

The truth state is a motorcycle model in the 2D plane

$$\mathbf{x}_t = \begin{bmatrix} r_{xi} \\ r_{yi} \\ v_{xb} \\ \psi \\ \phi \\ \mathbf{b}_a \\ \mathbf{b}_g \\ \mathbf{r}_{c/i}^i \end{bmatrix} \quad (1)$$

The corresponding dynamics are

$$\dot{\mathbf{x}}_t = \begin{bmatrix} v_{xb} \cos \psi \\ v_{xb} \sin \psi \\ a \\ \frac{v_{xb}}{L} \tan \phi \\ \xi \\ -\frac{1}{\tau_a} \mathbf{b}_a + \mathbf{w}_a \\ -\frac{1}{\tau_g} \mathbf{b}_g + \mathbf{w}_g \\ \mathbf{0} \end{bmatrix} \quad (2)$$

The continuous measurements consist of accelerometer and gyro measurements, where the y component includes the lateral accelerations felt during a turn and the z component includes gravity.

$$\tilde{\mathbf{a}}^b = \begin{bmatrix} a & \frac{v_{xb}^2}{L} \tan \phi & -g \end{bmatrix}^T + \mathbf{b}_a + \mathbf{n}_a \quad (3)$$

$$\tilde{\boldsymbol{\omega}}_{b/i}^b = \begin{bmatrix} 0 & 0 & \frac{v_{xb}}{L} \tan \phi \end{bmatrix}^T + \mathbf{b}_g + \mathbf{n}_g \quad (4)$$

The design states model is a conventional inertial navigation system augmented with the position of the circuit

$$\mathbf{x} = \begin{bmatrix} \mathbf{r}_{b/i}^i \\ \mathbf{v}_{b/i}^i \\ q_i^b \\ \mathbf{b}_a \\ \mathbf{b}_g \\ \mathbf{r}_{c/i}^i \end{bmatrix} \quad (5)$$

The dynamics are defined as

$$\dot{\mathbf{x}} = \begin{bmatrix} \mathbf{v}_{b/i}^i \\ T_b^i \left(\tilde{\mathbf{a}}^b - \mathbf{b}_a - \mathbf{n}_a \right) + \mathbf{g}^i \\ \frac{1}{2} \begin{bmatrix} 0 \\ \tilde{\boldsymbol{\omega}}_{b/i}^b - \mathbf{b}_g - \mathbf{n}_g \\ -\frac{1}{\tau_a} \mathbf{b}_a + \mathbf{w}_a \\ -\frac{1}{\tau_g} \mathbf{b}_g + \mathbf{w}_g \\ \mathbf{0} \end{bmatrix} \otimes \mathbf{q}_i^b \end{bmatrix} \quad (6)$$

The method for propagating the navigation states is

$$\dot{\hat{\mathbf{x}}} = \begin{bmatrix} \hat{\mathbf{v}}_{b/i}^i \\ \hat{T}_b^i(\hat{\mathbf{q}}_i^b) \left(\hat{\mathbf{a}}^b - \hat{\mathbf{b}}_a \right) + \mathbf{g}^i \\ \frac{1}{2} \begin{bmatrix} 0 \\ \hat{\boldsymbol{\omega}}_{b/i}^b - \hat{\mathbf{b}}_g \\ -\frac{1}{\tau_a} \hat{\mathbf{b}}_a \\ -\frac{1}{\tau_g} \hat{\mathbf{b}}_g \\ \mathbf{0} \end{bmatrix} \otimes \mathbf{q}_i^b \end{bmatrix} \quad (7)$$

The relationship between the navigation state, error state, and the true navigation state is the following

$$\begin{bmatrix} \mathbf{r}_{b/i}^i \\ \mathbf{v}_{b/i}^i \\ \mathbf{q}_i^b \\ \mathbf{b}_a \\ \mathbf{b}_g \\ \mathbf{r}_{c/i}^i \end{bmatrix} = \begin{bmatrix} \hat{\mathbf{r}}_{b/i}^i + \delta \mathbf{r}_{b/i}^i \\ \hat{\mathbf{v}}_{b/i}^i + \delta \mathbf{v}_{b/i}^i \\ \begin{bmatrix} 1 \\ \frac{\delta \boldsymbol{\theta}_b^b}{2} \end{bmatrix} \otimes \hat{\mathbf{q}}_i^b \\ \hat{\mathbf{b}}_a + \delta \mathbf{b}_a \\ \hat{\mathbf{b}}_g + \delta \mathbf{b}_g \\ \hat{\mathbf{r}}_{c/i}^i + \delta \mathbf{r}_{c/i}^i \end{bmatrix} \quad (8)$$

The error injection mapping is the following

$$\begin{bmatrix} \hat{\mathbf{r}}_{b/i}^i \\ \hat{\mathbf{v}}_{b/i}^i \\ \hat{\mathbf{q}}_i^b \\ \hat{\mathbf{b}}_a \\ \hat{\mathbf{b}}_g \\ \hat{\mathbf{r}}_{c/i}^i \end{bmatrix} = \begin{bmatrix} \mathbf{r}_{b/i}^i - \delta \mathbf{r}_{b/i}^i \\ \mathbf{v}_{b/i}^i - \delta \mathbf{v}_{b/i}^i \\ \begin{bmatrix} 1 \\ -\frac{\delta \boldsymbol{\theta}_b^b}{2} \end{bmatrix} \otimes \mathbf{q}_i^b \\ \mathbf{b}_a - \delta \mathbf{b}_a \\ \mathbf{b}_g - \delta \mathbf{b}_g \\ \mathbf{r}_{c/i}^i - \delta \mathbf{r}_{c/i}^i \end{bmatrix} \quad (9)$$

The error calculation mapping is the following, where it is assumed that the quaternion contains the scalar in the first element of a 4 element vector

$$\begin{bmatrix} \delta \mathbf{r}_{b/i}^i \\ \delta \mathbf{v}_{b/i}^i \\ \delta \boldsymbol{\theta}_b^b \\ \delta \mathbf{b}_a \\ \delta \mathbf{b}_g \\ \delta \mathbf{r}_{c/i}^i \end{bmatrix} = \begin{bmatrix} \mathbf{r}_{b/i}^i - \hat{\mathbf{r}}_{b/i}^i \\ \mathbf{v}_{b/i}^i - \hat{\mathbf{v}}_{b/i}^i \\ 2 \begin{bmatrix} 0_{3 \times 1} & I_{3 \times 3} \end{bmatrix} \mathbf{q}_i^b \otimes (\hat{\mathbf{q}}_i^b)^* \\ \mathbf{b}_a - \hat{\mathbf{b}}_a \\ \mathbf{b}_g - \hat{\mathbf{b}}_g \\ \mathbf{r}_{c/i}^i - \hat{\mathbf{r}}_{c/i}^i \end{bmatrix} \quad (10)$$

Finally, the mapping between truth and design states is

$$\begin{bmatrix} \mathbf{r}_{b/i}^i \\ \mathbf{v}_{b/i}^i \\ q_i^b \\ \mathbf{b}_a \\ \mathbf{b}_g \\ \mathbf{r}_{c/i}^i \end{bmatrix} = \begin{bmatrix} \begin{bmatrix} r_{xi} \\ r_{yi} \\ 0 \end{bmatrix} \\ \begin{bmatrix} v_{xb} \cos \psi \\ v_{xb} \sin \psi \\ 0 \end{bmatrix} \\ \cos\left(\frac{\psi}{2}\right) \\ 0 \\ 0 \\ \sin\left(\frac{\psi}{2}\right) \\ \mathbf{b}_a \\ \mathbf{b}_g \\ \mathbf{r}_{c/i}^i \end{bmatrix} \quad (11)$$