Control Challenges: Solutions

lacopo Moles

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1 Introduction

1.1 Intro

This is a collection of write ups on how to solve the various problems presented by Github user "Janismac".

1.2 What do I need?

1.2.1 Software

- A real OS like Linux or Windows.
- The Julia Programming Language
 - Clone the repo
 - Activate the package by running in your terminal:

```
julia --project -e 'using Pkg; Pkg.instantiate()'
```

• (Nice to have) OpenModelica Editor

1.2.2 Theory

- Basic Julia knowledge
- Basic JS knowledge
- · Control Theory knowledge
 - Frequency Based Control
 - State Space Based control
- Misc knowledge:
 - Linear Algebra

¹MacOs should be supported in theory but it's not tested.

- Differential Equations

Part I The Damped Mass problem

Modeling

To better understand the problem let's take a peek at how the simulated model works.

Listing 1.1 BlockOnSlope.js

```
Models.BlockOnSlope.prototype.vars =
                                                                (1)
   g: 9.81,
                  // distance from objective s
   x: 0,
                 // velocity v
   dx: 0,
   slope: 1,  // slope coefficient alpha = dy/dx in the
    F: 0,
                 // Requested u
                 // Saturated u
    F_cmd: 0,
   friction: 0, // Coulomb friction coefficient mu
                  // Simulation Time
   T: 0,
};
Models.BlockOnSlope.prototype.simulate = function (dt,
   controlFunc)
{
    this.F_cmd = controlFunc({x:this.x,dx:this.dx,T:this.T});
    if(typeof this.F_cmd != 'number' || isNaN(this.F_cmd)) throw

→ "Error: The controlFunction must return a number.";

    this.F_cmd = Math.max(-20, Math.min(20, this.F_cmd));
                                                                (2)
    integrationStep(this, ['x', 'dx', 'F'], dt);
}
Models.BlockOnSlope.prototype.ode = function (x)
{
   return [
       x[1],
        (x[2]) - (Math.sin(this.slope) * this.g) - (this.friction
   * x[1]),
       20.0 * (this.F_cmd - x[2])
    ];
}
```

- 1) The model has obviously some default values for the parameters that can be modified for the different scenarios.
- 2 The control command u is generated by the controlFunction(block) function provided by us. There are some checks to see if it's a number. If it's acceptable then it passes through a saturation between ± 20 .
- (3) The model is a simple ODE with equations:

$$\begin{cases} \dot{s} = v \\ \dot{v} = F - \sin(\alpha) \cdot g - \mu \cdot v \\ \dot{F} = -20 \cdot F + 20 \cdot u_{sat} \end{cases}$$

Converting it in state-space representation:

$$\begin{bmatrix} \dot{s} \\ \dot{v} \\ \dot{F} \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & -\mu & 1 \\ 0 & 0 & -20 \end{bmatrix} \begin{bmatrix} s \\ v \\ F \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ u_{sat} \end{bmatrix} + \begin{bmatrix} 0 \\ -sin(\alpha) \cdot g \\ 0 \end{bmatrix}$$
$$\begin{bmatrix} s \\ v \\ F \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} s \\ v \\ F \end{bmatrix}$$

Obviously the gravitational term acts as a disturbance.

2 Block without Friction

Position Control with friction. Using Pole Placement + PD.

2.1 State Space representation

We can convert the set of ODE into a state space representation. The final bode plot of the block position is:

```
using DiscretePIDs, ControlSystems, Plots, LinearAlgebra
# System parameters
Ts = 0.02 # sampling time
Tf = 2.5; #final simulation time
g = 9.81 \# gravity
\alpha = 0.0 \text{ # slope}
\mu = 1.0 # friction coefficient
x_0 = -2.0 # starting position
dx_0 = 0.0 # starting velocity
\tau = 20.0 \text{ # torque constant}
# State Space Matrix
A = \begin{bmatrix} 0 & 1 & 0 \end{bmatrix}
    0 - \mu 1
    0 \ 0 \ -\tau];
B = [0]
    τ];
C = [1 \ 0 \ 0]
    0 1 0];
sys = ss(A, B, C, 0.0) # Continuous
plot!(bodeplot(tf(sys)),pzmap(tf(sys)))
```

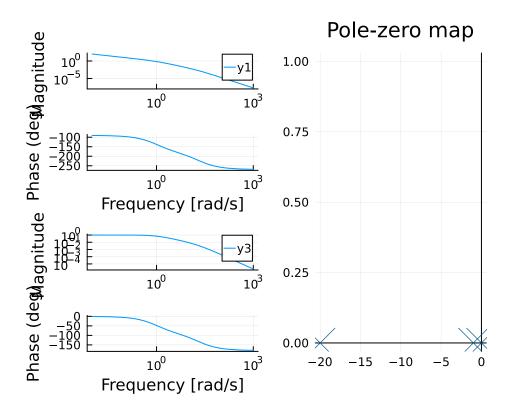


Figure 2.1: Starting Bode Plot and PZ Map

It has the shape we expect from a motor + friction. Slow pole for the mass + friction and a faster pole for the current & inductance.

Numerically they are:

display(eigvals(A))

```
3-element Vector{Float64}:
  -20.0
```

-1.0 0.0

We see that we start with all the pole in the left-half plane, which is good.

2.2 Pole Placement

We can design a controller with pole placement.

For some reason pole placement doesn't work for the observer, I use a Kalman Filter with random fast values.

```
observability(A, C).isobservable &
controllability(A, B).iscontrollable; #OK

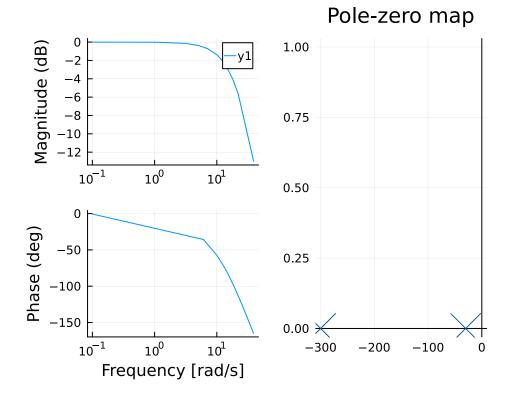
ε = 0.01;
pp = 15.0;
poles_cont = -2.0 * [pp + ε, pp - ε, pp];
L = real(place(sys, poles_cont, :c));

poles_obs = poles_cont * 10.0;
K = place(1.0 * A', 1.0 * C', poles_obs)'
cont = observer_controller(sys, L, K; direct=false);
```

We can check the effect of the new controller on the loop

```
closedLoop = feedback(sys * cont)
print(poles(closedLoop));
setPlotScale("dB")
plot!(bodeplot(closedLoop[1, 1], 0.1:40), pzmap(closedLoop))
```

ComplexF64[-29.979998924597755 + 0.0im, -30.000002152199972 + 0.0im, -30.019998923202337 + 0.0im, -300.000000000004 + 0.0im, -300.199999999752 + 0.0im, -299.80000000004117 + 0.0im]



We can compare this to the open-loop response in @start-bode. We can see that we achieve unitary gain throughout the whole low-frequency range.

We can convert the pole placement controller into the standard PD gain form.

```
K = L[1];
Ti = 0;
Td = L[2] / L[1];
pid = DiscretePID(; K, Ts, Ti, Td);
```

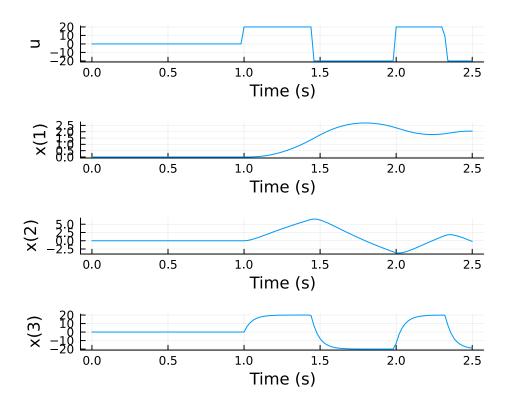
2.3 Simulation

We can simulate this with a motor that only outputs the position:

```
sysreal = ss(A, B, [1 0 0], 0.0)
ctrl = function (x, t)
    y = (sysreal.C*x)[] # measurement
    d = 0 * [1.0]
                     # disturbance
    r = 2.0 * (t >= 1) # reference
    \# u = pid(r, y) \# control signal
    # u + d # Plant input is control signal + disturbance
    # u =1
    e = x - [r; 0.0; 0.0]
    e[3] = 0.0 # torque not observable, just ignore it in the

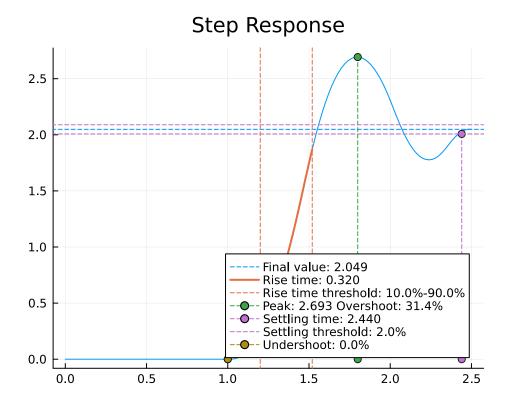
→ final feedback

    u = -L * e + d
    u = [maximum([-20.0 minimum([20.0 u])])]
end
t = 0:Ts:Tf
res = lsim(sysreal, ctrl, t)
display(plot(res,
    plotu=true,
    plotx=true,
    ploty=false
    ))
ylabel!("u", sp=1);
ylabel!("x", sp=2);
ylabel!("v", sp=3);
ylabel!("T", sp=4);
```



For more stats:

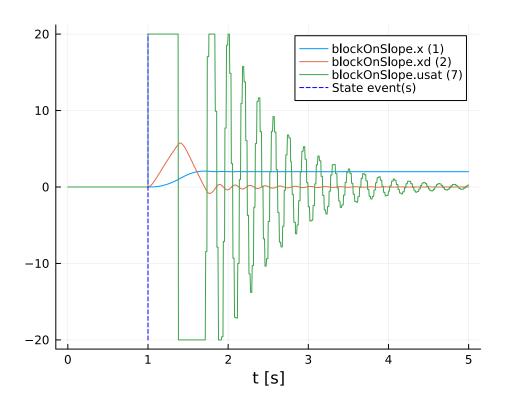
```
si = stepinfo(res);
plot(si);title!("Step Response")
```



We can also simulate it in a SIMULINK-like environment:

```
using FMI, DifferentialEquations
fmuPath = abspath(joinpath(@__DIR__,
  " " " " ,
  "modelica",
  "ControlChallenges",
  "ControlChallenges.BlockOnSlope_Challenges.Examples.WithFrictio_

    n.fmu"))
fmu = loadFMU(fmuPath);
simData = simulateME(
    fmu,
    (0.0, 5.0);
    recordValues=["blockOnSlope.x",
    "blockOnSlope.xd",
    "blockOnSlope.usat"],
    showProgress=false);
unloadFMU(fmu);
plot(simData, states=false, timeEvents=false)
```



There is a slight difference between the lsim simulation and the FMU simulation. I need to recheck some stuff.

3 Block With Friction

Position Control with friction. Using Pole Placement + PD.

3.1 Response Analysis

```
using CCS: blockModel using ControlSystems, Plots, LinearAlgebra, \hookrightarrow RobustAndOptimalControl, PlotThemes theme(:wong) contSys = blockModel.csys(;g = 0, \alpha = 0 , \mu = 1, \tau =20) plot!(bodeplot(contSys[1,1]),pzmap(contSys))
```

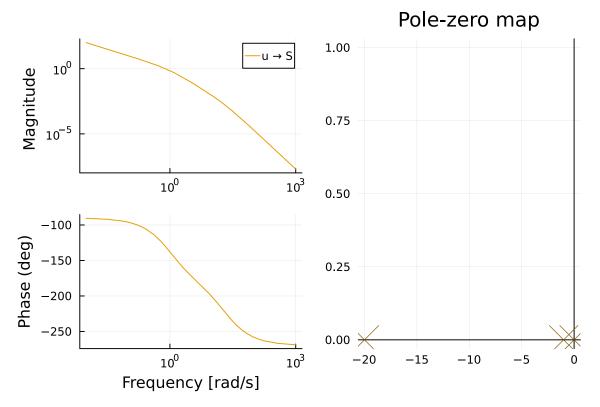


Figure 3.1: Starting Bode Plot and PZ Map

It has the shape we expect from a motor + friction. Slow pole for the mass + friction and a faster pole for the current & inductance.

Numerically they are:

```
display(eigvals(contSys.A))
```

```
3-element Vector{Float64}:
```

-20.0

-1.0

0.0

We see that we start with all the poles in the left-half plane, which is good.

3.2 Pole Placement

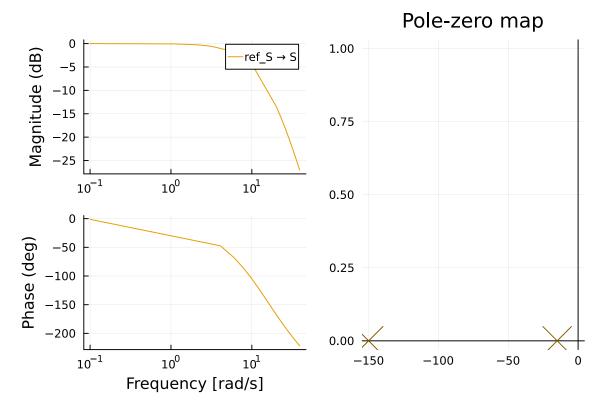
We can design a controller with pole placement.

For some reason pole placement doesn't work for the observer, I use a Kalman Filter with random fast values.

We can check the effect of the new controller on the loop

```
closedLoop = feedback( contSys * fsf_controller);
print(poles(closedLoop));
setPlotScale("dB")
plot!(bodeplot(closedLoop[1,1], 0.1:40), pzmap(closedLoop))

ComplexF64[-14.990000366343788 + 0.0im, -14.99999999966673722 +
0.0im, -15.010000366982666 + 0.0im, -149.9999999999986 + 0.0im,
-150.100000000002432 + 0.0im, -149.89999999999607 + 0.0im]
```



We can compare this to the open-loop response in @start-bode. We can see that we achieve unitary gain throughout the whole low-frequency range.

We can convert the pole placement controller into the standard PD gain form.

```
using DiscretePIDs
Ts = 0.02 # sampling time
Tf = 2.5; #final simulation time

K = L[1];
Ti = 0;
Td = L[2] / L[1];
pid = DiscretePID(; K, Ts, Ti, Td);
```

3.3 Simulation

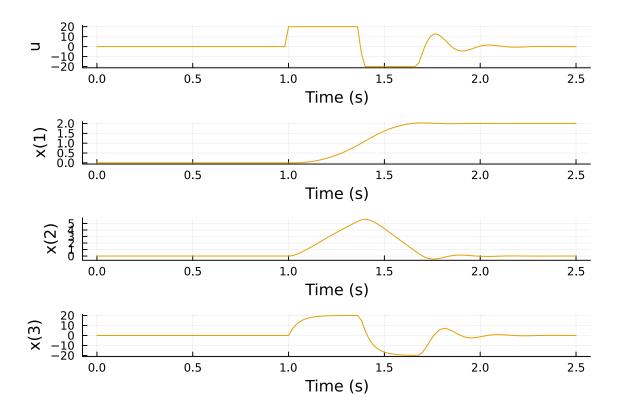
We can simulate this with a motor that only outputs the position:

```
sysreal = ss(contSys.A, contSys.B, [1 0 0], 0.0)
ctrl = function (x, t)
```

```
y = (sysreal.C*x)[] # measurement
    d = 0 * [1.0] # disturbance
    r = 2.0 * (t >= 1) # reference
    \# u = pid(r, y) \# control signal
    # u + d # Plant input is control signal + disturbance
    # u =1
    e = x - [r; 0.0; 0.0]
    e[3] = 0.0 # torque not observable, just ignore it in the

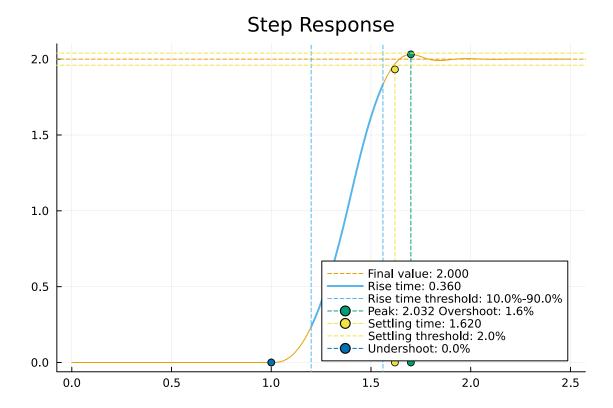
→ final feedback

    u = -L * e + d
    u = [maximum([-20.0 minimum([20.0 u])])]
end
t = 0:Ts:Tf
res = lsim(sysreal, ctrl, t)
display(plot(res,
    plotu=true,
    plotx=true,
    ploty=false
    ))
ylabel!("u", sp=1);
ylabel!("x", sp=2);
ylabel!("v", sp=3);
ylabel!("T", sp=4);
```



For more stats:

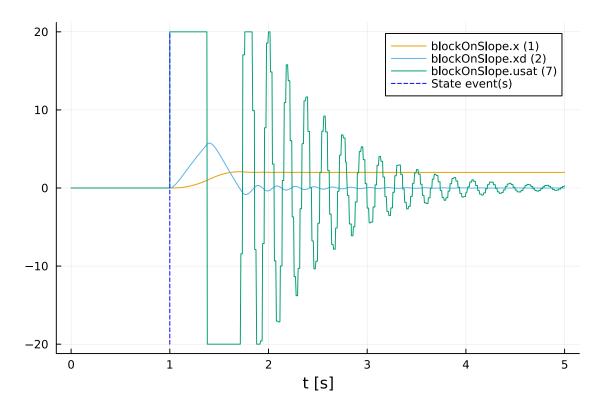
```
si = stepinfo(res);
plot(si);title!("Step Response")
```



We can also simulate it in a SIMULINK-like environment:

```
using FMI, DifferentialEquations
fmuPath = abspath(joinpath(@__DIR__,
  "..","..",
  "modelica",
  "ControlChallenges",
  "ControlChallenges.BlockOnSlope_Challenges.Examples.WithFrictio_

    n.fmu"))
fmu = loadFMU(fmuPath);
simData = simulateME(
    fmu,
    (0.0, 5.0);
    recordValues=["blockOnSlope.x",
    "blockOnSlope.xd",
    "blockOnSlope.usat"],
    showProgress=false);
unloadFMU(fmu);
plot(simData, states=false, timeEvents=false)
```



There is a slight difference between the lsim simulation and the FMU simulation. I need to recheck some stuff.

4 Block on a slope

Position Control with friction. Using Pole Placement + PD.

4.1 Response Analysis

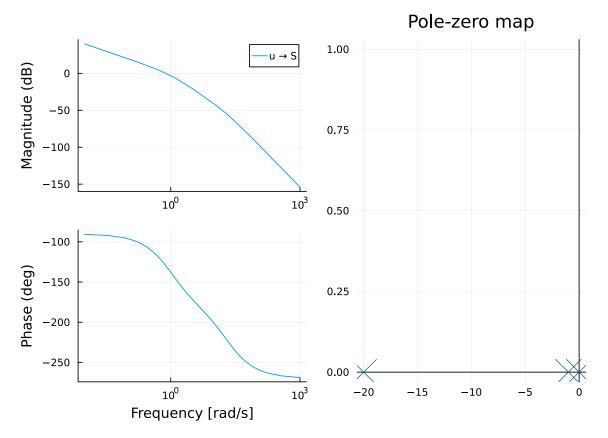


Figure 4.1: Starting Bode Plot and PZ Map

It has the shape we expect from a motor + friction. Slow pole for the mass + friction and a faster pole for the current & inductance.

Numerically they are:

```
display(eigvals(contSys.A))
```

3-element Vector{Float64}:

-20.0

-1.0

0.0

We see that we start with all the poles in the left-half plane, which is good.

4.2 Pole Placement

We can design a controller with pole placement.

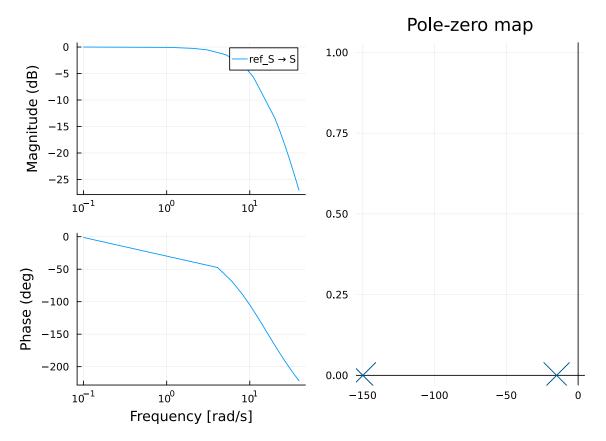
For some reason pole placement doesn't work for the observer, I use a Kalman Filter with random fast values.

```
observability(contSys.A,contSys.C).isobservable || error("System

    is not observable")

controllability(contSys.A,contSys.B).iscontrollable ||
→ error("System is not controllable")
\varepsilon = 0.01;
pp = 15.0;
poles_cont = - [pp + \epsilon, pp - \epsilon, pp];
L = real(place(contSys, poles_cont, :c));
poles_obs = poles_cont * 10.0;
K = place(contSys, poles_obs, :o)
obs_controller = observer_controller(contSys, L, K; direct=false);
fsf_controller = named_ss(obs_controller, u = [:ref_S, :ref_V], y
\Rightarrow = [:u]
NamedStateSpace{Continuous, Float64}
  -150.0
                                  8.033684828490095e-12
                                                             0.0
                                                             1.0
     1.0915557686859107e-5
                               -279.999999999851
                             -17530.98989999806
                                                           -44.0
 -3374.9970813429577
B =
 150.0
                               0.999999999919663
  -1.0915557686859107e-5
                             278.999999999851
  -0.0014186570429435138 16899.989999998063
 168.74992500000002 31.549995000000003 1.2000000000000000
 0.0 0.0
Continuous-time state-space model
With state names: x1 x2 x3
     input names: ref_S ref_V
     output names: u
We can check the effect of the new controller on the loop
closedLoop = feedback( contSys * fsf_controller);
print(poles(closedLoop));
setPlotScale("dB")
plot!(bodeplot(closedLoop[1,1], 0.1:40), pzmap(closedLoop))
```

ComplexF64[-14.990000366343788 + 0.0im, -14.999999266673722 + 0.0im, -15.010000366982666 + 0.0im, -149.999999999986 + 0.0im, -150.10000000002432 + 0.0im, -149.8999999999607 + 0.0im]



We can compare this to the open-loop response in @start-bode. We can see that we achieve unitary gain throughout the whole low-frequency range.

We can convert the pole placement controller into the standard PD gain form.

```
using DiscretePIDs
Ts = 0.02 # sampling time
Tf = 2.5; #final simulation time

K = L[1];
Ti = 0;
Td = L[2] / L[1];
pid = DiscretePID(; K, Ts, Ti, Td);
```

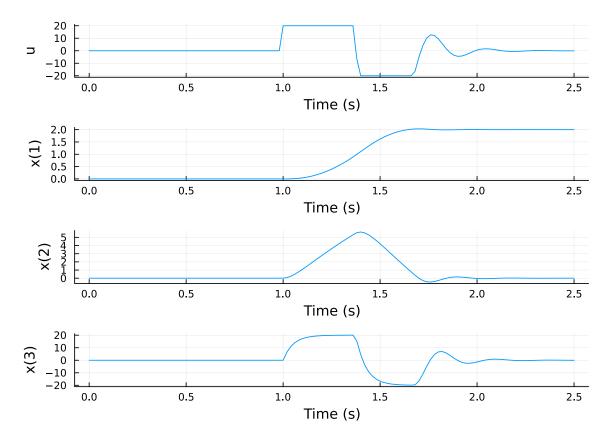
4.3 Simulation

We can simulate this with a motor that only outputs the position:

```
sysreal = ss(contSys.A, contSys.B, [1 0 0], 0.0)
ctrl = function (x, t)
    y = (sysreal.C*x)[] # measurement
    d = 0 * [1.0]
                      # disturbance
    r = 2.0 * (t >= 1) # reference
    \# u = pid(r, y) \# control signal
    # u + d # Plant input is control signal + disturbance
    \# u = 1
    e = x - [r; 0.0; 0.0]
    e[3] = 0.0 # torque not observable, just ignore it in the

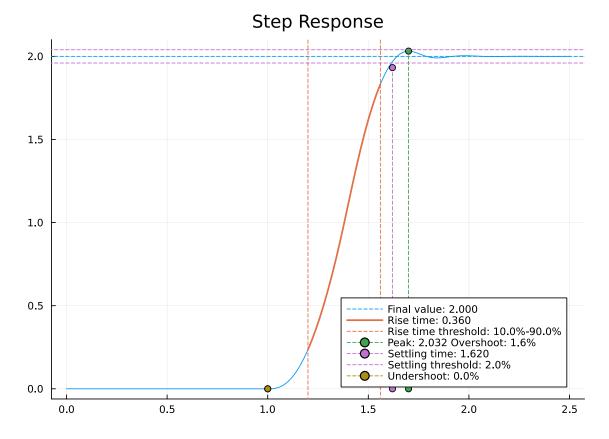
→ final feedback

    u = -L * e + d
    u = [maximum([-20.0 minimum([20.0 u])])]
end
t = 0:Ts:Tf
res = lsim(sysreal, ctrl, t)
display(plot(res,
    plotu=true,
    plotx=true,
    ploty=false
    ))
ylabel!("u", sp=1);
ylabel!("x", sp=2);
ylabel!("v", sp=3);
ylabel!("T", sp=4);
```



For more stats:

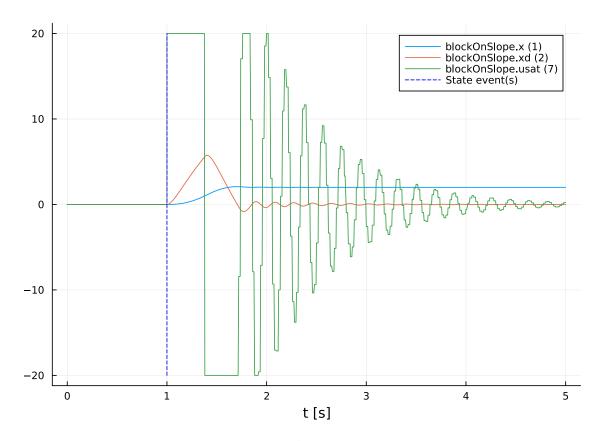
```
si = stepinfo(res);
plot(si);title!("Step Response")
```



We can also simulate it in a SIMULINK-like environment:

```
using FMI, DifferentialEquations
fmuPath = abspath(joinpath(@__DIR___,
 "..","..",
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  "ControlChallenges",
  "ControlChallenges.BlockOnSlope_Challenges.Examples.WithFrictio_

    n.fmu"))
fmu = loadFMU(fmuPath);
simData = simulateME(
    fmu,
    (0.0, 5.0);
    recordValues=["blockOnSlope.x",
    "blockOnSlope.xd",
    "blockOnSlope.usat"],
    showProgress=false);
unloadFMU(fmu);
plot(simData, states=false, timeEvents=false)
```



There is a slight difference between the lsim simulation and the FMU simulation. I need to recheck some stuff.

A Performance tricks

A.1 Hurwitz Check

Create our nice model. Assume to have run the poles function and that you have a vector of eigenvalues. For simplicity I will create an arbitrary vector with the first 100 values in -1 and the last 100 values as random around 0.

A.1.1 for loop

With a naive approach we check if all the elements are in the LHP: make a function that iterates and returns false if it hits a pole with positive real part.

```
function isHurwitz(v)
    for i in eachindex(v)
        if real(v[i])>0.0
        return false
        end
    end
    return true
end

@benchmark isHurwitz($(Ref(vbig))[])
```

BenchmarkTools.Trial: 10000 samples with 987 evaluations per sample.

```
Range (min ... max): 50.557 ns ... 389.564 ns | GC (min ... max): 0.00\% ... 0.00\% Time (median): 53.698 ns | GC (median): 0.00\% Time (mean \pm \sigma): 56.542 ns \pm 13.874 ns | GC (mean \pm \sigma): 0.00\% \pm 0.00%
```

```
50.6 ns Histogram: log(frequency) by time 121 ns <
```

Memory estimate: 0 bytes, allocs estimate: 0.

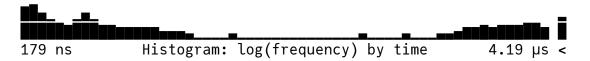
We have our baseline. We can probably squeeze out some more performance but I'm still a Julia noob.

A.1.2 all()

Let's try using some of the built-in declarative functions:

@benchmark all(real(\$vbig).<=0.0)</pre>

BenchmarkTools.Trial: 10000 samples with 755 evaluations per sample.



Memory estimate: 1.75 KiB, allocs estimate: 5.

Simple all(), when given a tuple it checks if all the values are True, otherwise it stops when it encounters the first False.

We can see that it's a tad slower. This is because it's creating a new vector with just the real parts, then it's creating a new vector with only the boolean results and then it's checking if there are any False results. This results in a lot of allocations and wasted resources.

```
@benchmark all(<=(0.0),real($vbig))</pre>
```

BenchmarkTools.Trial: 10000 samples with 776 evaluations per sample.

```
156 ns Histogram: log(frequency) by time 2.58 µs <
```

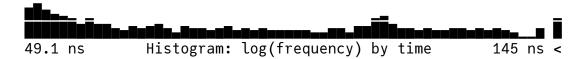
Memory estimate: 1.62 KiB, allocs estimate: 2.

A smarter way is to skip on of the allocations by creating the vector of real parts and then checking row by row if the non-positivity check fails.

```
@benchmark all(i -> real(i)<=0.0,$vbig)</pre>
```

BenchmarkTools.Trial: 10000 samples with 987 evaluations per sample.

```
Range (min ... max): 49.139 ns ... 826.545 ns | GC (min ... max): 0.00\% ... 0.00\% Time (median): 51.165 ns | GC (median): 0.00\% Time (mean \pm \sigma): 55.618 ns \pm 22.280 ns | GC (mean \pm \sigma): 0.00\% \pm 0.00\%
```



Memory estimate: 0 bytes, allocs estimate: 0.

We can do better: Instead of converting into real the full vector it checks element by element if it's in the LHP. It returns false at the first failure. We finally have a comparable result to the benchmark function but in a more compact way.

Is it cleaner? That's subjective.

A.1.3 mapreduce()

Finally we try the MapReduce approach. This allows a better utilization of your processor without the necessity of learning parallel programming.

```
@benchmark mapreduce(i->real(i)<=0.0, &, $vbig)</pre>
```

BenchmarkTools.Trial: 10000 samples with 990 evaluations per sample.

```
Range (min ... max): 43.737 ns ... 747.172 ns | GC (min ... max): 0.00\% ... 0.00\% Time (median): 44.343 ns | GC (median): 0.00\% Time (mean \pm \sigma): 48.952 ns \pm 20.482 ns | GC (mean \pm \sigma): 0.00\% \pm 0.00%
```

```
43.7 ns Histogram: log(frequency) by time 131 ns <
```

Memory estimate: 0 bytes, allocs estimate: 0.

We squeeze the last bit of performance and beat the initial benchmark, not by much but still appreciable.