Hydrostatic, ideal-gas reference states in spherical coordinates

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1 Basic assumptions

We wish to derive the thermodynamic state for an ideal, hydrostatic gas in spherical coordinates, assuming a known specific entropy stratification $\overline{S}(r)$ and gravitational acceleration $g(r)$. In keeping with the convention used in, e.g., `Rayleigh` and `ASH`, we will denote the thermal profiles of this reference state using overbars. In mathematical terms, we have:

$$\frac{d\overline{P}}{dr} = -\overline{\rho}(r)g(r) \qquad \text{(hydrostatic balance)}, \tag{1}$$

$$\text{and} \qquad \overline{P}(r) = \overline{\rho}(r)\mathcal{R}\overline{T}(r) \qquad \text{(ideal gas law)}. \tag{2}$$

Here, $\overline{P}(r)$ is the pressure, $\overline{\rho}(r)$ the density, $\overline{T}(r)$ the temperature, and $\mathcal{R}$ the gas constant. We further assume that the number of degrees of freedom (d.o.f.) is constant throughout, so that $\mathcal{R}$ is independent of radius. We note the relationship between the specific heats for an ideal gas:

$$c_\mathrm{p} = \Gamma_1 c_\mathrm{v} = \frac{\Gamma_1 \mathcal{R}}{\Gamma_1 - 1}, \tag{3}$$

where $\Gamma_1 := c_\mathrm{p}/c_\mathrm{v}$.

We note the First Law of Thermodynamics for the radial thermodynamic gradients (easiest starting point is $\overline{T}d\overline{S} = c_\mathrm{v}d\overline{T} - (\overline{P}/\overline{\rho}^2)d\overline{\rho}$):

$$\frac{1}{c_\mathrm{v}}\frac{d\overline{S}}{dr} = \frac{d\ln\overline{T}}{dr} - (\Gamma_1 - 1)\frac{d\ln\overline{\rho}}{dr}. \tag{4}$$

Differentiating the ideal gas law (2) gives

$$\frac{d\ln\overline{T}}{dr} = \frac{d\ln\rho}{dr} + \frac{d\ln T}{dr}. \tag{5}$$

Combining Equations (4) and (5) yields the following useful forms of the First Law:

$$\frac{1}{c_\mathrm{p}}\frac{d\overline{S}}{dr} = \frac{1}{\Gamma_1}\frac{d\ln\overline{T}}{dr} - \frac{\Gamma_1 - 1}{\Gamma_1}\frac{d\ln\overline{\rho}}{dr} \tag{6a}$$

$$= \frac{1}{\Gamma_1} \frac{d \ln \overline{P}}{dr} - \frac{d \ln \overline{\rho}}{dr} \tag{6b}$$

$$= \frac{d \ln \overline{T}}{dr} - \frac{\Gamma_1 - 1}{\Gamma_1} \frac{d \ln \overline{P}}{dr} \tag{6c}$$

Using Equations (3) and (6), we can derive an ordinary differential equation for the temperature:

$$\boxed{\frac{d\overline{T}}{dr} - \left[\frac{1}{c_{\mathrm{p}}} \frac{d\overline{S}}{dr} \right] \overline{T}(r) = -\frac{g(r)}{c_{\mathrm{p}}}.} \tag{7}$$

We can solve Equation (7) via integrating factors, yielding

$$\overline{T}(r) = -\frac{e^{\overline{S}(r)/c_{\mathrm{p}}}}{c_{\mathrm{p}}} \int_{r_0}^{r} g(x) e^{-\overline{S}(x)/c_{\mathrm{p}}} dx + \overline{T}_0 e^{[\overline{S}(x) - \overline{S}_0]/c_{\mathrm{p}}} \tag{8}$$

Here, we have defined r_0 as an arbitrary radius from which to start the integration. Accordingly, we define the temperature, pressure, density, and entropy at r_0 as $\overline{T}_0$, $\overline{P}_0$, $\overline{\rho}_0$, and $\overline{S}_0$, respectively.

Note that in equation (8), adding a constant σ to the entropy ($\overline{S} \longrightarrow \overline{S} + \sigma$) has no effect on the profile $\overline{T}(r)$. Only the relative stratification of entropy is important. We therefore set $\overline{S}_0 := 0$ in what follows. Equation (8) thus becomes

$$\boxed{\overline{T}(r) = e^{\overline{S}(r)/c_{\mathrm{p}}} \left[\overline{T}_0 - \int_{r_0}^{r} \frac{g(x)}{c_{\mathrm{p}}} e^{-\overline{S}(x)/c_{\mathrm{p}}} dx \right].} \tag{9}$$

With $\overline{T}(r)$ now obtained, we can obtain $\overline{P}(r)$ through integrating the First Law in its form (6c):

$$\boxed{\overline{P}(r) = \overline{P}_0 e^{-\overline{S}(r)/\mathcal{R}} \left[\frac{\overline{T}(r)}{\overline{T}_0} \right]^{\Gamma_1/(\Gamma_1 - 1)}.} \tag{10}$$

Finally, $\overline{\rho}(r)$ is determined from Equation (2):

$$\boxed{\overline{\rho}(r) = \overline{\rho}_0 e^{-\overline{S}(r)/\mathcal{R}} \left[\frac{\overline{T}(r)}{\overline{T}_0} \right]^{1/(\Gamma_1 - 1)}.} \tag{11}$$

Thus, the full state of the atmosphere is purely determined by the entropy stratification $d\overline{S}/dr$, the gravitational acceleration $g(r)$, and the two constants $\overline{T}_0$ and $\overline{P}_0$ (or $\overline{T}_0$ and $\overline{\rho}_0$, etc.) It is well-known that with an equation of state, all the thermodynamic variables can be written as functions of the other two. Effectively, we have chosen our two "fundamental variables" to be the entropy and pressure (because of the hydrostatic assumption, we can replace pressure by gravity).

The state specified in equations (9)–(11) is completely general, relying only on the assumptions of a hydrostatic, ideal gas with position-independent specific heats. To move

forward, we must specify $d\overline{S}/dr$ and $g(r)$. For relatively thin convection zones (e.g., the Sun), it is safe to assume that the gravitational acceleration comes purely from a central spherically distributed mass, i.e.,

$$g(r) = \frac{GM_*}{r^2}, \tag{12}$$

where G is the Universal Gravitational Constant and M_* the stellar mass.

2   Adiabatic atmosphere

Considering the mathematical form of (9), the simplest atmosphere to derive is one that is adiabatic (constant-entropy):

$$\overline{S}(r) \equiv 0 \quad \text{and} \quad \frac{d\overline{S}}{dr} \equiv 0. \tag{13}$$

In this case, all the exponentials in (9) cancel to 1 and we find

$$\overline{T}(r) = -\frac{GM_*}{c_\mathrm{p}} \int_{r_0}^{r} \frac{dx}{x^2} + \overline{T}_0$$

or

$$\overline{T}(r) = \overline{T}_0\left[\tilde{a}\left(\frac{r_0}{r}\right) + (1 - \tilde{a})\right] \qquad \text{(adiabatic atmosphere)}, \tag{14}$$

$$\text{where} \quad \tilde{a} := \frac{GM_*}{c_\mathrm{p}\overline{T}_0 r_0}. \tag{15}$$

Then, Equations (10) and (11) yield

$$\overline{P}(r) = \overline{P}_0\left[\tilde{a}\left(\frac{r_0}{r}\right) + (1 - \tilde{a})\right]^{\Gamma_1/(\Gamma_1 - 1)} \qquad \text{(adiabatic atmosphere)} \tag{16}$$

$$\text{and} \quad \overline{\rho}(r) = \overline{\rho}_0\left[\tilde{a}\left(\frac{r_0}{r}\right) + (1 - \tilde{a})\right]^{1/(\Gamma_1 - 1)} \qquad \text{(adiabatic atmosphere)}. \tag{17}$$

Note: to avoid negative thermodynamic quantities, we must ensure that the argument

$$\tilde{a}\left(\frac{r_0}{r}\right) + (1 - \tilde{a}) > 0. \tag{18}$$

This leads to the conditions on available radii r (for our particular choices of M_*, or $\mathcal{R}$, r_0 and $\overline{T}_0$) for which the derived atmosphere is valid:

$$0 < r < \frac{\tilde{a}r_0}{\tilde{a} - 1} \qquad \tilde{a} > 1 \tag{19a}$$

$$r > 0 \qquad \tilde{a} \leq 1. \tag{19b}$$

3   Polytropes

The starting assumption for a "polytrope" is that the temperature gradient is divergenceless—i.e., there is a constant flux due to radiative diffusion throughout the fluid layer. If we assume, for simplicity, a constant radiative diffusion coefficient, then $\nabla^2 \overline{T} = 0$, which, in spherical coordinates, is:

$$\overline{T}(r) = \frac{A}{r} + B. \tag{20}$$

The integration constants A and B in Equation (20) are arbitrary, but one is eliminated from the condition $T(r_0) = \overline{T}_0$, leaving

$$\boxed{\overline{T}(r) = \overline{T}_0 \left[a\left(\frac{r_0}{r}\right) + (1-a) \right] \qquad \text{(polytropic atmosphere),}} \tag{21}$$

where the new constant $a := A/\overline{T}_0 r_0$ is dimensionless. Note the similarity of the argument $[a(r_0/r) + (1-a)]$ in Equation (21) (which was derived by assuming a divergenceless temperature gradient) to the argument in Equation (14) (which was derived by assuming the gas was adiabatic).

Using Equation (2) to eliminate $\overline{\rho}(r)$ from Equation (1) gives

$$\overline{P}(r) = \overline{P}_0 \exp\left[-\frac{1}{\mathcal{R}} \int_{r_0}^{r} \frac{g(x)}{\overline{T}(x)} dx \right],$$

from which

$$\boxed{\overline{P}(r) = \overline{P}_0 \left[a\left(\frac{r_0}{r}\right) + (1-a) \right]^{n+1} \qquad \text{(polytropic atmosphere),}} \tag{22}$$

where we have defined the *polytropic index* n to be

$$n := \frac{1}{a}\frac{GM_*}{\mathcal{R}\overline{T}_0 r_0} - 1 \iff a = \frac{GM_*}{(n+1)\mathcal{R}\overline{T}_0 r_0}. \tag{23}$$

From the ideal gas law, the density is then

$$\boxed{\overline{\rho}(r) = \overline{\rho}_0 \left[a\left(\frac{r_0}{r}\right) + (1-a) \right]^{n} \qquad \text{(polytropic atmosphere).}} \tag{24}$$

As for the adiabatic atmosphere (see Equation (19)), the choices for M_*, $\mathcal{R}$, r_0, $\overline{T}_0$, and n determine the range of radii for which the polytrope is valid:

$$0 < r < \frac{ar_0}{a-1} \qquad a > 1 \tag{25a}$$

$$r > 0 \qquad a \le 1. \tag{25b}$$

Note that for the polytrope, in addition to the two constants $\overline{P}_0$ and $\overline{T}_0$, there is another constant n (or equivalently, a). Specifying n is the same as specifying $d\overline{S}/dr$. For, plugging Equations (21)–(24) (we only need two of them) into any form of (6) yields

$$\frac{d\overline{S}}{dr} = \frac{c_{\mathrm{p}}}{r_0}\left(\frac{n - \tilde{n}}{\tilde{n} + 1}\right)\left[\frac{a}{a(r_0/r) + (1 - a)}\right] \tag{26a}$$

$$\text{and} \quad \overline{S}(r) = c_{\mathrm{p}}\left(\frac{n - \tilde{n}}{\tilde{n} + 1}\right)\left\{\ln\left(\frac{r}{r_0}\right) - \ln\left[a + (1 - a)\left(\frac{r}{r_0}\right)\right]\right\} \tag{26b}$$

$$\text{(polytropic atmosphere),}$$

where

$$\tilde{n} = \frac{1}{\tilde{a}}\frac{GM_*}{\mathcal{R}\overline{T}_0 r_0} - 1 \coloneqq \frac{1}{\Gamma_1 - 1}. \tag{27}$$

From (26a), it is obvious that $n = \tilde{n}$ (or $a = \tilde{a}$) corresponds to an adiabatic atmosphere (as we have already shown in (14)–(17)), while

$$n > \tilde{n} \iff \frac{d\overline{S}}{dr} > 0 \text{ (atmosphere is stable to convection)} \tag{28}$$

$$\text{and} \quad n < \tilde{n} \iff \frac{d\overline{S}}{dr} < 0 \text{ (atmosphere is unstable to convection).} \tag{29}$$

(Because of the condition on the radii, Equation (25)—the quantity in square brackets in Equation (26a) is always positive).

From Equations (21)–(26a) that the limit $n \to \infty$ simply corresponds to an isothermal atmosphere:

$$\overline{T}(r) \to \overline{T}_0, \tag{30}$$

$$\overline{P}(r) \to \overline{P}_0 \exp\left[\frac{GM_*}{\mathcal{R}\overline{T}_0 r_0}\left(\frac{r_0}{r} - 1\right)\right], \tag{31}$$

$$\overline{\rho}(r) \to \overline{\rho}_0 \exp\left[\frac{GM_*}{\mathcal{R}\overline{T}_0 r_0}\left(\frac{r_0}{r} - 1\right)\right], \tag{32}$$

$$\frac{d\overline{S}}{dr} \to \frac{GM_*}{\overline{T}_0 r^2}, \tag{33}$$

$$\text{and} \quad \overline{S}(r) \to \frac{GM_*}{\overline{T}_0 r_0}\left(1 - \frac{r_0}{r}\right) \tag{34}$$

$$\text{(polytropic atmosphere as } n \to \infty).$$

If one tries to increase the "stiffness" (entropy gradient) of the system by increasing n, there is therefore a fundamental limit imposed by the polytropic formulation. Similarly, the total entropy contrast from top to bottom and all logarithmic derivatives of the thermodynamic variables have an upper bound, meaning that all scale heights (which typically set the size of fluid motions) have a lower bound. *These bounds are reached for an isothermal atmosphere.*

5

3.1 Polytrope in terms of overall density stratification

For an adiabatic, polytropic convection zone (CZ) sitting atop a stably stratified radiative zone (RZ), it is often convenient to choose the reference radius to be boundary between RZ and CZ, i.e., $r_0 = r_{\rm m}$ (subscript m for "middle radius"). In the work of Jones et al. (2011) and in the Rayleigh code (Featherstone 2018), the polytrope is initiated using the middle density $\rho_{\rm m}$ and the number of density scale heights N_ρ across the CZ , as opposed to the two middle-boundary values $p_{\rm m}$ and $T_{\rm m}$. Here $N_\rho := \ln(\rho_{\rm m}/\rho_{\rm o})$, where $\rho_{\rm m}$ and $\rho_{\rm o}$ are the density values at the middle and outer boundaries of the shell, respectively. We can recast (21)–(24) in terms of $\rho_{\rm m}$ and N_ρ by using (23) and (24) to yield

$$a = \frac{e^{N_\rho/n} - 1}{(1-\beta)e^{N_\rho/n}} \quad \text{and} \quad T_{\rm m} = \frac{(1-\beta)e^{N_\rho/n}}{e^{N_\rho/n} - 1} \frac{GM_*}{(n+1)\mathcal{R}r_{\rm m}}, \tag{35}$$

where we have defined the aspect ratio of the CZ,

$$\beta := \frac{r_{\rm m}}{r_{\rm o}} < 1. \tag{36}$$

Thus, instead of specifying $T_{\rm m}$ and $p_{\rm m}$, we can specify $\rho_{\rm m}$ and N_ρ; $T_{\rm m}$ is then determined through (35) and $p_{\rm m}$ through the ideal gas law.

3.2 Polytrope with respect to the center of the CZ

Jones et al. (2011) define the polytrope using the variables at the center of the CZ (i.e., in our notation $r_0 = r_c := (r_{\rm m} + r_{\rm o})/2$). In that case, (21)–(24) become

$$\overline{T}(r) = T_c\left[a_c\left(\frac{r_c}{r}\right) + (1-a_c)\right], \tag{37}$$

$$\overline{P}(r) = p_c\left[a_c\left(\frac{r_c}{r}\right) + (1-a_c)\right]^{n+1}, \tag{38}$$

$$\overline{\rho}(r) = \rho_c\left[a_c\left(\frac{r_c}{r}\right) + (1-a_c)\right]^{n}, \tag{39}$$

where

$$a_c := \frac{GM_*}{(n+1)\mathcal{R}T_c r_c}. \tag{40}$$

Using a similar computation as the one leading to (35), one can show that

$$a_c = \frac{2\beta(e^{N_\rho/n} - 1)}{(1-\beta)(\beta e^{N_\rho/n} + 1)}. \tag{41}$$

Defining

$$d := r_{\rm o} - r_{\rm m}, \tag{42}$$

$$c_0 := 1 - a_c = \frac{(1+\beta)(1-\beta e^{N_\rho/n})}{(1-\beta)(\beta e^{N_\rho/n} + 1)}, \tag{43}$$

$$c_1 := \left(\frac{r_c}{d}\right) a_c = \frac{(1+\beta)\beta(e^{N_\rho/n} - 1)}{(1-\beta)^2(\beta e^{N_\rho/n} + 1)}, \tag{44}$$

$$\text{and} \quad \tilde{\zeta}(r) := a_c\left(\frac{r_c}{r}\right) + (1 - a_c) = c_0 + c_1\left(\frac{d}{r}\right), \tag{45}$$

(37)–(39) become

$$\overline{T}(r) = T_c\tilde{\zeta}(r), \quad \overline{P}(r) = p_c[\tilde{\zeta}(r)]^{n+1}, \quad \overline{\rho}(r) = \rho_c[\tilde{\zeta}(r)]^n. \tag{46}$$

With significantly more algebra, we can also see that if we define

$$\tilde{\zeta}_o := \tilde{\zeta}(r_o) = \frac{1+\beta}{\beta e^{N_\rho/n} + 1}, \tag{47}$$

then

$$c_0 = \frac{2\tilde{\zeta}_o - \beta - 1}{1 - \beta} \quad \text{and} \quad c_1 = \frac{(1+\beta)(1 - \tilde{\zeta}_o)}{(1-\beta)^2}, \tag{48}$$

yielding exactly the formulation for the polytrope in Jones et al. (2011).

Both the formulation with respect to the center of the shell (45)–(48) and the formulation with respect to the middle boundary using (21)–(24) (also (35) if specifying ρ_m and N_ρ instead of p_m and T_m) are mathematically equivalent. However, given the substantial extra notation involved in defining the constants c_0 and c_1, it seems preferable to use the latter formulation.

3.3   Stable vs. unstable polytropes

Figure 1 (Figure 2) shows a sample of convectively stable (unstable) polytropes for various values of the polytropic index n in a solar-like convection zone. For very high values of n (Figure 1), the entropy gradient profile asymptotes to its maximum value and the temperature profile becomes flat—in agreement with the discussion surrounding Equation (30). For very low values of n (highly unstable polytropes; Figure 2), the constant a becomes significantly greater than 1, and the argument $\zeta(r)$ becomes negative within the convection zone, giving complex values for $\overline{P}(r)$ and $\overline{\rho}(r)$ for r greater than the radius at which $\zeta = 0$ (the exception to this rule is the special case $n = 1$). Thus, the polytropic formulation is unphysical for domains with large enough extent; the same is true for the stable polytropes, but the radius at which $\zeta = 0$ is quite far outside the convection zone.

3.4   Atmosphere with constant entropy gradient

A simple example of a fluid layer that is stable to convection is one with a constant "stiffness," or entropy gradient. If we consider an RZ extending from the inner radius r_i of the shell to the middle of the shell r_m, we can write

$$\boxed{\overline{S}(r) = kc_\mathrm{p}\left(\frac{r}{r_\mathrm{m}} - 1\right) \quad \text{and} \quad \frac{d\overline{S}}{dr} = \frac{kc_\mathrm{p}}{r_\mathrm{m}} \quad \text{(constant entropy gradient)},} \tag{49}$$

where k is a dimensionless constant (> 0) representing the stiffness of the stable region. We can then use (9) to find $\overline{T}(r)$:

$$\overline{T}(r) = -\frac{GM_*}{c_{\mathrm{p}}}\left\{e^{k[(r/r_{\mathrm{m}})-1]}\right\} \underbrace{\int_{r_{\mathrm{m}}}^{r} \frac{e^{-k[(r/r_{\mathrm{m}})-1]}dx}{x^2}}_{:=\mathscr{I}(r)} + T_{\mathrm{m}}e^{k[(r/r_{\mathrm{m}})-1]}. \tag{50}$$

The integral $\mathscr{I}(r)$ can be recast in terms of the exponential integral function

$$E_n(x) := \int_1^\infty \frac{e^{-xt}}{t^n}dt = x^{n-1}\int_x^\infty \frac{e^{-t}}{t^n}dt, \tag{51}$$

yielding

$$\boxed{\overline{T}(r) = T_{\mathrm{m}}\left\{\left[e^k\tilde{a}\left(\frac{r_{\mathrm{m}}}{r}\right)E_2\left(\frac{kr}{r_{\mathrm{m}}}\right) + (1 - e^k E_2(k)\tilde{a})\right]e^{k[(r/r_{\mathrm{m}})-1]}\right\}, \qquad (52\mathrm{a})}$$

$$\boxed{\text{with} \quad \tilde{a} := \frac{GM_*}{c_{\mathrm{p}}T_{\mathrm{m}}r_{\mathrm{m}}} \text{ (again).} \qquad (52\mathrm{b})}$$

$$\boxed{\text{(constant entropy gradient).}}$$

Using (10) and (11) then yields

$$\boxed{\begin{aligned}
\overline{P}(r) &= p_{\mathrm{m}}\exp\left[-\frac{\gamma}{\gamma-1}k\left(\frac{r}{r_{\mathrm{m}}}-1\right)\right] \\
&\times \left\{\left[e^k\tilde{a}\left(\frac{r_{\mathrm{m}}}{r}\right)E_2\left(\frac{kr}{r_{\mathrm{m}}}\right) + (1 - e^k E_2(k)\tilde{a})\right]e^{k[(r/r_{\mathrm{m}})-1]}\right\}^{\gamma/(\gamma-1)} \\[1em]
\text{and} \quad \overline{\rho}(r) &= \rho_{\mathrm{m}}\exp\left[-\frac{\gamma}{\gamma-1}k\left(\frac{r}{r_{\mathrm{m}}}\right)\right] \\
&\times \left\{\left[e^k\tilde{a}\left(\frac{r_{\mathrm{m}}}{r}\right)E_2\left(\frac{kr}{r_{\mathrm{m}}}\right) + (1 - e^k E_2(k)\tilde{a})\right]e^{k[(r/r_{\mathrm{m}})-1]}\right\}^{1/(\gamma-1)}
\end{aligned}}$$

$$\boxed{\text{(constant entropy gradient).}}$$

(53), (54)

Clearly if $k = 0$, we recover (14)–(17) for an adiabatic atmosphere (note that $E_n(0) \equiv 1$ for all n).

Using (7), one can show that for small stiffnesses (k close to 0), $dT/dr < 0$ throughout the entire RZ, implying a monotonically decreasing temperature profile. However, for $k > k_c$, where

$$k_c := \frac{GM_*}{c_{\mathrm{p}}T_{\mathrm{m}}r_{\mathrm{m}}}, \tag{55}$$

the temperature gradient at $r = r_{\mathrm{m}}$ becomes positive, and there is a temperature inversion somewhere for $r < r_{\mathrm{m}}$. Interestingly, the entropy gradient associated with this transition, $\frac{d\overline{S}}{dr}_c = k_c c_{\mathrm{p}}/r_{\mathrm{m}} = GM_*/T_{\mathrm{m}}r_{\mathrm{m}}^2$ is exactly the same as the entropy gradient at $r = r_{\mathrm{m}}$ for an

isothermal atmosphere (or the upper limit on the entropy gradient for a polytropic atmosphere as $n \to \infty$). For solar values (namely $M = M_\odot$, $r_{\mathrm{m}} = 5.0 \times 10^{10}$ cm, $T_{\mathrm{m}} = 2.1 \times 10^6$ K, and $c_{\mathrm{p}} = 3.5 \times 10^8$ erg g^{-1} K^{-1}),

$$k_c = 3.59. \tag{56}$$

Figures 3 and 4 show stable fluid layers in a solar-like radiative zone for stable polytropes and constant-entropy fluid layers, respectively. In Figure 3, a range of polytropic indices n are used to more or less give entropy-gradient magnitudes matching those set by the k-values of Figure 4. For $k > 3.59$ (the black and chartreuse curves in Figure 4), the entropy gradients for the constant-gradient layer begin to exceed those of the polytrope, and there is furthermore a noticeable temperature inversion within the radiative zone.

4   Hyperbolic (exponential) matching of entropy gradient between CZ and RZ

We consider a domain in radius of $(r_{\mathrm{i}}, \mathrm{Ro})$ with the middle radius r_{m} lying in this interval. We simulate a convection zone (CZ) in the region $(r_{\mathrm{m}}, \mathrm{Ro})$ overlying a radiative zone (stable region; RZ) in the region $(r_{\mathrm{i}}, r_{\mathrm{m}})$. In order to smoothly match a constant-entropy-gradient RZ ($\frac{d\overline{S}}{dr} = \mathrm{constant} > 0$) to a marginally stable CZ ($\frac{d\overline{S}}{dr} \equiv 0$), we can use hyperbolic trigonometric functions:

$$\overline{S}(r) = \frac{kc_{\mathrm{p}}}{r_{\mathrm{m}}} \left\{ \frac{1}{2} \left[(r - r_{\mathrm{m}}) - \delta \ln \cosh \left(\frac{r - r_{\mathrm{m}}}{\delta} \right) \right] \right\} \tag{57}$$

$$\frac{ds}{dr} = \frac{kc_{\mathrm{p}}}{r_{\mathrm{m}}} \left\{ \frac{1}{2} \left[1 - \tanh \left(\frac{r - r_{\mathrm{m}}}{\delta} \right) \right] \right\}. \tag{58}$$

$$\frac{d^2 s}{dr^2} = -\frac{kc_{\mathrm{p}}}{r_{\mathrm{m}}} \left(\frac{1}{2\delta} \right) \mathrm{sech}^2 \left(\frac{r - r_{\mathrm{m}}}{\delta} \right) \tag{59}$$

We then find the full thermodynamic profiles using the integral relations in (9)—(11).

Figures 5 and 6 show the thermodynamic states defined by the entropy profile (57) for a range of δ-values and k-values. The hyperbolic matching condition has the disadvantage that the layer is slightly non-adiabatic even in the CZ—i.e., the tanh function does not decay quickly enough; indeed, the profile $(1/2)(1 - \tanh(x))$ is still 0.0025 for $x = 3$. From Figure 5, the problem is diminished for very rapid transitions (small δ) but this is also seen to create large spikes in the logarithmic derivatives.

5   Quartic matching of entropy gradient between CZ and RZ

In order to better control precisely where the descending downflow plumes begin to overshoot, we can demand that entropy gradient is *exactly* zero in the CZ, transitioning to a nonzero

value (over a width δ) by means of a twice-differentiable piece-wise function for the entropy profile (the entropy gradient $\frac{d\overline{S}}{dr}$ is once-differentiable and has a quartic form):

$$\overline{S}(r) = \begin{cases} \frac{8}{15}kc_{\mathrm{p}}\left(\frac{\delta}{r_{\mathrm{m}}}\right) + kc_{\mathrm{p}}\left(\frac{r}{r_{\mathrm{m}}} - 1\right) & r \leq r_{\mathrm{m}} - \delta \\ kc_{\mathrm{p}}\left(\frac{\delta}{r_{\mathrm{m}}}\right)\left[\frac{2}{3}\left(\frac{r-r_{\mathrm{m}}}{\delta}\right)^3 - \frac{1}{5}\left(\frac{r-r_{\mathrm{m}}}{\delta}\right)^5\right] & r_{\mathrm{m}} - \delta < r < r_{\mathrm{m}} \\ 0 & r \geq r_{\mathrm{m}} \end{cases} \quad (60)$$

$$\frac{ds}{dr} = \begin{cases} \frac{kc_{\mathrm{p}}}{r_{\mathrm{m}}} & r \leq r_{\mathrm{m}} - \delta \\ \frac{kc_{\mathrm{p}}}{r_{\mathrm{m}}}\left\{1 - \left[1 - \left(\frac{r-r_{\mathrm{m}}}{\delta}\right)^2\right]^2\right\} & r_{\mathrm{m}} - \delta < r < r_{\mathrm{m}} \\ 0 & r \geq r_{\mathrm{m}} \end{cases} \quad (61)$$

$$\frac{d^2s}{dr^2} = \begin{cases} 0 & r \leq r_{\mathrm{m}} - \delta \\ \frac{4}{\delta}\frac{kc_{\mathrm{p}}}{r_{\mathrm{m}}}\left[1 - \left(\frac{r-r_{\mathrm{m}}}{\delta}\right)^2\right]\left(\frac{r-r_{\mathrm{m}}}{\delta}\right) & r_{\mathrm{m}} - \delta < r < r_{\mathrm{m}} \\ 0 & r \geq r_{\mathrm{m}} \end{cases} \quad (62)$$

Figures 7 and 8 show the thermodynamic states defined by the entropy profile (60) for a range of δ-values and k-values. We can see that the transition width δ is "strict" in the sense that the entropy gradient is *exactly* equal to its asymptotic values outside the transition region. Thus, the thermodynamic profiles in the CZ are exactly that of an adiabatic polytrope. However, this sharper transition is also seen to create sharper spikes in the logarithmic derivatives.

References

Featherstone, N., 2018, Rayleigh 0.9.1, doi: http://doi.org/10.5281/zenodo.1236565

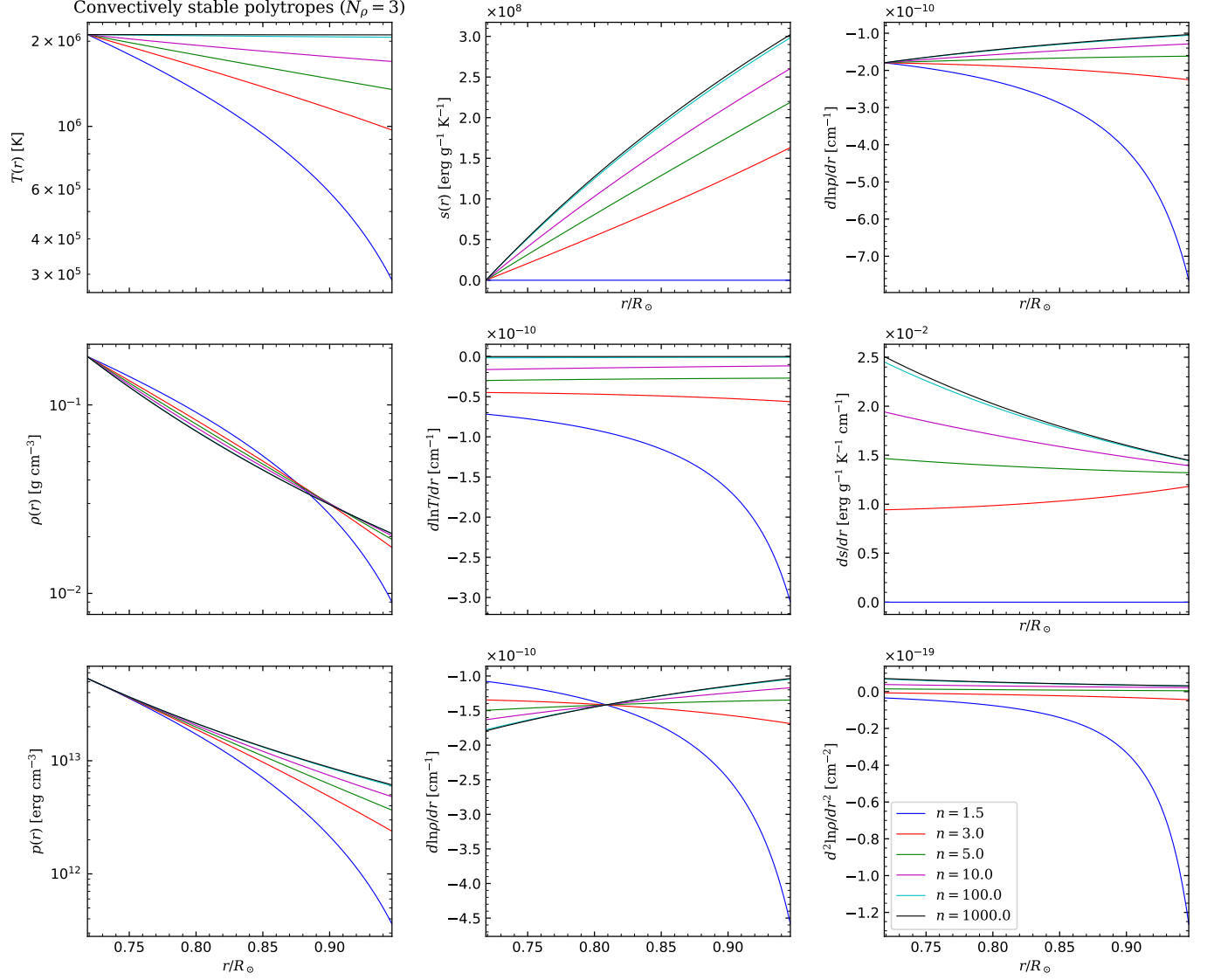Jones, C.A., Boronski, P., Brun, A.S., et al., 2011, Icarus, 216, 120

Figure 1: Sample of convectively stable polytropes for a solar-like CZ ($n \geq 1.5$). The dimensional/geometric values for the polytrope (i.e., , Ro, ρ_i, M, c_p) are the solar values preceding (56), and $N_\rho = 3$.
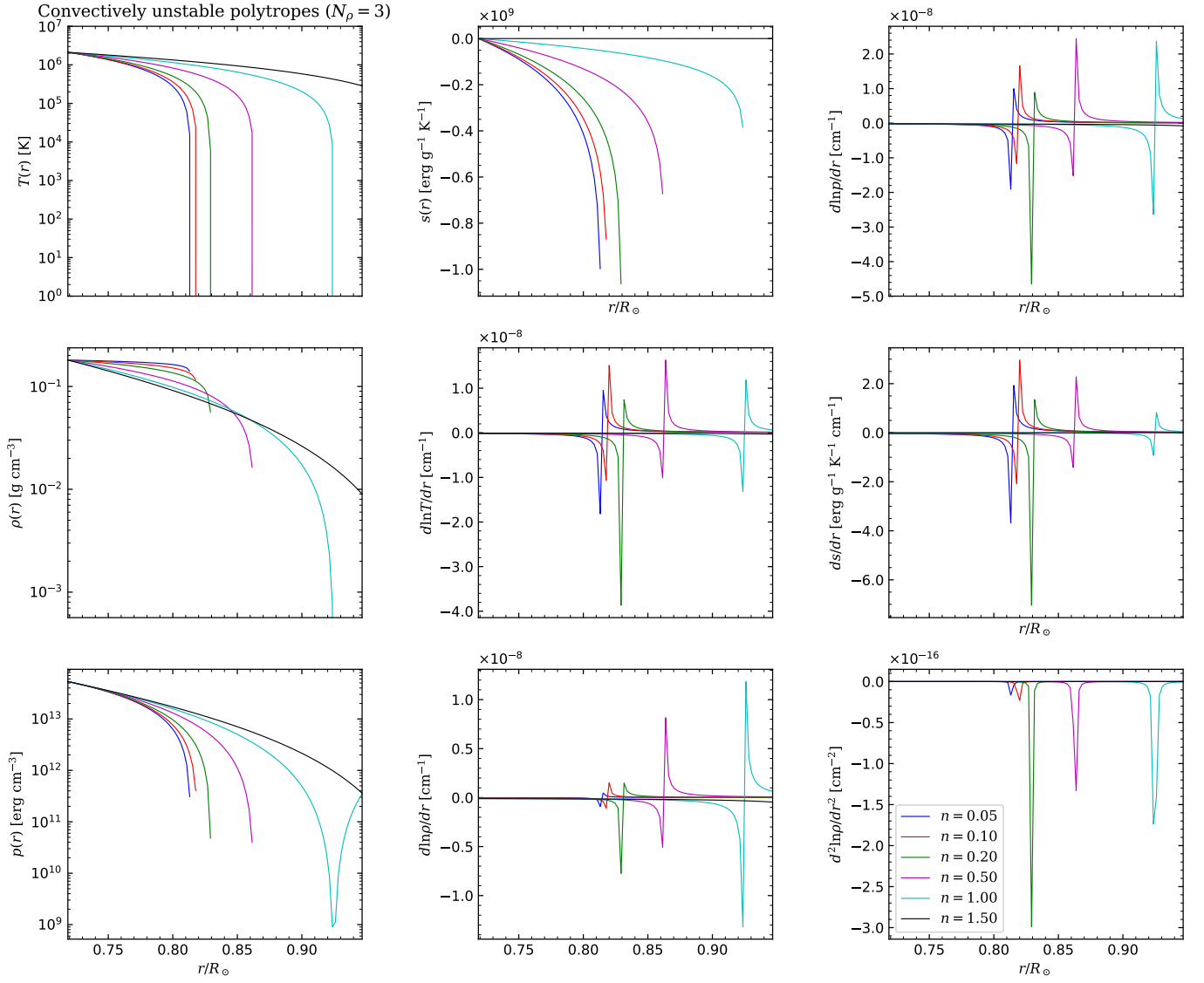
Figure 2: Sample of convectively unstable polytropes for a solar-like CZ ($n \leq 1.5$), with the same dimensional parameters as Figure 1.
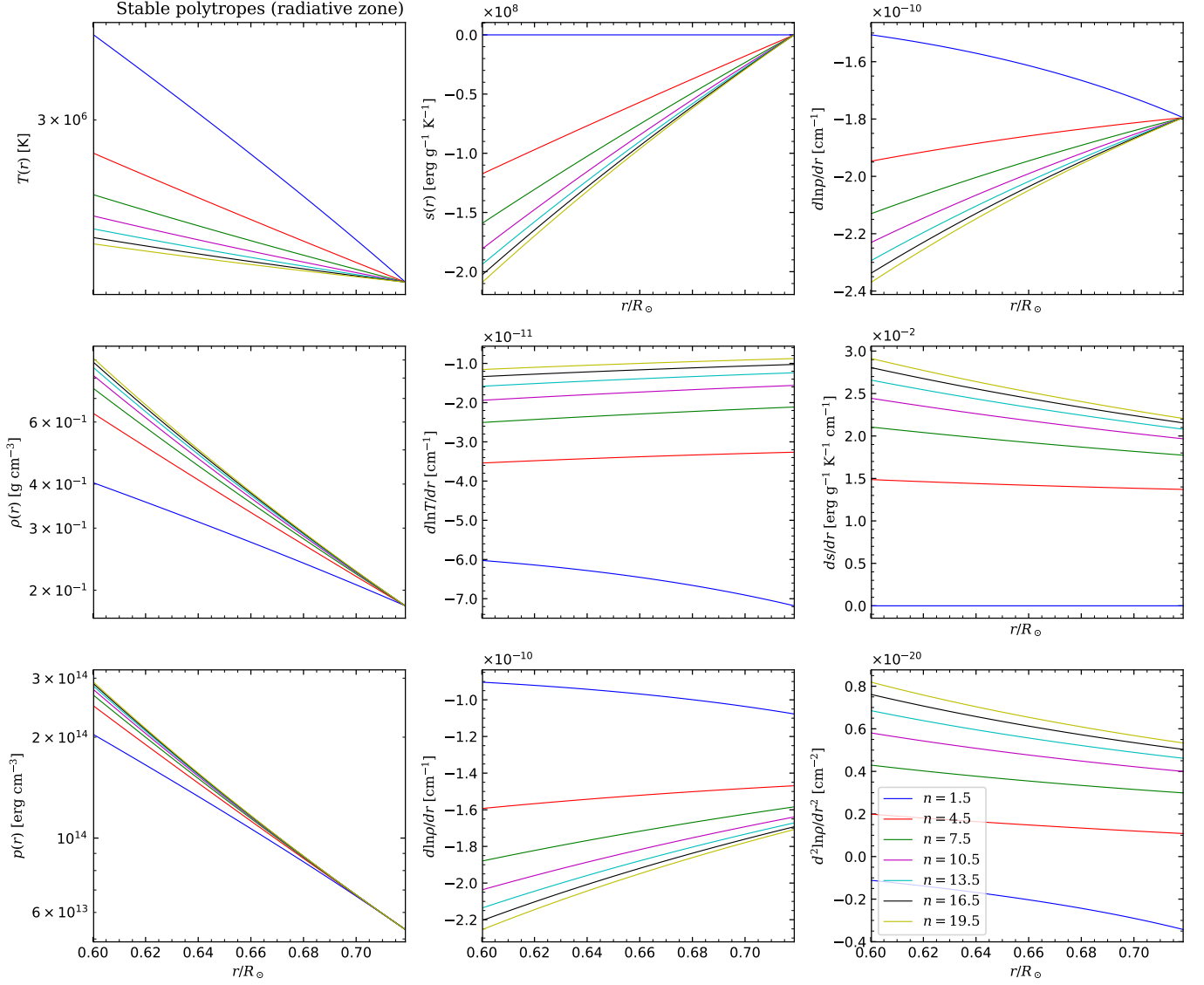
Figure 3: Sample of convectively stable polytropes for a solar-like RZ ($n \geq 1.5$). Similar to Figure 1, except the radius range is ($r_\mathrm{i} = 4.176 \times 10^{10}$ cm, $r_\mathrm{m} = 5.00 \times 10^{10}$ cm) instead of (r_m, Ro).
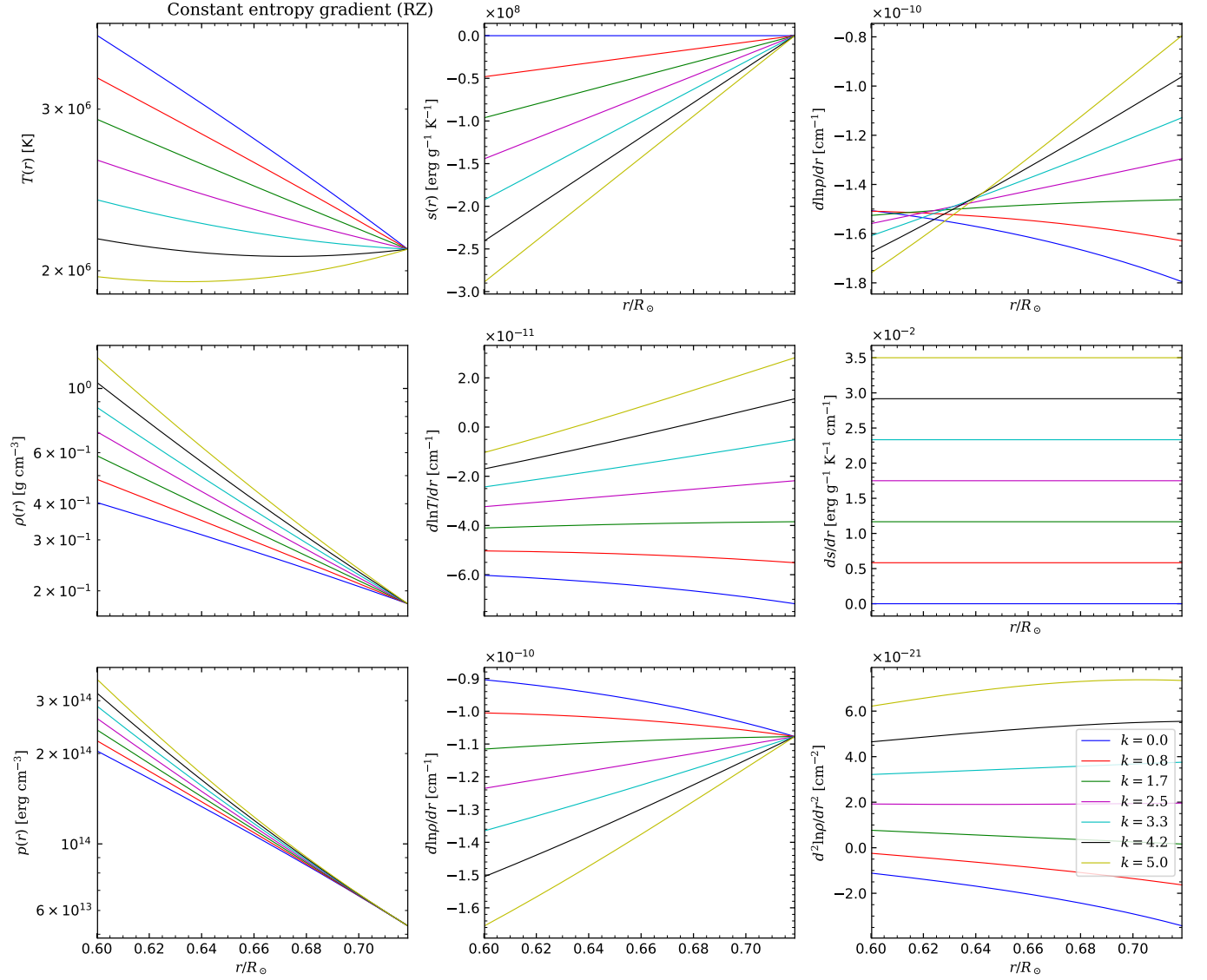
Figure 4: Sample of constant-entropy-gradient gas layers for a solar-like RZ, with values of k chosen to give entropy gradients more or less matching those of Figure 3.
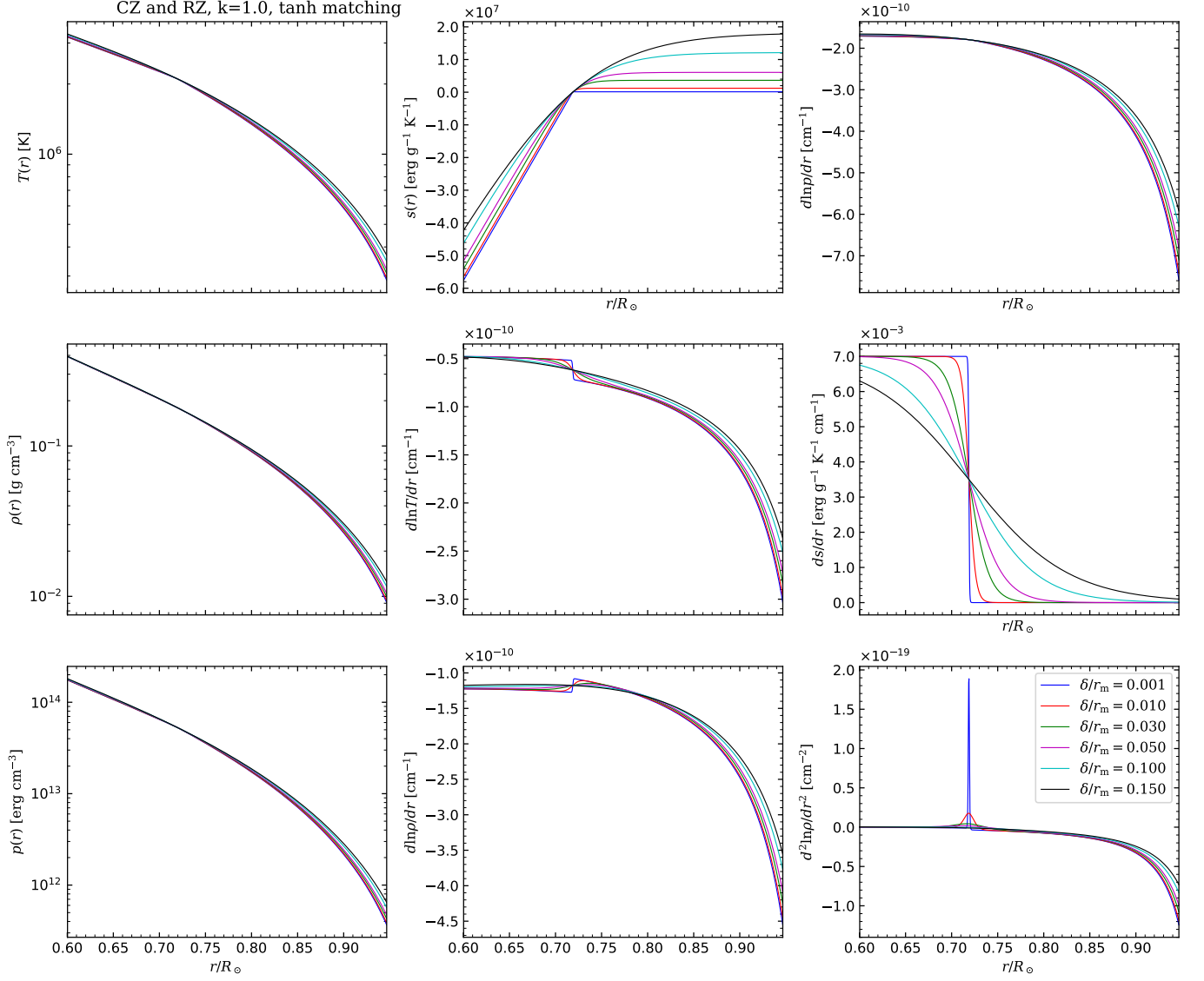
Figure 5: Combined CZ and RZ fluid layer with entropy gradient profiles matched via hyperbolic tangents—different transition thicknesses δ, with $k = 1$ in all cases.
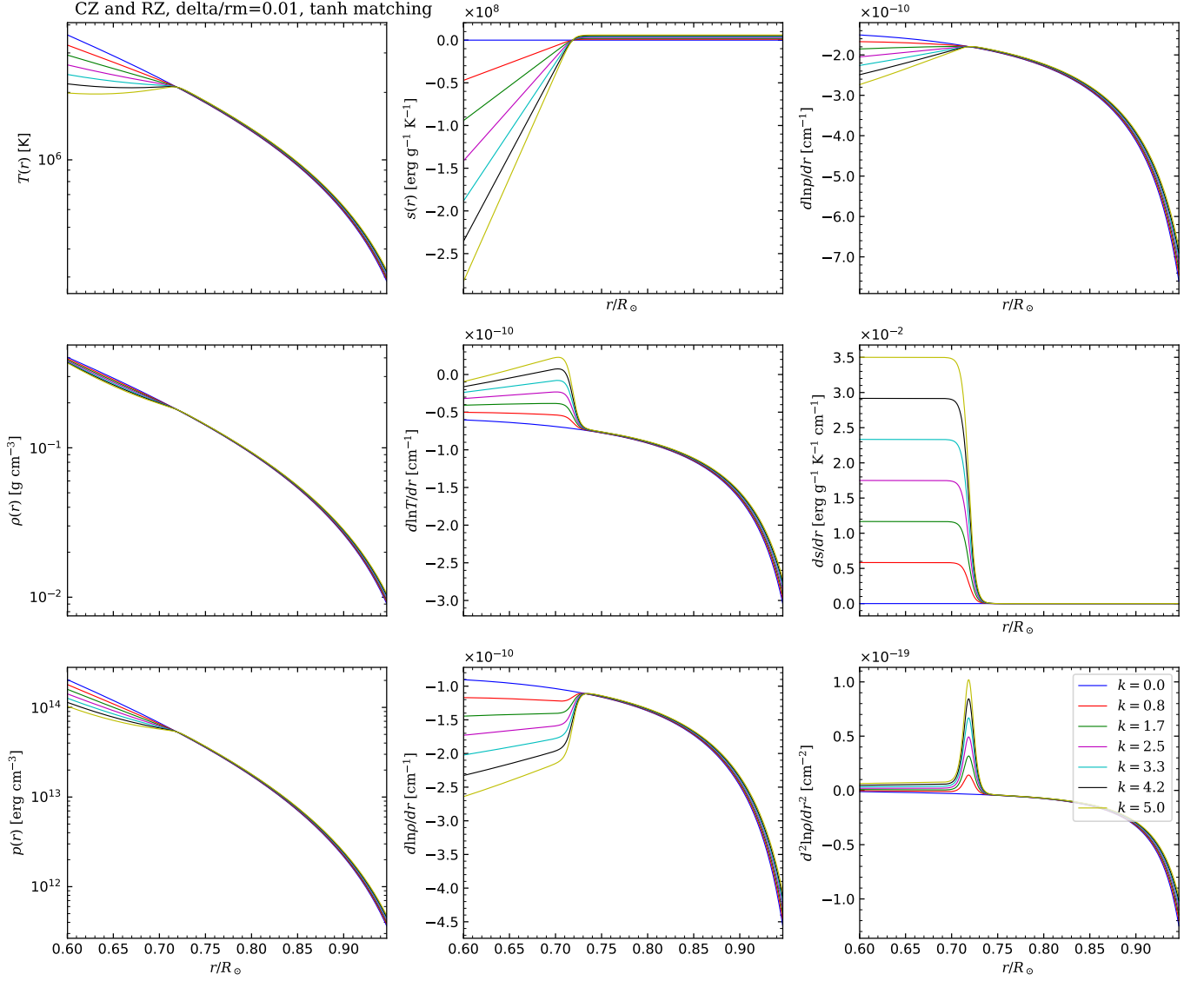
Figure 6: Combined CZ and RZ fluid layer with entropy gradient profiles matched via hyperbolic tangents—different levels of stiffness k, with $\delta/r_{\mathrm{m}} = 0.01$ in all cases.
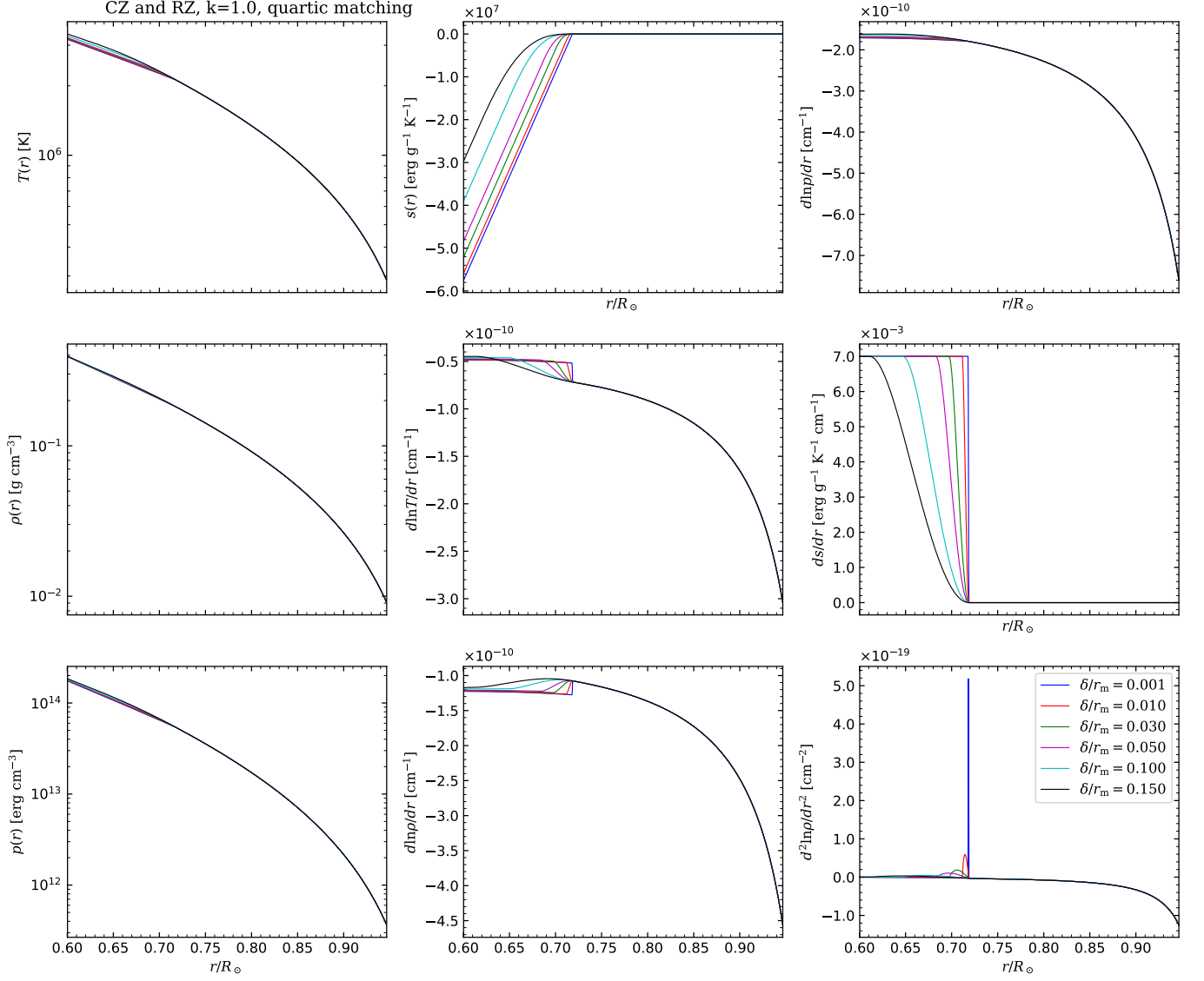
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Figure 7: Combined CZ and RZ fluid layer with entropy gradient profiles matched via quartic functions—different transition thicknesses δ, with $k = 1$ in all cases.
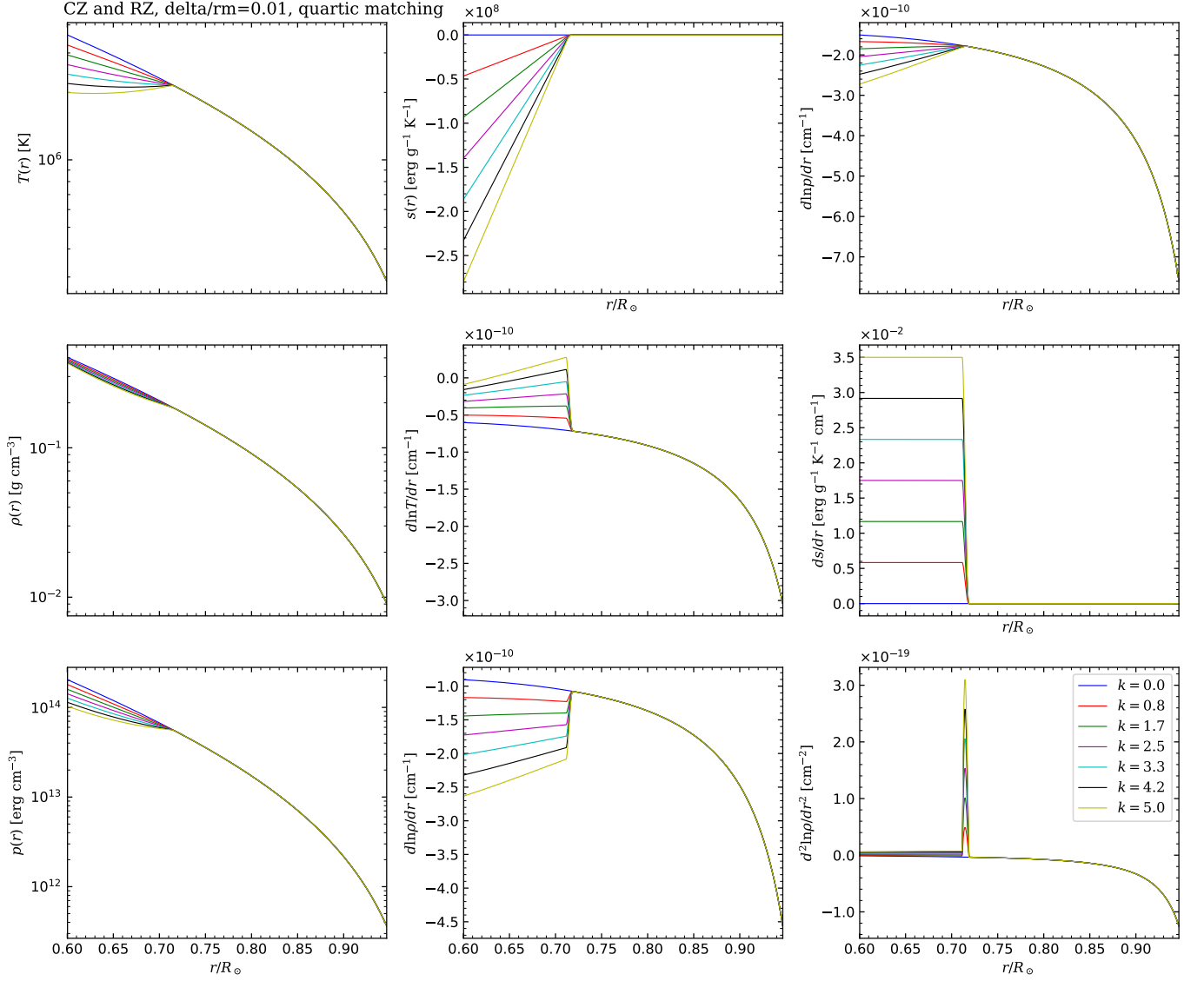
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Figure 8: Combined CZ and RZ fluid layer with entropy gradient profiles matched via quartic functions—different levels of stiffness k, with $\delta/r_{\mathrm{m}} = 0.01$ in all cases.