ENGSCI YEAR 2 WINTER 2022 NOTES

FOR CLASS CONTENT AFTER READING WEEK

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PHY294 Quantum & Thermal Physics

Section 1

Statistical Mechanics

Subsection 1.1

Lecture 1: Ideal Gas Law

We begin our discussion on statistical mechanics with the guiding question, "What is temperature". We will first derive the ideal gas law PV=nRT, which most should be familiar with.

Imagining a single particle bouncing around elastically in 2D box with speed v_x . If we were to look at the sides of the box we will see intermittent spikes of force experienced [by the box walls],

$$F_x = m \frac{2v_x}{\Delta t_c} \tag{1.1}$$

Over time can get the average force

$$F_x = m \frac{2_x}{\Delta t} \tag{1.2}$$

which allows us to derive an expression for pressure, which is just force over area

$$P = \frac{F_x}{A} = \frac{mv_x^2}{V} \tag{1.3}$$

For n particles it then becomes

$$P = \sum_{i=1}^{N} \frac{mv_{x,i}^2}{V} = \frac{m}{V} \sum_{i=1}^{N} v_{x,i}^2$$
(1.4)

Assuming that that $v_x = v_y = v_z^{-1}$, we may extend this to 3 dimensions

¹ This is reasonable, is it not?

$$P = \frac{mv^2}{3} \frac{N}{V} \tag{1.5}$$

Now, compare this expression and that of the ideal gas law to find that temperature is a measure of the average kinetic energy per particle

Note that
$$\frac{mv^2}{3} = kT \rightarrow \frac{mv^2}{3k} = 2\frac{\overline{E}}{3k}$$

$$T = \frac{mv^2}{3k} = \frac{2\overline{E}}{3k} \tag{1.6}$$

DIELECTRICS 2

$ECE 259 \\ Electromagnetism$

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Section 2

Dielectrics

Subsection 2.1

Lecture 15: Boundary Conditions for Dielectrics

Remark Recall, at a conductor/free-space interface, $E_{+}=0$, $E_{n}=\frac{\rho_{s}}{\varepsilon_{o}}$

Consider an interface between two generic dielectrics (Fig. 1).

Theorem 1

$$\oint_{c} \vec{E} \cdot d\vec{l} = 0 \tag{2.1}$$

Intuition

The two integrals parallel to the dielectrics will cancel out, and so will those perpendicular.

This implies that the tangential component of the \vec{E} field is continuous across the boundary,

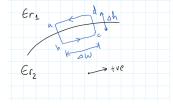


Figure 1. Dielectric interface

$$E_{1t} = E_{2t} (2.2)$$

However we get a bit of a different result when working in 3 dimensions where the interface is a surface instead of a line.

Theorem 2

$$\oint_{S} \vec{D} \cdot d\vec{s} = \rho_{S} \Delta \to (\vec{D_{1}} - \vec{D_{2}}) \cdot \vec{a_{n2}} = \rho_{S}$$
(2.3)

 a_n denotes normal component.

Note: $\vec{D} = \varepsilon_0 \vec{E} + \vec{p} = \dots \varepsilon \vec{E}$

Proof

As $\Delta h \to 0$

$$\oint_{S} \vec{D} \cdot d\vec{s} = \int_{top} \vec{D_{1}} \cdot d\vec{s} + \int_{bottom} + \vec{D_{2}} \cdot d\vec{s}$$

$$= \vec{D_{1}} \cdot \vec{a_{n2}} \Delta S + \vec{D} \cdot \vec{a_{n1}} \Delta S$$

$$= \vec{D_{1}} \cdot \vec{a_{n2}} \Delta S - \vec{D} \cdot \vec{a_{n2}} \Delta S$$

$$= \rho_{S} \Delta S$$
(2.4)

Solving these problems usually involves finding the tangential and normal components through Eq. 2.2 and 2.3 then applying Pythagoras.

DIELECTRICS

Lecture 16: Capacitors

Subsection 2.2

Lecture 16: Capacitors

Definition 1

A capacitor is a device consisting of two isolated conductors for storing energy in the form of electrostatic potential energy.

The energy stored in a capacitor is equal to the energy it takes to charge a capacitor from a discharged state to a charged state.

A capacitor's $capacitance^2$ is defined as

$$C = \frac{Q}{V} \tag{2.5}$$

and has units $[C] = \frac{C}{V}F(\text{Farads})$

Capacitance is calculated as follows

- 1. choose a coordinate system
- 2. Assume +Q/-Q on the conductors
- 3. Find \vec{E} from Q distribution
- 4. Find $V_{AB} = \int_A^B \vec{E} \cdot d\vec{l}$ where A carries the negative charge and B carries positive.
- 5. Apply $C = \frac{Q}{V}$

An isolated conductor can also have "capacitance" if the potine coordinate of lyisinfar and on the physical attance refers to the charge on the physical attributes of the capacitor, one conductor.

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\mathbf{III}

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result

Leibniz integral $g(y) = \frac{d}{dy} \int_{-\infty}^{u^{-1}(y)} f(t) dt$

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rule,

ECE286 Probability and Statistics

Section 3

Probability Distributions

Subsection 3.1

Lecture 14: functions of random variables

In the discrete case, given X with PMF f(x), we can define an *invertible* function Y where Y = u(X), therefore can write $X = u^{-1}(Y)$. If g(y) is the distribution of Y

$$g(y) = P(Y = y)$$

$$= P(u^{-1}(Y) = u^{-1}(y))$$

$$= f(u^{-1}(y))$$
(3.1)

In the continuous case we may arrive at

$$g(y) = f(u^{-1}(y)) \left| \frac{du^{-1}(y)}{dy} \right|$$
 (3.2)

Definition 2

The r^{th} moment about the origin of the random variable X is

$$\mu_r = E[X^r] = \begin{cases} \sum_x x^r f(x) & X \text{discrete} \\ \int_{-\infty}^{\infty} x^r f(x) dx & X \text{continuous} \end{cases}$$
(3.3)

- The mean is the first moment
- For variance, $\sigma^2 = E[X^2] \mu^2 \rightarrow \sigma^2 = \mu \ell_2 \mu^2$

Definition 3

The moment-generating function of X is defined as

$$\mu_r = E[X^{tX}] = \begin{cases} \sum_x e^{tx} f(x) & X \text{discrete} \\ \int_{-\infty}^{\infty} e^{tx} f(x) dx & X \text{continuous} \end{cases}$$
(3.4)

In general

$$\mu_r = \frac{d^r M_X(t)}{dt^r} \bigg|_{t=0} \tag{3.5}$$

Subsection 3.2

Lecture 15: More on moment generating functions

By definition and completing the square,

$$M_X(T) = \int_{-\infty}^{\infty} e^{tx} \frac{1}{\sqrt{t2\pi\sigma}e^{-\frac{(x-\mu)^2}{2\sigma^2}}dx}$$

$$= \int_{-\infty}^{\infty} \frac{1}{\sqrt{t2\pi\sigma}e^{-\frac{x^2 - 2(x-\mu)^2 + \mu^2}{2\sigma^2}}dx}$$

$$= e^{\frac{2\mu t + t^2\sigma^2}{2}} \int_{-\infty}^{\infty} \frac{1}{\sqrt{2\pi\sigma}} \exp\left\{-\frac{(x - (\mu + t\sigma^2))^2}{2\sigma^2}\right\} dx$$

 $=e^{\frac{2\mu t+t^2\sigma^2}{2}} \quad (3.6) \quad \text{The integrand is just a normal PDF and thus integrates to one}$

PART

IV

TEP327 Engineering and Law

Torts can be identified by

- Elements of negligence can be identified
- There exists a duty of care
- Was the standard of duty of care breached?
- Did that breach of standard cause damage to the plaintiff?

Comment

Must be careful about the standard of care met or not met. E.x. in the in-class bike example one could argue that in designing the gear the engineer should expect that the gear could be commercialized and mass-produced later on for mass-market. On the other hand it is reasonable to argue that having to design the gear to be used by unskilled 16-year-olds is an unreasonable and outside the standard of care.

Trespass is strict liability. Ignorance of the law is no excuse.