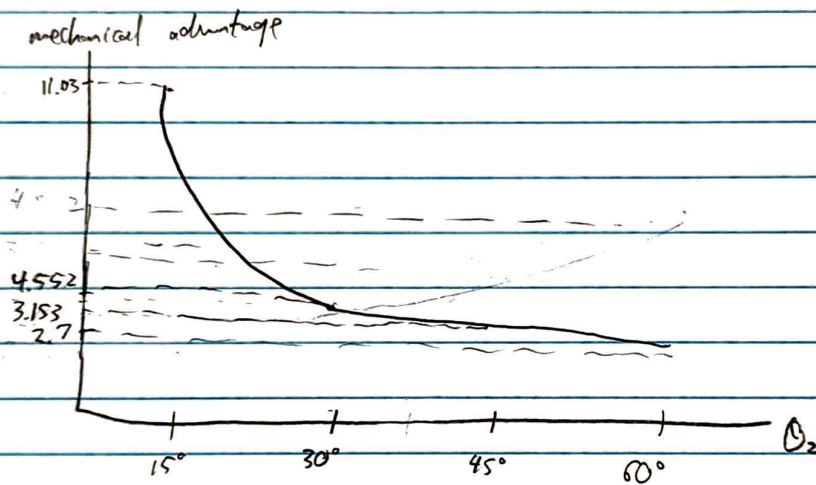
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problem b) From part a, mechanical advantage ( $\theta_2$ ) =

$$\frac{l_{cm}}{l_2 \cos \theta_2 - l_2 \sin \theta_2 \cdot \frac{-l_4 - l_2 \cos \theta_2}{l_3}} \cdot \frac{1}{\sin \left( \cos^{-1} \left( \frac{-l_4 - l_2 \cos \theta_2}{l_3} \right) \right)}$$

graphing from  $\theta_2 = 105^\circ$  to  $\theta_2 = 150^\circ$  (I defined  $\theta_2$  as  $90 +$  angle given, I used complementary angle for cleanliness)

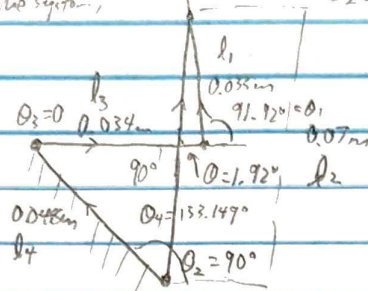
From desmos:



jhe 24.78

problem 2:

Using cod to determine the possible angles at instant of contact, given  $O_2O_4$  doesn't fully define the system, an angle for  $O_2O_4$  is required, assumed angle is  $133.149^\circ$ .



$$\frac{d}{dt}(\bar{R}_4 + \bar{R}_3 + \bar{R}_1 - \bar{R}_2) = 0$$

$$l_3 j \omega_3 e^{j\theta_3} + l_1 j \omega_1 e^{j\theta_1} - l_2 j \omega_2 e^{j\theta_2} = 0$$

$$\text{Re: } -l_3 \omega_3 \sin \theta_3 - l_1 \omega_1 \sin \theta_1 + l_2 \omega_2 \sin \theta_2 = 0, \quad 0 - 0.03478 \omega_1 + 0.07 \omega_2 = 0, \quad \omega_1 = 2.001 \omega_2$$

$$\text{Im: } l_3 \omega_3 \cos \theta_3 + l_1 \omega_1 \cos \theta_1 - l_2 \omega_2 \cos \theta_2 = 0, \quad 0.034 \omega_3 - 0.002346 \omega_2 = 0$$

$$\omega_3 = 0.069 \omega_2$$

$$P_{in} = F_{in} \cdot 0.138 \text{ m} \cdot \omega_2$$

$$P_{out} = F_{out} \cdot \omega_3 \cdot 0.082 \text{ m} \quad P_{in} = P_{out}$$

$$\text{mechanical advantage} = \frac{F_{out}}{F_{in}} = \frac{0.138 \text{ m} \cdot \omega_2}{0.082 \text{ m} \cdot 0.069 \omega_2} = 24.4$$

mechanical advantage  $\approx 24.4$ , if  $\theta$  of link  $O_2O_4$  is  $133.149^\circ$



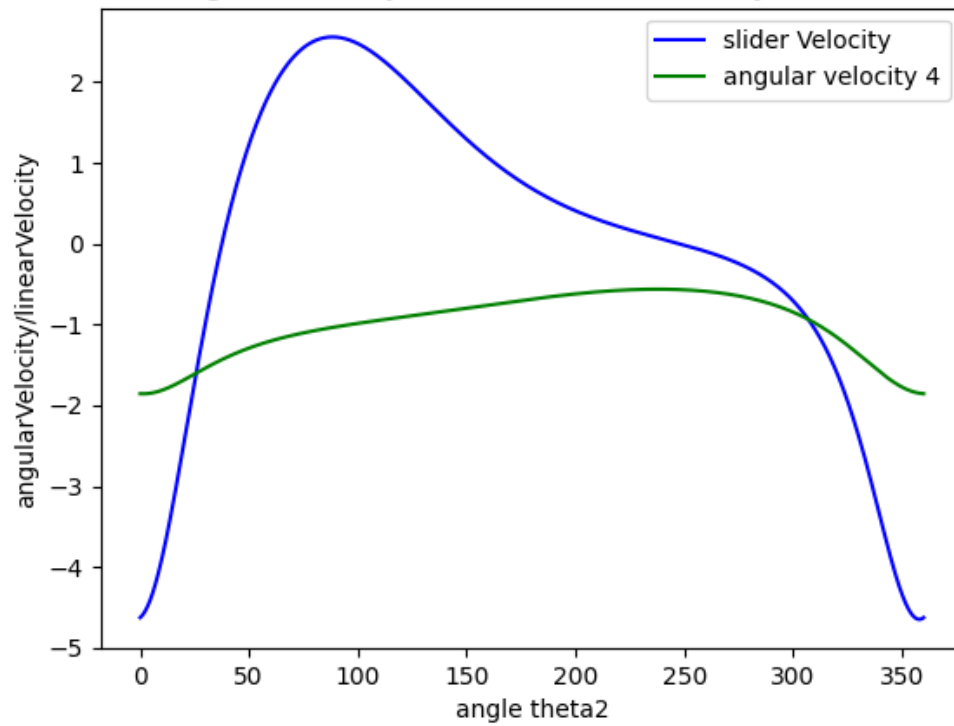
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problem 3: percent deviation over  $240^\circ$  to  $270^\circ$ :  $-202.76\%$

percent deviation over  $190^\circ$  to  $315^\circ$ :  $-386.29\%$

graphs are attached.

Link 4 Angular Velocity and Slider linear Velocity versus Theta 2



Slider linear Velocity versus Theta 2

