Control Challenges: Solutions

Iacopo Moles

Table of contents

1 Introduction

1.1 Intro

This is a collection of write ups on how to solve the various problems presented by Github user "Janismac".

1.2 What do I need?

1.2.1 Software

- A real OS like Linux or Windows. [1]
- The Julia Programming Language
  - Clone the repo
  - Activate the package by running in your terminal:

    ```
    julia --project -e 'using Pkg; Pkg.instantiate()'
    ```
- (Nice to have) OpenModelica Editor

1.2.2 Theory

- Basic Julia knowledge
- Basic JS knowledge
- Control Theory knowledge
  - Frequency Based Control
  - State Space Based control
- Misc knowledge:
  - Linear Algebra

[1] MacOs should be supported in theory but it's not tested.

- Differential Equations

Part I

The Damped Mass problem

Modeling

To better understand the problem let's take a peek at how the simulated model works.

Listing 1.1 `BlockOnSlope.js`

```
Models.BlockOnSlope.prototype.vars =
{                                                                    ①
    g: 9.81,
    x: 0,           // distance from objective s
    dx: 0,          // velocity v
    slope: 1,       // slope coefficient alpha = dy/dx in the
     ↪  cartesian plane
    F: 0,           // Requested u
    F_cmd: 0,       // Saturated u
    friction: 0,    // Coulomb friction coefficient mu
    T: 0,           // Simulation Time
};

Models.BlockOnSlope.prototype.simulate = function (dt,
 ↪  controlFunc)
{
    this.F_cmd = controlFunc({x:this.x,dx:this.dx,T:this.T});
    if(typeof this.F_cmd != 'number' || isNaN(this.F_cmd)) throw
     ↪  "Error: The controlFunction must return a number.";
    this.F_cmd = Math.max(-20,Math.min(20,this.F_cmd));              ②
    integrationStep(this, ['x', 'dx', 'F'], dt);
}

Models.BlockOnSlope.prototype.ode = function (x)
{
    return [
        x[1],                                                        ③
        (x[2]) - (Math.sin(this.slope) * this.g) - (this.friction
 ↪  * x[1]),
        20.0 * (this.F_cmd - x[2])
    ];
}
```

① The model has obviously some default values for the parameters that can be modified for the different scenarios.

② The control command u is generated by the `controlFunction(block)` function provided by us. There are some checks to see if it's a number. If it's acceptable then it passes through a saturation between ± 20.

③ The model is a simple ODE with equations:

$$\begin{cases} \dot{s} = v \\ \dot{v} = F - sin(\alpha) \cdot g - \mu \cdot v \\ \dot{F} = -20 \cdot F + 20 \cdot u_{sat} \end{cases}$$

Converting it in state-space representation:

$$\begin{bmatrix} \dot{s} \\ \dot{v} \\ \dot{F} \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & -\mu & 1 \\ 0 & 0 & -20 \end{bmatrix} \begin{bmatrix} s \\ v \\ F \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ u_{sat} \end{bmatrix} + \begin{bmatrix} 0 \\ -sin(\alpha) \cdot g \\ 0 \end{bmatrix}$$

$$\begin{bmatrix} s \\ v \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} s \\ v \\ F \end{bmatrix}$$

Obviously the gravitational term acts as a disturbance.

2 Block without Friction

Position Control with friction. Using Pole Placement + PD.

2.1 State Space representation

We can convert the set of ODE into a state space representation. The final bode plot of the block position is:

```
using DiscretePIDs, ControlSystems, Plots, LinearAlgebra

# System parameters
Ts = 0.02 # sampling time
Tf = 2.5; #final simulation time
g = 9.81 #gravity
α = 0.0 # slope
μ = 1.0 # friction coefficient
x_0 = -2.0 # starting position
dx_0 = 0.0 # starting velocity
τ = 20.0 # torque constant

# State Space Matrix
A = [0 1 0
    0 -μ 1
    0 0 -τ];
B = [0
    0
    τ];
C = [1 0 0
    0 1 0];

sys = ss(A, B, C, 0.0)      # Continuous

plot!(bodeplot(tf(sys)),pzmap(tf(sys)))
```

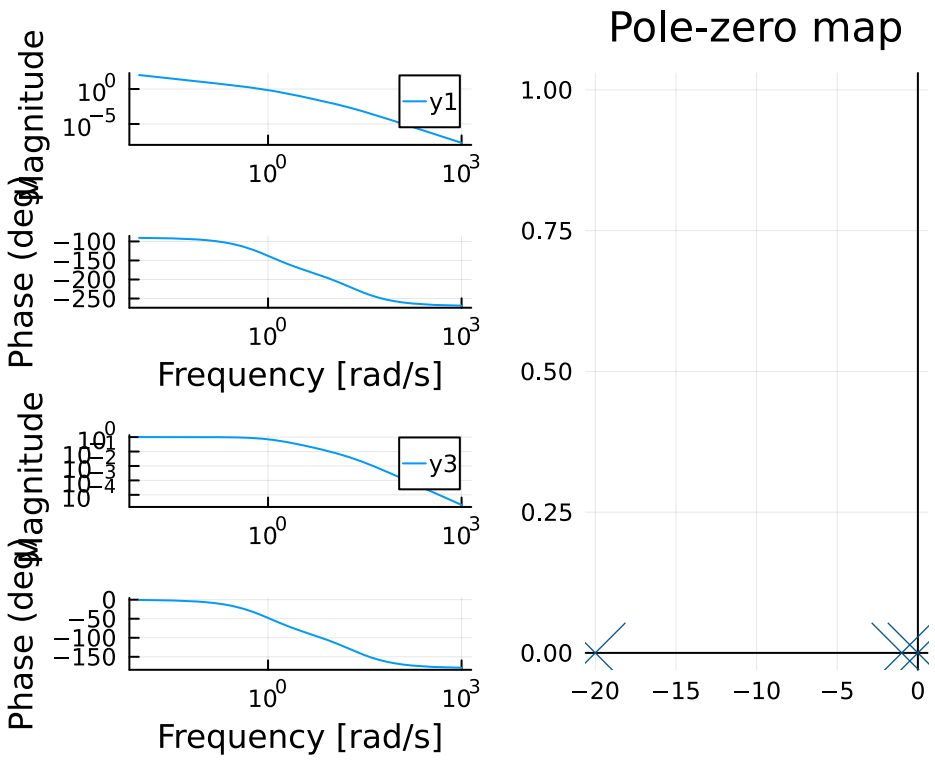


Figure 2.1: Starting Bode Plot and PZ Map

It has the shape we expect from a motor + friction. Slow pole for the mass + friction and a faster pole for the current & inductance.

Numerically they are:

```
display(eigvals(A))
```

```
3-element Vector{Float64}:
 -20.0
  -1.0
   0.0
```

We see that we start with all the pole in the left-half plane, which is good.

2.2 Pole Placement

We can design a controller with pole placement.

For some reason pole placement doesn't work for the observer, I use a Kalman Filter with random fast values.

```
observability(A, C).isobservable &
controllability(A, B).iscontrollable; #OK

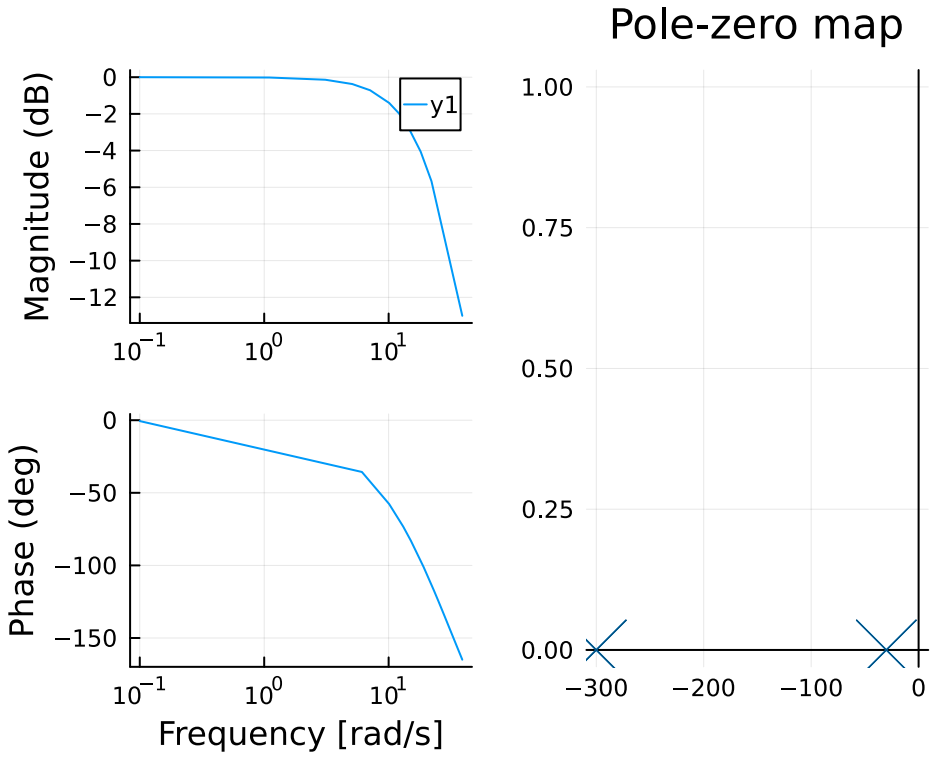
ε = 0.01;
pp = 15.0;
poles_cont = -2.0 * [pp + ε, pp - ε, pp];
L = real(place(sys, poles_cont, :c));

poles_obs = poles_cont * 10.0;
K = place(1.0 * A', 1.0 * C', poles_obs)'
cont = observer_controller(sys, L, K; direct=false);
```

We can check the effect of the new controller on the loop

```
closedLoop = feedback(sys * cont)
print(poles(closedLoop));
setPlotScale("dB")
plot!(bodeplot(closedLoop[1, 1], 0.1:40), pzmap(closedLoop))
```

```
ComplexF64[-29.979998924597755 + 0.0im, -30.000002152199972 +
0.0im, -30.019998923202337 + 0.0im, -300.0000000000004 + 0.0im,
-300.1999999999752 + 0.0im, -299.80000000004117 + 0.0im]
```



We can compare this to the open-loop response in @start-bode. We can see that we achieve unitary gain throughout the whole low-frequency range.

We can convert the pole placement controller into the standard PD gain form.

```
K = L[1];
Ti = 0;
Td = L[2] / L[1];
pid = DiscretePID(; K, Ts, Ti, Td);
```

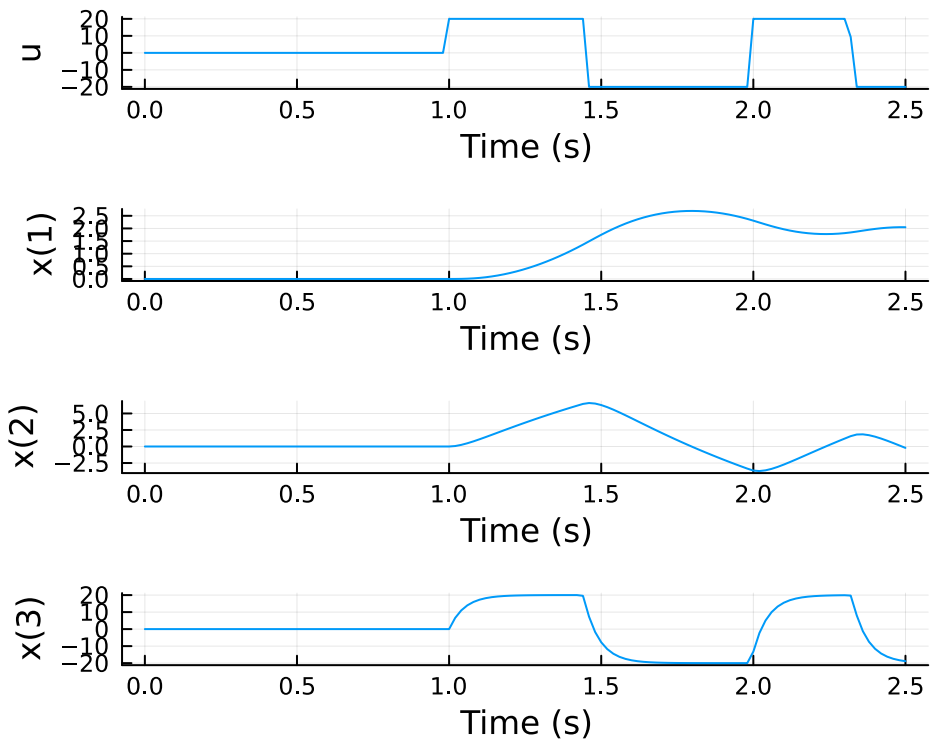
2.3 Simulation

We can simulate this with a motor that only outputs the position:

```
sysreal = ss(A, B, [1 0 0], 0.0)
ctrl = function (x, t)
    y = (sysreal.C*x)[] # measurement
    d = 0 * [1.0]         # disturbance
    r = 2.0 * (t >= 1) # reference
    # u = pid(r, y) # control signal
    # u + d # Plant input is control signal + disturbance
    # u =1
    e = x - [r; 0.0; 0.0]
    e[3] = 0.0 # torque not observable, just ignore it in the
     ↪  final feedback
    u = -L * e + d
    u = [maximum([-20.0 minimum([20.0 u])])]
end
t = 0:Ts:Tf

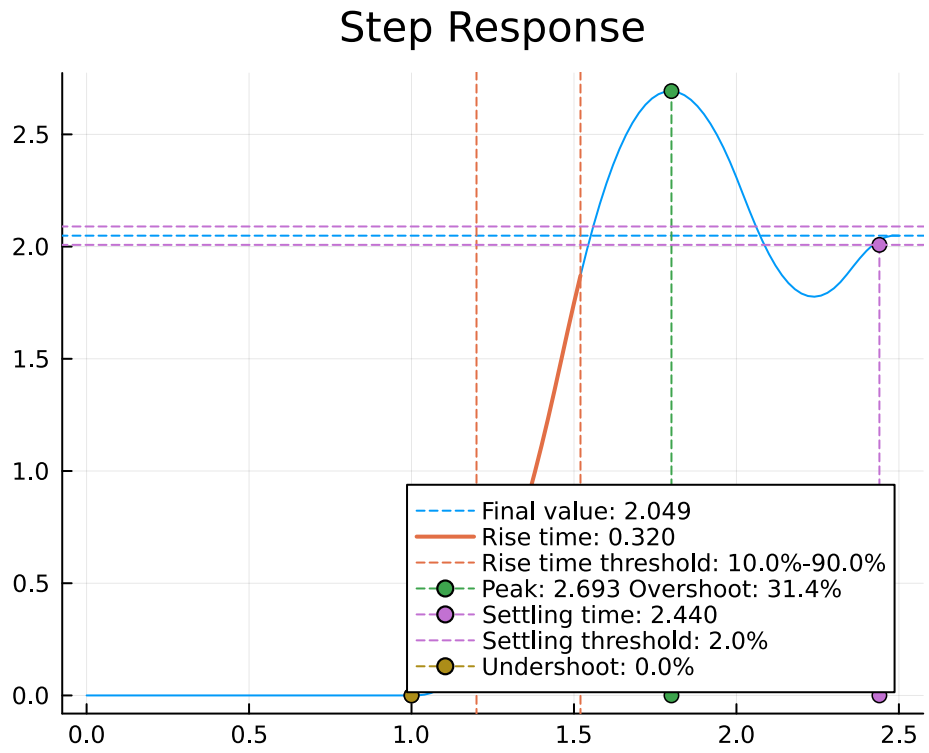
res = lsim(sysreal, ctrl, t)

display(plot(res,
    plotu=true,
    plotx=true,
    ploty=false
    ))
ylabel!("u", sp=1);
ylabel!("x", sp=2);
ylabel!("v", sp=3);
ylabel!("T", sp=4);
```



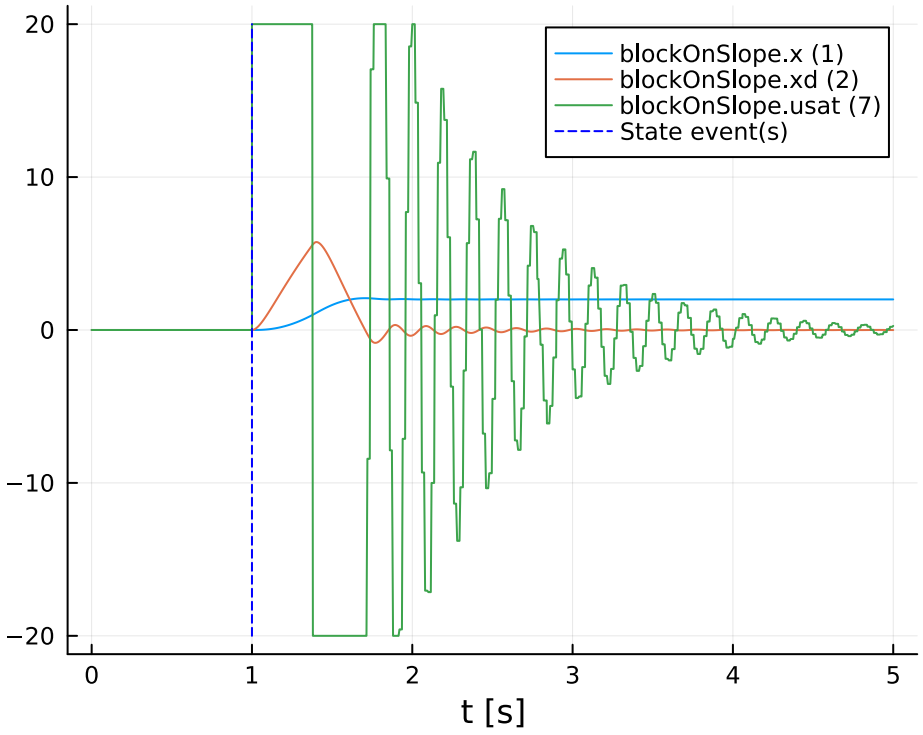
For more stats:

```
si = stepinfo(res);
plot(si);title!("Step Response")
```



We can also simulate it in a SIMULINK-like environment:

```
using FMI, DifferentialEquations
fmuPath = abspath(joinpath(@__DIR__,
  "..","..",
  "modelica",
  "ControlChallenges",
  "ControlChallenges.BlockOnSlope_Challenges.Examples.WithFrictio
   ↪  n.fmu"))
fmu = loadFMU(fmuPath);
simData = simulateME(
    fmu,
    (0.0, 5.0);
    recordValues=["blockOnSlope.x",
    "blockOnSlope.xd",
    "blockOnSlope.usat"],
    showProgress=false);
unloadFMU(fmu);
plot(simData, states=false, timeEvents=false)
```



There is a slight difference between the `lsim` simulation and the FMU simulation. I need to recheck some stuff.

3 Block With Friction

Position Control with friction. Using Pole Placement + PD.

3.1 Response Analysis

```
using CCS
using ControlSystems, Plots, LinearAlgebra,
 ↪  RobustAndOptimalControl
CCS.setupEnv()

contSys = CCS.blockModel.csys(;g = 0, α = 0 , μ = 1, τ =20)
plot!(bodeplot(contSys[1,1]),pzmap(contSys))
```

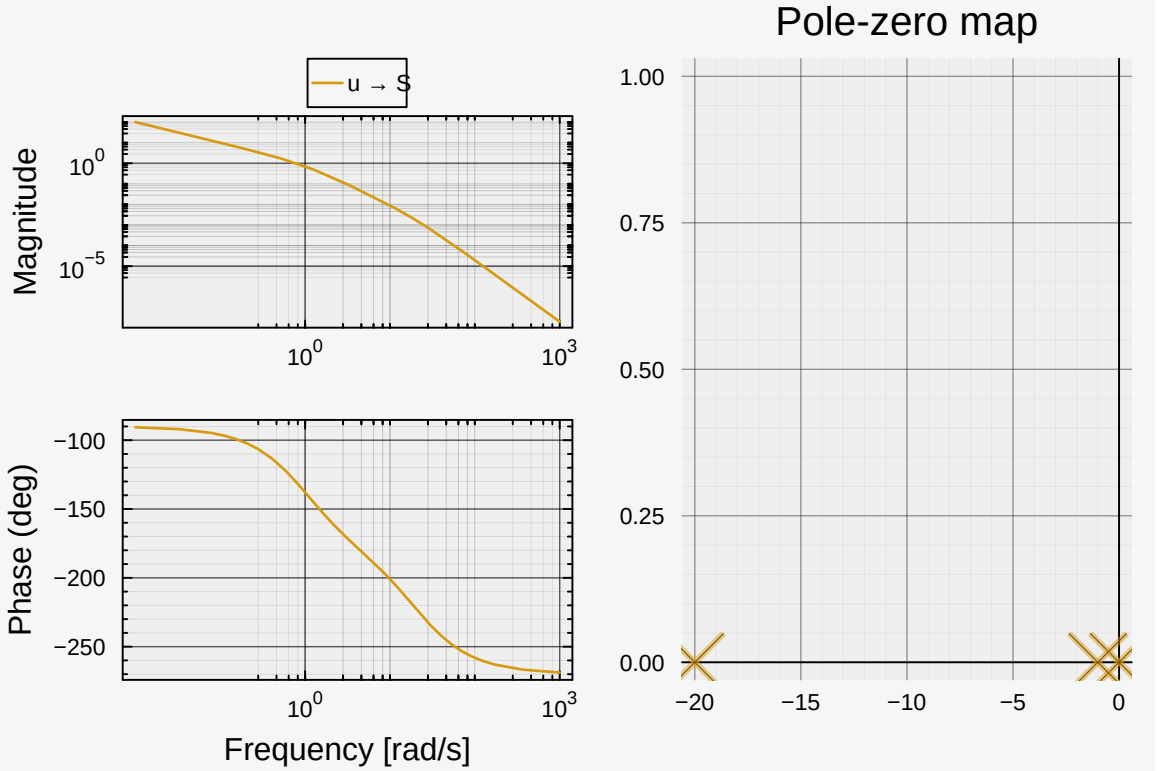


Figure 3.1: Starting Bode Plot and PZ Map

It has the shape we expect from a motor + friction. Slow pole for the mass + friction and a faster pole for the current & inductance.

Numerically they are:

```
display(eigvals(contSys.A))
```

```
3-element Vector{Float64}:
 -20.0
  -1.0
   0.0
```

We see that we start with all the poles in the left-half plane, which is good.

3.2 Pole Placement

We can design a controller with pole placement.

For some reason pole placement doesn't work for the observer, I use a Kalman Filter with random fast values.

```
observability(contSys.A,contSys.C).isobservable || error("System
 ↪  is not observable")
controllability(contSys.A,contSys.B).iscontrollable ||
 ↪  error("System is not controllable")

ε = 0.01;
pp = 15.0;
poles_cont = - [pp + ε, pp - ε, pp];
L = real(place(contSys, poles_cont, :c));


poles_obs = poles_cont * 10.0;
K = place(contSys, poles_obs, :o)
obs_controller = observer_controller(contSys, L, K; direct=false);
fsf_controller = named_ss(obs_controller, u = [:ref_S, :ref_V], y
 ↪  = [:u]);
```

We can check the effect of the new controller on the loop

```
closedLoop = feedback( contSys * fsf_controller);
print(poles(closedLoop));
setPlotScale("dB")
plot!(bodeplot(closedLoop[1,1], 0.1:40), pzmap(closedLoop))
```

```
ComplexF64[-14.990000366343788 + 0.0im, -14.999999266673722 +
0.0im, -15.010000366982666 + 0.0im, -149.99999999999986 + 0.0im,
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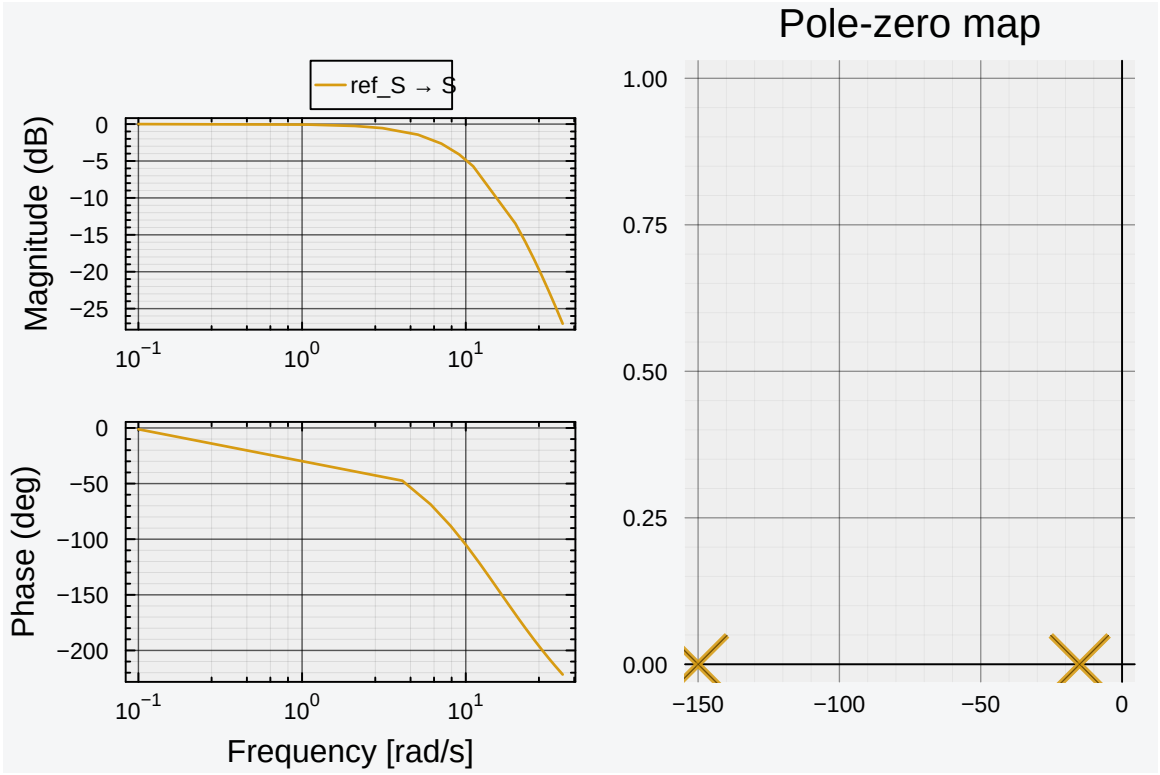
```



We can compare this to the open-loop response in @start-bode. We can see that we achieve unitary gain throughout the whole low-frequency range.

We can convert the pole placement controller into the standard PD gain form.

```
using DiscretePIDs
Ts = 0.02 # sampling time
Tf = 2.5; #final simulation time

K = L[1];
Ti = 0;
Td = L[2] / L[1];

pid = DiscretePID(; K, Ts, Ti, Td);
```

3.3 Simulation

We can simulate this with a motor that only outputs the position:

```
sysreal = ss(contSys.A, contSys.B, [1 0 0], 0.0)
ctrl = function (x, t)
```

```
    y = (sysreal.C*x)[] # measurement
    d = 0 * [1.0]        # disturbance
    r = 2.0 * (t >= 1) # reference
    # u = pid(r, y) # control signal
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    e = x - [r; 0.0; 0.0]
    e[3] = 0.0 # torque not observable, just ignore it in the
     ↪ final feedback
    u = -L * e + d
    u = [maximum([-20.0 minimum([20.0 u])])]
end
t = 0:Ts:Tf

res = lsim(sysreal, ctrl, t)

display(plot(res,
    plotu=true,
    plotx=true,
    ploty=false
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ylabel!("u", sp=1);
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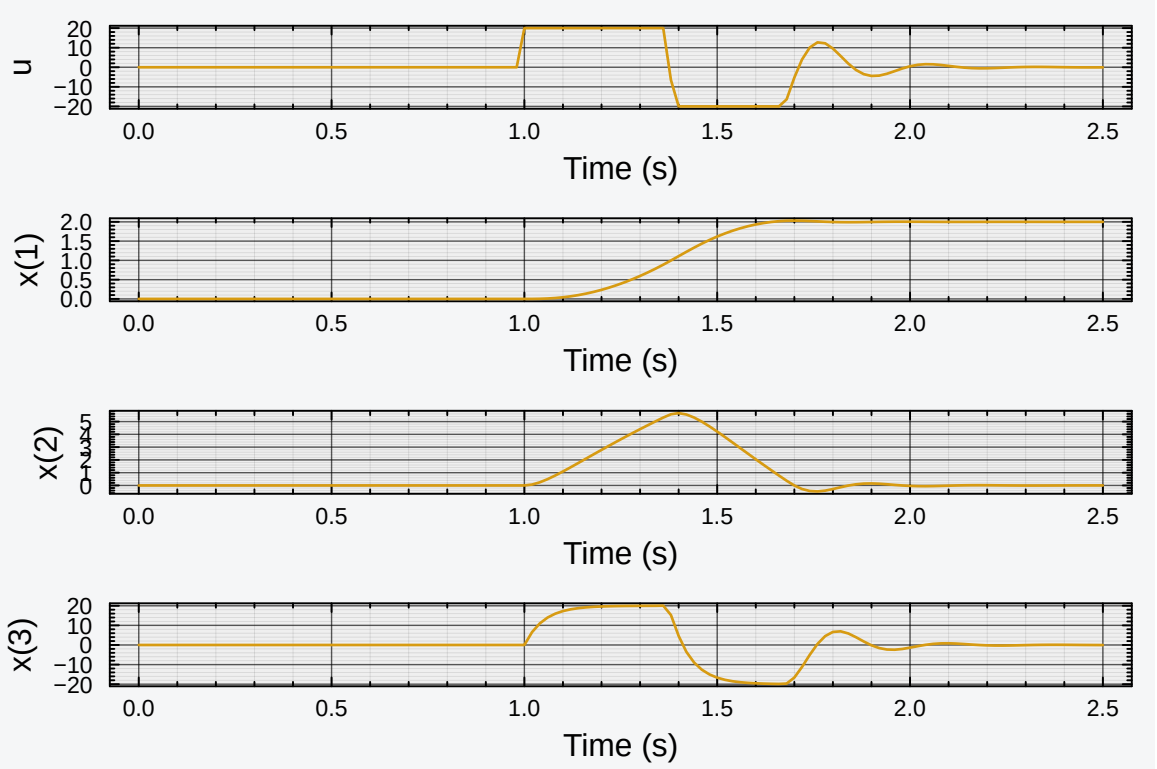

For more stats:

```
si = stepinfo(res);
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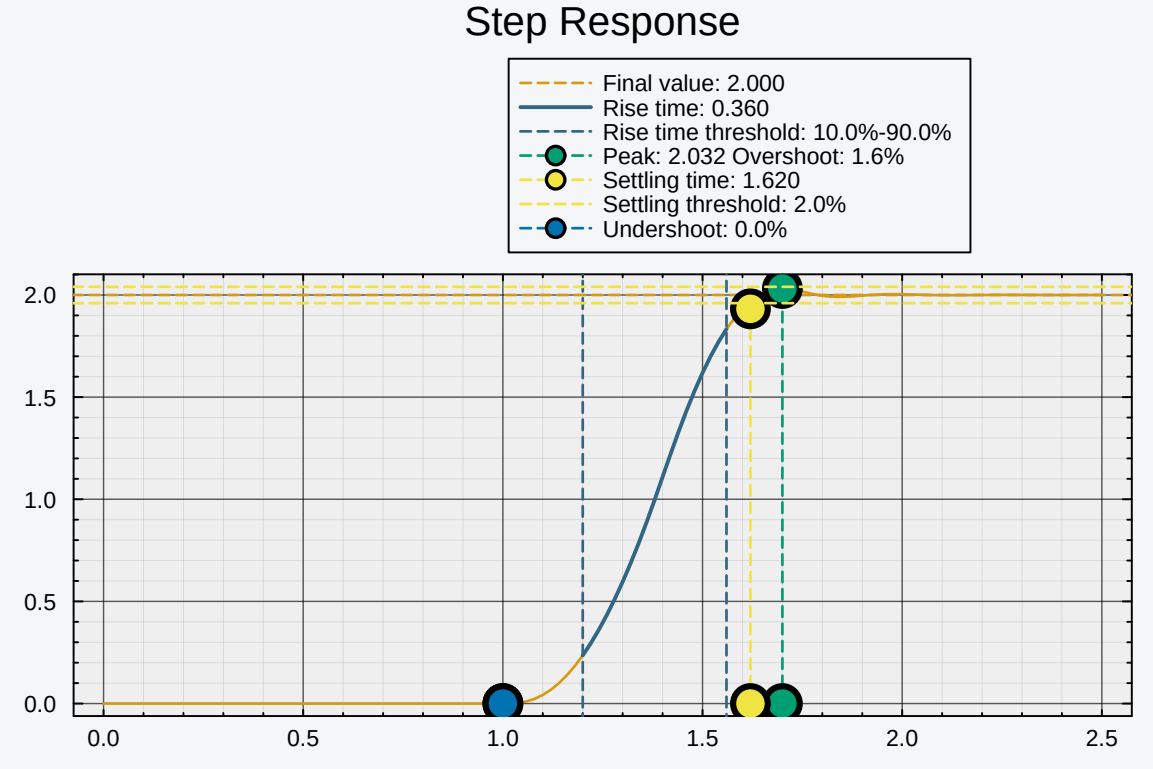

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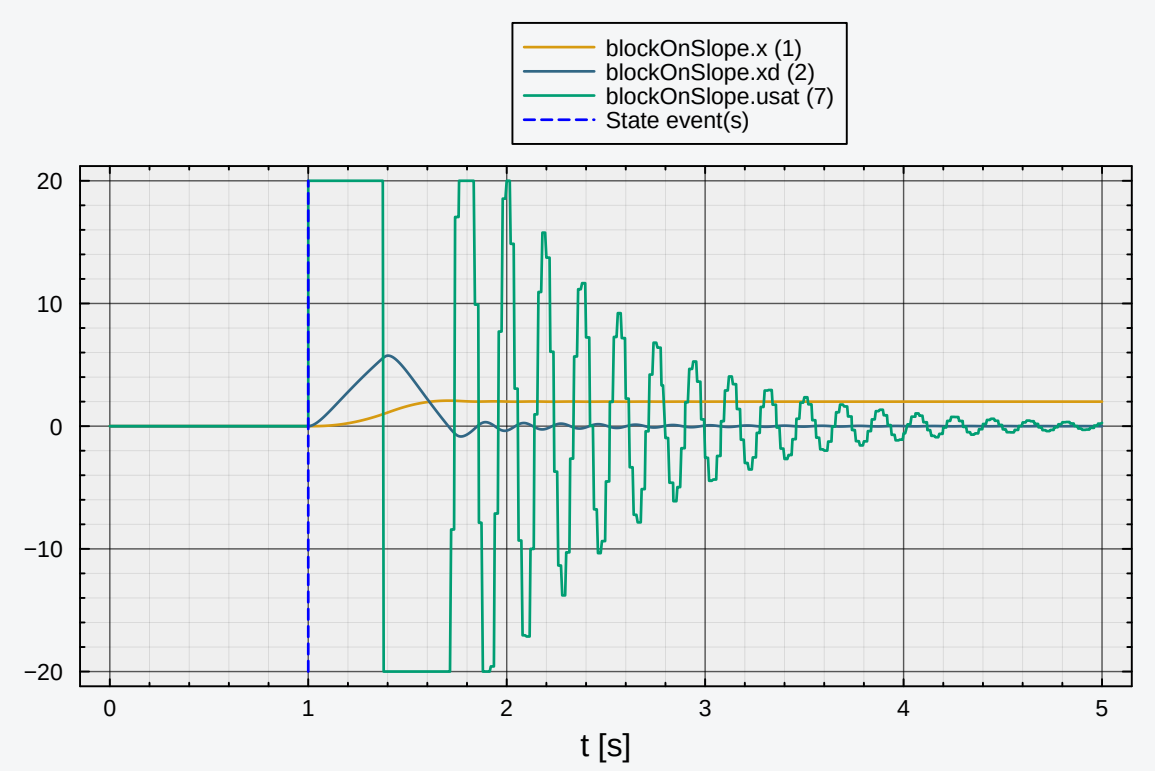
    showProgress=false);
unloadFMU(fmu);
plot(simData, states=false, timeEvents=false)
```



There is a slight difference between the `lsim` simulation and the FMU simulation. I need to recheck some stuff.

4 Block on a slope

Position Control with friction. Using Pole Placement + PD.

4.1 Response Analysis

```
using CCS
using ControlSystems, Plots, LinearAlgebra,
 ↪  RobustAndOptimalControl
CCS.setupEnv()

contSys = CCS.blockModel.csys(;g = 0, α = 0 , μ = 1, τ =20)
plot!(bodeplot(contSys[1,1]),pzmap(contSys))
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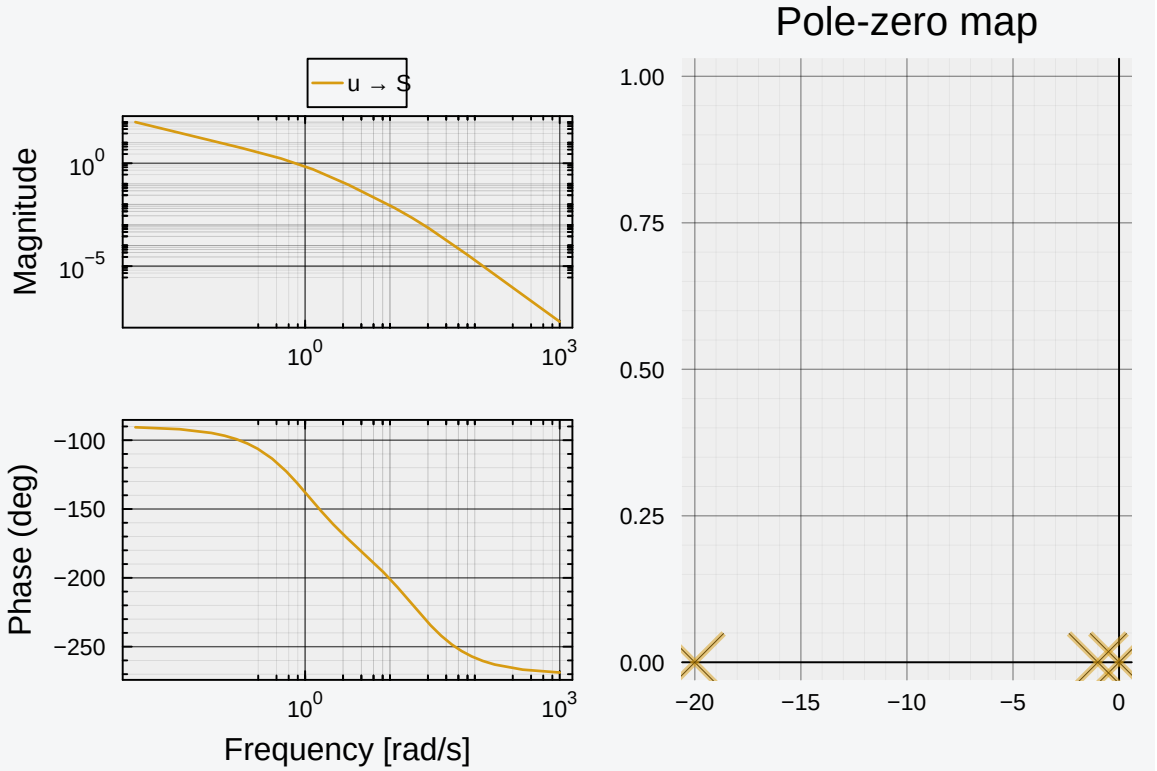

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It has the shape we expect from a motor + friction. Slow pole for the mass + friction and a faster pole for the current & inductance.

Numerically they are:

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display(eigvals(contSys.A))
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```
3-element Vector{Float64}:
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We see that we start with all the poles in the left-half plane, which is good.

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We can design a controller with pole placement.

For some reason pole placement doesn't work for the observer, I use a Kalman Filter with random fast values.

```
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controllability(contSys.A,contSys.B).iscontrollable ||
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ε = 0.01;
pp = 15.0;
poles_cont = - [pp + ε, pp - ε, pp];
L = real(place(contSys, poles_cont, :c));


poles_obs = poles_cont * 10.0;
K = place(contSys, poles_obs, :o)
obs_controller = observer_controller(contSys, L, K; direct=false);
fsf_controller = named_ss(obs_controller, u = [:ref_S, :ref_V], y
 ↪  = [:u])
```

```
NamedStateSpace{Continuous, Float64}
A =
  -150.0                        8.033684828490095e-12    0.0
     1.0915557686859107e-5    -279.9999999999851          1.0
 -3374.9970813429577        -17530.98989999806          -44.0
B =
 150.0                         0.9999999999919663
  -1.0915557686859107e-5     278.9999999999851
  -0.0014186570429435138   16899.989999998063
C =
 168.74992500000002  31.549995000000003  1.2000000000000002
D =
 0.0  0.0

Continuous-time state-space model
With state  names: x1 x2 x3
     input  names: ref_S ref_V
     output names: u
```

We can check the effect of the new controller on the loop

```
closedLoop = feedback( contSys * fsf_controller);
print(poles(closedLoop));
setPlotScale("dB")
plot!(bodeplot(closedLoop[1,1], 0.1:40), pzmap(closedLoop))
```

```
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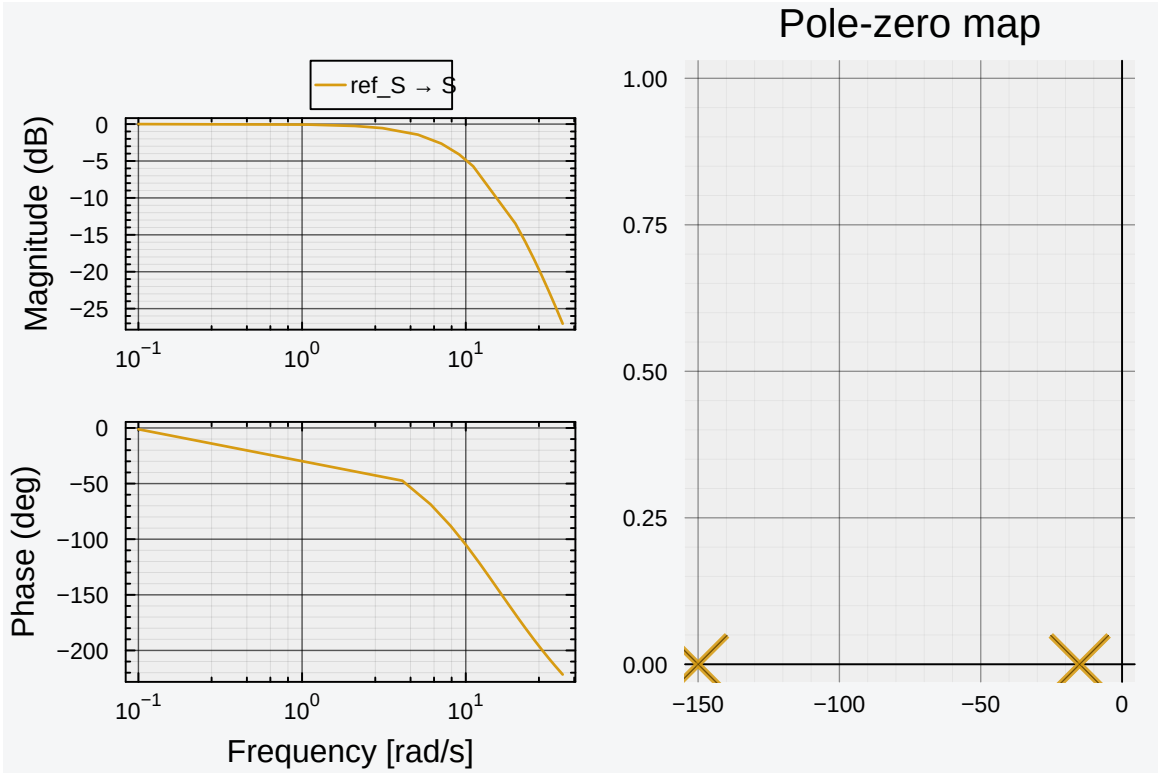

We can compare this to the open-loop response in @start-bode. We can see that we achieve unitary gain throughout the whole low-frequency range.

We can convert the pole placement controller into the standard PD gain form.

```
using DiscretePIDs
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K = L[1];
Ti = 0;
Td = L[2] / L[1];

pid = DiscretePID(; K, Ts, Ti, Td);
```

4.3 Simulation

We can simulate this with a motor that only outputs the position:

```
sysreal = ss(contSys.A, contSys.B, [1 0 0], 0.0)
ctrl = function (x, t)
```

```
    y = (sysreal.C*x)[] # measurement
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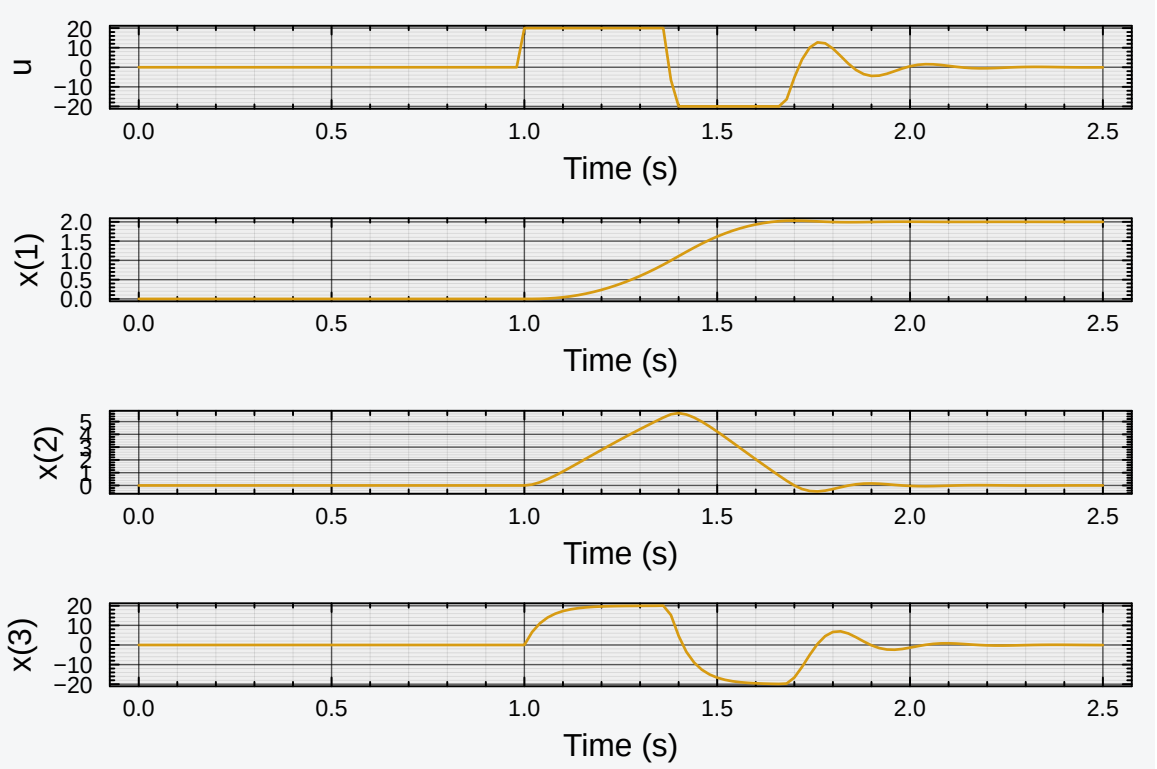
    e = x - [r; 0.0; 0.0]
    e[3] = 0.0 # torque not observable, just ignore it in the
     ↪  final feedback
    u = -L * e + d
    u = [maximum([-20.0 minimum([20.0 u])])]
end
t = 0:Ts:Tf

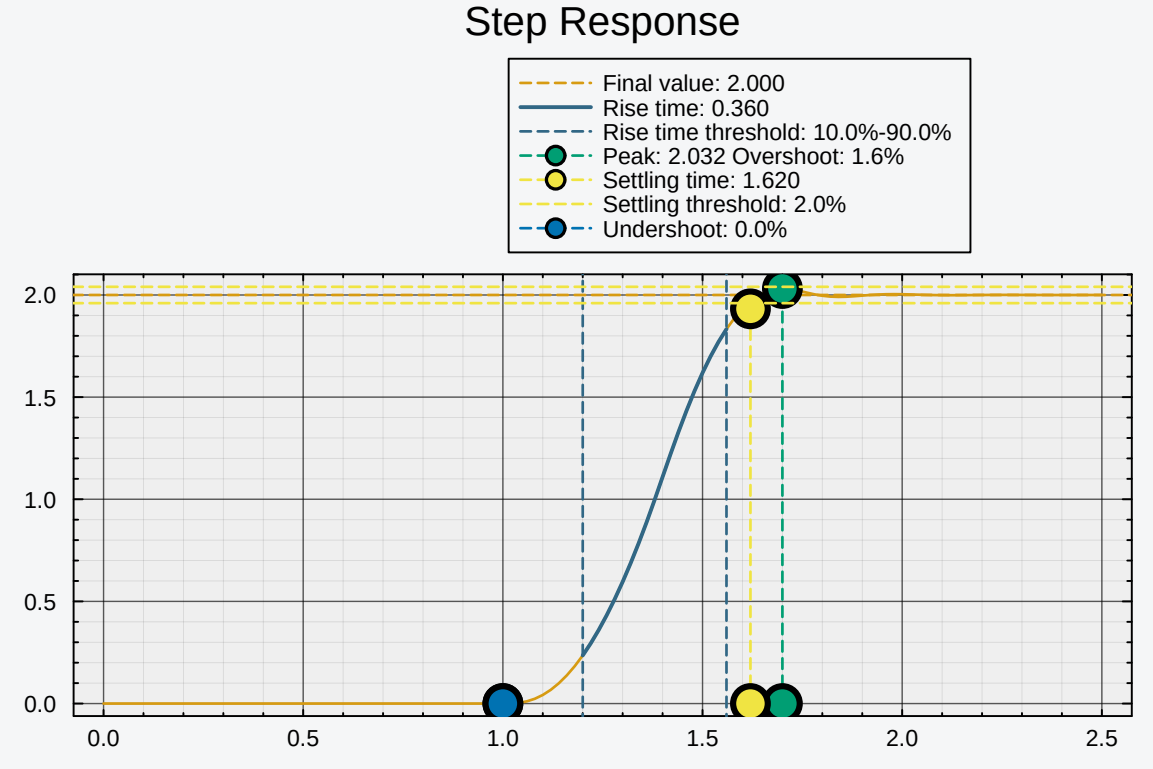
res = lsim(sysreal, ctrl, t)

display(plot(res,
    plotu=true,
    plotx=true,
    ploty=false
    ))
ylabel!("u", sp=1);
ylabel!("x", sp=2);
ylabel!("v", sp=3);
ylabel!("T", sp=4);
```



For more stats:

```
si = stepinfo(res);
plot(si);title!("Step Response")
```



We can also simulate it in a SIMULINK-like environment:

```
using FMI, DifferentialEquations
fmuPath = abspath(joinpath(@__DIR__,
  "..","..",
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fmu = loadFMU(fmuPath);
simData = simulateME(
    fmu,
    (0.0, 5.0);
    recordValues=["blockOnSlope.x",
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    "blockOnSlope.usat"],
    showProgress=false);
unloadFMU(fmu);
plot(simData, states=false, timeEvents=false)
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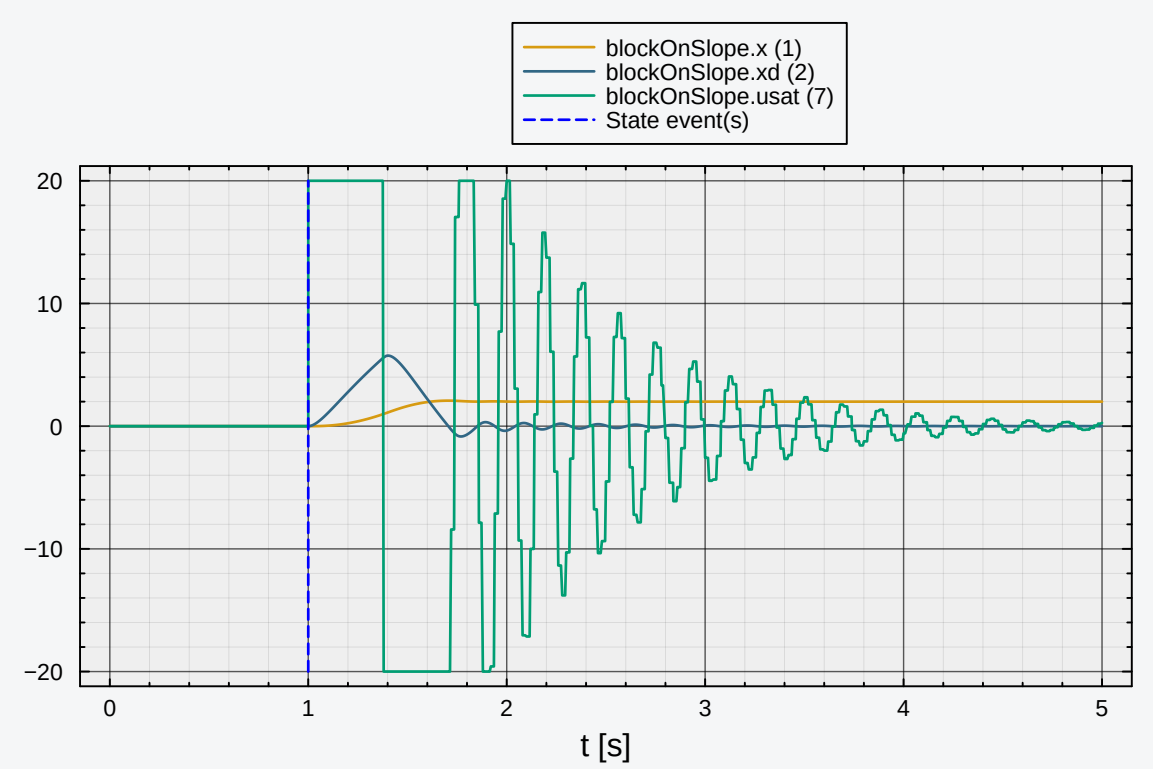

There is a slight difference between the `lsim` simulation and the FMU simulation. I need to recheck some stuff.

A Performance tricks

A.1 Hurwitz Check

Create our nice model. Assume to have run the `poles` function and that you have a vector of eigenvalues. For simplicity I will create an arbitrary vector with the first 100 values in -1 and the last 100 values as random around 0.

```
using BenchmarkTools

vbig = [zeros(ComplexF64,100).-1 ; rand(ComplexF64,100).-0.5];

vbig[[1,end]]
```

```
2-element Vector{ComplexF64}:
                  -1.0 + 0.0im
 -0.030437584033531584 + 0.17283801604223903im
```

A.1.1 for loop

With a naive approach we check if all the elements are in the LHP: make a function that iterates and returns false if it hits a pole with positive real part.

```
function isHurwitz(v)
    for i in eachindex(v)
        if real(v[i])>0.0
            return false
        end
    end
    return true
end

@benchmark isHurwitz($(Ref(vbig))[])
```

```
BenchmarkTools.Trial: 10000 samples with 987 evaluations per
sample.
```

```
 Range (min … max):  49.949 ns … 969.301 ns  ┊ GC (min … max):
0.00% … 0.00%
 Time  (median):     54.306 ns               ┊ GC (median):
0.00%
 Time  (mean ± σ):   57.041 ns ±  22.237 ns  ┊ GC (mean ± σ):
0.00% ± 0.00%
```


```
 Memory estimate: 0 bytes, allocs estimate: 0.
```

We have our baseline. We can probably squeeze out some more performance but I'm still a Julia noob.

A.1.2 all()

Let's try using some of the built-in declarative functions:

```
@benchmark all(real($vbig).<=0.0)
```

```
BenchmarkTools.Trial: 10000 samples with 746 evaluations per
sample.
 Range (min … max):  183.378 ns …  22.068 μs  ┊ GC (min … max):
0.00% … 97.78%
 Time  (median):     261.662 ns               ┊ GC (median):
0.00%
 Time  (mean ± σ):   445.850 ns ± 864.436 ns  ┊ GC (mean ± σ):
32.85% ± 16.78%
```


```
 Memory estimate: 1.75 KiB, allocs estimate: 5.
```

Simple `all()`, when given a tuple it checks if all the values are `True`, otherwise it stops when it encounters the first `False`.

We can see that it's a tad slower. This is because it's creating a new vector with just the real parts, then it's creating a new vector with only the boolean results and then it's checking if there are any False results.

This results in a lot of allocations and wasted resources.

```
@benchmark all(<=(0.0),real($vbig))
```

```
BenchmarkTools.Trial: 10000 samples with 759 evaluations per
sample.
 Range (min … max):  144.664 ns …  31.398 μs  ┊ GC (min … max):
 0.00% … 97.98%
 Time  (median):     226.746 ns               ┊ GC (median):
 0.00%
 Time  (mean ± σ):   344.335 ns ± 699.060 ns  ┊ GC (mean ± σ):
 22.41% ± 15.26%
```


```
 Memory estimate: 1.62 KiB, allocs estimate: 2.
```

A smarter way is to skip on of the allocations by creating the vector of real parts and then checking row by row if the non-positivity check fails.

```
@benchmark all(i -> real(i)<=0.0,$vbig)
```

```
BenchmarkTools.Trial: 10000 samples with 987 evaluations per
sample.
 Range (min … max):  49.139 ns …  2.022 μs  ┊ GC (min … max):
 0.00% … 0.00%
 Time  (median):     51.773 ns               ┊ GC (median):
 0.00%
 Time  (mean ± σ):   53.295 ns ± 22.061 ns  ┊ GC (mean ± σ):
 0.00% ± 0.00%
```


```
 Memory estimate: 0 bytes, allocs estimate: 0.
```

We can do better: Instead of converting into real the full vector it checks element by element if it's in the LHP. It returns false at the first failure. We finally have a comparable result to the benchmark function but in a more compact way.

Is it cleaner? That's subjective.

A.1.3 mapreduce()

Finally we try the MapReduce approach. This allows a better utilization of your processor without the necessity of learning parallel programming.

```
@benchmark mapreduce(i->real(i)<=0.0, &, $vbig)
```

```
BenchmarkTools.Trial: 10000 samples with 993 evaluations per
sample.
 Range (min … max):  42.095 ns … 692.346 ns  ┊ GC (min … max):
 0.00% … 0.00%
 Time  (median):     43.807 ns               ┊ GC (median):
 0.00%
 Time  (mean ± σ):   46.318 ns ±  15.245 ns  ┊ GC (mean ± σ):
 0.00% ± 0.00%
```


```
 Memory estimate: 0 bytes, allocs estimate: 0.
```

We squeeze the last bit of performance and beat the initial benchmark, not by much but still appreciable.