

# Some Issues in the Simulation of Two-Phase Flows: the relative velocity

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# Multiphase flows

What models are available

- two-fluid models
  - VOF, Euler-Euler
  - equations are solved for each phase
  - Computational expensive
- single-fluid models
  - mixture model
  - one equation only
  - Computational much more effective
  - robust just in equilibrium states
  - loss of relative velocity between phases

# Our approach

In our program

- we use the mixture model
- take the relative velocity into account
- formulate it as a relative velocity conservation equation
- implement the Lax-Friedrichs flux
- ready for 1D and 2D cases
- simple meshes only

# Our system model

Mass conservation:

$$\frac{\partial}{\partial t}(\rho) + \frac{\partial}{\partial x}(\rho u) + \frac{\partial}{\partial y}(\rho u) = S_1$$

Momentum conservation:

$$\frac{\partial}{\partial t}(\rho u_x) + \frac{\partial}{\partial x}(\rho u_x^2 + \rho c(1-c)u_{r,x}^2 + P) + \partial_y(\rho u_x u_y + \rho c(1-c)u_{r,x} u_{r,y}) = S_2$$

$$\frac{\partial}{\partial t}(\rho u_y) + \frac{\partial}{\partial y}(\rho u_y^2 + \rho c(1-c)u_{r,y}^2 + P) + \partial_x(\rho u_x u_y + \rho c(1-c)u_{r,x} u_{r,y}) = S_3$$

$\rho$  is the mixture density,  $u$  is the mixture velocity in  $x$  and  $y$  direction,  $c$  is the gas mass void fraction,  $P$  is the pressure which is the same between the gas and liquid,  $u_r$  is the relative velocity between the two phases and  $\psi(P)$  is a function that recounts the gas and liquid phases through the momentum equations.

# Our system model

relative velocity conservation:

$$\begin{aligned} \frac{\partial}{\partial t}(u_{r,x}) + \frac{\partial}{\partial x}(u_x u_{r,x} + (1 - 2c)\frac{u_{r,x}^2}{2} + \psi(P)) + \\ \frac{\partial}{\partial y}(u_x u_{r,y} + u_y u_{r,x} + (1 - 2c)u_{r,x} u_{r,y}) = S_4 \\ \frac{\partial}{\partial t}(u_{r,y}) + \frac{\partial}{\partial y}(u_y u_{r,y} + (1 - 2c)\frac{u_{r,y}^2}{2} + \psi(P)) + \\ \frac{\partial}{\partial x}(u_x u_{r,y} + u_y u_{r,x} + (1 - 2c)u_{r,x} u_{r,y}) = S_5 \end{aligned}$$

# Courant-Friedrichs-Lewy number

With this model the CFL number has to be  $< 1$

- easy in 1D and structured meshes
- difficult in 2D and unstructured meshes
- $\Delta t$  can be calculated from the eigenvalues of the Jacobien matrices
- 2 Solutions in 2D: Splitting and non-splitting scheme

# Implementation of the splitting scheme

Rewrite:

$$\frac{\partial U}{\partial t} + \frac{\partial F(U)}{\partial x} + \frac{\partial G(U)}{\partial y} = \frac{\partial U}{\partial t} + J_x(U) \frac{\partial U}{\partial x} + J_y(U) \frac{\partial U}{\partial y} = S(U), \quad (1)$$

with the fluxes  $F(U)$  and  $G(U)$  and the Jacobien  $J_x = \frac{\partial F}{\partial U}$  and  $J_y = \frac{\partial G}{\partial U}$ .

In the splitting scheme the fields are updated first in one direction with Lax-Friedrichs scheme according to

$$F_{i+1/2}^{LF} = \frac{1}{2} (F_i^n + F_{i+1}^n) + \frac{\Delta x}{2\Delta t} (U_i^n - U_{i+1}^n). \quad (2)$$

# Implementation of the splitting scheme

This is followed by the update step

$$U_i^{n+1} = U_i^n + \frac{\Delta t}{\Delta x} \left( F_{i-1/2}^{n,LF} - F_{i+1/2}^{n,LF} \right), \quad (3)$$

and with the new values in the second direction. In such case, the scheme converges for

$$\Delta t = C_{cfl} \cdot \min \left( \frac{\Delta x}{\lambda_x}, \frac{\Delta y}{\lambda_y} \right), \quad (4)$$

with  $\lambda_{x/y}$  being the largest eigenvalue of  $J_x$  and  $J_y$  respectively and  $C_{cfl} \leq 1$ .



# Implementation of the non-splitting scheme

In the non-splitting scheme the two-dimensional Lax-Friedrichs flux is updated in one step using

$$\Delta t = \frac{C_{cfl}}{\frac{\lambda_{max;x}}{\Delta x} + \frac{\lambda_{max;y}}{\Delta y}}. \quad (5)$$

We compared our results to OpenFOAM

- OpenFOAM solves the standard mixture model
- no information about the relative velocity
- Kurganov and Tadmor central-upwind scheme
- CFL number is calculated in a different way

# Results

Our test case is a rarefaction wave: Initial conditions

- left side velocity is negative
- right side velocity is positive
- density is uniform

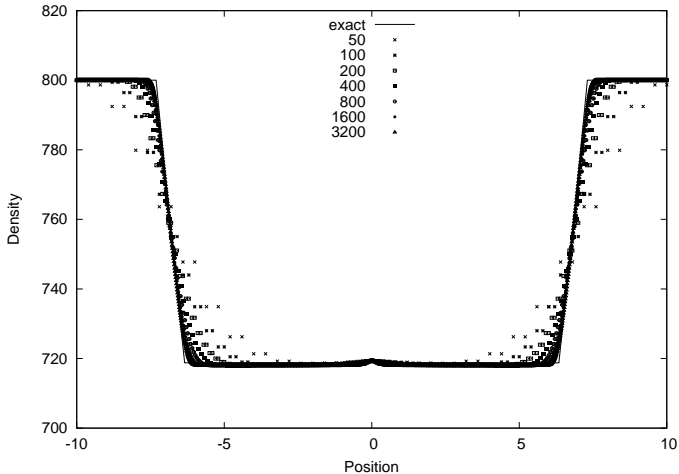


Figure : Rarefaction-waves propagation within an air-water mixture: mixture density for different lattice sizes with  $C_{cfl} = 0.9$ , compared to the exact results in one-dimension.

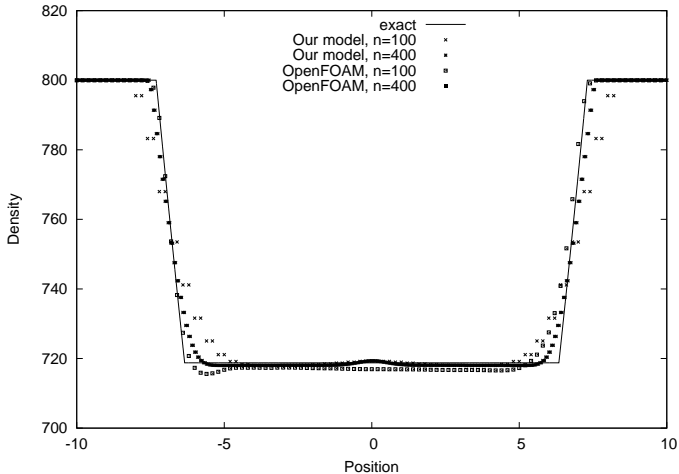


Figure : Rarefaction-waves propagation within an air-water mixture: mixture density profile computed with the mixture model of OpenFOAM and with the current model.

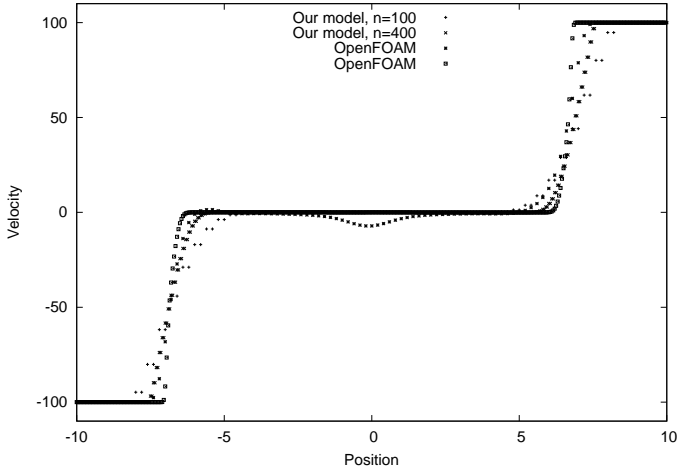


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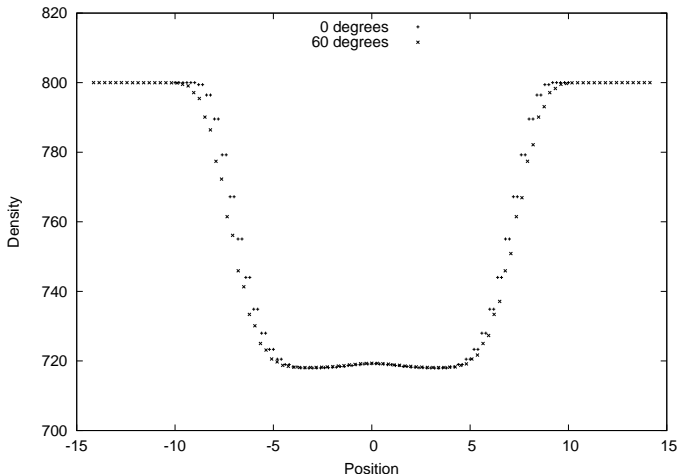


Figure : Rarefaction-waves propagation within an air-water mixture: mixture density profile for a rarefaction wave going in x-direction and with an angle of 60 degrees between the wave and the x-direction.

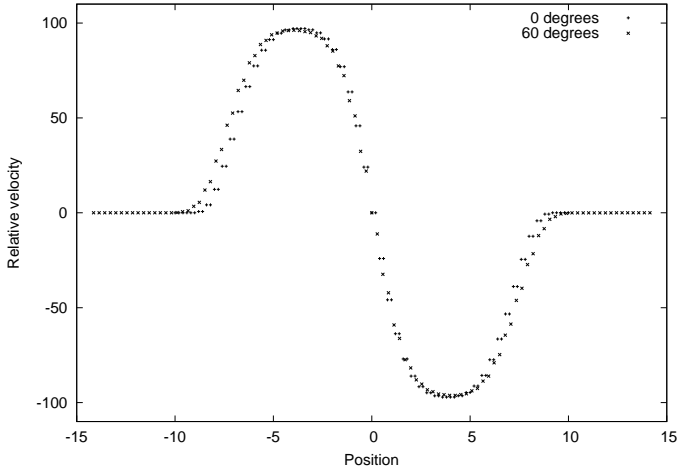


Figure : Rarefaction-waves propagation within an air-water mixture: relative velocity profile for a rarefaction wave going in x-direction and with an angle of 60 degrees between the wave and the x-direction.



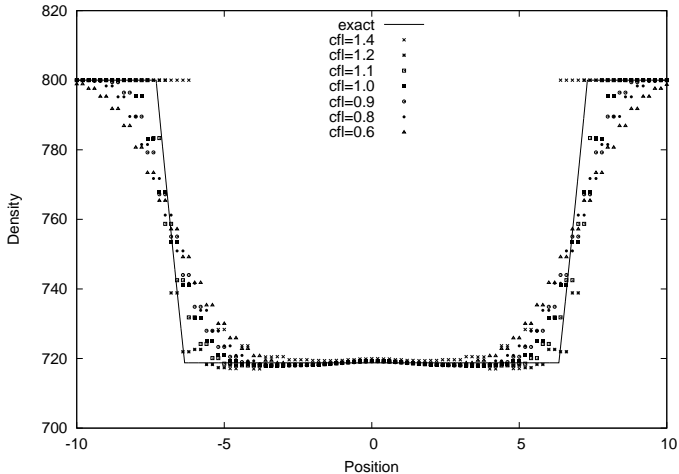


Figure : Rarefaction-waves propagation within an air-water mixture: mixture density profile for a rarefaction wave going in  $x$ -direction with different CFL numbers

# Conclusions and current work

- We get good agreement between OpenFOAM and our model
- Rarefactions can be reproduced
- Our model is very sensitive to different CFL numbers within the non-splitting scheme
- Use different flux schemes
- extend our model to unstructured meshes
- implement it in OpenFOAM