Control Challenges: Solutions

lacopo Moles

Table of contents

1	1.1 Intro	3 3 3 3
Ι	Block on a Slope	5
2		6
3	3.1 State Space representation	8 9 11
4	4.1 Response Analysis 1 4.2 Pole Placement 1	4 14 15 16
5	5.1 Response Analysis 2 5.2 Pole Placement 2	21 22 24
Αŗ	opendices 2	8
Α	A.1 Hurwitz Check	28 28 29

1 Introduction

1.1 Intro

This is a collection of write ups on how to solve the various problems presented by Github user¹ "Janismac".

1.2 What do I need?

1.2.1 Software

- A real OS like Linux or Windows. 2
- The Julia Programming Language³
 - Clone the repo⁴
 - Activate the package by running in your terminal:

```
julia --project -e 'using Pkg; Pkg.instantiate()'
```

(Nice to have) OpenModelica Editor⁵

1.2.2 Theory

- · Basic Julia knowledge
- Basic JS knowledge
- Control Theory knowledge
 - Frequency Based Control
 - State Space Based control
- Misc knowledge:
 - Linear Algebra

¹https://janismac.github.io/ControlChallenges/

²MacOs should be supported in theory but it's not tested.

³https://julialang.org/install/

⁴https://github.com/icpmoles/controlchallengessolutions

⁵https://openmodelica.org/

1 Introduction

- Differential Equations

Part I Block on a Slope

2 The Damped Mass problem

2.1 Modeling

To better understand the problem let's take a peek¹ at how the simulated model works.

Listing 2.1 BlockOnSlope.js

```
Models.BlockOnSlope.prototype.vars =
                                                                  (1)
   g: 9.81,
                  // distance from objective s
   x: 0,
                 // velocity v
   dx: 0,
   slope: 1,
                 // slope coefficient alpha = dy/dx in the
    // Requested u
   F: 0,
   F_cmd: 0, // Saturated u
   friction: 0, // Coulomb friction coefficient mu
   T: 0.
                  // Simulation Time
};
Models.BlockOnSlope.prototype.simulate = function (dt, controlFunc)
{
    this.F_cmd = controlFunc({x:this.x,dx:this.dx,T:this.T});
   if(typeof this.F_cmd != 'number' || isNaN(this.F_cmd)) throw
    □ "Error: The controlFunction must return a number.";
    this.F_cmd = Math.max(-20, Math.min(20, this.F_cmd));
                                                                  (2)
   integrationStep(this, `['x', 'dx', `F'], dt);
}
Models.BlockOnSlope.prototype.ode = function (x)
{
   return [
       x[1],
        (x[2]) - (Math.sin(this.slope) * this.g) - (this.friction *
   x[1]),
       20.0 * (this.F_cmd - x[2])
    ];
}
```

¹https://github.com/janismac/ControlChallenges/blob/gh-pages/js/models/BlockOnSlope.js

2 The Damped Mass problem

- 1 The model has obviously some default values for the parameters that can be modified for the different scenarios.
- ② The control command u is generated by the controlFunction(block) function provided by us. There are some checks to see if it's a number. If it's acceptable then it passes through a saturation between ± 20 .
- (3) The model is a simple ODE with equations:

$$\begin{cases} \dot{s} = v \\ \dot{v} = F - \sin(\alpha) \cdot g - \mu \cdot v \\ \dot{F} = -20 \cdot F + 20 \cdot u_{sat} \end{cases}$$

Converting it in state-space representation:

$$\begin{bmatrix} \dot{s} \\ \dot{v} \\ \dot{F} \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & -\mu & 1 \\ 0 & 0 & -20 \end{bmatrix} \begin{bmatrix} s \\ v \\ F \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ u_{sat} \end{bmatrix} + \begin{bmatrix} 0 \\ -\sin(\alpha) \cdot g \\ 0 \end{bmatrix}$$
$$\begin{bmatrix} s \\ v \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} s \\ v \\ F \end{bmatrix}$$

Obviously the gravitational term acts as a disturbance.

3 Block without Friction

Position Control with friction. Using Pole Placement + PD.

3.1 State Space representation

We can convert the set of ODE into a state space representation. The final bode plot of the block position is:

```
using DiscretePIDs, ControlSystems, Plots, LinearAlgebra
# System parameters
Ts = 0.02 # sampling time
Tf = 2.5; #final simulation time
g = 9.81 \# gravity
\alpha = 0.0 \text{ # slope}
\mu = 1.0 # friction coefficient
x_0 = -2.0 # starting position
dx_0 = 0.0 # starting velocity
\tau = 20.0 \text{ # torque constant}
# State Space Matrix
A = \begin{bmatrix} 0 & 1 & 0 \end{bmatrix}
    0 - \mu 1
    0 \ 0 \ -\tau];
B = [0]
    0
    τ];
C = [1 \ 0 \ 0]
    0 1 0];
sys = ss(A, B, C, 0.0) # Continuous
plot!(bodeplot(tf(sys)),pzmap(tf(sys)))
```

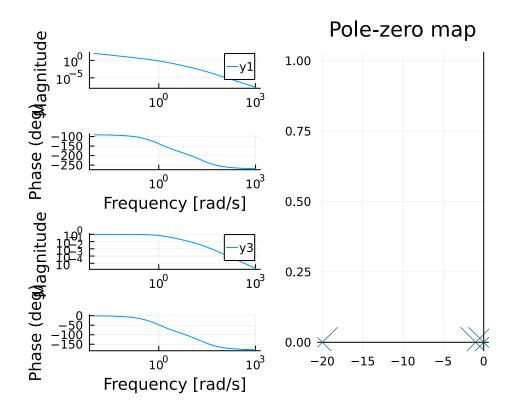


Figure 3.1: Starting Bode Plot and PZ Map

It has the shape we expect from a motor + friction. Slow pole for the mass + friction and a faster pole for the current & inductance.

Numerically they are:

display(eigvals(A))

3-element Vector{Float64}:

-20.0

-1.0

0.0

We see that we start with all the pole in the left-half plane, which is good.

3.2 Pole Placement

We can design a controller with pole placement.

For some reason pole placement doesn't work for the observer, I use a Kalman Filter with random fast values.

```
observability(A, C).isobservable &
controllability(A, B).iscontrollable; #OK

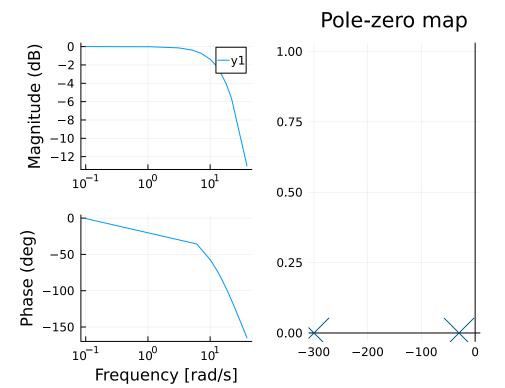
ε = 0.01;
pp = 15.0;
poles_cont = -2.0 * [pp + ε, pp - ε, pp];
L = real(place(sys, poles_cont, :c));

poles_obs = poles_cont * 10.0;
K = place(1.0 * A', 1.0 * C', poles_obs)'
cont = observer_controller(sys, L, K; direct=false);
```

We can check the effect of the new controller on the loop

```
closedLoop = feedback(sys * cont)
print(poles(closedLoop));
setPlotScale("dB")
plot!(bodeplot(closedLoop[1, 1], 0.1:40), pzmap(closedLoop))
```

ComplexF64[-29.979998924597755 + 0.0im, -30.000002152199972 + 0.0im, -30.019998923202337 + 0.0im, -300.000000000004 + 0.0im, -300.199999999752 + 0.0im, -299.80000000004117 + 0.0im]



We can compare this to the open-loop response in @start-bode. We can see that we achieve unitary gain throughout the whole low-frequency range.

We can convert the pole placement controller into the standard PD gain form.

```
K = L[1];
Ti = 0;
Td = L[2] / L[1];
pid = DiscretePID(; K, Ts, Ti, Td);
```

3.3 Simulation

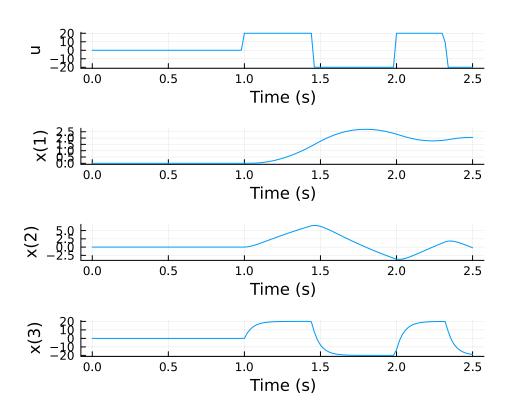
We can simulate this with a motor that only outputs the position:

```
sysreal = ss(A, B, [1 0 0], 0.0)
ctrl = function (x, t)
    y = (sysreal.C*x)[] # measurement
    d = 0 * [1.0]
                         # disturbance
    r = 2.0 * (t >= 1) # reference
    \# u = pid(r, y) \# control signal
    # u + d # Plant input is control signal + disturbance
    # u =1
    e = x - [r; 0.0; 0.0]
    e[3] = 0.0 # torque not observable, just ignore it in the final

    feedback

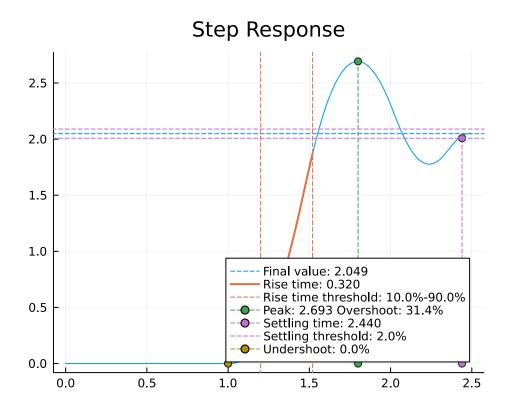
    u = -L * e + d
    u = [maximum([-20.0 minimum([20.0 u])])]
end
t = 0:Ts:Tf
res = lsim(sysreal, ctrl, t)
display(plot(res,
     plotu=true,
     plotx=true,
     ploty=false
    ))
ylabel!("u", sp=1);
ylabel!("x", sp=2);
ylabel!("v", sp=3);
ylabel!("T", sp=4);
```

3 Block without Friction



For more stats:

```
si = stepinfo(res);
plot(si);title!("Step Response")
```

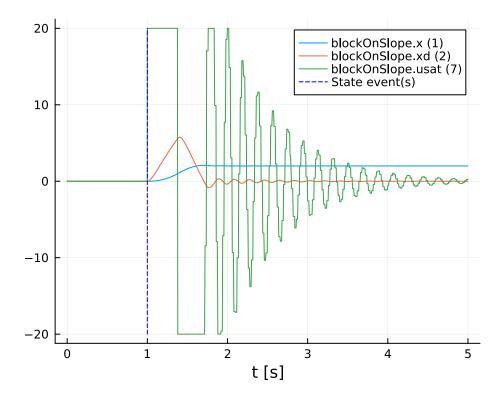


We can also simulate it in a SIMULINK-like environment:

```
using FMI, DifferentialEquations
fmuPath = abspath(joinpath(@__DIR___,
  " , " , " , " ,
  "modélica",
  "ControlChallenges",
  "ControlChallenges.BlockOnSlope_Challenges.Examples.WithFriction.f

   mu"))

fmu = loadFMU(fmuPath);
simData = simulateME(
    fmu,
    (0.0, 5.0);
    recordValues=["blockOnSlope.x",
    "blockOnSlope.xd",
    "blockOnSlope.usat"],
    showProgress=false);
unloadFMU(fmu);
plot(simData, states=false, timeEvents=false)
```



There is a slight difference between the lsim simulation and the FMU simulation. I need to recheck some stuff.

4 Block With Friction

Position Control with friction. Using Pole Placement + PD.

4.1 Response Analysis

```
using CCS using ControlSystems, Plots, LinearAlgebra, RobustAndOptimalControl CCS.setupEnv() contSys = CCS.blockModel.csys(;g = 0, \alpha = 0 , \mu = 1, \tau =20) plot!(bodeplot(contSys[1,1]),pzmap(contSys))
```

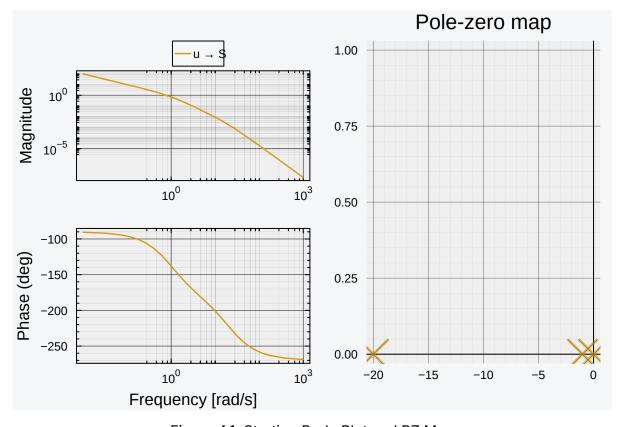


Figure 4.1: Starting Bode Plot and PZ Map

4 Block With Friction

It has the shape we expect from a motor + friction. Slow pole for the mass + friction and a faster pole for the current & inductance.

Numerically they are:

```
display(eigvals(contSys.A))
3-element Vector{Float64}:
  -20.0
  -1.0
   0.0
```

We see that we start with all the poles in the left-half plane, which is good.

4.2 Pole Placement

We can design a controller with pole placement.

For some reason pole placement doesn't work for the observer, I use a Kalman Filter with random fast values.

```
observability(contSys.A,contSys.C).isobservable || error("System is
    not observable")
controllability(contSys.A,contSys.B).iscontrollable || error("System
    is not controllable")

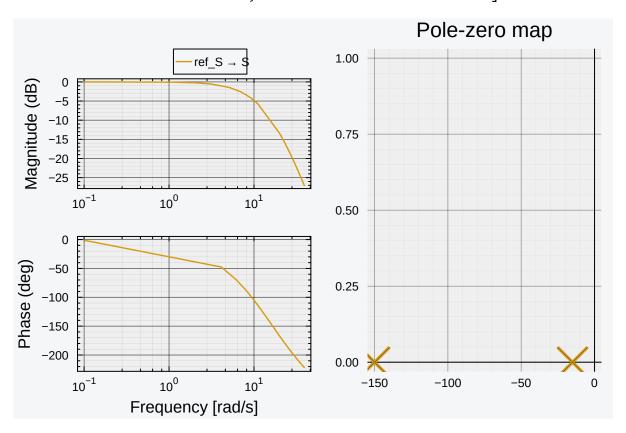
ε = 0.01;
pp = 15.0;
poles_cont = - [pp + ε, pp - ε, pp];
L = real(place(contSys, poles_cont, :c));

poles_obs = poles_cont * 10.0;
K = place(contSys, poles_obs, :o)
obs_controller = observer_controller(contSys, L, K; direct=false);
fsf_controller = named_ss(obs_controller, u = [:ref_S, :ref_V], y =
    [:u]);
```

We can check the effect of the new controller on the loop

```
closedLoop = feedback( contSys * fsf_controller);
print(poles(closedLoop));
setPlotScale("dB")
plot!(bodeplot(closedLoop[1,1], 0.1:40), pzmap(closedLoop))
```

```
ComplexF64[-14.990000366343788 + 0.0im, -14.999999266673722 + 0.0im, -15.010000366982666 + 0.0im, -149.99999999986 + 0.0im, -150.10000000002432 + 0.0im, -149.899999999607 + 0.0im]
```



We can compare this to the open-loop response in @start-bode. We can see that we achieve unitary gain throughout the whole low-frequency range.

We can convert the pole placement controller into the standard PD gain form.

```
using DiscretePIDs
Ts = 0.02 # sampling time
Tf = 2.5; #final simulation time

K = L[1];
Ti = 0;
Td = L[2] / L[1];
pid = DiscretePID(; K, Ts, Ti, Td);
```

4.3 Simulation

We can simulate this with a motor that only outputs the position:

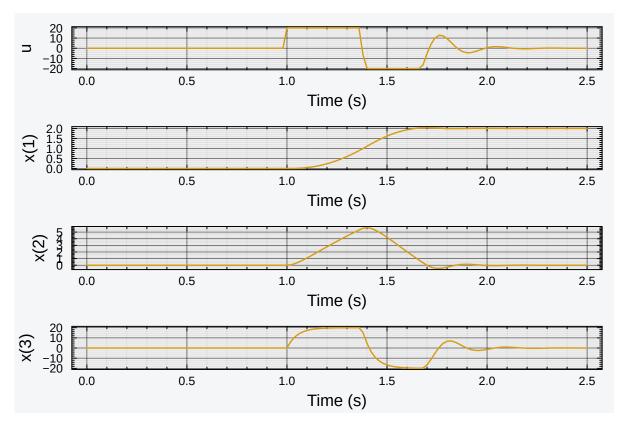
4 Block With Friction

```
sysreal = ss(contSys.A, contSys.B, [1 0 0], 0.0)
ctrl = function (x, t)
    y = (sysreal.C*x)[] # measurement
    d = 0 * [1.0]
                       # disturbance
    r = 2.0 * (t >= 1) # reference
    \# u = pid(r, y) \# control signal
    # u + d # Plant input is control signal + disturbance
    # u =1
    e = x - [r; 0.0; 0.0]
    e[3] = 0.0 # torque not observable, just ignore it in the final

    feedback

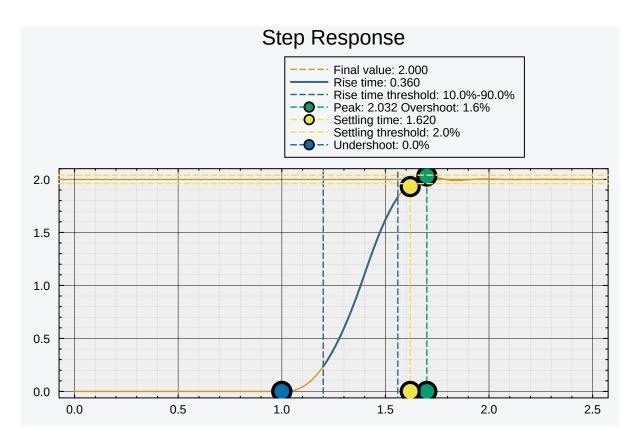
    u = -L * e + d
    u = [maximum([-20.0 minimum([20.0 u])])]
end
t = 0:Ts:Tf
res = lsim(sysreal, ctrl, t)
display(plot(res,
    plotu=true,
    plotx=true,
    ploty=false
    ))
ylabel!("u", sp=1);
ylabel!("x", sp=2);
ylabel!("v", sp=3);
ylabel!("T", sp=4);
```

4 Block With Friction



For more stats:

```
si = stepinfo(res);
plot(si);title!("Step Response")
```



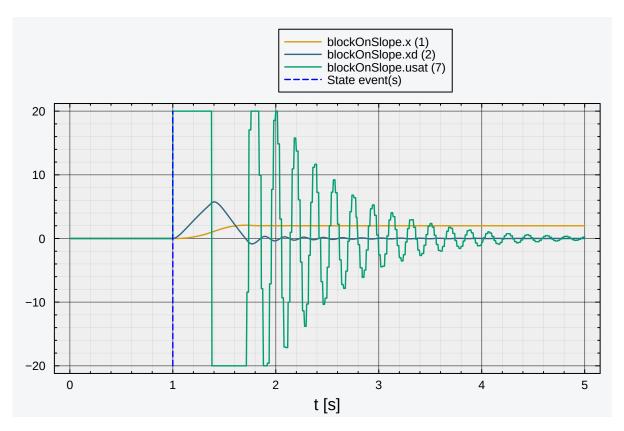
We can also simulate it in a SIMULINK-like environment:

```
using FMI, DifferentialEquations
fmuPath = abspath(joinpath(@__DIR___,
  " " " " " ,
  "modélica",
  "ControlChallenges",
  "ControlChallenges.BlockOnSlope_Challenges.Examples.WithFriction.f

  mu"))

fmu = loadFMU(fmuPath);
simData = simulateME(
    fmu,
    (0.0, 5.0);
    recordValues=["blockOnSlope.x",
    "blockOnSlope.xd",
    "blockOnSlope.usat"],
    showProgress=false);
unloadFMU(fmu);
plot(simData, states=false, timeEvents=false)
```

4 Block With Friction



There is a slight difference between the lsim simulation and the FMU simulation. I need to recheck some stuff.

Position Control with friction. Using Pole Placement + PD.

5.1 Response Analysis

```
using CCS using ControlSystems, Plots, LinearAlgebra, RobustAndOptimalControl CCS.setupEnv() contSys = CCS.blockModel.csys(;g = 0, \alpha = 0 , \mu = 1, \tau =20) plot!(bodeplot(contSys[1,1]),pzmap(contSys))
```

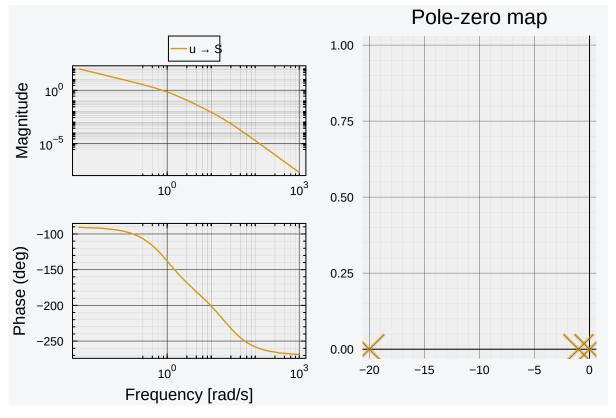


Figure 5.1: Starting Bode Plot and PZ Map

It has the shape we expect from a motor + friction. Slow pole for the mass + friction and a faster pole for the current & inductance.

Numerically they are:

```
display(eigvals(contSys.A))
3-element Vector{Float64}:
  -20.0
  -1.0
   0.0
```

We see that we start with all the poles in the left-half plane, which is good.

5.2 Pole Placement

C =

We can design a controller with pole placement.

For some reason pole placement doesn't work for the observer, I use a Kalman Filter with random fast values.

```
observability(contSys.A,contSys.C).isobservable | error("System is

    not observable")

controllability(contSys.A,contSys.B).iscontrollable || error("System

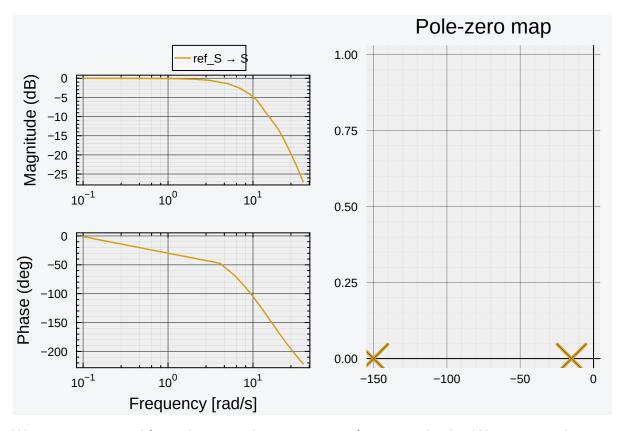
    is not controllable")

\varepsilon = 0.01;
pp = 15.0;
poles_cont = - [pp + \epsilon, pp - \epsilon, pp];
L = real(place(contSys, poles_cont, :c));
poles_obs = poles_cont * 10.0;
K = place(contSys, poles_obs, :o)
obs_controller = observer_controller(contSys, L, K; direct=false);
fsf_controller = named_ss(obs_controller, u = [:ref_S, :ref_V], y =
 NamedStateSpace{Continuous, Float64}
A =
  -150.0
                                  8.033684828490095e-12
                                                            0.0
     1.0915557686859107e-5
                               -279.999999999851
                                                            1.0
 -3374.9970813429577
                                                          -44.0
                             -17530.98989999806
B =
 150.0
                               0.999999999919663
  -1.0915557686859107e-5
                             278.999999999851
  -0.0014186570429435138 16899.989999998063
```

We can check the effect of the new controller on the loop

```
closedLoop = feedback( contSys * fsf_controller);
print(poles(closedLoop));
setPlotScale("dB")
plot!(bodeplot(closedLoop[1,1], 0.1:40), pzmap(closedLoop))
```

```
ComplexF64[-14.990000366343788 + 0.0im, -14.999999266673722 + 0.0im, -15.010000366982666 + 0.0im, -149.99999999986 + 0.0im, -150.10000000002432 + 0.0im, -149.899999999607 + 0.0im]
```



We can compare this to the open-loop response in @start-bode. We can see that we achieve unitary gain throughout the whole low-frequency range.

We can convert the pole placement controller into the standard PD gain form.

```
using DiscretePIDs
Ts = 0.02 # sampling time
Tf = 2.5; #final simulation time

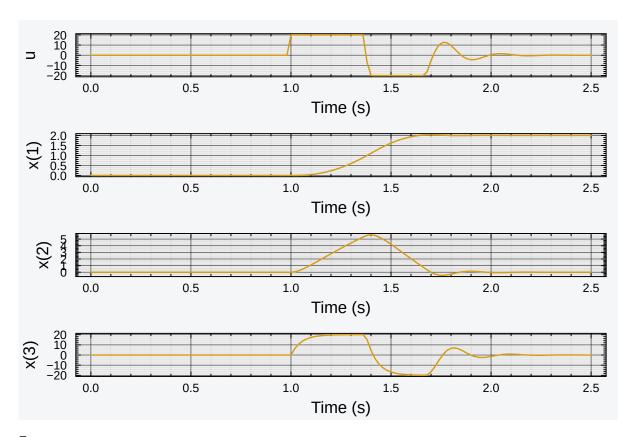
K = L[1];
Ti = 0;
Td = L[2] / L[1];
pid = DiscretePID(; K, Ts, Ti, Td);
```

5.3 Simulation

We can simulate this with a motor that only outputs the position:

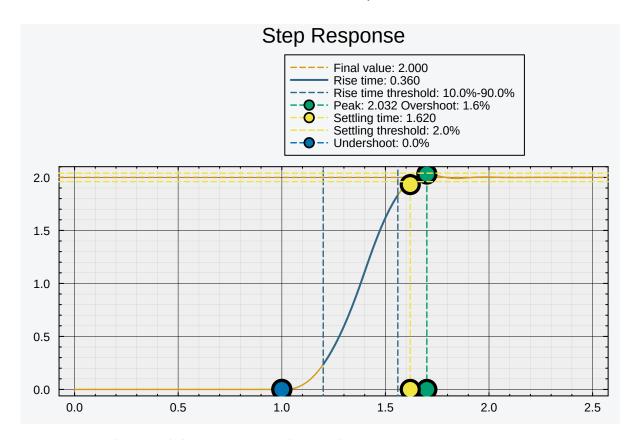
```
sysreal = ss(contSys.A, contSys.B, [1 0 0], 0.0)
ctrl = function (x, t)
    y = (sysreal.C*x)[] # measurement
    d = 0 * [1.0]
                         # disturbance
    r = 2.0 * (t >= 1) # reference
    \# u = pid(r, y) \# control signal
    # u + d # Plant input is control signal + disturbance
    # u =1
    e = x - [r; 0.0; 0.0]
    e[3] = 0.0 # torque not observable, just ignore it in the final
     → feedback
    u = -L * e + d
    u = [maximum([-20.0 minimum([20.0 u])])]
end
t = 0:Ts:Tf
res = lsim(sysreal, ctrl, t)
display(plot(res,
    plotu=true,
    plotx=true.
    ploty=false
    ))
ylabel!("u", sp=1);
ylabel!("x", sp=2);
ylabel!("v", sp=3);
ylabel!("T", sp=4);
```

5 Block on a slope



For more stats:

```
si = stepinfo(res);
plot(si);title!("Step Response")
```

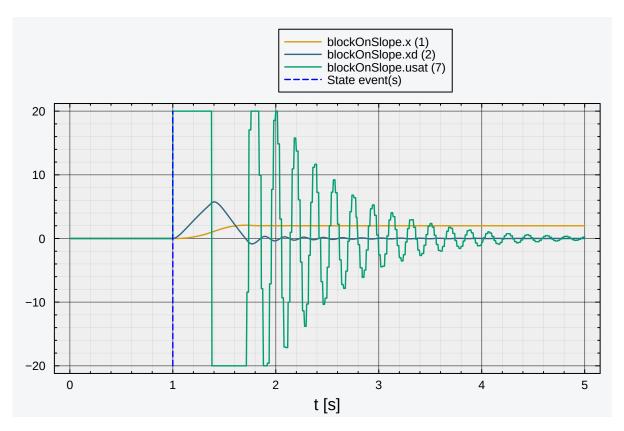


We can also simulate it in a SIMULINK-like environment:

```
using FMI, DifferentialEquations
fmuPath = abspath(joinpath(@__DIR___,
  " " " " " ,
  "modélica",
  "ControlChallenges",
  "ControlChallenges.BlockOnSlope_Challenges.Examples.WithFriction.f

   mu"))

fmu = loadFMU(fmuPath);
simData = simulateME(
    fmu,
    (0.0, 5.0);
    recordValues=["blockOnSlope.x",
    "blockOnSlope.xd",
    "blockOnSlope.usat"],
    showProgress=false);
unloadFMU(fmu);
plot(simData, states=false, timeEvents=false)
```



There is a slight difference between the lsim simulation and the FMU simulation. I need to recheck some stuff.

A.1 Hurwitz Check

Create our nice model. Assume to have run the poles function and that you have a vector of eigenvalues. For simplicity I will create an arbitrary vector with the first 100 values in -1 and the last 100 values as random around 0.

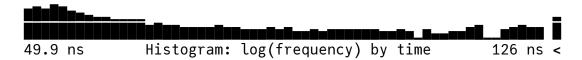
A.1.1 for loop

With a naive approach we check if all the elements are in the LHP: make a function that iterates and returns false if it hits a pole with positive real part.

```
function isHurwitz(v)
    for i in eachindex(v)
        if real(v[i])>0.0
            return false
        end
    end
    return true
end

@benchmark isHurwitz($(Ref(vbig))[])
```

```
BenchmarkTools.Trial: 10000 samples with 987 evaluations per sample. Range (min ... max): 49.949 ns ... 969.301 ns | GC (min ... max) : 0.00\%  ... 0.00% Time (median): 54.306 ns | GC (median) : 0.00\%  Time (mean \pm \sigma): 57.041 ns \pm 22.237 ns | GC (mean <math>\pm \sigma): 0.00% \pm 0.00\%
```



Memory estimate: 0 bytes, allocs estimate: 0.

We have our baseline. We can probably squeeze out some more performance but I'm still a Julia noob.

A.1.2 all()

32.85% ± 16.78%

Let's try using some of the built-in declarative functions:

@benchmark all(real(\$vbig).<=0.0)</pre>

183 ns Histogram: $\log(\text{frequency})$ by time 5.1 $\mu s <$

Memory estimate: 1.75 KiB, allocs estimate: 5.

Simple all(), when given a tuple it checks if all the values are True, otherwise it stops when it encounters the first False.

We can see that it's a tad slower. This is because it's creating a new vector with just the real parts, then it's creating a new vector with only the boolean results and then it's checking if there are any False results.

This results in a lot of allocations and wasted resources.

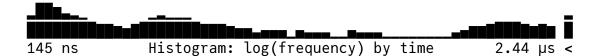
@benchmark all(<=(0.0),real(\$vbig))</pre>

```
BenchmarkTools.Trial: 10000 samples with 759 evaluations per sample.
```

```
Range (min ... max): 144.664 ns ... 31.398 µs | GC (min ... max): 0.00% ... 97.98%

Time (median): 226.746 ns | GC (median): 0.00%
```

Time (mean $\pm \sigma$): 344.335 ns \pm 699.060 ns | GC (mean $\pm \sigma$): 22.41% \pm 15.26%



Memory estimate: 1.62 KiB, allocs estimate: 2.

A smarter way is to skip on of the allocations by creating the vector of real parts and then checking row by row if the non-positivity check fails.

```
@benchmark all(i -> real(i)<=0.0,$vbig)</pre>
```

```
BenchmarkTools.Trial: 10000 samples with 987 evaluations per sample. Range (min … max): 49.139 ns … 2.022 \mus | GC (min … max): 0.00% … 0.00% Time (median): 51.773 ns | GC (median): 0.00% Time (mean \pm \sigma): 53.295 ns \pm 22.061 ns | GC (mean \pm \sigma): 0.00% \pm 0.00%
```



Memory estimate: 0 bytes, allocs estimate: 0.

We can do better: Instead of converting into real the full vector it checks element by element if it's in the LHP. It returns false at the first failure. We finally have a comparable result to the benchmark function but in a more compact way.

Is it cleaner? That's subjective.

A.1.3 mapreduce()

Finally we try the MapReduce approach. This allows a better utilization of your processor without the necessity of learning parallel programming.

```
@benchmark mapreduce(i->real(i)<=0.0, &, $vbig)</pre>
```

```
BenchmarkTools.Trial: 10000 samples with 993 evaluations per sample. Range (min ... max): 42.095 ns ... 692.346 ns \frac{1}{2} GC (min ... max): 0.00% ... 0.00% \frac{1}{2} Time (median): 43.807 ns \frac{1}{2} GC (median): 0.00% \frac{1}{2} GC (mean \frac{1}{2} \frac{1}{2} GC (mean \frac{1}{2} \frac{1}{2} \frac{1}{2} GC (mean \frac{1}{2} \frac{1}
```



Memory estimate: 0 bytes, allocs estimate: 0.

We squeeze the last bit of performance and beat the initial benchmark, not by much but still appreciable.