

# The movement equation

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## 1 The problem

$$\begin{cases} m \frac{dv}{dt} = \beta v_d + \frac{m}{\tau} (v_d - v) - 2k(2r - d)v \\ 2r - d = B \ln \left( \frac{\beta v_d}{A} \right) \\ v(0) = v_0 \end{cases} \quad (1)$$

The equation can be expressed in the following reduced magnitudes

$$\begin{cases} v^* &= v/v_d \\ t^* &= t/\tau \\ z^* &= (2r - d)/B \\ k^* &= k\tau B/m \\ \beta^* &= \beta\tau/m \end{cases} \quad (2)$$

The reduced equation in new variables read (the “\*” has been omitted for clarity reasons)

$$\begin{cases} \frac{dv}{dt} + (1 + 2kz)v = 1 + \beta \\ v(0) = v_0 \end{cases} \quad (3)$$

## 2 The velocity

$$\frac{dv}{(1 + \beta) - (1 + 2kz)v} = dt \quad (4)$$

$$-\frac{1}{1 + 2kz} \ln[(1 + \beta) - (1 + 2kz)v] + C = t \quad (5)$$

$$v = \frac{1 + \beta}{1 + 2kz} - C \exp[-(1 + 2kz)t] \quad (6)$$

where the parameter  $C$  is related to the initial conditions as

$$C = \frac{1 + \beta}{1 + 2kz} - v_0 \quad (7)$$

## 3 The position

The velocity is  $v = dx/dt$  (in non-reduced variables). Then

$$v^* = \frac{v}{v_d} = \frac{1}{v_d} \frac{dx}{dt} = \frac{1}{v_d \tau} \frac{dx}{dt^*} \quad (8)$$

Thus, the reduced position can be defined as  $x^* = x/v_d\tau$ . The reduced position as a function of  $t^*$  is (the “\*” has been omitted for clarity reasons)

$$x = D + \frac{1 + \beta}{1 + 2kz} t + \frac{C}{1 + 2kz} \exp[-(1 + 2kz)t] \quad (9)$$

where the parameter  $D$  is related to the initial conditions as

$$D = x_0 + \frac{v_0}{1 + 2kz} - \frac{1 + \beta}{(1 + 2kz)^2} \quad (10)$$

## 4 Relation between position-velocity

Recalling the differential relation (4) and the definition  $v = dx/dt$  (in reduced units), both magnitudes are related by

$$\frac{v dv}{(1 + \beta) - (1 + 2kz)v} = dx \quad (11)$$

Therefore,

$$-\frac{v}{1+2kz} - \frac{1+\beta}{(1+2kz)^2} \ln[(1+\beta)-(1+2kz)v] + C = x \quad (12)$$

where the argument of  $\ln(\cdot)$  is supposed to be positive. Otherwise, the modulus of the argument should be computed.

We can further introduce the stationary value for the velocity  $v$  from eq. (3) as

$$v_\infty = \frac{1+\beta}{1+2kz} \quad (13)$$

(in reduced units). Thus, eq. (11) reads

$$v + v_\infty \ln[v_\infty - v] + D = -(1+2kz)x \quad (14)$$

Notice that at the initial condition

$$D = -(1+2kz)x_0 - v_0 - v_\infty \ln[v_\infty - v_0] \quad (15)$$

and the eq. (14) can be expressed in terms of the initial and ending condition as

$$v - v_0 + v_\infty \ln \left[ \frac{v_\infty - v}{v_\infty - v_0} \right] = -(1+2kz)(x - x_0) \quad (16)$$

`h=xmax/n;`

```
while i<n,
    v(i)=v0+h*(b/v0-a);
    x(i)=x0+h;
    v0=v(i);
    x0=x(i);
end
```

where

$$\begin{cases} 1+\beta &= 1+\sqrt{225} = 16 \\ 1+2kz &= 1+274z \end{cases} \quad (18)$$

Notice that  $z$  is the (reduced) compression parameter  $(2r-d)/B$ . No further condition has been achieved till now. For example, the balance between the repulsive force and the bulk social force  $\beta v_d$  gives

$$\frac{2r-d}{B} = \ln(\beta v_d/A) \quad (19)$$

where

$$\beta v_d = \frac{\sqrt{N}m}{\tau A} v_d \simeq v_d \quad (20)$$

Thus, the  $z$  parameter should vary at least between  $0 \leq z \leq 2$ . Notice, however, that  $z$  becomes relevant beyond  $1/274 \simeq 0.003$ .

## 5 The numerical solution

The numerical solution can be obtained from eq. (11).

$$\frac{v_{i+1} - v_i}{h} \simeq \frac{1+\beta}{v_i} - (1+2kz) \quad (17)$$

for  $v(0) = v_0$ . The small increment  $h$  represents the step width of the position. That is,  $x_{i+1} = x_i + h$ . The code for computing the velocity is as follows (in Matlab/Octave)

```
i=1;
n=10000;

x0=0;
v0=1; % could also be v0=0;
xmax=1;
```