Control Challenges: Solutions

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1 Introduction

1.1 Intro

This is a collection of write ups on how to solve the various problems presented by Github user "Janismac".

1.2 What do I need?

1.2.1 Software

- A real OS like Linux or Windows.
- The Julia Programming Language
 - Clone the repo
 - Activate the package by running in your terminal:

```
julia --project -e 'using Pkg; Pkg.instantiate()'
```

• (Nice to have) OpenModelica Editor

1.2.2 Theory

- Basic Julia knowledge
- · Basic JS knowledge
- · Control Theory knowledge
 - Frequency Based Control
 - State Space Based control
- Misc knowledge:
 - Linear Algebra

¹MacOs should be supported in theory but it's not tested.

- Differential Equations

Part I The Damped Mass problem

Modeling

To better understand the problem let's take a peek at how the simulated model works.

Listing 1.1 BlockOnSlope.js

```
Models.BlockOnSlope.prototype.vars =
                                                               (1)
   g: 9.81,
   x: 0,
                  // distance from objective s
                  // velocity v
   dx: 0,
   slope: 1, // slope coefficient alpha = dy/dx in the
    F: 0,
                  // Requested u
   F_cmd: 0,
                  // Saturated u
   friction: 0, // Coulomb friction coefficient mu
                  // Simulation Time
   T: 0,
};
Models.BlockOnSlope.prototype.simulate = function (dt,
   controlFunc)
{
   this.F_cmd = controlFunc({x:this.x,dx:this.dx,T:this.T});
   if(typeof this.F_{cmd} \neq "number" \mid | isNaN(this.<math>F_{cmd})) throw
    → "Error: The controlFunction must return a number.";
   this.F_{cmd} = Math.max(-20, Math.min(20, this.F_{cmd}));
                                                               (2)
   integrationStep(this, ['x', 'dx', 'F'], dt);
}
Models.BlockOnSlope.prototype.ode = function (x)
{
   return [
        x[1]
                                                               (3)
        (x[2]) - (Math.sin(this.slope) * this.g) -
   (this.friction * x[1]),
        20.0 * (this.F_cmd - x[2])
   ];
}
```

- 1) The model has obviously some default values for the parameters that can be modified for the different scenarios.
- ② The control command u is generated by the **controlFunction(block)** function provided by us. There are some checks to see if it's a number. If it's acceptable then it passes through a saturation between ± 20 .

(3) The model is a simple ODE with equations:

$$\begin{cases} \dot{s} = v \\ \dot{v} = F - \sin(\alpha) \cdot g - \mu \cdot v \\ \dot{F} = -20 \cdot F + 20 \cdot u_{sat} \end{cases}$$

Converting it in state-space representation:

$$\begin{bmatrix} \dot{s} \\ \dot{v} \\ \dot{F} \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & -\mu & 1 \\ 0 & 0 & -20 \end{bmatrix} \begin{bmatrix} s \\ v \\ F \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ u_{sat} \end{bmatrix} + \begin{bmatrix} 0 \\ -\sin(\alpha) \cdot g \\ 0 \end{bmatrix}$$

$$\begin{bmatrix} s \\ v \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} s \\ v \\ F \end{bmatrix}$$

Obviously the gravitational term acts as a disturbance.

2 Block without Friction

Position Control with friction. Using Pole Placement + PD.

2.1 State Space representation

We can convert the set of ODE into a state space representation. The final bode plot of the block position is:

```
using DiscretePIDs, ControlSystems, Plots, LinearAlgebra
# System parameters
Ts = 0.02 # sampling time
Tf = 2.5; #final simulation time
q = 9.81 #gravity
\alpha = 0.0 \# slope
\mu = 1.0 # friction coefficient
x_0 = -2.0 # starting position
dx_0 = 0.0 \# starting velocity
\tau = 20.0 \text{ # torque constant}
# State Space Matrix
A = [0 1 0]
    0 - \mu 1
    0 0 -τ];
B = [0]
    τ];
C = [1 \ 0 \ 0]
    0 1 0];
sys = ss(A, B, C, 0.0) # Continuous
plot!(bodeplot(tf(sys)),pzmap(tf(sys)))
```

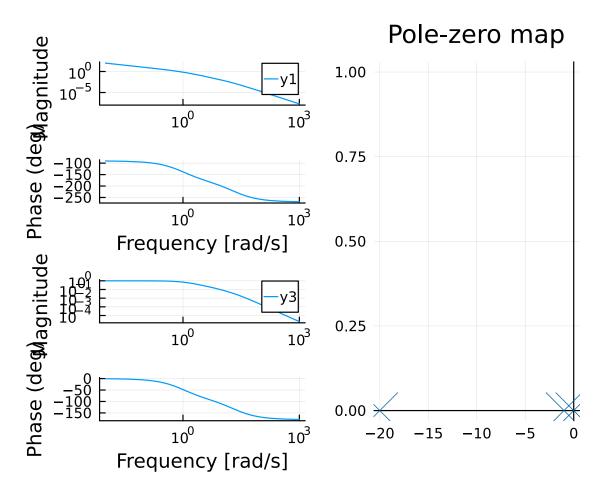


Figure 2.1: Starting Bode Plot and PZ Map

It has the shape we expect from a motor + friction. Slow pole for the mass + friction and a faster pole for the current & inductance.

Numerically they are:

display(eigvals(A))

```
3-element Vector{Float64}:
-20.0
-1.0
0.0
```

We see that we start with all the pole in the left-half plane, which is good.

2.2 Pole Placement

We can design a controller with pole placement.

For some reason pole placement doesn't work for the observer, I use a Kalman Filter with random fast values.

```
observability(A, C).isobservable &
controllability(A, B).iscontrollable; #OK

ε = 0.01;
pp = 15.0;
poles_cont = -2.0 * [pp + ε, pp - ε, pp];
L = real(place(sys, poles_cont, :c));

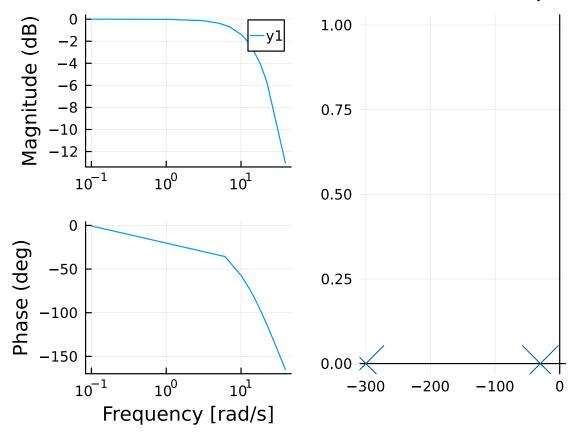
poles_obs = poles_cont * 10.0;
K = place(1.0 * A', 1.0 * C', poles_obs)'
cont = observer_controller(sys, L, K; direct=false);
```

We can check the effect of the new controller on the loop

```
closedLoop = feedback(sys * cont)
print(poles(closedLoop));
setPlotScale("dB")
plot!(bodeplot(closedLoop[1, 1], 0.1:40), pzmap(closedLoop))
```

```
ComplexF64[-29.979998924597755 + 0.0im, -30.000002152199972 + 0.0im, -30.019998923202337 + 0.0im, -300.000000000004 + 0.0im, -300.19999999752 + 0.0im, -299.80000000004117 + 0.0im]
```

Pole-zero map



We can compare this to the open-loop response in @start-bode. We can see that we achieve unitary gain throughout the whole low-frequency range.

We can convert the pole placement controller into the standard PD gain form.

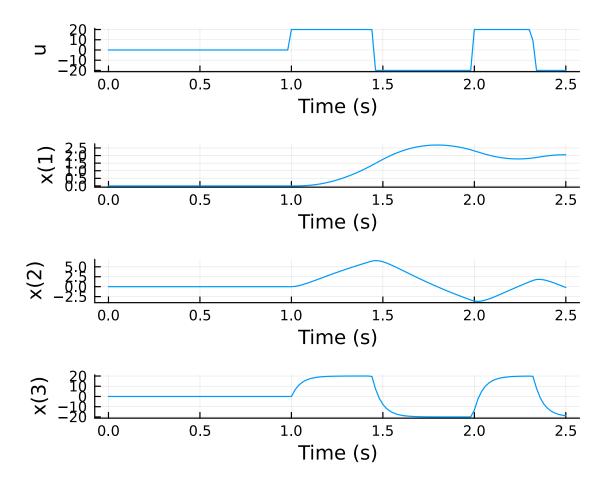
```
K = L[1];
Ti = 0;
Td = L[2] / L[1];
pid = DiscretePID(; K, Ts, Ti, Td);
```

2.3 Simulation

We can simulate this with a motor that only outputs the position:

```
sysreal = ss(A, B, [1 0 0], 0.0)
ctrl = function (x, t)
    y = (sysreal.C*x)[] # measurement
```

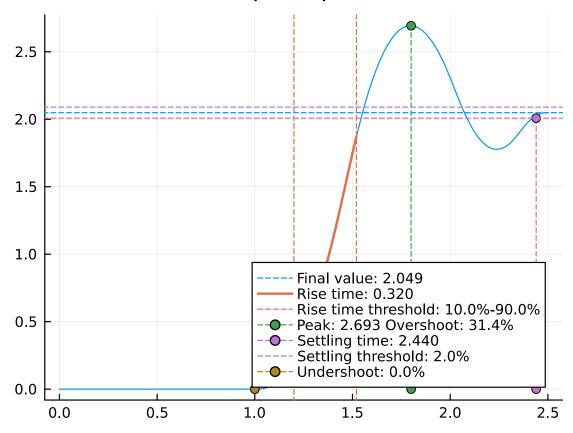
```
d = 0 * [1.0] # disturbance
    r = 2.0 * (t \ge 1) # reference
    # u = pid(r, y) # control signal
    # u + d # Plant input is control signal + disturbance
    # u =1
    e = x - [r; 0.0; 0.0]
    e[3] = 0.0 # torque not observable, just ignore it in the
     → final feedback
    u = -L * e + d
    u = [maximum([-20.0 minimum([20.0 u])])]
end
t = 0:Ts:Tf
res = lsim(sysreal, ctrl, t)
display(plot(res,
    plotu=true,
    plotx=true,
    ploty=false
    ))
ylabel!("u", sp=1);
ylabel!("x", sp=2);
ylabel!("v", sp=3);
ylabel!("T", sp=4);
```



For more stats:

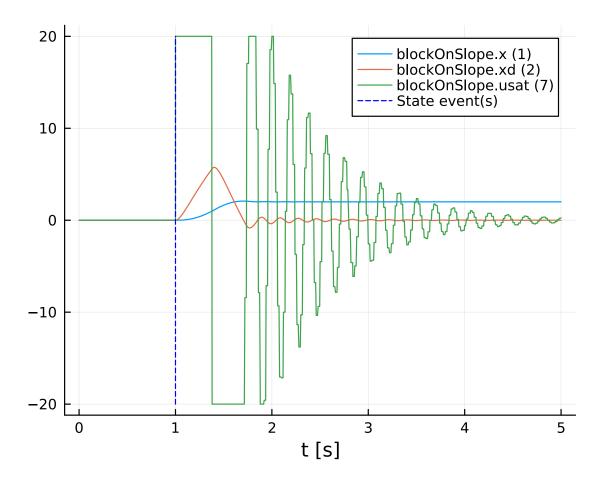
```
si = stepinfo(res);
plot(si);title!("Step Response")
```

Step Response



We can also simulate it in a SIMULINK-like environment:

```
using FMI, DifferentialEquations
fmuPath = abspath(joinpath(@__DIR___,
 "..","..."
  "modelica",
  "ControlChallenges",
  "ControlChallenges.BlockOnSlope_Challenges.Examples.WithFrict
  → ion.fmu"))
fmu = loadFMU(fmuPath);
simData = simulateME(
    fmu,
    (0.0, 5.0);
    recordValues=["blockOnSlope.x",
    "blockOnSlope.xd",
    "blockOnSlope.usat"],
    showProgress=false);
unloadFMU(fmu);
plot(simData, states=false, timeEvents=false)
```



There is a slight difference between the lsim simulation and the FMU simulation. I need to recheck some stuff.

3 Block With Friction

Position Control with friction. Using Pole Placement + PD.

3.1 Response Analysis

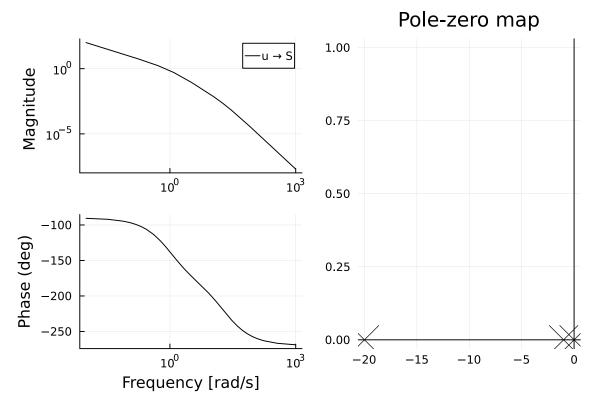


Figure 3.1: Starting Bode Plot and PZ Map

It has the shape we expect from a motor + friction. Slow pole for the mass + friction and a faster pole for the current & inductance.

Numerically they are:

display(eigvals(contSys.A))

3-element Vector{Float64}:

-20.0

-1.0

0.0

We see that we start with all the poles in the left-half plane, which is good.

3.2 Pole Placement

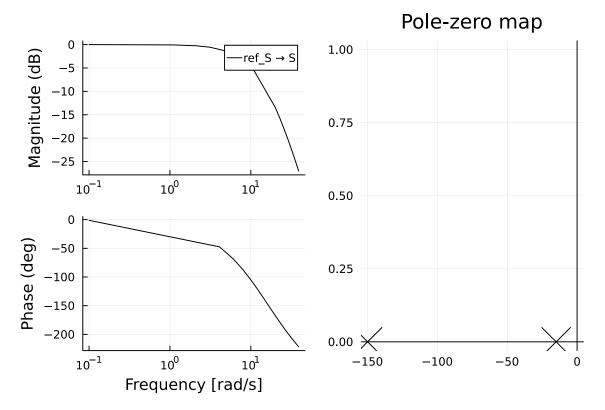
We can design a controller with pole placement.

For some reason pole placement doesn't work for the observer, I use a Kalman Filter with random fast values.

We can check the effect of the new controller on the loop

```
closedLoop = feedback( contSys * fsf_controller);
print(poles(closedLoop));
setPlotScale("dB")
plot!(bodeplot(closedLoop[1,1], 0.1:40), pzmap(closedLoop))
```

ComplexF64[-14.990000366343788 + 0.0im, -14.999999266673722 + 0.0im, -15.010000366982666 + 0.0im, -149.99999999999986 + 0.0im, -150.1000000002432 + 0.0im, -149.8999999999607 + 0.0im]



We can compare this to the open-loop response in @start-bode. We can see that we achieve unitary gain throughout the whole low-frequency range.

We can convert the pole placement controller into the standard PD gain form.

```
using DiscretePIDs
Ts = 0.02 # sampling time
Tf = 2.5; #final simulation time

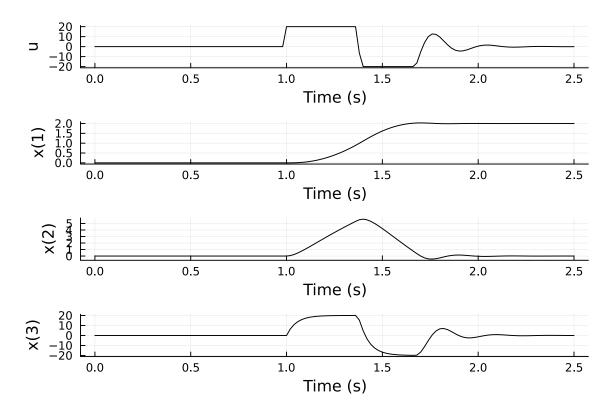
K = L[1];
Ti = 0;
Td = L[2] / L[1];
pid = DiscretePID(; K, Ts, Ti, Td);
```

3.3 Simulation

We can simulate this with a motor that only outputs the position:

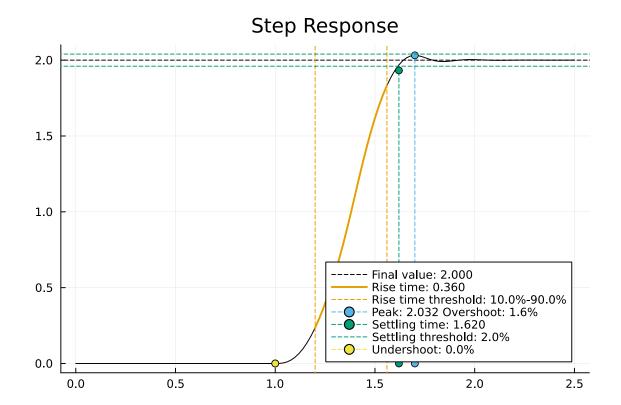
```
sysreal = ss(contSys.A, contSys.B, [1 0 0], 0.0)
ctrl = function (x, t)
```

```
y = (sysreal.C*x)[] # measurement
    d = 0 * [1.0] # disturbance
    r = 2.0 * (t \ge 1) # reference
    # u = pid(r, y) # control signal
    # u + d # Plant input is control signal + disturbance
    # u =1
    e = x - [r; 0.0; 0.0]
    e[3] = 0.0 # torque not observable, just ignore it in the
     → final feedback
    u = -L * e + d
    u = [maximum([-20.0 minimum([20.0 u])])]
end
t = 0:Ts:Tf
res = lsim(sysreal, ctrl, t)
display(plot(res,
    plotu=true,
    plotx=true,
    ploty=false
ylabel!("u", sp=1);
ylabel!("x", sp=2);
ylabel!("v", sp=3);
ylabel!("T", sp=4);
```



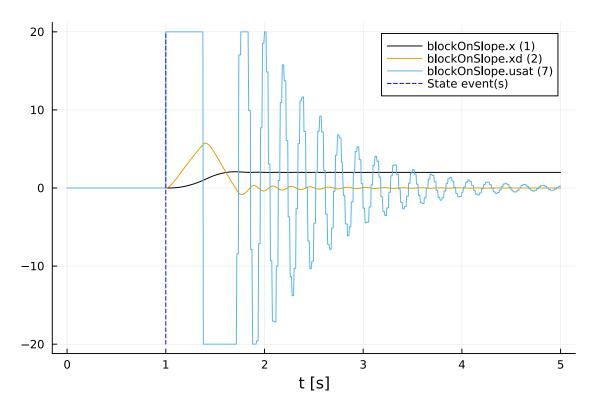
For more stats:

```
si = stepinfo(res);
plot(si);title!("Step Response")
```



We can also simulate it in a SIMULINK-like environment:

```
using FMI, DifferentialEquations
fmuPath = abspath(joinpath(@__DIR___,
  "..",".."
  "modelica",
  "ControlChallenges",
  "ControlChallenges.BlockOnSlope_Challenges.Examples.WithFrict
  → ion.fmu"))
fmu = loadFMU(fmuPath);
simData = simulateME(
    fmu,
    (0.0, 5.0);
    recordValues=["blockOnSlope.x",
    "blockOnSlope.xd",
    "blockOnSlope.usat"],
    showProgress=false);
unloadFMU(fmu);
plot(simData, states=false, timeEvents=false)
```



There is a slight difference between the <code>lsim</code> simulation and the FMU simulation. I need to recheck some stuff.

4 Block on a slope

Position Control with friction. Using Pole Placement + PD.

4.1 Response Analysis

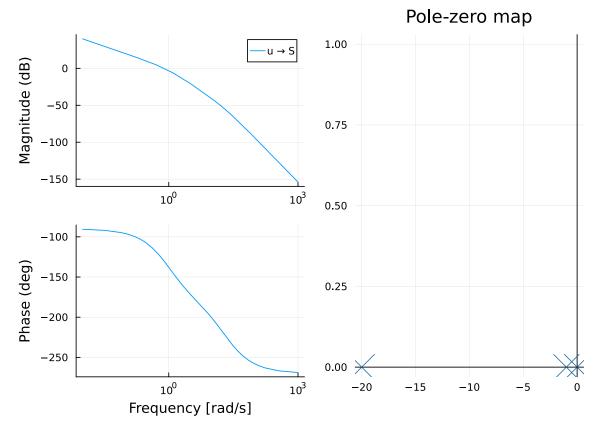


Figure 4.1: Starting Bode Plot and PZ Map

It has the shape we expect from a motor + friction. Slow pole for the mass + friction and a faster pole for the current & inductance.

Numerically they are:

display(eigvals(contSys.A))

3-element Vector{Float64}:

- -20.0
 - -1.0
 - 0.0

We see that we start with all the poles in the left-half plane, which is good.

4.2 Pole Placement

We can design a controller with pole placement.

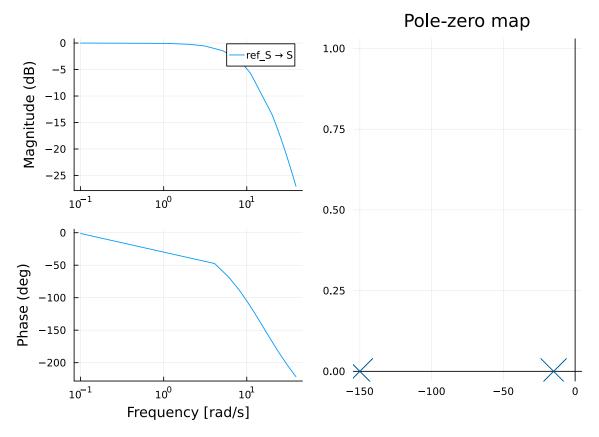
For some reason pole placement doesn't work for the observer, I use a Kalman Filter with random fast values.

```
observability(contSys.A,contSys.C).isobservable || error("System

    is not observable")

controllability(contSys.A,contSys.B).iscontrollable ||
 → error("System is not controllable")
\varepsilon = 0.01;
pp = 15.0;
poles_cont = -[pp + \epsilon, pp - \epsilon, pp];
L = real(place(contSys, poles_cont, :c));
poles_obs = poles_cont * 10.0;
K = place(contSys, poles_obs, :o)
obs_controller = observer_controller(contSys, L, K;
→ direct=false);
fsf_controller = named_ss(obs_controller, u = [:ref_S, :ref_V],
 \rightarrow y = [:u])
NamedStateSpace{Continuous, Float64}
A =
  -150.0
                                   8.033684828490095e-12
                                                             0.0
     1.0915557686859107e-5
                               -279.999999999851
                                                             1.0
 -3374.9970813429577
                             -17530.98989999806
                                                          -44.0
B =
 150.0
                               0.999999999919663
  -1.0915557686859107e-5
                             278.999999999851
  -0.0014186570429435138 16899.989999998063
 168.74992500000002 31.54999500000003 1.2000000000000002
D =
 0.0
      0.0
Continuous-time state-space model
With state names: x1 x2 x3
     input names: ref_S ref_V
     output names: u
We can check the effect of the new controller on the loop
closedLoop = feedback( contSys * fsf_controller);
print(poles(closedLoop));
setPlotScale("dB")
plot!(bodeplot(closedLoop[1,1], 0.1:40), pzmap(closedLoop))
```

ComplexF64[-14.990000366343788 + 0.0im, -14.999999266673722 + 0.0im, -15.010000366982666 + 0.0im, -149.9999999999986 + 0.0im, -150.1000000002432 + 0.0im, -149.899999999607 + 0.0im]



We can compare this to the open-loop response in @start-bode. We can see that we achieve unitary gain throughout the whole low-frequency range.

We can convert the pole placement controller into the standard PD gain form.

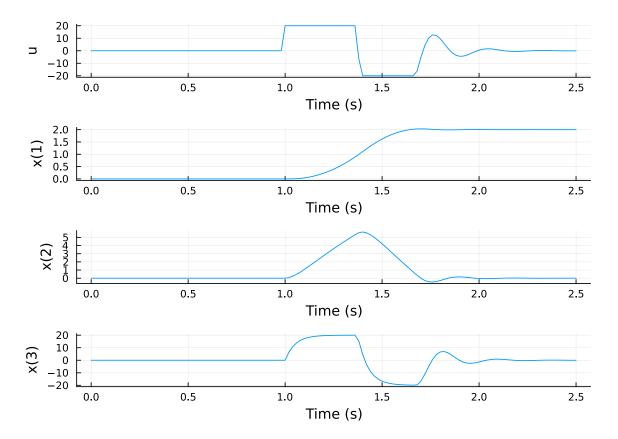
```
using DiscretePIDs
Ts = 0.02 # sampling time
Tf = 2.5; #final simulation time

K = L[1];
Ti = 0;
Td = L[2] / L[1];
pid = DiscretePID(; K, Ts, Ti, Td);
```

4.3 Simulation

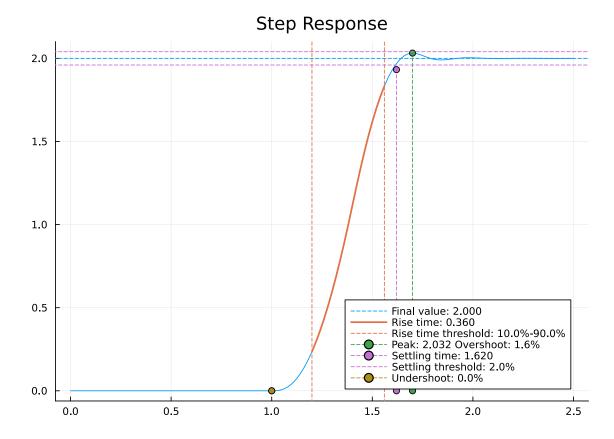
We can simulate this with a motor that only outputs the position:

```
sysreal = ss(contSys.A, contSys.B, [1 0 0], 0.0)
ctrl = function (x, t)
    y = (sysreal.C*x)[] # measurement
    d = 0 * [1.0]
                    # disturbance
    r = 2.0 * (t \ge 1) # reference
    # u = pid(r, y) # control signal
    # u + d # Plant input is control signal + disturbance
    \# u = 1
    e = x - [r; 0.0; 0.0]
    e[3] = 0.0 # torque not observable, just ignore it in the
    → final feedback
    u = -L * e + d
    u = [maximum([-20.0 minimum([20.0 u])])]
end
t = 0:Ts:Tf
res = lsim(sysreal, ctrl, t)
display(plot(res,
    plotu=true,
    plotx=true,
    ploty=false
    ))
ylabel!("u", sp=1);
ylabel!("x", sp=2);
ylabel!("v", sp=3);
ylabel!("T", sp=4);
```



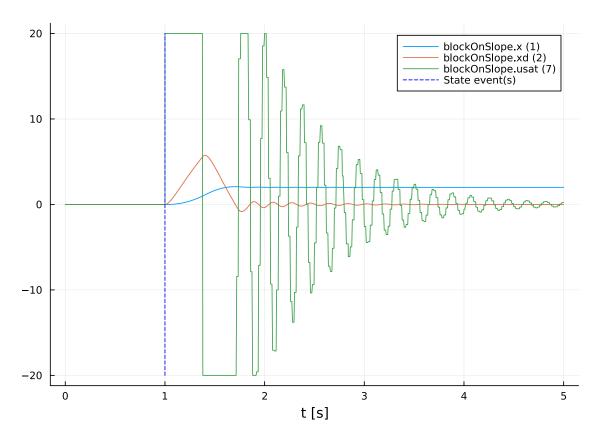
For more stats:

```
si = stepinfo(res);
plot(si);title!("Step Response")
```



We can also simulate it in a SIMULINK-like environment:

```
using FMI, DifferentialEquations
fmuPath = abspath(joinpath(@__DIR___,
  "..","..",
  "modelica",
  "ControlChallenges",
  "ControlChallenges.BlockOnSlope_Challenges.Examples.WithFrict
  → ion.fmu"))
fmu = loadFMU(fmuPath);
simData = simulateME(
    fmu,
    (0.0, 5.0);
    recordValues=["blockOnSlope.x",
    "blockOnSlope.xd",
    "blockOnSlope.usat"],
    showProgress=false);
unloadFMU(fmu);
plot(simData, states=false, timeEvents=false)
```



There is a slight difference between the <code>lsim</code> simulation and the FMU simulation. I need to recheck some stuff.

5 Performance tricks

5.1 Hurwitz Check

Create our nice model. Assume to have run the **poles** function and that you have a vector of eigenvalues. For simplicity I will create an arbitrary vector with the first 100 values in -1 and the last 100 values as random around 0.

```
using BenchmarkTools
vbig = [zeros(ComplexF64,100).-1 ; rand(ComplexF64,100).-0.5];
vbig[[1,end]]
```

Then with a naive approach we check if all the elements are in the LHP.

```
@benchmark all(real(vbig).≤0)
```

BenchmarkTools.Trial: 10000 samples with 264 evaluations per sample.

```
Range (min ... max): 298.864 ns ... 64.470 \mus | GC (min ... max): 0.00% ... 98.48% 

Time (median): 335.227 ns | GC (median): 0.00% 

Time (mean \pm \sigma): 532.914 ns \pm 1.490 \mus | GC (mean \pm \sigma): 27.39% \pm 11.09%
```

```
299 ns Histogram: log(frequency) by time 8.4 μs <
```

Memory estimate: 1.78 KiB, allocs estimate: 6.

The whole vector of complex numbers gets converted to real and then we check row by row if it's non-positive. The whole check one by one results in a vector with booleans that gets checked one by one if it contains false values.

@benchmark all(≤(0),real(vbig))

BenchmarkTools.Trial: 10000 samples with 205 evaluations per sample.

```
366 ns Histogram: log(frequency) by time 2.27 µs <
```

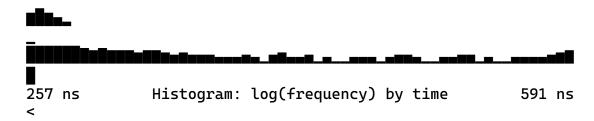
Memory estimate: 1.62 KiB, allocs estimate: 2.

For now we can skip the full evaluation of non-positivity: the first time it encounters a positive numbers it returns false. This improves the performance a little bit.

@benchmark all(i → real(i) ≤ 0, vbig)

BenchmarkTools.Trial: 10000 samples with 340 evaluations per sample.

```
Range (min ... max): 257.353 ns ... 999.706 ns \vdots GC (min ... max): 0.00% ... 0.00% ... 266.765 ns \vdots GC (median): 0.00% Time (mean \pm \sigma): 273.065 ns \pm 44.546 ns \vdots GC (mean \pm \sigma): 0.00% \pm 0.00%
```



Memory estimate: 0 bytes, allocs estimate: 0.

This is the final form. Instead of converting into real the full vector it checks element by element if it's in the LHP. It returns false at the first failure.