Experimental Evaluation of Control Policies for Segway Robot in Dynamic Environments

Ian Buckley, Niharika Arora, Varun Murali

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ECE 6552: Nonlinear System Project

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- A hybrid approach applies the benefits and mitigates the shortcomings of both
- A nonlinear navigation control protocol can achieve navigational objectives while reacting to unexpected obstacles

System Description

Robotic Platform

Figure 1: Jeeves - A modified Segway based robot mounted with a Primesense, Microsfot Kinect, Roboteye RE05, Hokuyo LTM-30x laser and the UR5. Currently modified to include the casters for static stability

Unicycle Dynamics

$$\begin{pmatrix} \dot{r} \\ \dot{\theta} \end{pmatrix} = \begin{pmatrix} -v\,\cos(\delta) \\ \frac{v}{r}\,\sin(\delta) \end{pmatrix} \quad (1)$$

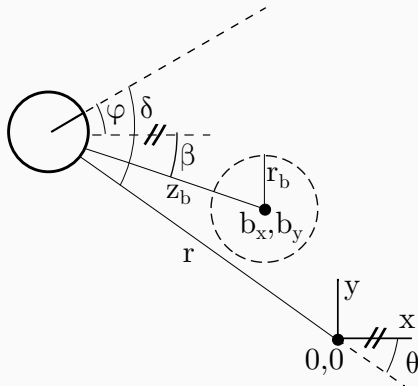$$\dot{\delta} = \frac{v}{r}\,\sin(\delta) + \omega \quad (2)$$

Figure 2: Egocentric Polar Unicycle Dynamics with Obstacle

Approach

Objectives

Soft Constraints

- Navigate to target location
- Drive the state of the robot to zero (e.g. $\dot{x} = (\dot{r}, \dot{\theta}, \dot{delta})^T \to 0$)

Hard Constraints

- Avoid obstacles
- The distance to the obstacle must not exceed a minimum distance (e.g. $z_b > z_{safe}$)

System Constraints

- Inputs should not exceed threshold values
- $0 < v < v_{max}$ and $0 < \omega < \omega_{max}$

A switched mode *quadratic programming controller* that **simultaneously** satisfies the soft constraints, hard constraints, and system constraints was designed.

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Feedback linearization of this objective by choosing the angular velocity:

$$\omega = -\frac{v}{r}\left[k_2 z_1 + \left(1 + \frac{k_1}{1 + (k_1\theta)^2}\right) \sin(z_1 + \arctan(-k_1\theta))\right]$$

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$$\dot{z}_1 = -k_2 \frac{v}{r} z_1$$

$$\implies \textit{Stabilization of the steering objective}$$

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$$\dot{V} < 0$$

$$\implies \textit{Stabilization of the state to zero}$$

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$$\dot{V} = -rv\cos(\arctan(k_1\beta)) + \theta v \sin(\arctan(-k_1\beta))$$

$$\dot{V} \nleq 0$$

$\implies$ *The second steering control drives the state away from zero*

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Hard Constraint as ZBF [4],[5],[6]

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$$\dot{h}(x) =$$

Switched Mode QP Controller

Results

needs octo plots!

Experimental Results

needs robots!

Conclusions

References I

L. E. Kavraki, P. Svestka, J. C. Latombe, and M. H. Overmars, "Probabilistic roadmaps for path planning in high-dimensional configuration spaces," in *RIEEE Transactions on Robotics and Automation (Volume:12 , Issue: 4)*. IEEE, 1996, pp. 566–580.

O. Khatib, "Real-time obstacle avoidance for manipulators and mobile robots," in *Robotics and Automation. Proceedings. 1985 IEEE International Conference on (Volume:2)*. IEEE, 1985, pp. 500–505.

J. J. Park and B. Kuipers, "A smooth control law for graceful motion of differential wheeled mobile robots in 2d environment," in *Robotics and Automation (ICRA), 2011 IEEE International Conference on*. IEEE, 2011, pp. 4896–4902.

References II

📄 A. D. Ames, J. W. Grizzles, and P. Tabuada, "Control barrier function based quadratic programs with application to adaptive cruise control," in *53rd IEEE Conference on Decision and Control.* IEEE, 2014, pp. 6271–6278.

📄 X. Xu, P. Tabuada, J. W. Grizzle, and A. D. Ames, "Robustness of control barrier functions for safety critical control," in *Analysis and Design of Hybrid Systems(Volume 48)*, 2015, pp. 54–61.

📄 A. D. Ames, K. Galloway, K. Sreenath, and J. W. Grizzle, "Rapidly exponentially stabilizing control lyapunov functions and hybrid zero dynamics," in *IEEE Transactions on Automatic Control (Volume:59 , Issue: 4)*. IEEE, 2014, pp. 876–891.

Questions?