Control Theory: Tutorial with Julia

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1 Introduction

1.1 Intro

This is a collection of write ups on how to solve the various problems presented by Github user¹ "Janismac".

1.2 What do I need?

1.2.1 Software

- A real OS like Linux or Windows.
- The Julia Programming Language³
 - Clone the repo4
 - Activate the package by running in your terminal:

```
julia --project -e 'using Pkg; Pkg.instantiate()'
```

• (Nice to have) OpenModelica Editor⁵

1.2.2 Theory

- Basic Julia knowledge
- Basic JS knowledge
- · Control Theory knowledge
 - Frequency Based Control
 - State Space Based control
- Misc knowledge:
 - Linear Algebra
 - Differential Equations

¹https://janismac.github.io/ControlChallenges/

²MacOs should be supported in theory but it's not tested.

³https://julialang.org/install/

https://github.com/icpmoles/controlchallengessolutions

⁵https://openmodelica.org/

Part I Block on a Slope

2 The Damped Mass problem

2.1 Modeling

To better understand the problem let's take a peek¹ at how the simulated model works.

Listing 2.1 BlockOnSlope.js

```
Models.BlockOnSlope.prototype.vars =
                                                                                                        1
    g: 9.81,
    x: 0.
                     // distance from objective s
    dx: 0,
                    // velocity v
// slope coefficient alpha = dy/dx in the cartesian plane
    slope: 1,
                    // Requested u
    F: 0,
    F_cmd: 0,
                    // Saturated u
// Coulomb friction coefficient mu
    friction: 0,
                     // Simulation Time
    T: 0,
};
Models.BlockOnSlope.prototype.simulate = function (dt, controlFunc)
    this.F_cmd = controlFunc({x:this.x,dx:this.dx,T:this.T});
    if(typeof this.F_cmd != 'number' || isNaN(this.F_cmd)) throw "Error: The controlFunction
     ⇔ must return a number.";
    this.F_cmd = Math.max(-20,Math.min(20,this.F_cmd));
integrationStep(this, ['x', 'dx', 'F'], dt);
                                                                                                        2
}
Models.BlockOnSlope.prototype.ode = function (x)
    return [
         x[1]
                                                                                                        (3)
         (x[2]) - (Math.sin(this.slope) * this.g) - (this.friction * x[1]),
         20.0 * (this.F_cmd - x[2])
    ];
}
```

- ① The model has obviously some default values for the parameters that can be modified for the different scenarios.
- $\tilde{2}$ The control command u is generated by the controlFunction(block) function provided by us. There are some checks to see if it's a number. If it's acceptable then it passes through a saturation between ± 20 .
- $\ensuremath{\mathfrak{3}}$ The model is a simple ODE with equations:

$$\begin{cases} \dot{s} = v \\ \dot{v} = F - sin(\alpha) \cdot g - \mu \cdot v \\ \dot{F} = -20 \cdot F + 20 \cdot u_{sat} \end{cases}$$

Converting it in state-space representation:

$$\begin{bmatrix} \dot{s} \\ \dot{v} \\ \dot{F} \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & -\mu & 1 \\ 0 & 0 & -20 \end{bmatrix} \begin{bmatrix} s \\ v \\ F \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ u_{sat} \end{bmatrix} + \begin{bmatrix} 0 \\ -\sin(\alpha) \cdot g \end{bmatrix}$$
$$\begin{bmatrix} s \\ v \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} s \\ F \end{bmatrix}$$

Obviously the gravitational term acts as a disturbance.

¹https://github.com/janismac/ControlChallenges/blob/gh-pages/js/models/BlockOnSlope.js

3 Block without Friction

Position Control with friction. Using Pole Placement + PD.

3.1 State Space representation

We can convert the set of ODE into a state space representation. The final bode plot of the block position is:

```
using DiscretePIDs, ControlSystems, Plots, LinearAlgebra
# System parameters
Ts = 0.02 # sampling time
Tf = 2.5; #final simulation time
g = 9.81 #gravity
\alpha = 0.0 \text{ # slope}
\mu = 1.0 # friction coefficient
x_0 = -2.0 # starting position

dx_0 = 0.0 # starting velocity
\tau = 20.0 \text{ # torque constant}
# State Space Matrix
A = \begin{bmatrix} 0 & 1 & 0 \end{bmatrix}
     0 -µ 1
     0 0 -τ];
B = [0]
C = \begin{bmatrix} 1 & 0 & 0 \\ 1 & 0 & 0 \end{bmatrix}
     0 1 0];
sys = ss(A, B, C, 0.0)
                                     # Continuous
plot!(bodeplot(tf(sys)),pzmap(tf(sys)))
```

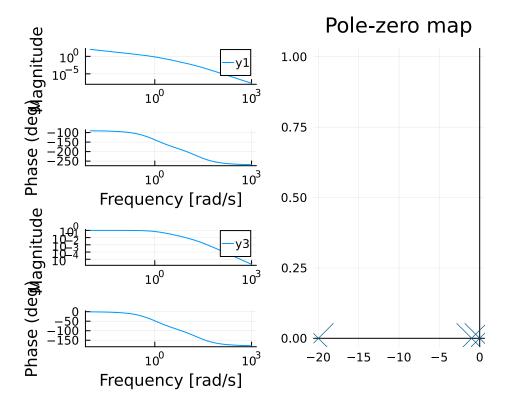


Figure 3.1: Starting Bode Plot and PZ Map

It has the shape we expect from a motor + friction. Slow pole for the mass + friction and a faster pole for the current & inductance.

Numerically they are:

```
display(eigvals(A))
3-element Vector{Float64}:
   -20.0
   -1.0
    0.0
```

We see that we start with all the pole in the left-half plane, which is good.

3.2 Pole Placement

We can design a controller with pole placement.

For some reason pole placement doesn't work for the observer, I use a Kalman Filter with random fast values.

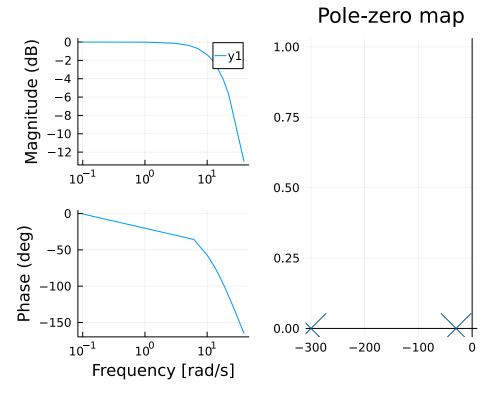
```
observability(A, C).isobservable &
controllability(A, B).iscontrollable; #OK

ε = 0.01;
pp = 15.0;
poles_cont = -2.0 * [pp + ε, pp - ε, pp];
L = real(place(sys, poles_cont, :c));

poles_obs = poles_cont * 10.0;
K = place(1.0 * A', 1.0 * C', poles_obs)'
cont = observer_controller(sys, L, K; direct=false);
```

We can check the effect of the new controller on the loop

```
closedLoop = feedback(sys * cont)
print(poles(closedLoop));
setPlotScale("dB")
plot!(bodeplot(closedLoop[1, 1], 0.1:40), pzmap(closedLoop))
```



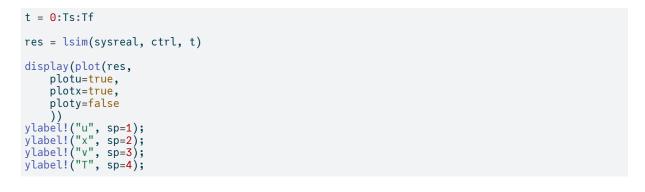
We can compare this to the open-loop response in @start-bode. We can see that we achieve unitary gain throughout the whole low-frequency range.

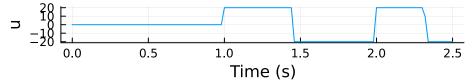
We can convert the pole placement controller into the standard PD gain form.

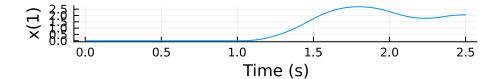
```
K = L[1];
Ti = 0;
Td = L[2] / L[1];
pid = DiscretePID(; K, Ts, Ti, Td);
```

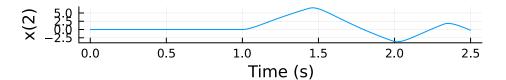
3.3 Simulation

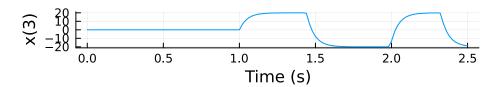
We can simulate this with a motor that only outputs the position:





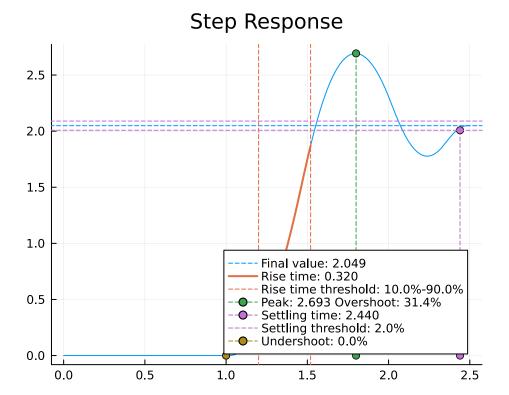




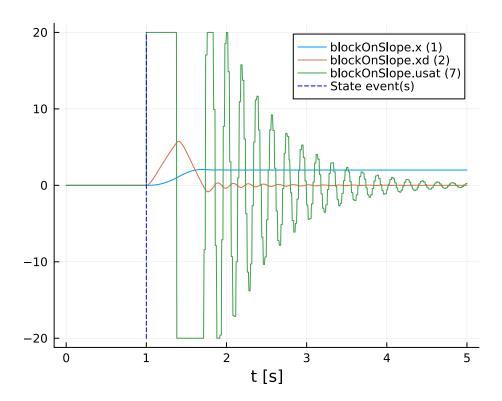


For more stats:

```
si = stepinfo(res);
plot(si);title!("Step Response")
```



We can also simulate it in a SIMULINK-like environment:



There is a slight difference between the lsim simulation and the FMU simulation. I need to recheck some stuff.

4 Block With Friction

Position Control with friction. Using Pole Placement + PD.

4.1 Response Analysis

```
using CCS using ControlSystems, Plots, LinearAlgebra, RobustAndOptimalControl CCS.setupEnv() contSys = CCS.blockModel.csys(;g = 0, \alpha = 0 , \mu = 1, \tau =20) plot!(bodeplot(contSys[1,1]),pzmap(contSys))
```

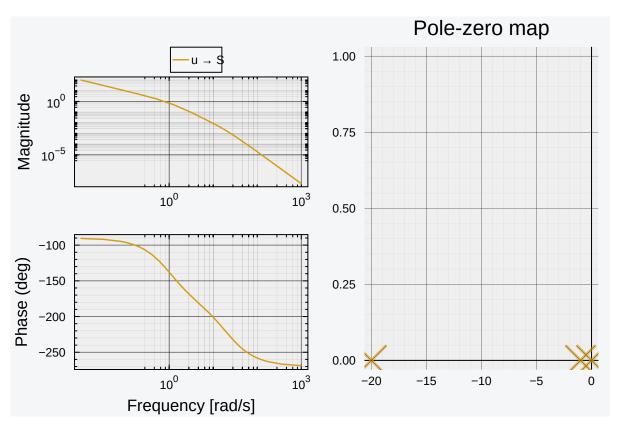


Figure 4.1: Starting Bode Plot and PZ Map

It has the shape we expect from a motor + friction. Slow pole for the mass + friction and a faster pole for the current & inductance.

Numerically they are:

display(eigvals(contSys.A))

```
3-element Vector{Float64}:
    -20.0
    -1.0
    0.0
```

We see that we start with all the poles in the left-half plane, which is good.

4.2 Pole Placement

We can design a controller with pole placement.

For some reason pole placement doesn't work for the observer, I use a Kalman Filter with random fast values.

```
observability(contSys.A,contSys.C).isobservable || error("System is not observable")
controllability(contSys.A,contSys.B).iscontrollable || error("System is not controllable")

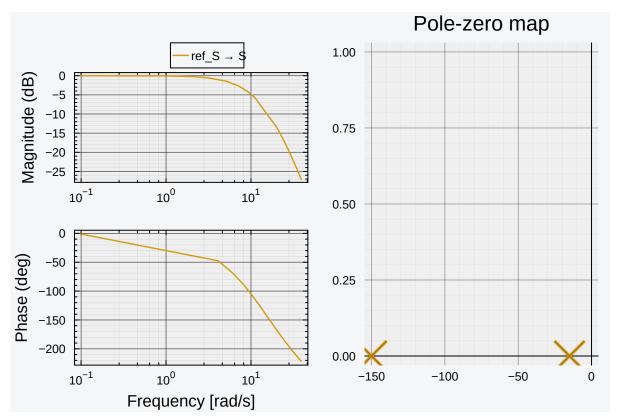
ε = 0.01;
pp = 15.0;
poles_cont = - [pp + ε, pp - ε, pp];
L = real(place(contSys, poles_cont, :c));

poles_obs = poles_cont * 10.0;
K = place(contSys, poles_obs, :o)
obs_controller = observer_controller(contSys, L, K; direct=false);
fsf_controller = named_ss(obs_controller, u = [:ref_S, :ref_V], y = [:u]);
```

We can check the effect of the new controller on the loop

```
closedLoop = feedback( contSys * fsf_controller);
print(poles(closedLoop));
setPlotScale("dB")
plot!(bodeplot(closedLoop[1,1], 0.1:40), pzmap(closedLoop))
```

ComplexF64[-14.990000366343788 + 0.0im, -14.999999266673722 + 0.0im, -15.010000366982666 + 0.0im, -149.999999999986 + 0.0im, -150.10000000002432 + 0.0im, -149.8999999999607 + 0.0im]



We can compare this to the open-loop response in @start-bode. We can see that we achieve unitary gain throughout the whole low-frequency range.

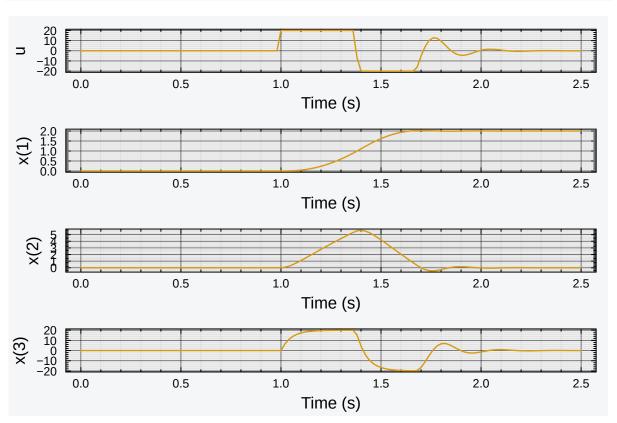
We can convert the pole placement controller into the standard PD gain form.

```
using DiscretePIDs
Ts = 0.02 # sampling time
Tf = 2.5; #final simulation time

K = L[1];
Ti = 0;
Td = L[2] / L[1];
pid = DiscretePID(; K, Ts, Ti, Td);
```

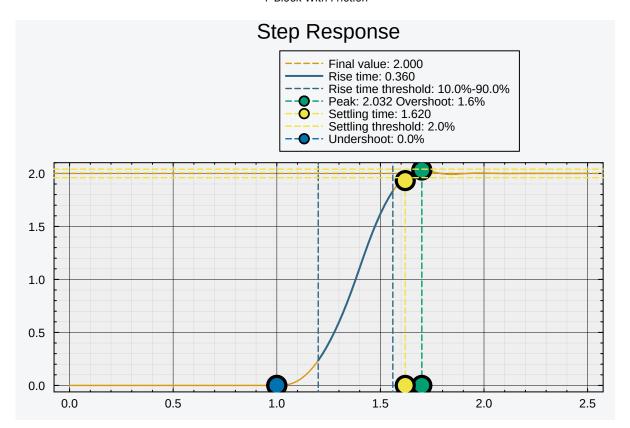
4.3 Simulation

We can simulate this with a motor that only outputs the position:



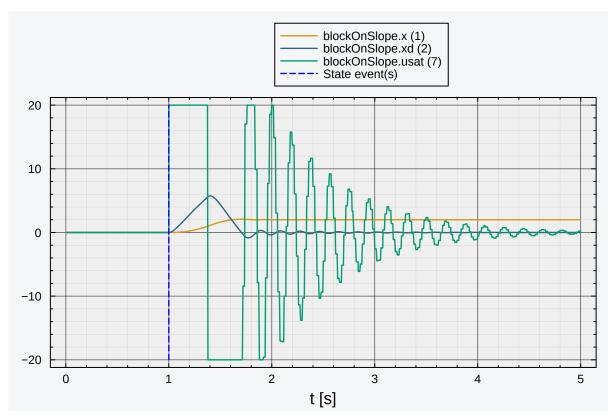
For more stats:

```
si = stepinfo(res);
plot(si);title!("Step Response")
```



We can also simulate it in a SIMULINK-like environment:

4 Block With Friction



There is a slight difference between the lsim simulation and the FMU simulation. I need to recheck some stuff.

5 Block on a slope

Position Control with friction. Using Pole Placement + PD.

5.1 Response Analysis

```
using CCS using ControlSystems, Plots, LinearAlgebra, RobustAndOptimalControl CCS.setupEnv() contSys = CCS.blockModel.csys(;g = 0, \alpha = 0 , \mu = 1, \tau =20) plot!(bodeplot(contSys[1,1]),pzmap(contSys))
```

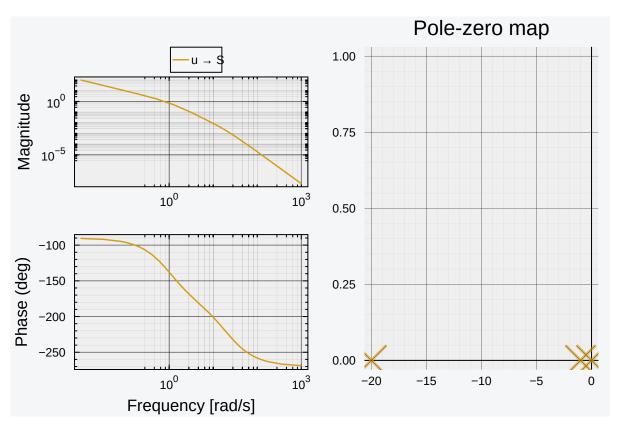


Figure 5.1: Starting Bode Plot and PZ Map

It has the shape we expect from a motor + friction. Slow pole for the mass + friction and a faster pole for the current & inductance.

Numerically they are:

display(eigvals(contSys.A))

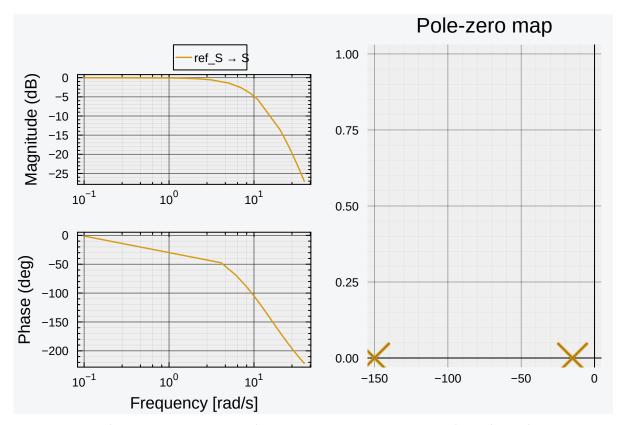
```
3-element Vector{Float64}:
    -20.0
    -1.0
    0.0
```

We see that we start with all the poles in the left-half plane, which is good.

5.2 Pole Placement

```
We can design a controller with pole placement.
For some reason pole placement doesn't work for the observer, I use a Kalman Filter with random fast values.
observability(contSys.A,contSys.C).isobservable || error("System is not observable")
controllability(contSys.A,contSys.B).iscontrollable || error("System is not controllable")
\epsilon = 0.01;
pp = 15.0;
poles_cont = - [pp + \epsilon, pp - \epsilon, pp];
L = real(place(contSys, poles_cont, :c));
poles_obs = poles_cont * 10.0;
K = place(contSys, poles_obs, :o)
obs_controller = observer_controller(contSys, L, K; direct=false);
fsf_controller = named_ss(obs_controller, u = [:ref_S, :ref_V], y = [:u])
NamedStateSpace{Continuous, Float64}
A =
  -150.0
                                   8.033684828490095e-12
                                                              0.0
     1.0915557686859107e-5
                                -279.999999999851
                                                              1.0
 -3374.9970813429577
                              -17530.98989999806
                                                             -44.0
B =
 150.0
                                0.999999999919663
  -1.0915557686859107e-5
                              278.999999999851
  -0.0014186570429435138 16899.989999998063
C =
 168.74992500000002 31.549995000000003 1.2000000000000002
D =
 0.0 0.0
Continuous-time state-space model
With state names: x1 x2 x3 input names: ref_S ref_V
     output names: u
We can check the effect of the new controller on the loop
closedLoop = feedback( contSys * fsf_controller);
print(poles(closedLoop));
setPlotScale("dB")
plot!(bodeplot(closedLoop[1,1], 0.1:40), pzmap(closedLoop))
ComplexF64[-14.990000366343788 + 0.0im, -14.999999266673722 + 0.0im, -15.010000366982666 +
```

0.0im, -149.999999999986 + 0.0im, -150.10000000002432 + 0.0im, -149.899999999607 + 0.0im]



We can compare this to the open-loop response in @start-bode. We can see that we achieve unitary gain throughout the whole low-frequency range.

We can convert the pole placement controller into the standard PD gain form.

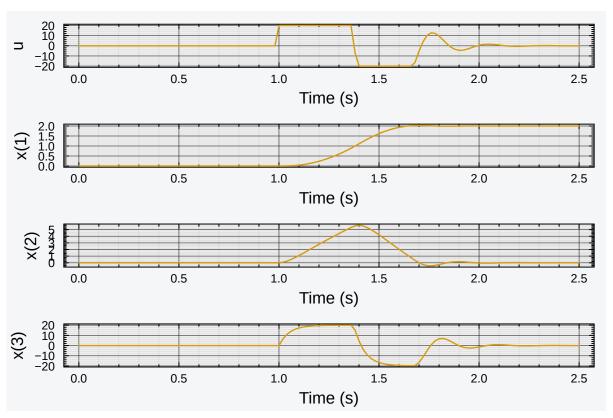
```
using DiscretePIDs
Ts = 0.02 # sampling time
Tf = 2.5; #final simulation time

K = L[1];
Ti = 0;
Td = L[2] / L[1];
pid = DiscretePID(; K, Ts, Ti, Td);
```

5.3 Simulation

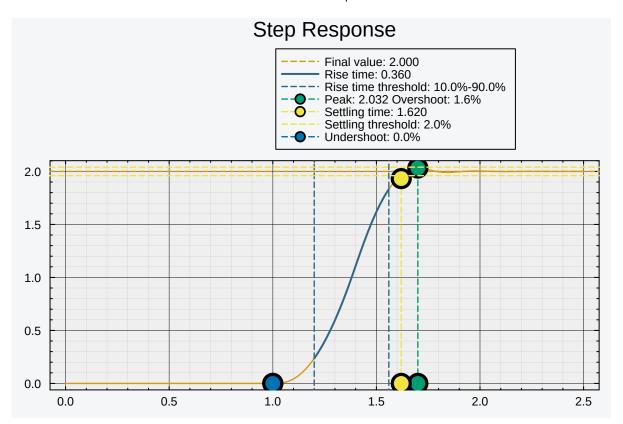
We can simulate this with a motor that only outputs the position:

```
display(plot(res,
    plotu=true,
    plotx=true,
    ploty=false
    ))
ylabel!("u", sp=1);
ylabel!("x", sp=2);
ylabel!("v", sp=3);
ylabel!("T", sp=4);
```

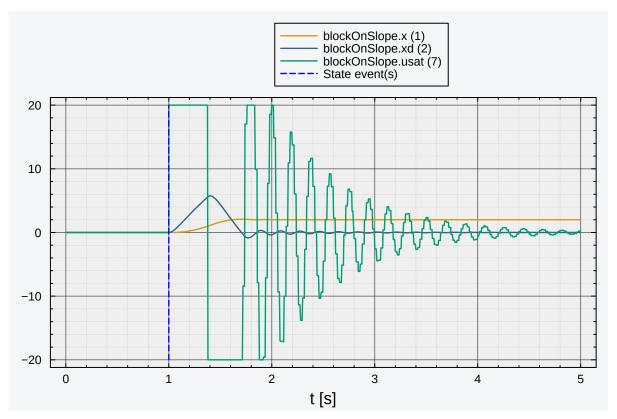


For more stats:

```
si = stepinfo(res);
plot(si);title!("Step Response")
```



We can also simulate it in a SIMULINK-like environment:



There is a slight difference between the lsim simulation and the FMU simulation. I need to recheck some stuff.

A Performance tricks

A.1 Hurwitz Check

Create our nice model. Assume to have run the poles function and that you have a vector of eigenvalues. For simplicity I will create an arbitrary vector with the first 100 values in -1 and the last 100 values as random around 0.

A.1.1 for loop

With a naive approach we check if all the elements are in the LHP: make a function that iterates and returns false if it hits a pole with positive real part.

```
function isHurwitz(v)
    for i in eachindex(v)
        if real(v[i])>0.0
            return false
        end
    end
    return true
end

@benchmark isHurwitz($(Ref(vbig))[])
```

```
BenchmarkTools.Trial: 10000 samples with 987 evaluations per sample. Range (min ... max): 49.949 ns ... 969.301 ns GC (min ... max): 0.00% ... 0.00% Time (median): 54.306 ns GC (median): 0.00% GC (mean \pm \sigma): 57.041 ns \pm 22.237 ns GC (mean \pm \sigma): 0.00% \pm 0.00%
```

Memory estimate: 0 bytes, allocs estimate: 0.

We have our baseline. We can probably squeeze out some more performance but I'm still a Julia noob.

A.1.2 all()

Let's try using some of the built-in declarative functions:

```
@benchmark all(real($vbig).<=0.0)</pre>
BenchmarkTools.Trial: 10000 samples with 746 evaluations per sample.
Range (min ... max): 183.378 ns ... 22.068 μs GC (min ... max): 0.00% ... 97.78%
Time (median): 261.662 ns GC (median): 0.00%
Time (mean ± σ): 445.850 ns ± 864.436 ns GC (mean ± σ): 32.85% ± 16.78%
```



Memory estimate: 1.75 KiB, allocs estimate: 5.

Simple all(), when given a tuple it checks if all the values are True, otherwise it stops when it encounters the first False.

We can see that it's a tad slower. This is because it's creating a new vector with just the real parts, then it's creating a new vector with only the boolean results and then it's checking if there are any False results.

This results in a lot of allocations and wasted resources.

```
@benchmark all(<=(0.0),real($vbig))</pre>
```

```
BenchmarkTools.Trial: 10000 samples with 759 evaluations per sample. Range (min … max): 144.664 ns … 31.398 \mus | GC (min … max): 0.00% … 97.98% Time (median): 226.746 ns | GC (median): 0.00% Time (mean \pm \sigma): 344.335 ns \pm 699.060 ns | GC (mean \pm \sigma): 22.41% \pm 15.26%
```

```
145 ns Histogram: log(frequency) by time 2.44 µs <
```

Memory estimate: 1.62 KiB, allocs estimate: 2.

A smarter way is to skip on of the allocations by creating the vector of real parts and then checking row by row if the non-positivity check fails.

```
@benchmark all(i -> real(i)<=0.0,$vbig)</pre>
```

```
BenchmarkTools.Trial: 10000 samples with 987 evaluations per sample. Range (min ... max): 49.139 ns ... 2.022 \mus | GC (min ... max): 0.00% ... 0.00% Time (median): 51.773 ns | GC (median): 0.00% Time (mean \pm \sigma): 53.295 ns \pm 22.061 ns | GC (mean \pm \sigma): 0.00% \pm 0.00%
```

```
49.1 ns Histogram: log(frequency) by time 116 ns <
```

Memory estimate: 0 bytes, allocs estimate: 0.

We can do better: Instead of converting into real the full vector it checks element by element if it's in the LHP. It returns false at the first failure. We finally have a comparable result to the benchmark function but in a more compact way. Is it cleaner? That's subjective.

A.1.3 mapreduce()

Finally we try the MapReduce approach. This allows a better utilization of your processor without the necessity of learning parallel programming.

```
@benchmark mapreduce(i->real(i)<=0.0, &, $vbig)</pre>
```

```
BenchmarkTools.Trial: 10000 samples with 993 evaluations per sample. Range (min … max): 42.095 ns … 692.346 ns GC (min … max): 0.00% … 0.00% Time (median): 43.807 ns GC (median): 0.00% GC (median): 0.00% \pm 0.00% GC (mean \pm \sigma): 0.00% \pm 0.00%
```



Memory estimate: 0 bytes, allocs estimate: 0.

We squeeze the last bit of performance and beat the initial benchmark, not by much but still appreciable.