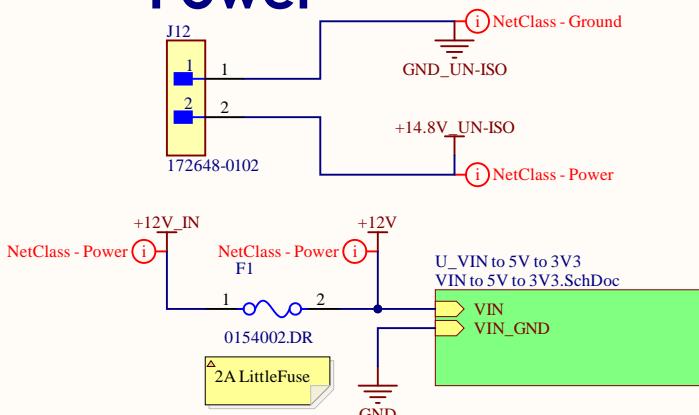
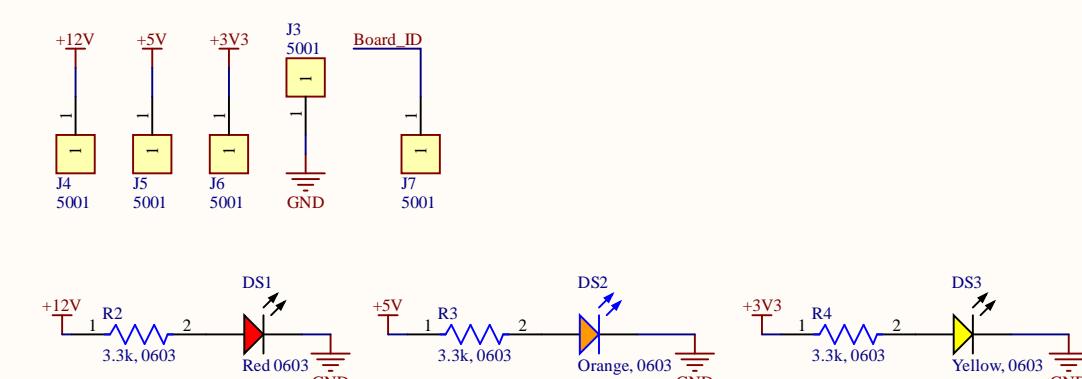


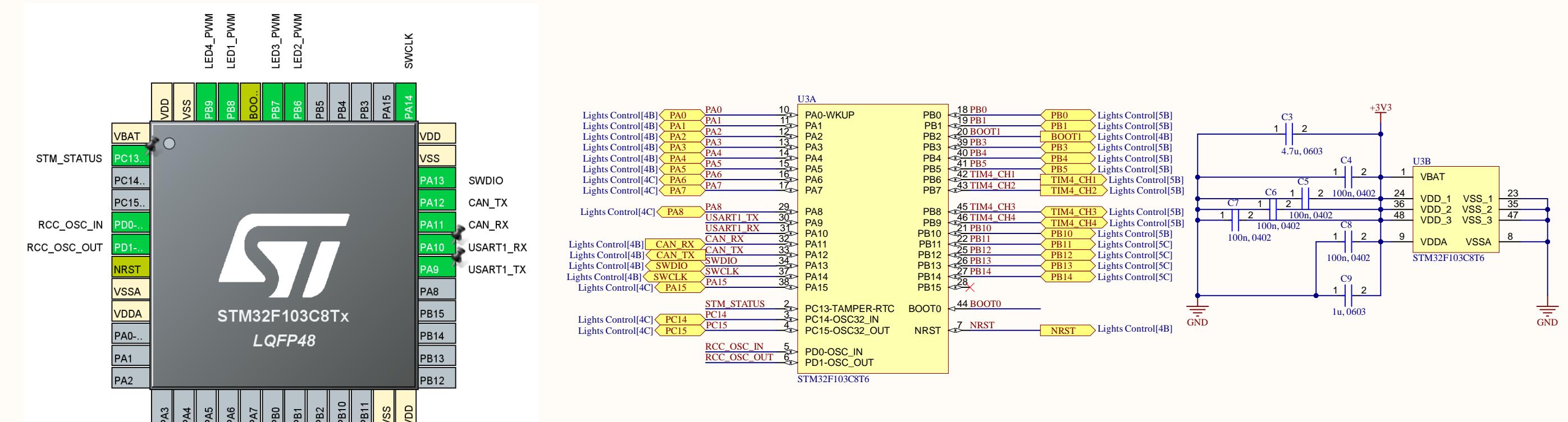
Power



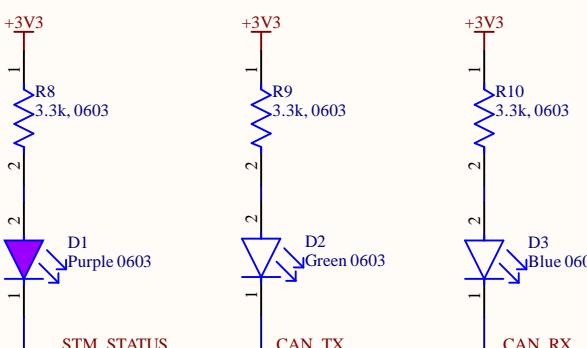
Sanity Checkers



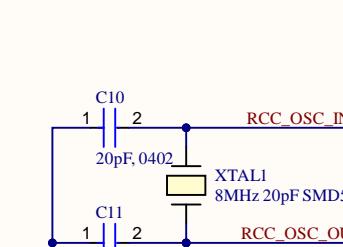
MCU



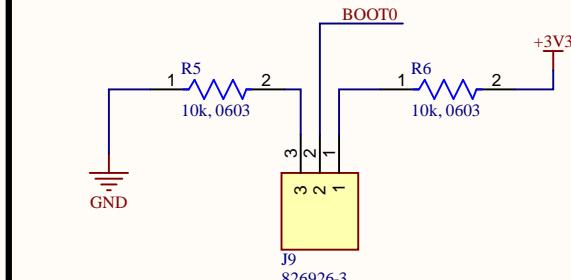
Indicator LEDs



Crystal

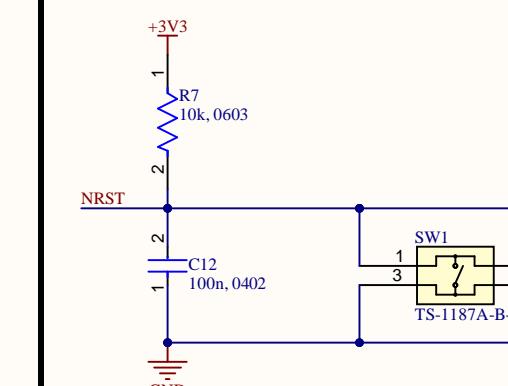


BOOT0 Header



Leave at Floating for normal operation

NRST Circuit

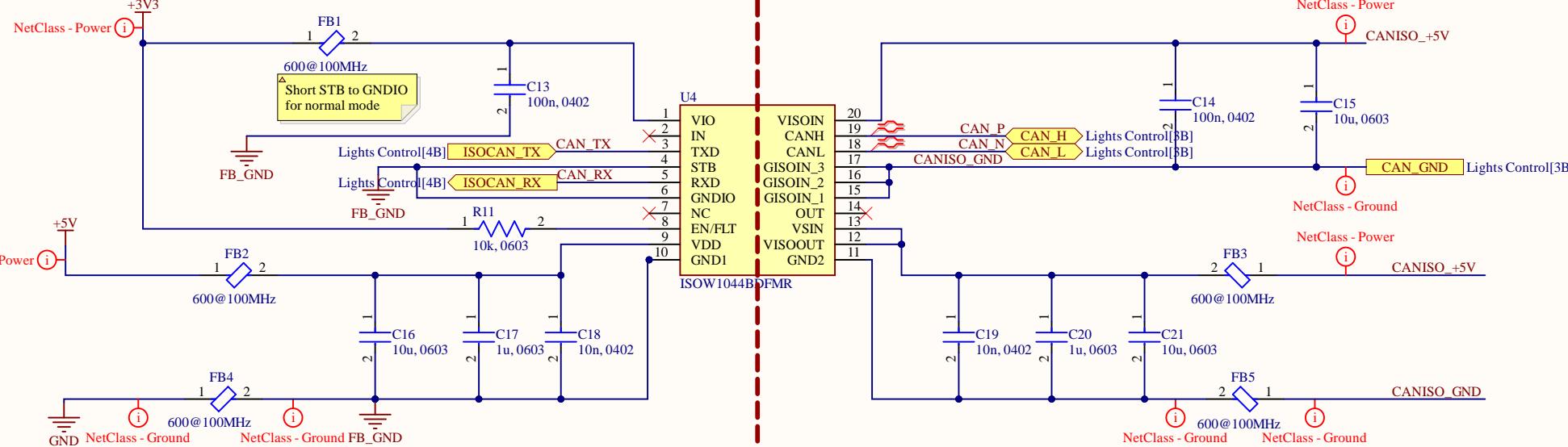


SWD Header

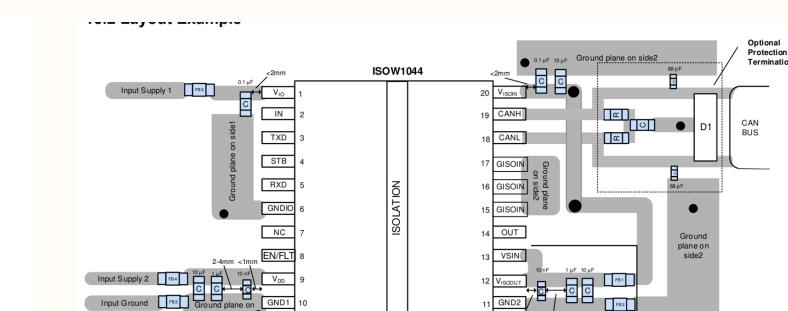
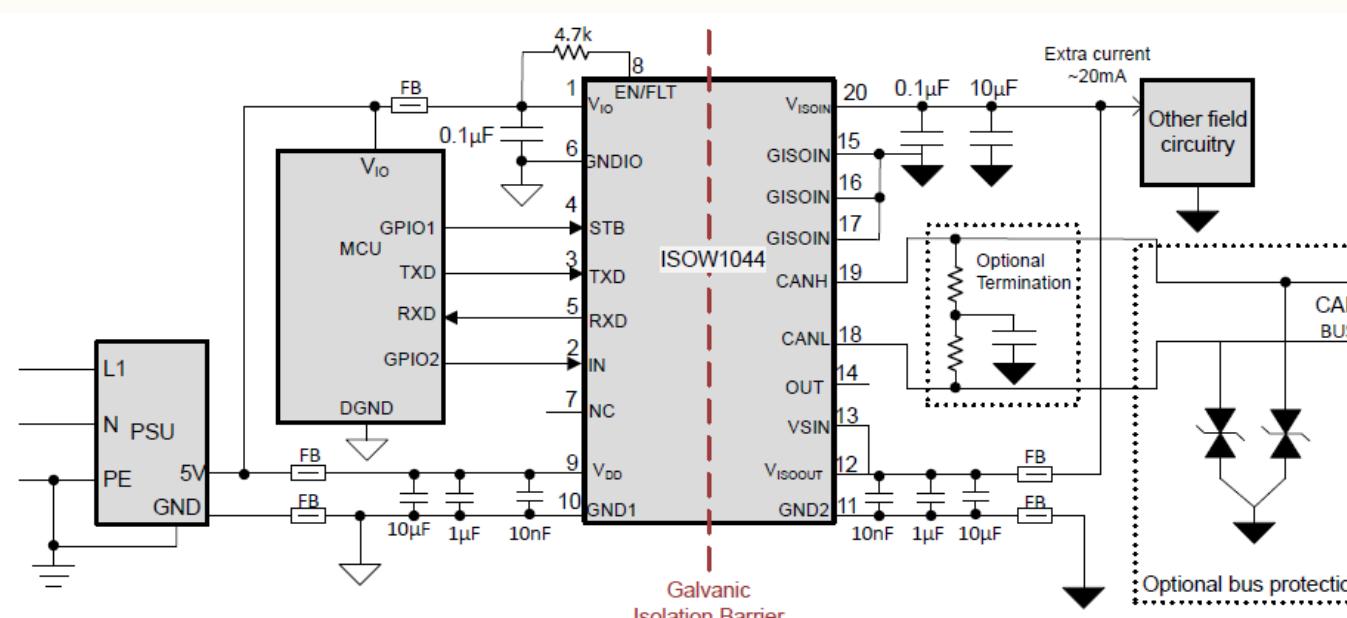


CAN Transceiver + DCDC Isolator

Test Points



Termination

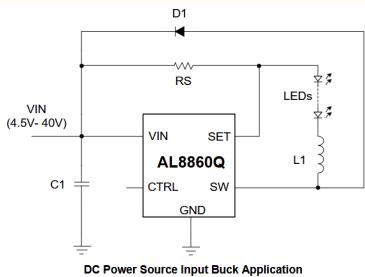


13 Layout 13.1 Layout Guidelines

Figure 11-1 shows the recommended placement and routing of device bypass capacitors. Below guidelines must be followed to achieve low emissions design:

- High frequency bypass capacitors 10 nF must be placed close to **V_{DD}** and **V_{ISOOUT}** pins, within 1 mm distance away from device pins. This is very essential for optimised radiated emissions performance. Ensure that these capacitors are 0402 size so that they offer least inductance (ESL).
- Bulk capacitors of atleast 10 µF must be placed on power converter input (**V_{DD}**) and output (**V_{ISOOUT}**) supply pins after the 10 nF capacitor with a distance of 2 - 4 mm, as shown in Layout Example.
- Traces on **V_{DD}** and **GND1** must be symmetric till bypass capacitors. Similarly traces on **V_{ISOOUT}** and **GND2** must be symmetric.
- Place two 0402 size Ferrite beads (Part number: BLM15EX331SN1) on power supply pins, one between **V_{ISOOUT}** and **V_{DD}** and the other between **GND2** (pin 11) and **GND1** (pin 15), as shown in example PCB layout, so that any high frequency noise from power converter output sees a high impedance before it goes to other components on PCB.
- Do not have any metal traces or ground pour within 4 mm of power converter output terminals **V_{ISOOUT}** (pin 12) and **GND2** (pin 11).
- Place the CAN BUS protection and filtering circuitry close to the bus connector to prevent transients, ESD, and noise from propagating onto the board. This layout example shows an optional transient voltage suppression (TVS) diode, **D1**, which may be implemented if the system-level requirements exceed the specified rating of the transmitter. This example also shows two optional 68pF bus filter capacitors.
- Common mode choke or ferrite beads on bus terminals (CANH/CANL) can minimise any high frequency noise that can couple of CAN bus cable which can act as antenna and amplify that noise. This will improve Radiated emissions performance at a system level.
- Following the layout guidelines of EVM as much as possible is highly recommended for a low radiated emissions design. EVM Link is available in [Related Documentation](#).

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A Pin Descriptions

Pin Number	Pin Name	Function
1	SET	Connect resistor R_s from this pin to VIN to define nominal average output current: $I_{OUT_NOM} = 0.1/R_s$
2, 3	GND	Ground
4	CTRL	Multi-function On/Off and brightness control pin: • Leave floating for normal operation. • Drive voltage below 0.2V to turn off output current. • Drive with DC voltage (0.3V < V_{CTRL} < 2.5V) to adjust output current from 0 to 100% of I_{OUT_NOM} . Linear adjustment ranges from 5% to 100% of I_{OUT_NOM} • Drive with PWM signal from open-collector or open-drain transistor to adjust output current. Linear adjustment ranges from 1% to 100% of I_{OUT_NOM} for $f < 500\text{Hz}$ • Connect a capacitor from this pin to ground to increase soft-start time. (Default soft-start time = 0.1ms. Additional soft-start time is approximately 1.5ms/1nF)
5, 6	SW	Drain of NDMOS switch.
7	N/C	No Connection.
8	VIN	Input voltage (4.5V to 40V). Decouple to ground with 10μF or higher X7R ceramic capacitor close to device.
EP	EP	Exposed pad. Connect to GND and thermal mass for enhanced thermal impedance. Should not be used as electrical ground conduction path.

B LED Current Configuration

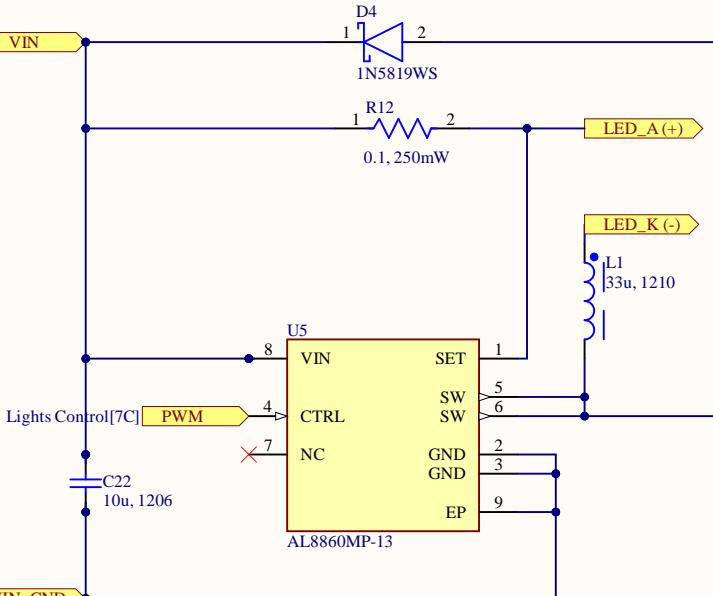
The nominal average output current in the LED(s) is determined by the value of the external current sense resistor (R_s) connected between VIN and SET and is given by:

$$I_{OUT(NOM)} = \frac{0.1}{R_s}$$

The table below gives values of nominal average output current for several preferred values of current setting resistor (R_s) in the typical application circuit shown on page 2.

R_s (Ω)	Nominal Average Output Current (mA)
0.066	1500
0.1	1000
0.13	760
0.15	667
0.3	333

Lights Control[7C], Digital Isolator[2C]



C Inductor Selection

Recommended inductor value for the AL8860 are in the range 33μH to 100μH. Higher inductance are recommended at higher supply voltages in order to minimize output current tolerance due to switching delays, which will result in increased ripple and lower efficiency. Higher inductance also results in a better line regulation. The inductor should be mounted as close to the device as possible with low resistance connections to SW pins.

The chosen coil should have saturation current higher than the peak output current and a continuous current rating above the required mean output current.

The inductor value should be chosen to maintain operating duty cycle and switch 'on/off' times within the specified limits over the supply voltage and load current range. The following equations can be used as a guide.

SW Switch 'On' time

$$t_{ON} = \frac{L \Delta I}{V_{IN} - V_{LED} - I_{LED}(R_s + R_L + R_{sw})}$$

SW Switch 'Off' time

$$t_{OFF} = \frac{L \Delta I}{V_{LED} + V_D + I_{LED}(R_s + R_L)}$$

Where: L is the coil inductance; R_L is the coil resistance; R_s is the current sense resistance; I_{LED} is the required LED current; ΔI is the coil peak-peak ripple current (Internally set to 0.40 x I_{LED}); V_{IN} is the supply voltage; V_{LED} is the total LED forward voltage; R_{sw} is the switch resistance (0.3Ω nominal); V_D is the diode forward voltage at the required load current.

D Title

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A

B

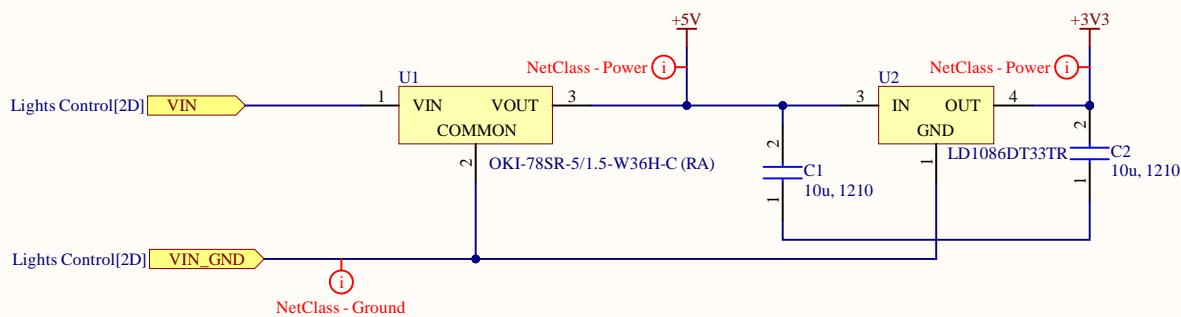
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C

C

D

D



Title

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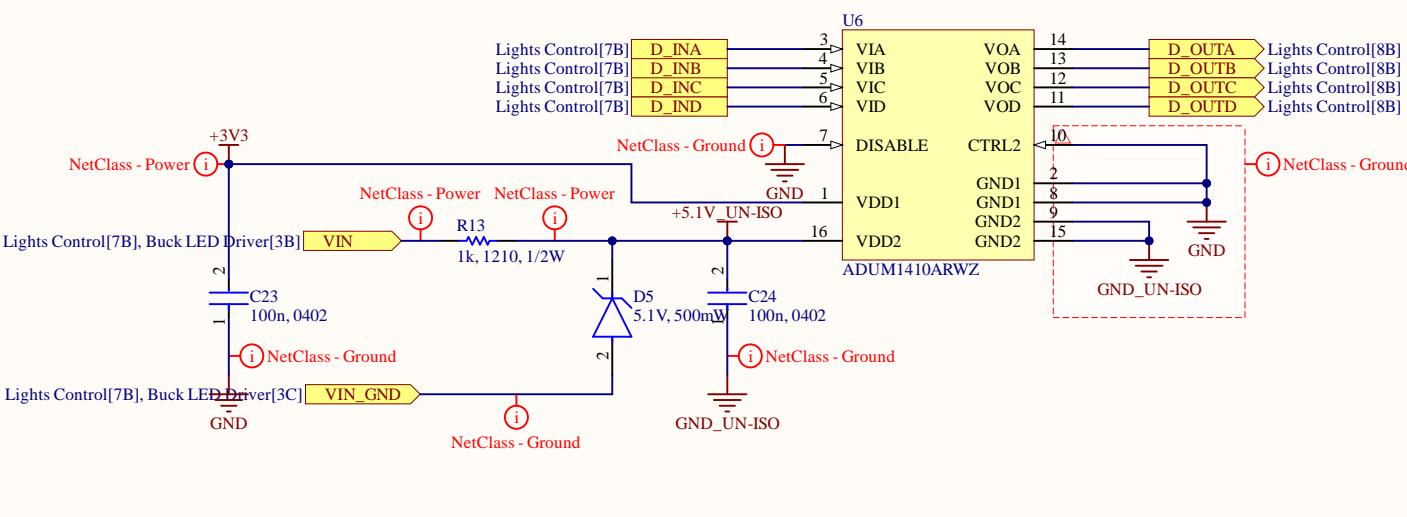
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Type	Marking	Zener Voltage Range ⁽¹⁾			Dynamic Impedance (at I_{zT})	Reverse Current		
		V_{zT} (at I_{zT})		I_{zT}		I_R		
		Min (V)	Nom (V)	Max (V)		(mA)	Max (μA)	
BZT52C2V0	WY	1.8	2.0	2.15	5	100	120	0.5
BZT52C2V2	WZ	2.08	2.2	2.33	5	100	120	0.7
BZT52C2V4	WX	2.28	2.4	2.56	5	100	120	1
BZT52C2V7	W1	2.5	2.7	2.9	5	110	120	1
BZT52C3V0	W2	2.8	3.0	3.2	5	120	50	1
BZT52C3V3	W3	3.1	3.3	3.5	5	130	20	1
BZT52C3V6	W4	3.4	3.6	3.8	5	130	10	1
BZT52C3V9	W5	3.7	3.9	4.1	5	130	5	1
BZT52C4V3	W6	4	4.3	4.6	5	130	5	1
BZT52C4V7	W7	4.4	4.7	5	5	130	2	1
BZT52C5V1	W8	4.8	5.1	5.4	5	130	2	1.5

https://www.lcsc.com/datasheet/lcsc_datasheet_2407261727_MDD-Microdiode-Semiconductor-BZT52C5V1_C173407.pdf



ADuM1410, Total Supply Current, Four Channels ¹				
DC to 2 Mbps				
V_{DD1} Supply Current 5 V/3 V Operation	$I_{DD1(5)} = 2.4$	mA	DC to 1 MHz logic signal frequency	
3 V/5 V Operation	$I_{DD1(3)} = 1.2$	mA	DC to 1 MHz logic signal frequency	
V_{DD2} Supply Current 5 V/3 V Operation	$I_{DD2(5)} = 0.8$	mA	DC to 1 MHz logic signal frequency	
3 V/5 V Operation	$I_{DD2(3)} = 1.2$	mA	DC to 1 MHz logic signal frequency	

https://www.lcsc.com/datasheet/lcsc_datasheet_1811011923_Analog-Devices-ADUM1410ARWZ-RL_C19052.pdf

¹ Reference: https://electronicsreference.com/analog/zener_diode_regulator/
For digital isolator power supply,
Using 500mW 5.1V zener diode,
 $I_{max} = P_{max} / V_z = 500mW / 5.1V = 98.03mA$
 $R_{batt, nominal} = 14.8V, no load$
 $R_{min} = (V_{in} - V_z) / I_{max} = (14.8V - 5.1V) / 68.6mA = 0.10k\Omega$
 $R_{max} = (V_{in} - V_z) / I_{min} = (14.8V - 5.1V) / (5mA) = 1.94k\Omega$
With load,
 $I_{min} = I_{zT} + I_{load} = 5mA + 1.6mA = 6.6mA$
 $R_{max} = (V_{in} - V_z) / I_{min} = 14.8V - 5.1V / 6.6mA = 1.46k\Omega$
 $R_{max} = 1.46k\Omega < R < R_{min} = 0.10k\Omega$
Chosen $R = 1k\Omega$, verify
 $I_{max, 1k} = (V_{in, max} - V_z) / R_{chosen} = (16.8 - 5.1) / 1k\Omega = 11.7mA > I_{min}$
 $I_{min, 1k} = (V_{in, min} - V_z) / R_{chosen} = (14.8 - 5.1) / 1k\Omega = 9.7mA > I_{min}$
Calculate max power dissipation across resistor:
 $P_{max} = I^2R = 11.7mA^2 \times 1k\Omega = 136.89mA$

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