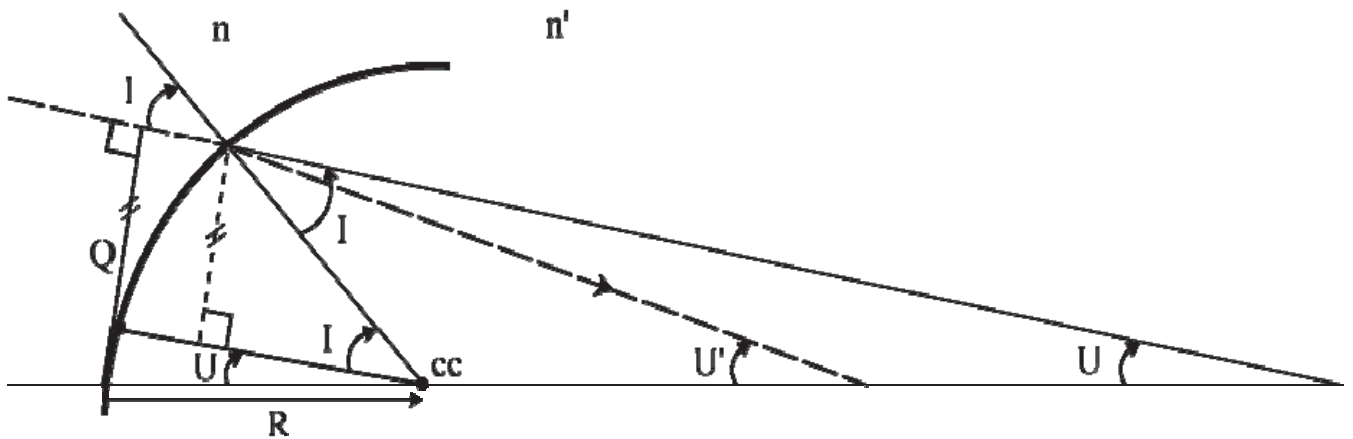
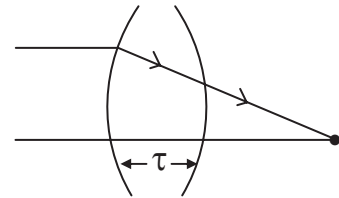


Exact Ray Trace

Analytical/exact ray tracing



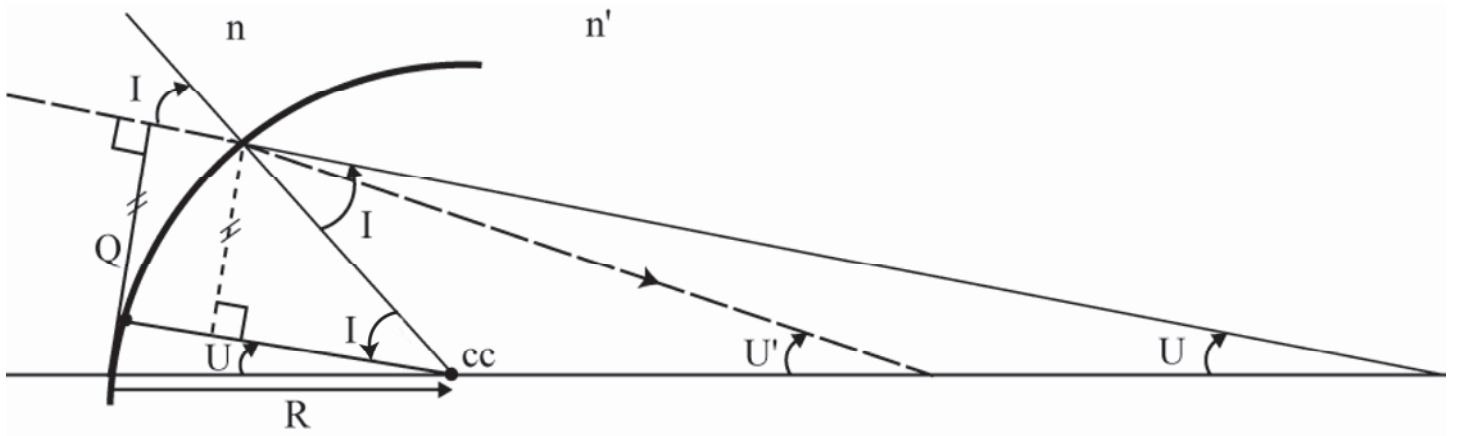
Q – U Method

- ray has height Q and $\angle U$

Givens:

1. Surface radius – R
2. n'
3. n
4. Q, U – ray description

* O'Shea, Elements of Modern Optics Design, Wiley (1985)

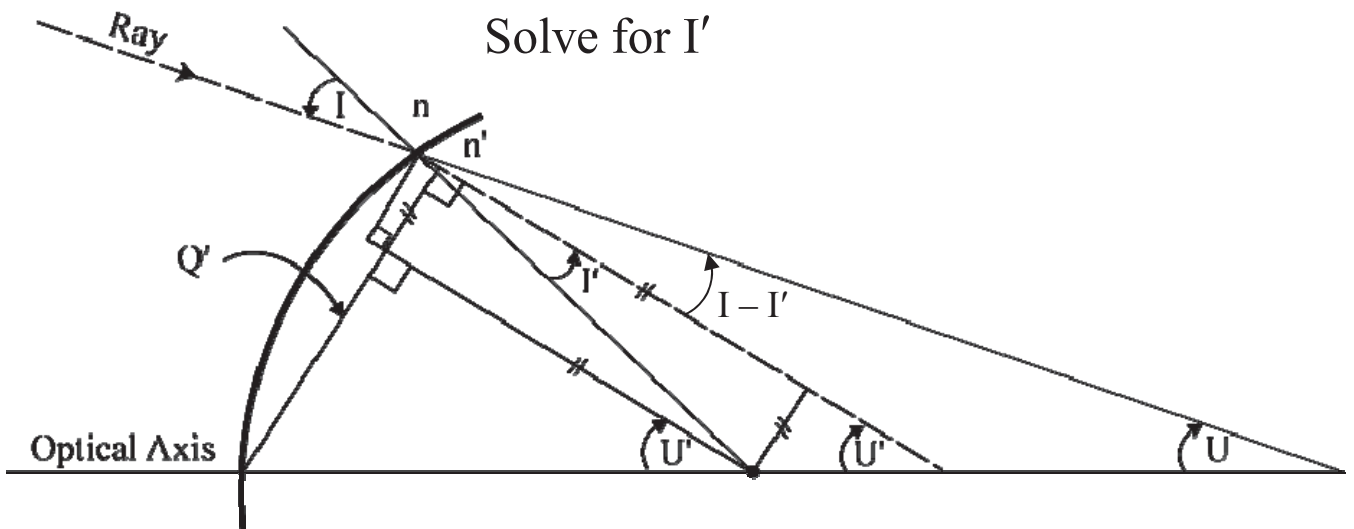


$$Q = R \sin I + R \sin(-U) = R \sin I - R \sin U$$

solve for I;

$$n' \sin I' = n \sin I$$

Solve for I'



We know I, I', and U. From the geometry we can derive

$$Q' = R \sin(-U') + R \sin I'$$

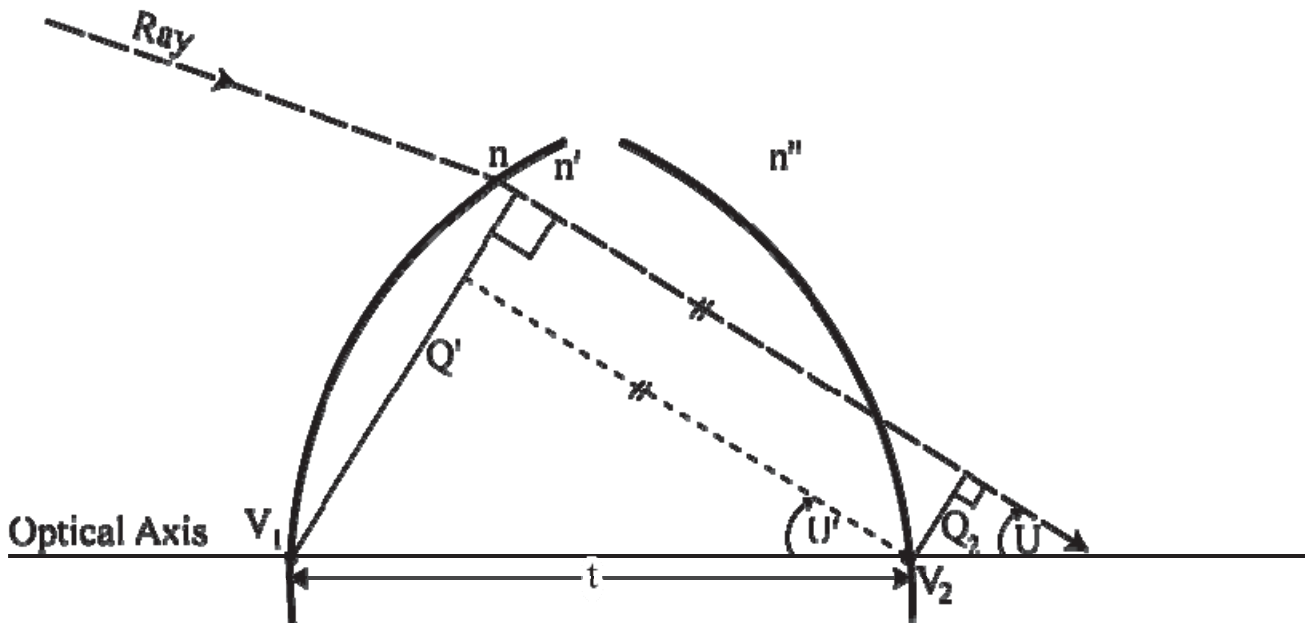
$$Q' = R(\sin I' - \sin U')$$

$$\text{Recall that } U' = U - I + I'$$

Therefore we now have a new ray, characterized by $Q' - U'$ of refracted ray just inside surface in space n' angle

Axial Transfer

Axial transfer of an exact ray to next surface, thickness (τ) away, where τ is vertex distances.



Surface₁ \rightarrow Q_1, Q_1'

Surface₂ \rightarrow Q_2, Q_2'

$$Q_2 = Q' - t \sin(-U')$$

U' is negative in sign convention

$$Q_2 = Q' + t \sin U'$$

Now we have $Q_2 U_2$ at surface₂, since $U_2 = U'$

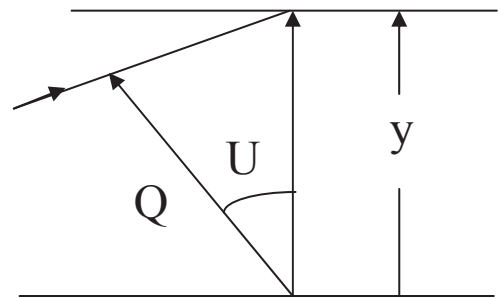
Plane Surface ($R = \infty$) problem

y = Exact ray height at surface, $R = \infty$

$$y = \frac{Q}{\cos U} = \frac{Q'}{\cos U'}$$

$$\sin U' = \frac{n}{n'} \sin U$$

$$Q' = Q \left(\frac{\cos U'}{\cos U} \right)$$



Q-U Ray Trace

From geometry of Q – U at the surface of a known input ray:

$$1) \quad Q = R \sin(-U) + R \sin I$$

find I from knowing Q and U

$$\sin I = \frac{Q}{R} - \sin(-U)$$

$$2) \quad \sin I' = \frac{n}{n'} \sin I$$

find I' from I via Snell's Law

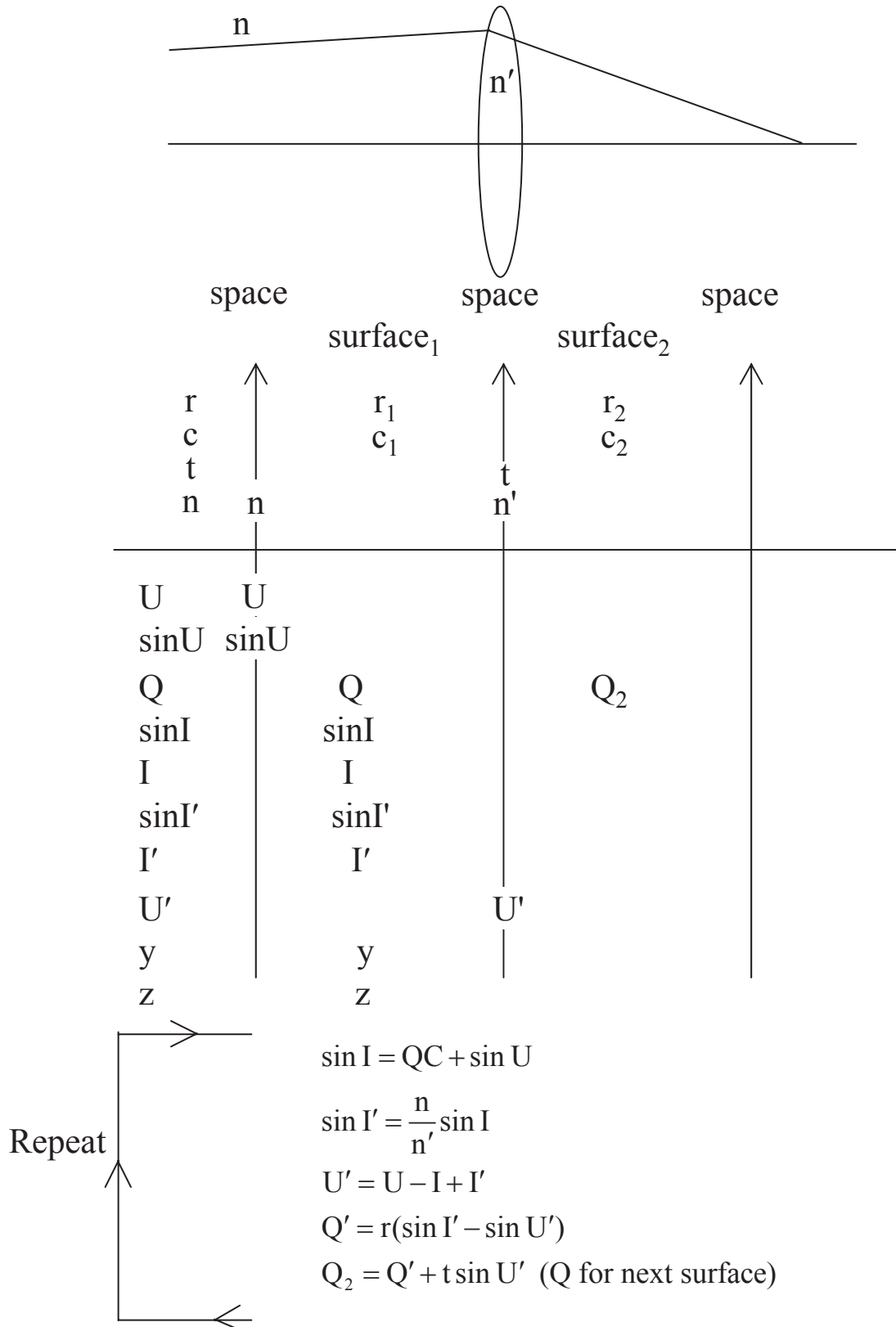
$$3) \quad U' = U + I' - I \quad [\text{Geometry}]$$

$$4) \quad Q' = R (\sin I' - \sin U')$$

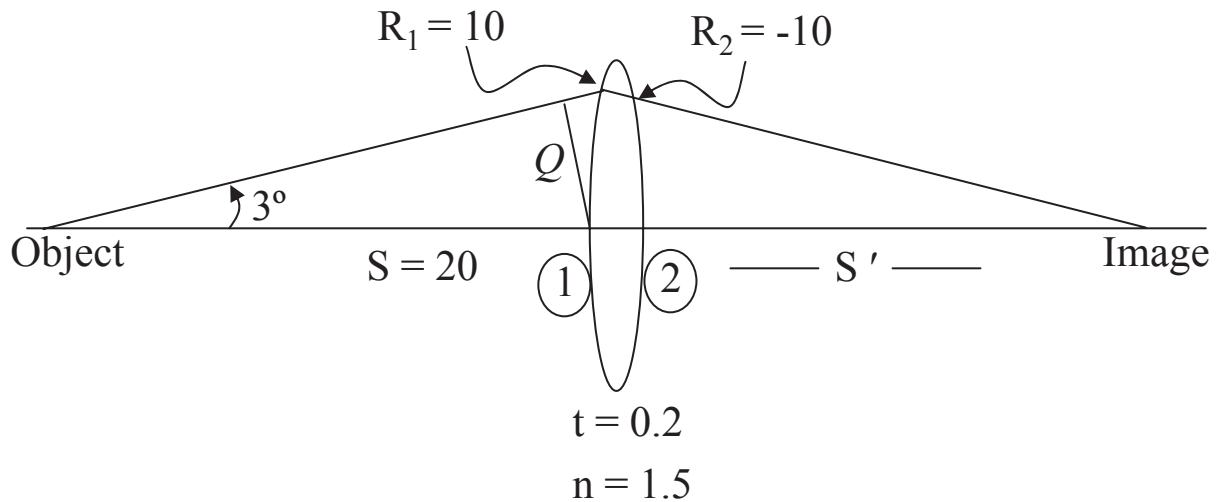
find Q'

$$5) \quad Q_2 = Q' + \tau \sin U' \text{ at next surface}$$

Exact Ray Trace (Q U Trace)



Example of Exact Ray Trace



Open/initial knowledge

$$Q = t \sin U = +20 \sin 3$$

$$Q = 1.046719$$

		surface ₁	surface ₂	
	r	10	-10	
	c	0.1	-0.1	
	t		0.2	
	n	1.0	1.5	1.0
U	3			
$\sin U$	0.52336			
Q		1.046719		
$\sin I$				
I				
$\sin I'$				
I'				
U'				
$\sin U'$				
Q'				

Exact Ray Tracing Table

Parameter	Object space	Surface ₁	Lens space	Surface ₂	Image space
r					
c					
t					
n					
U					
sinU					
Q					
sinI					
I					
sinI'					
I'					
U'					
sinU'					
Q'					
Q ₂					

Exact Ray Trace (Givens)

Parameter	Object space	Surface ₁	Lens space	Surface ₂	Image space
r		10		-10	
c		0.1		-0.1	
t	20		0.2		BFD = ??
n	1		1.5		1
U	3°				
sinU	0.52336				
Q		1.046719			
sinI					
I					
sinI'					
I'					
U'					
sinU'					
Q'					0
Q ₂					

Exact Ray Trace (Calculations)

Parameter	Object space	Surface ₁	Lens space	Surface ₂	Image space
r		10		-10	
c		0.1		-0.1	
t	20		0.2		BFD = ??
n	1		1.5		1
U	3°				
sinU	0.052336				
Q		1.046719			
sinI	0.157008				
I	9.033258°				
sinI'			0.104672		
I'			6.00826°		
U'			-0.025001		
sinU'			-0.000436		
Q'		1.04235			
Q ₂				1.050995	

Exact Ray Trace (Results)

Parameter	Object space	Surface ₁	Lens space	Surface ₂	Image space
r		1.0		-10	
c		0.1		-0.1	
t	20		0.2		19.506692
n	1		1.5		1
U	3°		√		
sinU	0.52336		√		
Q		1.046719		√	
sinI	0.157008				-0.1055388
I	9.033258°				-0.1057327
sinI'			0.104672		-0.1583037
I'			6.00826°		-0.1589725
U'			-0.025001		-0.0536761
sinU'			-0.000436		-0.0536503
Q'		1.04235			1.04653436
Q ₂				1.05099523	

$$BFD = t = \frac{Q'}{\sin U'} = \frac{1.04653436}{-0.0536503}$$

$$BFD = 19.506692$$

Aberrations of the Rotationally Symmetric Optical System

- Paraxial systems are perfect.
- Aberrations describe the deviation of real systems from this perfection.
- An aberrated system will have image locations and magnifications approximately the same as those predicted by the paraxial or Gaussian analysis.
- The paraxial image is often used as a reference for the measurement of aberrations.
- In geometrical optics, the object is considered to be a collection of independently radiating point sources – δf_n weighted by radiant flux.
- The image is the sum of the images of all of the point sources (independent irradiance patterns). There is no interference.