

## **Theoretical Questions**

***1. What other sensor would you use in order to create a more robust tracking in cases where there are disturbances? Implement a model of this sensor in the simulation.***

In the pure pursuit assignment, only a very simple GPS/INS sensor was modulated in order to measure the distance and the orientation of the car from the path.

The disadvantage of the GPS/INS sensor is that it does not warn against disturbances in the road that might prevent a free of obstacles, safe driving.

Therefore in order to alert against obstacles in the road at least two more sensors are advised:

1. Lidar sensor - The lidar is a method for determining ranges by targeting an object with a laser and measuring the time for the reflected light to return to receiver. using the Lidar will assist in alerting from obstacles and disturbances.

2. Vision sensors - vision sensors have the ability of alerting and notifying of disturbances in the road - passengers, obstacles, etc. There are day vision sensors (CCD) and night vision sensors(IR).

In cases of disruptions in the GPS inertial system it is advised to use also:

3. DTM - digital terrain maps that may assist in evaluating the position of the car in absence or corruption of a GPS system. In those cases, the DTM maps may work together with the standalone car gyros.

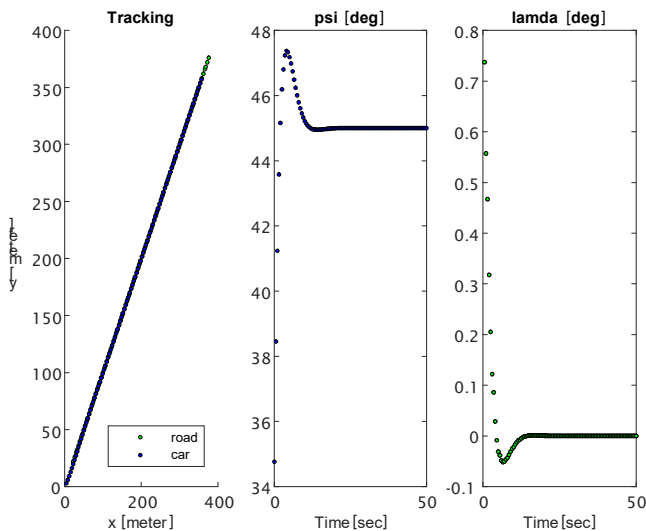
The most proper way of building a robust tracking car system is to combine all the sensors using a fusion algorithm.

## 2. What will be the steady state effect of a bias in mechanical road wheel servo? Show this effect in your simulation.

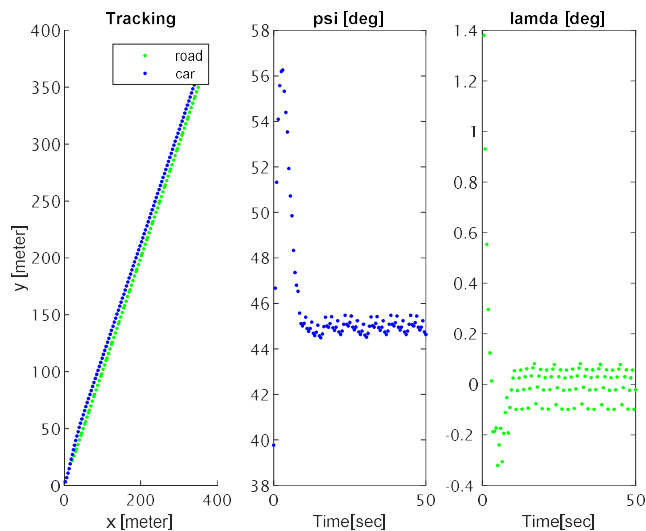
A steady state effect of a bias in the mechanical road wheel servo will prevent the control error to converge and therefore will lead to wheel command  $\delta$  to jitter around the true car wheel command.

The following graphs - the graphs were generated in matlab environment show the effect of a 1[deg] bias in the wheel angle vs. no bias in the wheel angle.

The scenario depicted in the graphs is of a straight line path that is oriented 45[deg] both to the x&y axis global system with an initial car psi angle=30[deg].



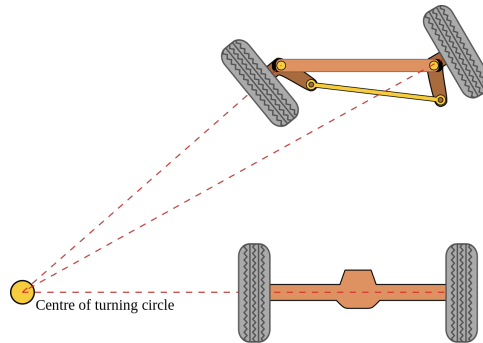
No bias in wheel servo: The wheel angle and car psi angle converge.



1[deg] bias in wheel servo: The wheel angle and the car psi do not converge and jitter around the true wheel angle.

**3. It is known that kinematic bicycle model is only valid in low speed  $\sim 5$  m/sec, suggest a model for higher speeds and state what cannot be neglected anymore?**

A model that can be used instead of the kinematic bicycle model is the Ackerman steering model - attached is an image of the model.



The slip wheel angle caused by slippery path cannot be neglected in higher speeds.

#### 4. Explain your consideration for the integration method and step size.

Considerations for integration method:

The state space for updating the car dynamics in the assignment is the following eq-[1]

$$[\text{eq-1}] \quad \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{\phi} \end{bmatrix} = \begin{bmatrix} v \cos(\delta) \\ v \sin(\delta) \\ v \cdot \tan(\delta) / L \end{bmatrix}$$

where:

$x, y$  - position coordinates.

$v, \delta, L$  - car velocity, wheel angle and length respectively.

A discrete integration method that was used in the simulation is a simplified method suitable for discrete states. however, the nature of the states above is **continuous** and for that purpose a trapezoid integration method would be more accurate.

Below is an example of the  $x$  state calculated in discrete and trapezoid methods:

*Discrete :*

$$x(k) = x(k-1) + dt \cdot \dot{x}(k)$$

*Trapezoid :*

$$x(k) = x(k-1) + \frac{dt}{2} \cdot (\dot{x}(k) + \dot{x}(k-1))$$

Consideration for step size:

The step size reasoning is strictly correlated to the required wheel dynamics. Since the simulation uses a 2[Hz]\* bandwidth transfer function from wheel angle command to wheel angle physical angle, a step size of 0.1[sec] was implemented as the computation frequency of the controller of 10[Hz].

The minimum frequency of the controller may be 4[Hz] but in order to have abilities of measuring physical phenomenon such as vibrations, self frequencies and etc. a higher implementation of computation frequency is recommended.

Also, the servo in this simulation is lacking, in the sense that in "real life" we will usually use a velocity loop and a current loop that usually run in much higher frequencies.

\*2[Hz] Is a naive consideration for the bandwidth of the wheel angle, As a low bandwidth will not respond to any transient change or spike in the path/road.

**5. Choose one component in the simulation and explain how you would improve it in order to get a more real world behavior.**

The **car Servo** can be improved in order to get a more real world behavior and accurate modeling using the following sub models:

1. Wheel friction model.
2. Stick slip model.
3. Wheel electrical motor plant dynamics.
4. Control loops and bandwidth (current/voltage, velocity, angle).
5. Disturbances to control loops.
6. Measurements sensors - encoders, gyros, resolvers, etc.
7. Measurements sensor errors and tolerances (bias, scale factors, noise, etc.).
9. System delays
10. BIT (Built in tests) - initial and continuous servo tests.

**6. What is needed to be considered on the look ahead distance for the reference look ahead point when the vehicle dynamics are not ideal? (optional)**

When the vehicle dynamics are not ideal and contain errors it is important that the look ahead distance would be a trade-of between a long enough distance, that avoids transient phenomenon in the path, but not too long in order to keep with the path.