

Hybrid backscattering model by a prolate spheroid

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The resonance scattering by a prolate spheroid (Ye, 1997):

$$f_{bs_0}^{res} = \frac{a_{esr} F_{spheroid}^2}{\left(\frac{\omega_{0esr}^2}{\omega^2}\right) F_{spheroid} - 1 - i k a_{esr} F_{spheroid}^2} \quad (1)$$

where

$$\omega_{0esr} = \frac{2\pi}{a_{esr}} \sqrt{\frac{3\gamma P_e}{\rho_w}} \quad (2a)$$

$$\omega_{spheroid} = \omega_{0esr} F_{spheroid}^{1/2}, \quad (2b)$$

$$F_{spheroid}^{1/2} = 2^{\frac{1}{2}} e_{ac}^{-\frac{1}{3}} (1 - e_{ac}^2)^{\frac{1}{4}} \left[\ln \left(\frac{1 + \sqrt{1 - e_{ac}^2}}{1 - \sqrt{1 - e_{ac}^2}} \right) \right]^{-\frac{1}{2}} \quad (2c)$$

where $e_{ac} = \frac{a}{c} < 1$ is the aspect ratio, the ratio of semi-minor to semi-major axis, and $e_{ac} = 1$ for the case of a sphere. It is easy to verify that $F_{spheroid} = 1$ for $e_{ac} = 1$, i.e., for the case of a sphere.

The corresponding differential backscattering cross section is then

$$\sigma_{bs_0}^{res}(ka_{esr}) = |f_{bs_0}^{res}|^2 = \frac{a_{esr}^2 F_{spheroid}^2}{\left[\left(\frac{\omega_{0esr}}{\omega} \right)^2 F_{spheroid}^2 - 1 \right]^2 + k^2 a_{esr}^2 F_{spheroid}^2}, \quad (3)$$

To add the angle of orientation dependent term, we use a Sinc function

$$\Theta(\theta) = \frac{\sin(kc \sin \theta)}{kc \sin \theta}, \quad (4)$$

where θ is the angle of orientation of the prolate spheroid (normal of the major axis) relative to the incident wave. The combined scattering angle-dependent scattering model is then

$$\sigma_{bs}^{res}(ka_{esr}, \theta) = \Theta(\theta) \sigma_{bs_0}^{res}(ka_{esr}) \quad (5)$$

For $ka_{esr} \gg 1$, or as $ka_{esr} \rightarrow \infty$, from the Kirchoff Approximation when frequency is very high, Eq. (64) of Gaunard (1985) and for $r, R \gg a_1, a_2 > \lambda$

$$\sigma_{bs}^{asymp}(\theta) = \frac{a_1(\theta)a_2(\theta)}{4} \quad (6)$$

It can be derived that for an ellipsoid with incident wave in the X-Z plane,

$$\sigma_{bs}^{asymp}(\theta) = \frac{\sigma_{bs_0} e_{ac}^4}{(\sin^2 \theta + e_{ac}^2 \cos^2 \theta)^2}, \quad (7)$$

where $\sigma_{bs_0} = \sigma_{bs}(0)$ is the broadside incidence:

$$\sigma_{bs_0} = \frac{c^2}{2a} \left(\frac{b^2}{2a} \right) = \frac{c^2}{4} e_{ba}^2, \quad (8)$$

where $e_{ba} = \frac{b}{a}$ and $e_{ba} = 1$ for a prolate spheroid.

We construct a following transition function (a transient response of a passive electric system to a step function, Alexander et al., 2013):

$$\sigma_{bs}^{hybrid}(ka_{esr}, \theta) = [\sigma_{bs}^{asymp}(\theta) - \sigma_{bs}^{res}(ka_{esr}, \theta)](1 - e^{-\alpha(ka_{esr} - k_T a_{esr})}) + \sigma_{bs}^{res}(ka_{esr}, \theta), \quad (9)$$

where k_T is the wave number corresponding to the frequency where the transition starts, α is a parameter governing the transition rate.

$$TS^{hybrid} = 10 \log_{10} \sigma_{bs}^{hybrid}(ka_{esr}, \theta) \quad (10)$$

Comparison of this analytical model with the numerical simulations using the Boundary Element Method (BEM) is shown in Fig. 1, where we plot the reduced target strength (RTS) as a function of ka_{esr} .

$$RTS^{hybrid} = 10 \log_{10} \left(\frac{\sigma_{bs}^{hybrid}(ka_{esr}, \theta)}{\sigma_{bs_0}} \right). \quad (11)$$

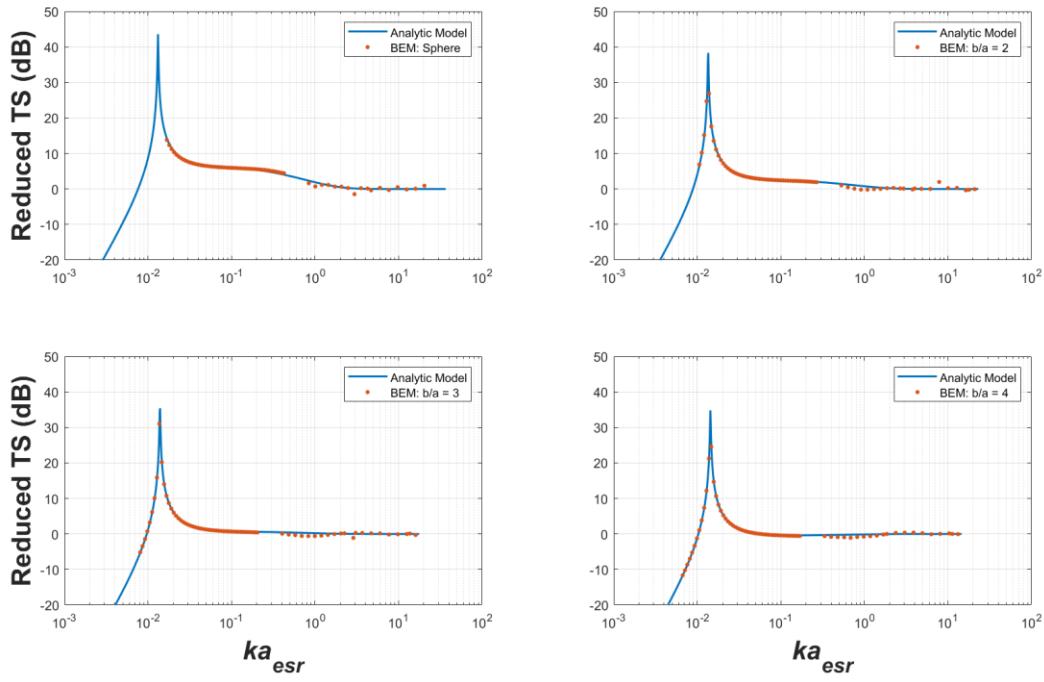


Figure 1. Comparison between the analytical model for prolate spheroids (Eq. 9) with the BEM simulations for aspect ratios of 1 (sphere), 2, 3, and 4, respectively, where the y-axis is the Reduced Target Strength, and x-axis is the dimensionless quantity ka_{esr} . In Eq. (9), a transition parameter $k_T a_{esr} = 0.1$ and $\alpha = 1.3$ are used in the hybrid model.

References

- Gaunaurd, G. C. 1985. Sonar cross sections of bodies partially insonified by finite sound beams, IEEE J. Ocean. Eng. 10: 213-230.
- Ye, Z. 1997. Low-frequency acoustic scattering by gas-filled prolate spheroids in liquids. *J. Acoust. Soc. Am.*, 101: 1945-1952. <https://doi.org/10.1121/1.418225>