

Stress, Mach & Multi-Grid LBM

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Projects Updates

Group1:

- ▶ ???

Group2:

- ▶ ???

Recommendations: align with repository

Inviscid flow (recap)

Euler Equation $\frac{\partial(\rho \mathbf{u})}{\partial t} + \nabla \cdot (\rho \mathbf{u} \mathbf{u}) = -\nabla p + \mathbf{F}$

rewritten as:

Cauchy Momentum Equation $\frac{\partial(\rho \mathbf{u})}{\partial t} + \nabla \cdot \Pi = \mathbf{F}$

with

Momentum Flux Density Tensor $\Pi_{\alpha\beta} = \rho u_{\alpha} u_{\beta} - \sigma_{\alpha\beta}$

and

Inviscid Stress Tensor $\sigma_{\alpha\beta} = -p\delta_{\alpha\beta}$

Viscous flow (recap)

Viscous Stress Tensor = Shear Stress + Normal Shear Stress:

$$\sigma'_{\alpha\beta} = \eta \left(\frac{\partial u_\alpha}{\partial x_\beta} + \frac{\partial u_\beta}{\partial x_\alpha} \right) + \left(\eta_B - \frac{2}{3}\eta \right) \delta_{\alpha\beta} \frac{\partial u_\gamma}{\partial x_\gamma}$$

with η Shear Viscosity and η_B Bulk Viscosity

For incompressible flow:

$$\sigma'_{\alpha\beta} = \eta \left(\frac{\partial u_\alpha}{\partial x_\beta} + \frac{\partial u_\beta}{\partial x_\alpha} \right)$$

Viscous flow (recap)

Stress Tensor = Deviatoric Stress + Pressure

$$\sigma_{\alpha\beta} = \sigma'_{\alpha\beta} - p\delta_{\alpha\beta}$$

Strain Rate Tensor:

$$\mathbf{S} = \frac{1}{2} \left(\nabla \mathbf{u} + \nabla \mathbf{u}^T \right)$$

Constitutive Law (Stress-Strain relationship): $\sigma = 2\mu\mathbf{S}$

Strain Rate $\dot{\gamma} = 2\sqrt{\mathbf{S} : \mathbf{S}}$

Directly from LBM (with forces):

$$\mathbf{S} = -\frac{3\omega}{2} \sum_p \mathbf{c}_p \mathbf{c}_p (f_p - f_p^{eq})$$

$$\sigma' = -\left(1 - \frac{\omega}{2}\right) \sum_p \mathbf{c}_p \mathbf{c}_p (f_p - f_p^{eq}) - \frac{1}{2} \left(1 - \frac{\omega}{2}\right) (\mathbf{F}\mathbf{u} + \mathbf{F}\mathbf{u}^T)$$

Stress on Walls

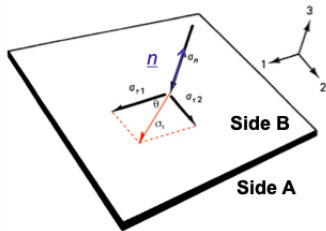
Stress acting on a plan at given point. Given the force exerted on a plane $d\mathbf{F}$, it can be decomposed as:

Normal Stress

$$\sigma_n = \frac{dF}{da} = \mathbf{n} \cdot \boldsymbol{\sigma} \mathbf{n}$$

Shear Stress

$$|\sigma_\tau| = \sqrt{(\boldsymbol{\sigma} \mathbf{n})^2 - (\mathbf{n} \cdot \boldsymbol{\sigma} \mathbf{n})^2}$$



Wall Shear Stress and Physiology

In hemodynamics $||\sigma||$ and $|\sigma_\tau|$ are important indicators for

- ▶ atherosclerotic plaque rupture
- ▶ plaque build-up
- ▶ aneurism

Computing this quantities locally and accurately is a crucial point in LBM-based hemodynamics.

Low Mach LBM

Reynolds number $Re = \frac{t_{diff}}{t_{conv}} = \frac{ul}{\nu}$ **Mach number** $Ma = \frac{t_{sound}}{t_{conv}} = \frac{u}{c_S}$

LBM is a quasi-compressible method. c_S is fixed to $c_S = 1/\sqrt{3}$, so lowering u can simulate low Ma . How to reproduce very low Ma ?

In this case, we do not match the real and simulated $Ma = \frac{u}{c_S}$, while we always want to match Re .

This approximation works well because flow structure depends very weakly on Mach for $Ma \ll 1$.

The big advantage is for the timestep $\Delta t = \frac{c_S \Delta x Ma}{u_{ph}} = \Delta x \frac{c_S Ma}{c_{ph} Ma_{ph}}$
(where c_{ph} is the physical speed of sound)

Post-Processing for pressure

Working at a different Ma however has a main difference on pressure.

Utilizing Bernoulli's equation for an incompressible flow, one can remap pressure to be substantially insensitive to Ma :

$$\frac{1}{2}u^2 + \frac{p}{\rho} = \frac{1}{2}u_{ref}^2 + \frac{p_{ref}}{\rho_{ref}}$$

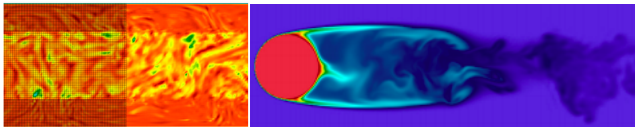
and by taking the reference values at the inlet, the post-processed pressure is

$$p = \rho \left[\frac{p_{in}}{\rho_{in}} + \frac{1}{2} (u_{in}^2 - u^2) \right]$$

You can reconsider your homework to estimate the effect of this correction.

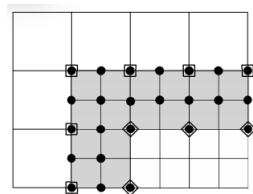
Multi-Grid LBM

Simulating generic systems require choosing carefully the levels of detail and consequently the local resolutions.



Multi-Grid LBM is based on cartesian meshes with 2^n spacing with:

- ▶ meshes have some overlap for proper interpolations (especially to handle $f - f^{eq}$)
- ▶ time-advances in 2^n
- ▶ viscosity scales as 2^n since $\sim \Delta x^2 / \Delta t$



Enforcing CFL condition everywhere is challenging, it is a good idea to change viscosity in low-resolution regions.

