

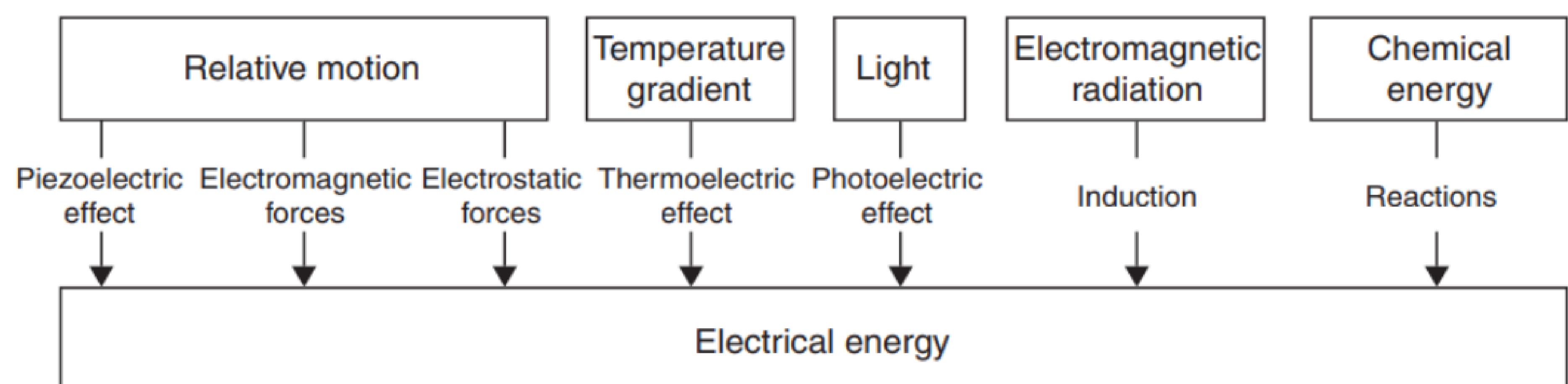
- ME (Mechanical-to elec) -> turbine → Piezo, electro
- CE (Chemical..) -> battery, fuel cell
- SE (Solar..) -> PV/SH
- RFE (Radio Frequency..) -> electromagnetic energy to elec
- TE (Thermal..) -> TEG

- Direct force
- Inertial force

- Seebeck :  $T \rightarrow e'$
- Peltier :  $e' \rightarrow T$

- Resonant
- Non-resonant

- Battery
- Fuel cell



Gas Law Formula		
Gas Law	Formula	Description
Boyle's Law	$PV_1 = P_2V_2$	At constant $T$ , as pressure increases, volume decreases.
Charles' Law	$\frac{V_1}{T_1} = \frac{V_2}{T_2}$	At constant $P$ , as volume increases, temperature increases.
Gay-Lussac's Law	$\frac{P_1}{T_1} = \frac{P_2}{T_2}$	At constant $V$ , as pressure increases, temperature increases.
Combined Law	$\frac{PV_1}{T_1} = \frac{P_2V_2}{T_2}$	Obtained by combining Boyle's Law, Charles' Law and Gay-Lussac's Law.
Ideal Gas Law	$PV = nRT$	$P = \rho \frac{M}{RT}$ molar mass $\frac{m}{n}$
V = volume in dm³ (litre)		
T = temperature in K		
P = pressure in kPa		R = ideal gas constant 0.0821 $\frac{\text{L} \cdot \text{atm}}{\text{mol} \cdot \text{K}}$
n = number of moles		

$$\text{Avogadro} \quad \frac{V_1}{n_1} = \frac{V_2}{n_2}$$

$$\eta_c = \frac{T_h - T_c}{T_h} \cdot T_c$$

$$\eta_{th} = \frac{w_{net}}{q_{in}} = 1 - \frac{q_{out}}{q_{in}}$$

absorbed solar radiation ( $S$ ) using:

$$S = G_T \times (\tau\alpha)_{av}$$

useful energy gain ( $\dot{Q}_u$ ) using:

$$\dot{Q}_u = A_c \times F_R \times [S - U_L(T_{in} - T_{amb})]$$

the outlet temperature ( $T_{out}$ ) of the working fluid using:

$$T_{out} = T_{in} + \frac{\dot{Q}_u}{\dot{m}c_p}$$

thermal efficiency ( $\eta$ ) of the collector:

$$\eta = \frac{\dot{Q}_u}{A_c G_T}$$

$$C_{geo} = \frac{A_a}{A_r}$$

$$U_L = \dot{Q}_s = \eta_0 \times A_a \times I_0 \times \text{heat transfer efficiency}$$

$$U = \bar{Q} + \bar{W}$$

internal energy

heat

work

$$Q = \int C dT \Rightarrow C \cdot \Delta T$$

$$W = P \cdot \Delta V$$

$\Delta V = 0 \Rightarrow \text{no work}$

$$ZT = (S^2 \sigma / \kappa_e + \kappa_L) T$$

$$\eta = \frac{P}{Q} = \frac{\Delta T}{T_H} \left( \frac{\sqrt{1+ZT}-1}{\sqrt{1+ZT}+\frac{T_C}{T_H}} \right)$$

$$P_{max} = \frac{(S\Delta T)^2}{4R} = \frac{(S\Delta T)^2 A}{4\rho L} \quad P_{max} = \frac{V_{oc}^2}{4R} = \frac{(n(S_p + S_n)\Delta T)^2}{4R}$$

The output power of the device ( $P_L$ ) can be expressed as:

$$P_L = P = \frac{V_L^2}{R_L} = \frac{\left(\frac{R_L V_{oc}}{R_L + R_L}\right)^2}{R_L}$$

$$P_{max} = \frac{V_{oc}^2}{4R} = \frac{(n(S_p + S_n)\Delta T)^2}{4R}$$

$$\text{Power} = \frac{1}{2} \rho A U^3 = \frac{1}{2} \rho \pi R^2 U^3$$

Friis Eq

$$P_R = P_T \cdot G_T \cdot G_R \left( \frac{d}{\lambda \pi d} \right)^2$$

$\tau$ : Transmitted  
 $\epsilon$ : received  
 $P$ : power (W)  
 $G$ : Antenna gains  
 $d$ : distance

# Thermal

- Thermal  $\rightarrow$  Kinetic  $E$  of molecules
  - $\text{total}$
  - Particle / vibration
  - rotational
  - move / translational
- Temp  $\rightarrow$  avg kin.  $E$  per particle
- Heat  $E \rightarrow$  amount of Thermal  $E$  transferred

## Law of thermodyn

- 0<sup>th</sup>  $\rightarrow$  temp.
- 1<sup>st</sup>  $\rightarrow$   $U = \bar{Q} + \bar{W}$ 
  - internal energy
  - heat
  - work $Q = \int C dT \rightarrow \Delta T$ 
 $W = P \cdot \Delta V$ 
 $\Delta V = 0 \rightarrow \text{no work}$
- 2<sup>nd</sup>  $\rightarrow$  phases (solid  $\rightarrow$  liq  $\rightarrow$  gas)
  - temperature
  - chaotic
- 3<sup>rd</sup>  $\rightarrow T = 0 \text{ K} \rightarrow$  absolute zero entropy

System type

- open  $\rightarrow$  mass &  $E$  transfer
- closed  $\rightarrow$  only  $E$  transfer
- isolated  $\rightarrow$  no transfer

between syst & surroundings

Path dependent properties?

Approach

- macro  $\rightarrow P \cdot T \cdot V \cdot n \cdot m$
- micro

## state

$$V = f(n, p, T) \text{ or } p = g(n, V, T)$$

3 H<sub>2</sub>(g, 1 bar, 100 °C)

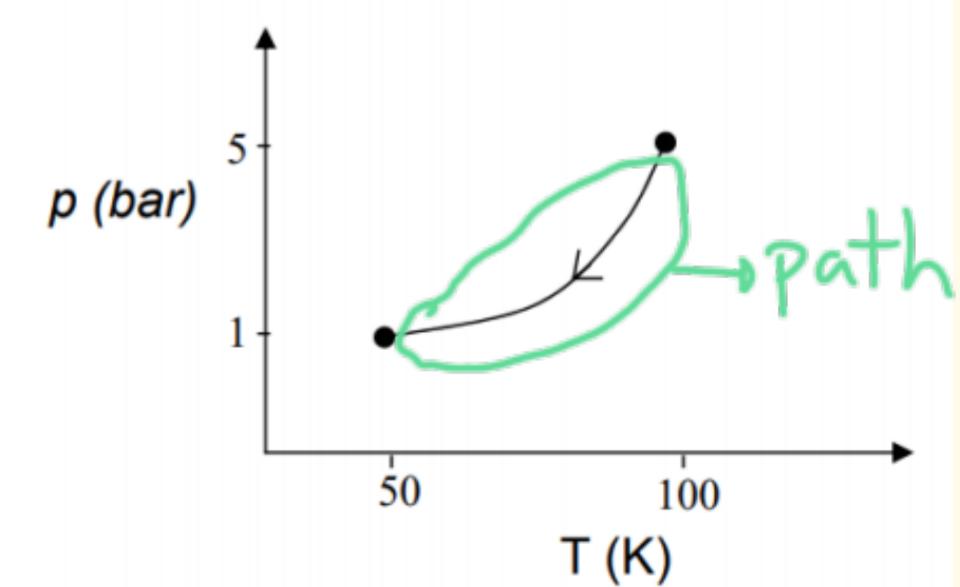
- 3 moles (n=3)
- gas
- p=1 bar
- T=100 °C

Change of state or Transformation

Notation:

$$\underbrace{3 \text{ H}_2(\text{g}, 5 \text{ bar}, 100^\circ\text{C})}_{\text{initial state}} = \underbrace{3 \text{ H}_2(\text{g}, 1 \text{ bar}, 50^\circ\text{C})}_{\text{final state}}$$

Path: Sequence of intermediate states



Process: Describes the Path

- ❖ Reversible (always in Equilibrium) water  $\longleftrightarrow$  ice
- ❖ Irreversible (defines direction of time) wood  $\rightarrow$  ash
- ❖ Adiabatic (no heat transfer between system and surroundings)  $\rightarrow Q=0$
- ❖ Isobaric (constant pressure)  $\rightarrow W+Q$
- ❖ Isothermal (constant temperature)  $\Delta T=0 \rightarrow Q=0$
- ❖ Isochoric (constant volume)  $\Delta V=0 \rightarrow W=0$

### Gas Law Formula

Gas Law	Formula	Description
<b>Boyle's Law</b>	$P_1V_1 = P_2V_2$	At constant $T$ , as pressure increases, volume decreases.
<b>Charles' Law</b>	$\frac{V_1}{T_1} = \frac{V_2}{T_2}$	At constant $P$ , as volume increases, temperature increases.
<b>Gay-Lussac's Law</b>	$\frac{P_1}{T_1} = \frac{P_2}{T_2}$	At constant $V$ , as pressure increases, temperature increases.
<b>Combined Law</b>	$\frac{P_1V_1}{T_1} = \frac{P_2V_2}{T_2}$	Obtained by combining Boyle's Law, Charles' Law and Gay-Lussac's Law.
<b>Ideal Gas Law</b>	$PV = nRT$	$P = \frac{nR}{V}$ molar mass $\frac{m}{n}$
$V$ = volume in $\text{dm}^3$ (litre) $T$ = temperature in K	$P$ = pressure in kPa $n$ = number of moles	$R$ = ideal gas constant $0.0821 \frac{\text{L} \cdot \text{atm}}{\text{mol} \cdot \text{K}}$

Avogadro  $\frac{V_1}{n_1} = \frac{V_2}{n_2}$

①  $2.02 \cancel{\text{atm}}$

②  $12.93 \text{ L}$

$$P = \frac{m}{V} \rightarrow P = \frac{F}{A}$$

$$\frac{F}{V \cdot A} =$$

# Thermal E

Parameter  $\rightarrow$  figure of merit  
efficiency

$$ZT = (S^2 \sigma / \kappa_e + \kappa_L) T$$

$$\eta = \frac{P}{Q} = \frac{\Delta T}{T_H} \left( \frac{\sqrt{1+ZT}-1}{\sqrt{1+ZT}+\frac{T_C}{T_H}} \right)$$

$$P_{max} = \frac{(S\Delta T)^2}{4R} = \frac{(S\Delta T)^2 A}{4\rho L}$$

$$P_{max} = \frac{V_{oc}^2}{4R} = \frac{(n(S_p + |S_n|)\Delta T)^2}{4R}$$

The output power of the device ( $P_L$ ) can be expressed as:

$$P_L = P = \frac{V_L^2}{R_L} = \frac{\left(\frac{R_L V_{oc}}{R + R_L}\right)^2}{R_L}$$

$$P_{max} = \frac{V_{oc}^2}{4R} = \frac{(n(S_p + |S_n|)\Delta T)^2}{4R}$$

Design a small thermoelectric generator to power a wearable health monitoring device using the temperature difference between the human body and the ambient environment.

Example calculation: Assume the body temperature is 37°C and the ambient temperature is 20°C. Design a TEG with a footprint of 5 cm<sup>2</sup> and a thickness of 5 mm to generate sufficient power to run the wearable device.

1. To design the TEG, we need to consider the following factors: Temperature difference:  $\Delta T = 37^\circ\text{C} - 20^\circ\text{C} = 17^\circ\text{C}$
2. Thermoelectric material properties: Seebeck coefficient, electrical resistivity, thermal conductivity
3. Geometric dimensions: cross-sectional area and length of the thermoelectric elements.
4. Using the

Group Session W3.docx - Word

File Home Insert Developer Draw Design Layout References Mailings Review View Developer Zotero Help Tell me what you want to do

AaBbCcDc AaBbCcCc AaBbCcCc AaBbCcCc

Normal No Spac... Heading 1 Heading 2 Title

Styles

Group Session

Thursday, 20<sup>th</sup> February 2025

A GPS tracking sensor requires 100 mW (0.1 W) of continuous power. A thermoelectric generator (TEG) will be used, utilizing a hot surface at 150°C and a cold side at 50°C.

Design a thermoelectric generator (TEG) to meet this requirement, considering:

1. Material selection (using Bismuth Telluride, Bi<sub>2</sub>Te<sub>3</sub>).
2. Number of thermocouples needed.
3. Leg sizing (length  $L$  and cross-section  $A$ ).
4. Required heat input.

Page 1 of 1 71 words English (Indonesia)

Sample calculation: Consider a TEG with a temperature difference of 200°C, a cross-sectional area of 10 cm<sup>2</sup>, and a length of 2 cm. Assume the thermoelectric material has a Seebeck coefficient of 200 µV/K, an electrical resistivity of 1 × 10<sup>-5</sup> Ω·m, and a thermal conductivity of 1.5 W/m·K. Calculate the power output of the TEG ([Bell, 2008](#)) ([Yazawa & Shakouri, 2011](#)).

S	0.0002	P	2
T	200		
A	0.001		
L	0.02		
elec rest	0.00001		
k	1.5		
		=	(B22*B23)^2*B24/(4*B26*B25)

Determine the conversion efficiency of a thermoelectric generator given the material's figure of merit and the temperature difference between the hot and cold sides.

Consider a thermoelectric material with a figure of merit,  $ZT$ , of 1.0. The hot-side temperature is 600 K, and the cold-side temperature is 300 K. Calculate the maximum theoretical efficiency of a thermoelectric generator using this material.

$$\eta = \frac{P}{Q} = \frac{\Delta T}{T_H} \left( \frac{\sqrt{1+ZT}-1}{\sqrt{1+ZT}+\frac{T_C}{T_H}} \right)$$

ZT	1	Eff	0.10819
Th	600	Carnot	0.5
Tc	300		
		=	((B30-B31)/B30)*(((1+B29)^(1/2)-1)/((1+B29)^(1/2)+(B31/B30)))

## WEEK 4

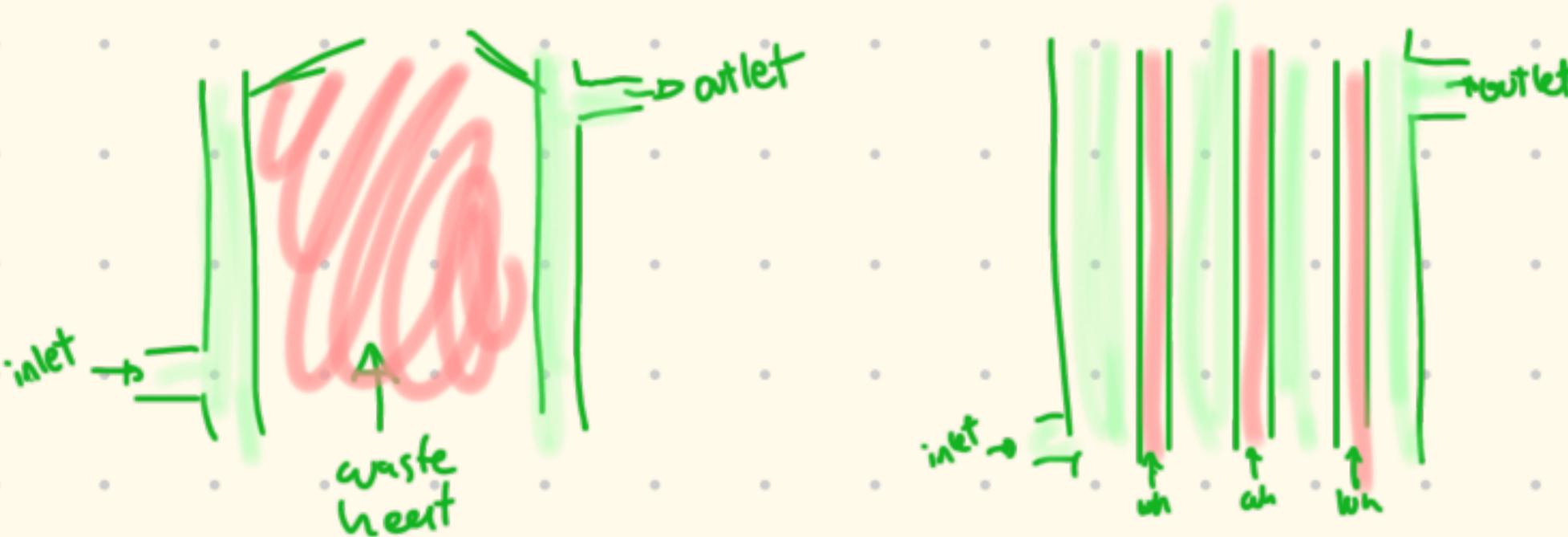
Type  
high  
med  
low

Tech  
heat ex  
 TEG  
 Org. rankine cycle  
 TPV  
 Piezo electric gen

Heat ex

• Recuperator area of flow

radiation convective



• Regeneration

• Organic rankine cycle

$$(q_{in} - q_{out}) + (w_{in} - w_{out}) = h_e - h_i$$

$$\text{Pump } (q = 0): \quad w_{\text{pump,in}} = h_2 - h_1$$

or,

$$w_{\text{pump,in}} = v(P_2 - P_1)$$

where

$$h_1 = h_f @ P_1 \quad \text{and} \quad v \cong v_1 = v_f @ P_1$$

$$\text{Boiler } (w = 0): \quad q_{in} = h_3 - h_2$$

$$\text{Turbine } (q = 0): \quad w_{\text{turb,out}} = h_3 - h_4$$

$$\text{Condenser } (w = 0): \quad q_{out} = h_4 - h_1$$

$$\eta_{th} = \frac{w_{net}}{q_{in}} = 1 - \frac{q_{out}}{q_{in}}$$

$$w_{net} = q_{in} - q_{out} = w_{\text{turb,out}} - w_{\text{pump,in}}$$

# Solar Thermal

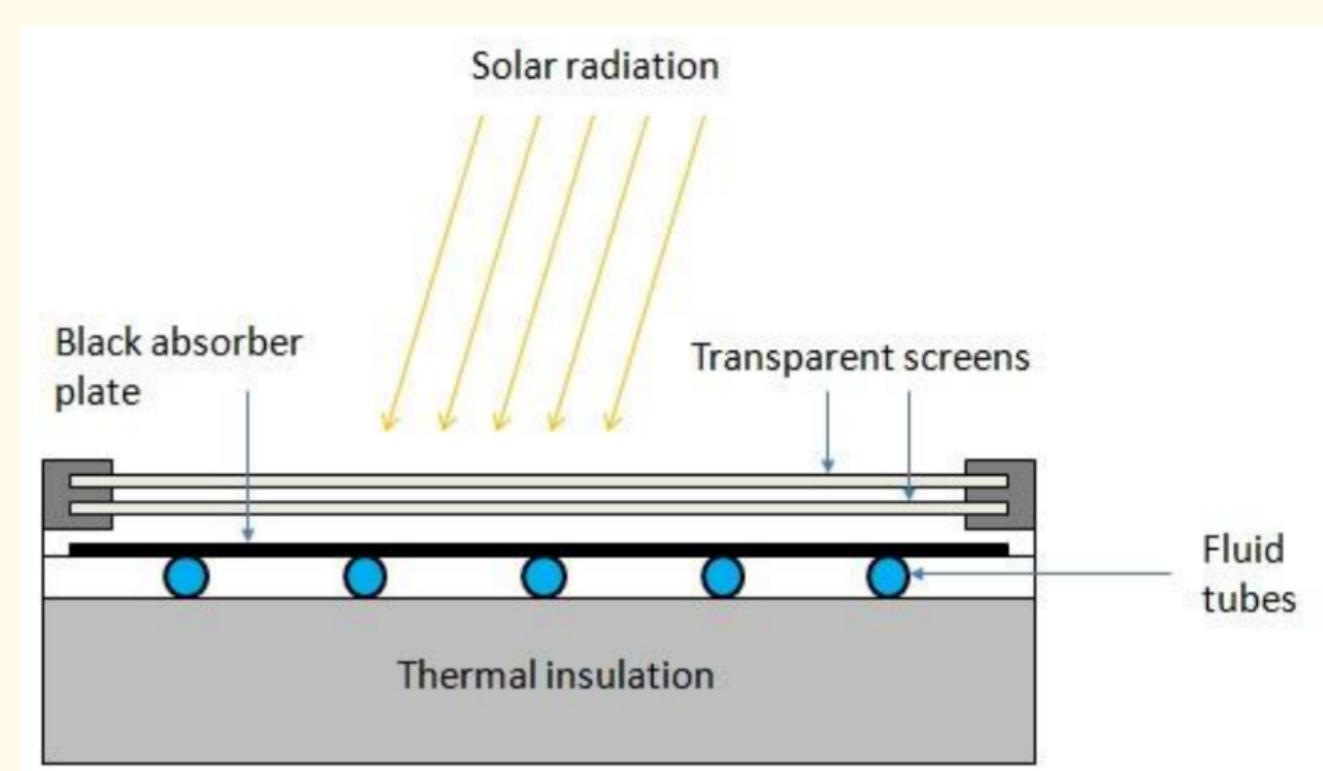
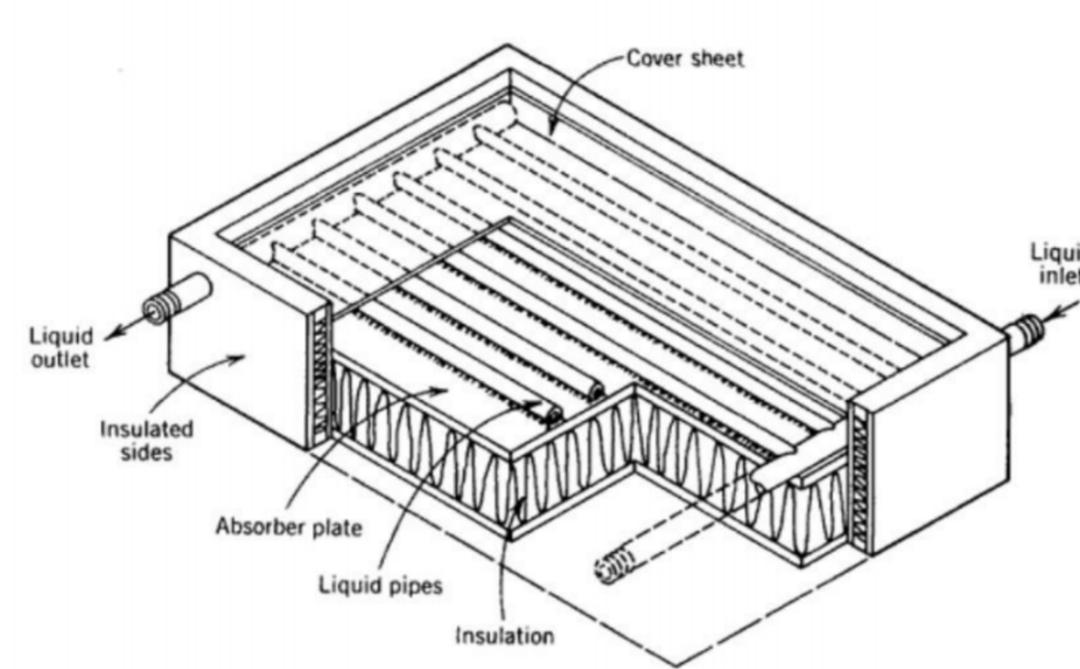
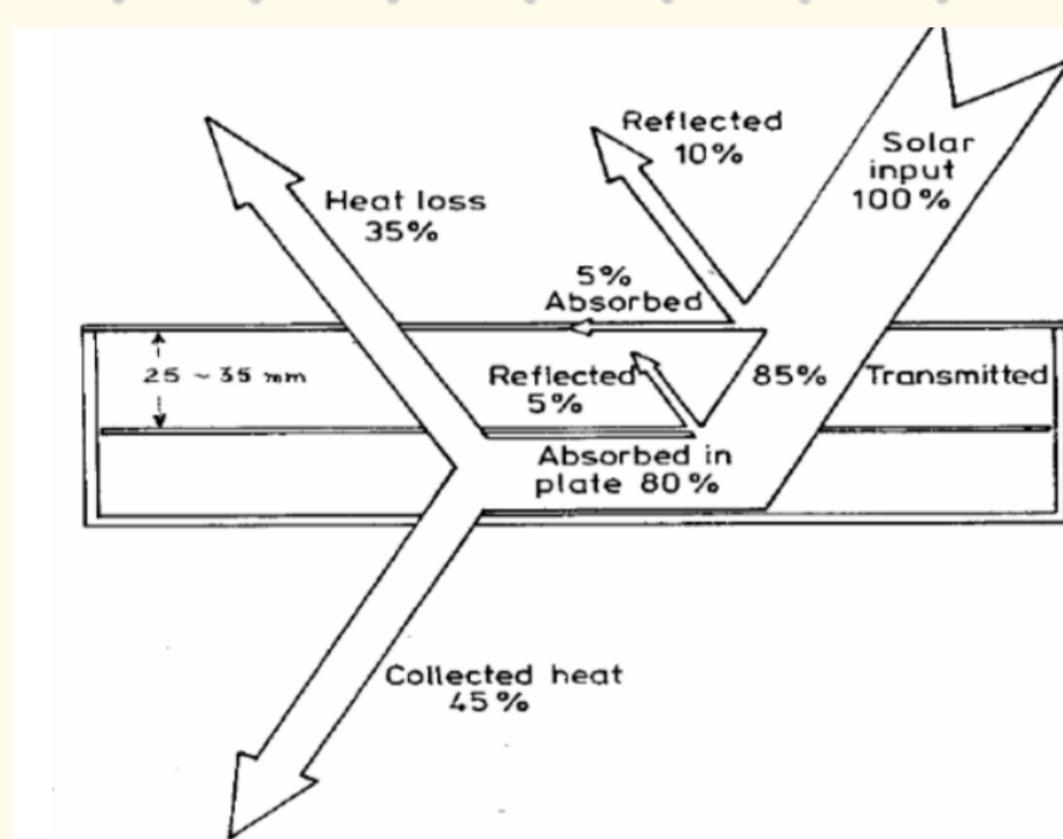
ST Application = heating, elect processed w/ TEP)

Mechanism { conduction → solid  
convection → fluid  
radiation → no medium

Type { w/o concentration → surface colc → tube colc  
→ 80 - 150 °C  
Concentrated → 300 - 500 °C

## Flat Plate Collectors (FPC)

in winter, usually 'Anti-Freeze Agent' is added so the working fluid will not freeze up.



# Wind & hydro

## Wind variability properties

- Turbulence intensity
- Turbulent kinetic energy
- Autocorrelation
- Integral time scale/length scale
- Power spectral density function

• wind speed & direction

• wind turbine turbines

- vortex-induced vibration
- galloping (transverse & wake)
- flutter
- turbulence-induced vibration

## Hydro

- ballistic electrostatic: droplet's inertia to electricity
- Small-Scale Windmill and Wind Turbine.
- Energy Harvesters Based on Vortex-Induced Vibrations
- Energy Harvesters Based on Galloping
- Energy Harvesters Based on Flutter (Model vs Cross-flow)
- 
- 

Technology analysis -

Pilih 1 tech. jelaskan teknik detail

