An Explicit, Positivity-Preserving Flux-Corrected Transport Scheme for the Transport Equation Using Continuous Finite Elements

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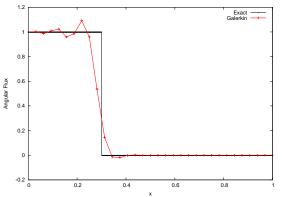
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 Numerical solution of transport equation prone to spurious oscillations and negativities in regions of discontinuities and sharp gradients:



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Objective and Plan

The Objective is to obtain a solution to the transport equation that

- uses CFEM not a traditional discretization for transport, but recent efforts have used CFEM for shock hydrodynamics
- is non-negative
- is free of spurious oscillations
- has high-order accuracy (2nd order)
- The **Plan** is the following:
 - Use a low-order, monotone, non-negative scheme in conjunction with a high-order scheme via the flux-corrected transport (FCT) algorithm to produce a high-order, non-negative scheme
 - monotonicity not guaranteed but demonstrated for most cases

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Problem Formulation

Model transport equation:

$$egin{aligned} &rac{1}{v}rac{\partial\psi}{\partial t}+\mathbf{\Omega}\cdot
abla\psi(\mathbf{x},t)+\Sigma(\mathbf{x})\psi(\mathbf{x},t)=q(\mathbf{x},t) \ & ext{(1)} \ & \Sigma(\mathbf{x})\geq 0, \qquad q(\mathbf{x},t)\geq 0 \end{aligned}$$

Define problem:

$$\psi(\mathbf{x}, \mathbf{0}) = \psi^{\mathbf{0}}(\mathbf{x}) \quad \forall \mathbf{x} \in \mathcal{D}$$
 (2)

$$\psi(\mathbf{x},t) = \psi^{inc}(\mathbf{x}) \quad \forall \mathbf{x} \in \partial \mathcal{D}^{inc}$$
(3)

CFEM solution:

$$\psi_h(\mathbf{x},t) = \sum_{j=1}^N U_j(t)\varphi_j(\mathbf{x}), \quad \varphi_j(\mathbf{x}) \in P_h^1$$
 (4)



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Temporal Discretization

- Fully explicit temporal schemes used here:
 - Forward Euler (FE)
 - Explicit Strong Stability Preserving Runge-Kutta methods, which can be expressed as a number of FE steps
 - Forward Euler scheme:

$$\mathbf{M}^{C} \frac{\mathbf{U}^{n+1} - \mathbf{U}^{n}}{\Delta t} + \mathbf{A} \mathbf{U}^{n} = \mathbf{b}^{n}$$
 (5)

$$M_{i,j}^{C} \equiv \int_{S_{i,i}} \varphi_i(\mathbf{x}) \varphi_j(\mathbf{x}) d\mathbf{x}$$
 (6)

$$A_{i,j} \equiv v \int_{S_{i,j}} (\mathbf{\Omega} \cdot \nabla \varphi_j(\mathbf{x}) + \Sigma(\mathbf{x})\varphi_j(\mathbf{x})) \varphi_i(\mathbf{x}) d\mathbf{x}$$
(7)
$$b_i^n \equiv v \int_{\mathbf{x}} q(\mathbf{x}, t^n)\varphi_i(\mathbf{x}) d\mathbf{x}$$
(8)



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Low-Order Scheme Definition

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• Lump mass matrix and add artificial viscosity:

$$\mathbf{M}^{L} \frac{\mathbf{U}^{L,n+1} - \mathbf{U}^{n}}{\Delta t} + (\mathbf{A} + \mathbf{D}^{L})\mathbf{U}^{n} = \mathbf{b}^{n}$$
(9)

$$D_{i,j}^{L} = \sum_{K \subset S_{i,j}} \nu_{K}^{L} b_{K}(\varphi_{j}, \varphi_{i})$$
(10)

$$b_{\mathcal{K}}(\varphi_{j},\varphi_{i}) \equiv \begin{cases} -\frac{1}{n_{\mathcal{K}}-1}|\mathcal{K}| & i \neq j, \quad i,j \in \mathcal{I}(\mathcal{K}) \\ |\mathcal{K}| & i = j, \quad i,j \in \mathcal{I}(\mathcal{K}) \\ 0 & i \notin \mathcal{I}(\mathcal{K}) | j \notin \mathcal{I}(\mathcal{K}) \end{cases}$$
(11)
$$\nu_{\mathcal{K}}^{L} \equiv \max_{i \neq j \in \mathcal{I}(\mathcal{K})} \frac{\max(0,A_{i,j})}{-\sum_{\mathcal{T} \subset S_{i,j}} b_{\mathcal{T}}(\varphi_{j},\varphi_{i})}$$
(12)

Low-Order Scheme Properties

- These definitions make (A + D^L) an M-matrix, which has the following desirable consequences for the low-order solution U^{L,n+1}:
 - monotonicity
 - non-negativity
 - satisfaction of a discrete maximum principle (DMP):

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$$W_i^-(\mathbf{U}^n) \le U_i^{L,n+1} \le W_i^+(\mathbf{U}^n) \qquad \forall i$$
 (13)

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$$W_i^{\pm}(\mathbf{U}^n) \equiv U_{\min,i}^n \left(1 - \frac{\Delta t}{m_i} \sum_j A_{i,j}^L\right) + \frac{\Delta t}{m_i} b_i^n \quad (14)$$

Undesirable consequence: first-order accuracy

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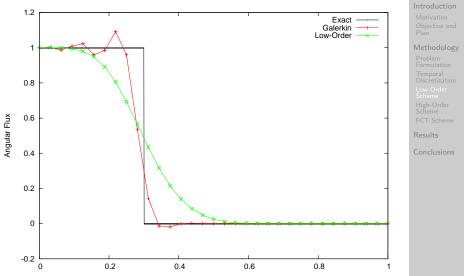
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Low-Order Scheme Results Example





High-Order Scheme



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Add high-order artificial viscosity:

$$\mathbf{M}^{C} \frac{\mathbf{U}^{H,n+1} - \mathbf{U}^{n}}{\Delta t} + (\mathbf{A} + \mathbf{D}^{H,n})\mathbf{U}^{n} = \mathbf{b}^{n} \qquad (15)$$

$$D_{i,j}^{H,n} = \sum_{K \subset S_{i,j}} \nu_K^{H,n} b_K(\varphi_j, \varphi_i)$$
(16)

$$\nu_K^{H,n} = \min(\nu_K^L, \nu_K^{E,n}) \tag{17}$$

The entropy-based artificial viscosity ν^{E,n}_K is proportional to local "entropy" production.



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■ One chooses a convex entropy function E(ψ) such as E(ψ) = ½ψ² and manipulates the transport equation to get an entropy residual:

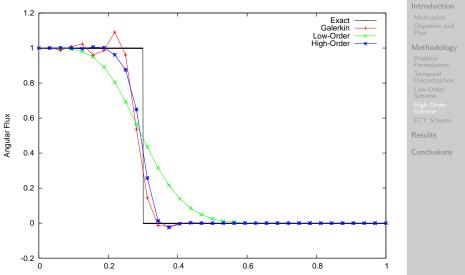
$$R_{\mathcal{K}}(\psi) = \left\| \frac{\partial E}{\partial t} + \frac{dE}{d\psi} \left(\mathbf{\Omega} \cdot \nabla \psi + \sigma \psi - q \right) \right\|_{L^{\infty}(\mathcal{K})}$$
(18)

 Entropy-based artificial viscosity is proportional to an entropy residual Rⁿ_K(\u03c6_h):

$$\nu_{K}^{E,n} = \frac{c_{E}R_{K}^{n}(\psi_{h}) + c_{J} \max_{F \in \partial K} J_{F}(\psi_{h}^{n})}{\|E(\psi_{h}^{n}) - \bar{E}(\psi_{h}^{n})\|_{L^{\infty}(\mathcal{D})}}$$
(19)

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- Initially developed in 1973 for finite difference discretizations of transport/conservation law problems and recently applied to finite element method
- Works by adding conservative fluxes to satisfy physical bounds on the solution
- Employs low-order scheme and high-order scheme
- Defines a *correction*, or *antidiffusion*, flux, which when added to the low-order scheme, produces the high-order scheme
- Limits this correction flux to enforce the physical bounds imposed

Flux Corrected Transport (FCT) Scheme Correction Flux Definition



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Define a correction flux **f**:

$$\mathbf{f} \text{ Def.:} \quad \mathbf{M}^{L} \frac{\mathbf{U}^{H,n+1} - \mathbf{U}^{n}}{\Delta t} + (\mathbf{A} + \mathbf{D}^{L})\mathbf{U}^{n} = \mathbf{b}^{n} + \mathbf{f}^{n}$$
Low-order:
$$\mathbf{M}^{L} \frac{\mathbf{U}^{L,n+1} - \mathbf{U}^{n}}{\Delta t} + (\mathbf{A} + \mathbf{D}^{L})\mathbf{U}^{n} = \mathbf{b}^{n}$$
High-order:
$$\mathbf{M}^{C} \frac{\mathbf{U}^{H,n+1} - \mathbf{U}^{n}}{\Delta t} + (\mathbf{A} + \mathbf{D}^{H,n})\mathbf{U}^{n} = \mathbf{b}^{n}$$

■ Thus **f** is

$$\mathbf{f}^{n} \equiv -(\mathbf{M}^{C} - \mathbf{M}^{L}) \frac{\mathbf{U}^{H,n+1} - \mathbf{U}^{n}}{\Delta t} + (\mathbf{D}^{L} - \mathbf{D}^{H,n}) \mathbf{U}^{n}$$
(20)

Flux Corrected Transport (FCT) Scheme

• Decompose **f** into internodal fluxes $F_{i,j}$: $f_i = \sum_i F_{i,j}$:

$$F_{i,j} = -M_{i,j}^{C} \left(\frac{dU_{j}}{dt}^{H,n+1} - \frac{dU_{i}}{dt}^{H,n+1} \right) + (D_{i,j}^{L} - D_{i,j}^{H})(U_{j}^{n} - U_{i}^{n})$$
(21)

■ The FCT scheme limits these fluxes with a limiter *L*:

$$\mathbf{M}^{L} \frac{\mathbf{U}^{n+1} - \mathbf{U}^{n}}{\Delta t} + \mathbf{A}^{L} \mathbf{U}^{n} = \mathbf{b} + \mathcal{L}[\mathbf{F}]$$
(22)

The limiter L enforces the discrete maximum principle:

$$W_i^{-}(\mathbf{U}^n) \le U_i^{n+1} \le W_i^{+}(\mathbf{U}^n) \qquad \forall i$$
(23)



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Flux Corrected Transport (FCT) Scheme Limiting Coefficient Definition



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■ Each correction flux F_{i,j} has an associated limiting coefficient L_{i,j}: L[F]_i = ∑_i L_{i,j}F_{i,j}:

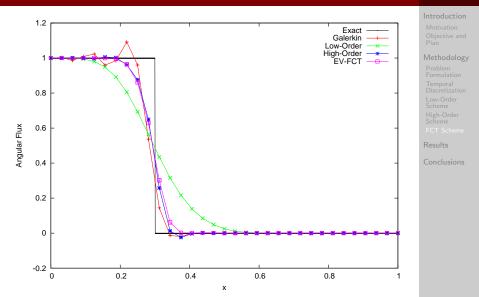
$$P_i^+ \equiv \sum_j \max(0, F_{i,j}) \qquad P_i^- \equiv \sum_j \min(0, F_{i,j}) \qquad (24)$$

$$Q_i^{\pm} \equiv m_i \frac{W_i^{\pm} - U_i^n}{\Delta t} + \sum_j A_{i,j}^L U_j^n - b_i \qquad (25)$$

$$R_{i}^{\pm} \equiv \begin{cases} 1 & P_{i}^{\pm} = 0\\ \min\left(1, \frac{Q_{i}^{\pm}}{P_{i}^{\pm}}\right) & P_{i}^{\pm} \neq 0 \end{cases}$$
(26)
$$\mathcal{L}_{i,j} \equiv \begin{cases} \min(R_{i}^{+}, R_{j}^{-}) & F_{i,j} \ge 0\\ \min(R_{i}^{-}, R_{i}^{+}) & F_{i,j} < 0 \end{cases}$$
(27)

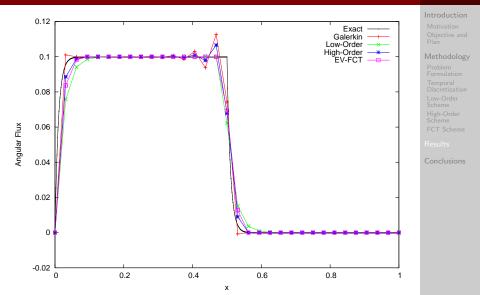
Flux Corrected Transport (FCT) Scheme Results Example





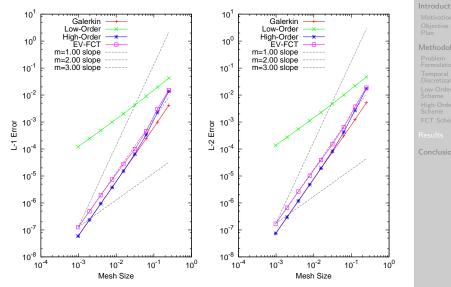
Results Source Problem Results





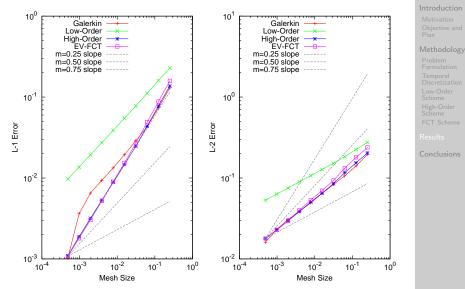
Results Smooth Problem Convergence Results (Using FE)





Results Non-smooth Problem Convergence Results (Using SSPRK33)





Conclusions



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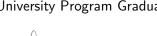
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- guaranteed non-negative, DMP-satisfying scheme
- monotonicity for problems tested, but not guaranteed
- theoretical convergence rates observed
- future work:
 - implicit time discretizations
 - steady-state
 - more complicated physics

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