

Study Material Template

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May 14, 2024

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The main tasks of Control Theory are

1. Stabilization
2. Tracking

1 Maths

2 Introduction

Dynamical systems

Let's consider the n th-order ordinary differential equation (ODE):

$$\mathbf{x}^{(n)} = \mathbf{f}(\mathbf{x}^{(n-1)}, \mathbf{x}^{(n-2)}, \dots, \ddot{\mathbf{x}}, \dot{\mathbf{x}}, \mathbf{x}, t),$$

where $x(t)$ is a solution for the system, and t is an independent variable (usually - time). This equation is called a **dynamical system** and it represents a dynamics of the system.

State of

In canonical form, linear ODE is represented in the following way:

$$a_n z^{(n)} + a_{n-1} z^{(n-1)} + \dots + a_2 \ddot{z} + a_1 \dot{z} + a_0 z = b_0$$

The set $\{\mathbf{x}, \dot{\mathbf{x}}, \dots, \mathbf{x}^{(n-1)}\}$ is called the **state of the system**.

In case if relationships between state, output and control is **linear**, we can formulate the model of system in following form:

$$\begin{cases} \dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{B}\mathbf{u} \\ \mathbf{y} = \mathbf{C}\mathbf{x} + \mathbf{D}\mathbf{u} \end{cases} \quad (1)$$

where $\mathbf{x} \in \mathbb{R}^n$ states of the system $\mathbf{y} \in \mathbb{R}^l$ output vector $\mathbf{u} \in \mathbb{R}^m$ control inputs $\mathbf{A} \in \mathbb{R}^{n \times n}$ state matrix $\mathbf{B} \in \mathbb{R}^{n \times m}$ input matrix $\mathbf{C} \in \mathbb{R}^{l \times n}$ output matrix $\mathbf{D} \in \mathbb{R}^{l \times m}$ feedforward matrix

If matrices \mathbf{A} , \mathbf{B} , \mathbf{C} , \mathbf{D} are time-independent, then we call such systems **time-invariant**.

More frequently we work with systems when the output does not depend on control.

$$\begin{cases} \dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{B}\mathbf{u} \\ \mathbf{y} = \mathbf{C}\mathbf{x} \end{cases} \quad (2)$$

State vector, Control vector

Input vector

3 Stability

3.1 Critical Point (Node)

Critical Point (Node)

Consider the following LTI:

$$\dot{x} = f(\mathbf{x}, t)$$

x_0 is called a **Node**, or **Critical Point**, if $f(x_0) = 0$.

3.2 Stability

A system is stable if:

$$\|x(0) - x_0\| < \delta \quad \|x(t) - x_0\| < \epsilon$$

4 Control

The main tasks of control theory include control design, trajectory tracking, and point-to-point control.

Control Design

Dynamical Systems

The task of **stabilizing control** is defining the control law that makes a certain solution of a dynamical system stable.

This is true for both linear and nonlinear systems.

Consider a Linear Time-Invariant (LTI) system:

$$\dot{x} = Ax + Bu,$$

and choose the control as a linear function of the state:

$$u = -Kx,$$

where K is the **control gain**.

Stability Condition

Then, the closed-loop system can be represented as:

$$\dot{x} = (A - BK)x.$$

The system is asymptotically stable if the eigenvalues of the matrix $A - BK$ have strictly negative real parts.

Trajectory Tracking

The task is to stabilize the system around a reference trajectory.

Let $x^*(t)$ and $u^*(t)$ be solutions for the system $\dot{x} = Ax + Bu$. This means that:

$$\dot{x}^* = Ax^* + Bu^*.$$

Define the error as $e = x^* - x$ and $v = u^* - u$.

Then, the error dynamics become:

$$\dot{e} = Ae + Bv.$$

To stabilize the system, suggest $v = -Ke$, then:

$$\dot{e} = (A - BK)e.$$

Therefore, the control law becomes:

$$u = u^* + K(x^* - x).$$

Point-to-Point Control

Point-to-point control differs from trajectory tracking in that the reference input is constant, $x^* = \text{const}$, and feed-forward control is also constant, $u^* = \text{const}$.

Since the error dynamics and the stabilizing control are the same as in trajectory tracking, the control law becomes:

$$u = K(x^* - x) + u^*.$$

The dynamics of the system become:

$$\dot{x} = (A - BK)x + BKx^* + Bu^*.$$

5 Topic 1

5.1 Subtopic 1.1

5.2 Subtopic 1.2

6 LQR

6.1 Intuition behind poles

In control theory, the system state-space equation

$$\dot{x} = Ax + Bu$$

$$y = Cx + Du$$

has the transfer function

$$G(s) = C(sI - A)^{-1}B + D.$$

Since $(sI - A)^{-1} = \text{adj}(sI - A) \det(sI - A)^{-1}$, where $\text{adj}(sI - A)$ is the adjugate of $sI - A$, the poles of $G(s)$ are the numbers that satisfy $\det(sI - A) = 0$. This is exactly the characteristic equation of matrix A , whose solutions are the eigenvalues of A .

6.2 LQR

In pole-placement method, we want to place the poles in the specific spots (or, we choose specific eigenvalues). But it is not intuitive where to place them, especially for complex systems, systems with numerous actuators. So, the new method is proposed. The key concept of the method lies in optimization of choosing K .

In LQR we find an optimal K by choosing parameters that are important to us, specifically how well the system performs and how much effort it takes to reach this performance.

If $Q \gg R$, then we are turning the problem of Let J be an additive cost function:

$$J(x_0, p(x, t)) = \int_0^\infty g(x, u)$$

Q - how bad if x is not where it is supposed to be. Q - nonnegative, positive semidefinite.

if the system is a positions, velocity, and $Q = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 10 & 0 \\ 0 & 0 & 0 & 100 \end{bmatrix}$ we penalize for

Suppose there is the best control law:

$$u = -kx$$

that minimizes the quadratic cost function.

$$J = \int x^T Q x + u^T R u$$

Hamiltonian-Jacobi-Bellman (HJB)

$$\min_u [g(x, u) + \frac{dJ}{dx} f(x, u)] = 0$$

Cost on effectiveness and energy to reach this effectiveness.

6.3 Subtopic 2.1

6.4 Subtopic 2.2

7 Observer

When the full state feedback is unavailable, we introduce an observer to estimate the state x .

We created a system with a controller, but how to check the current state of the system.

We can try to estimate it with the measurements, for example from sensors. But in real life the task is not that trivial due to some problems:

1. Lack of sensors. For a quadrotor we can not measure the height straight forwardly
2. Measurements can be imprecise or biased
3. Measurements can be only made in discrete time

The key problem arises when the output of the system y is not the whole state x , but $y = Cx$, which means that we are able to get the state partially.

These are just several problems that create the difficulties for us to measure the state of the system.

Let's introduce a new idea of how to introduce an observer in our system.

We estimate \hat{x} based on the history of y values.

x and y are the state and output (actual or true)

Estimation error

State estimation error:

$$\epsilon = \hat{x} - x$$

But since we do not know x , we cannot compute this error ϵ .

However, we can always find $y = C\hat{x} - y$.

Let's suggest that the dynamics should also hold for the observed state:

$$\dot{\hat{x}} = A\hat{x} + Bu$$

Let's introduce in our equation a linear correction law $-L y$. Since $y = C\hat{x} - y$, we get:

$$\dot{\hat{x}} = A\hat{x} + Bu + L(y - C\hat{x}) \quad (3)$$

This is called Luenberger observer.

But how to find suitable observer gain L ?

Let's subtract $\dot{x} = Ax + Bu$ from (?). The equation we got is the observer error dynamics:

With no knowledge of x and \hat{x} , we can define the stability of the system.

The observer $\dot{\epsilon} = (A - LC)\epsilon$ is stable.

7.1 Luenberger Observer

Based on the output y , we wish to estimate input x .

8 Filters

In literature, the system is frequently called a Plant, which in our case is a robot.

Static system

Static systems are linear systems for which the relation between input and output is constant

Dynamic system

Dynamic systems are linear systems for which the relation between input and output depends on time.

In Laplace domain, plant $Y(S) =$

Time does not appear in this equation, but if we rewrite it into ode form,

$$\ddot{y} + 5\dot{y} + y = u$$

For these systems, the output depends not only on the current (time-wise) value of input, but on the entire history of input values.

Static systems form algebraic linear equations. Dynamical systems create linear differential equations

For the system we can create the controller and Luenberger observer:

9 Controllability. Observability

Not always can we control the system. The same applies to an observer. Sometimes, we cannot obtain the full information that we desire from the system.

Let's suggest the tools which can inform us whether we can succeed in designing a controller or observer or not.

Controllability

A system is controllable on $t_0 \leq t \leq t_f$ if it is possible to find a control input $u(t)$ that would drive the system to a desired state $x(t_f)$ from any initial state x_0 .

Observability

A system is observable on $t_0 \leq t \leq t_f$ if it is possible to exactly estimate the state of the system $x(t_f)$, given any initial estimation error.

Observability (Alternative)

A system is observable on $t_0 \leq t \leq t_f$ if any initial state x_0 is uniquely determined by the output $y(t)$ on that interval.

Cayley-Hamilton Theorem: A matrix M satisfies its own characteristic equation.

A characteristic equation can be written like:

$$\lambda^n + a_{n-1}\lambda^{n-1} + a_{n-2}\lambda^{n-2} + \dots + a_0 = 0$$

So,

$$M^n + a_{n-1}M^{n-1} + a_{n-2}M^{n-2} + \dots + a_0I = 0$$

Meaning that M^n is a linear combination of $M^{n-1} + M^{n-2} + \dots + I$. Remember that if the system is controllable, we would be able to find such controller to the system, which would make the system stable, which means that the error goes to zero.

9.1 Controllability of Discrete LTI

Consider discrete LTI.

$$x_{i+1} = Ax_i + Bu_i$$

Let's expand it numerically:

$$x_2 = Ax_1 + Bu_1$$

$$x_3 = Ax_2 + Bu_2 = A(Ax_1 + Bu_1) + Bu_2 = A^2x_1 + ABu_1 + Bu_2$$

...

$$x_{n+1} = A^n x_1 + A^{n-1}Bu_1 + \dots + A^{n-k}Bu_k + \dots + Bu_n$$

$$x_{n+1} - A^n x_1 = \begin{bmatrix} B & AB & A^2B \end{bmatrix} \begin{bmatrix} u_n \\ u_{n-1} \\ \vdots \\ u_1 \end{bmatrix}$$

Thus, we showed that $x_{n+1} - A^n x_1$ must be in the column space of $C = \begin{bmatrix} B & AB & A^2B \end{bmatrix}$

Now, note that since x_{n+1} can be any real number and x_1 can take a zero value, \mathbb{R} must be in the column space of C. So, C must be a full-rank matrix.

Controllability

A system $x_{i+1} = Ax_i + Bu_i$ is controllable (or any state can be reached) if $C = [B \ AB \ A^2B]$ is full row rank.

9.2 Observability of Discrete LTI

Observability criterion shows whether it is in principle possible to estimate the system or not.

Consider a discrete LTI:

$$\begin{cases} x_{i+1} = Ax_i + Bu_i \\ y_i = Cx_i \end{cases}$$

And a Luenberger observer:

$$\hat{x}_{i+1} = A\hat{x}_i + Bu_i + L(y_i - C\hat{x}_i)$$

Change of variables: $e_i = \hat{x}_i - x_i$ will provide us with the following equation:

$$e_{i+1} = Ae_i + L(y_i - C\hat{x}_i)$$

$$e_{i+1} = Ae_i - LCe_i$$

Introduce the dual system (which is stable iff the original system is stable):

$$\epsilon_{i+1} = A^T \epsilon_i - C^T L^T \epsilon_i$$

$$\begin{cases} \epsilon_{i+1} = A^T \epsilon_i - C^T v_i \\ v_i = -L^T \epsilon_i \end{cases}$$

Controllability matrix for the system:

$$O^T = \begin{bmatrix} C^T & A^T C^T \dots & A^{T^{n-1}} C^T \end{bmatrix}$$

$$O = \begin{bmatrix} C \\ CA \\ \vdots \\ CA^{n-1} \end{bmatrix}$$

Observability

A system $x_{i+1} = Ax_i + Bu_i$ is **observable** (or observation error can go to 0 from any initial position) if $O = \begin{bmatrix} C \\ \vdots \\ CA \\ CA^{n-1} \end{bmatrix}$ is full column rank.

10 Kalman Filter

11 Reference materials

(Controllability. Observability)

12 Linearization

While linear models are present in the real world (examples include DC motors, 3D printers, and mass-spring-damper systems), the majority of real-world systems are nonlinear (such as cars, airplanes, robot arms, underwater robots, and almost any mechanical system with linkages).

However, there is a method to describe these systems using our toolkits - through linearization.

Linearization is the technique that enables us to create a linear model for a nonlinear system.

So, we can introduce linear models for nonlinear systems that could describe the system pretty well locally. We can do control for this local approximation.

12.1 Taylor expansion

Taylor expansion around node.

Let's consider a non-linear dynamical system $\dot{x} = f(x, u)$ and a Taylor expansion around the node (x_0, u_0) , i.e., $f(x_0, u_0) = 0$, $x_0 = \text{const}$, $u_0 = \text{const}$.

Recall the physical meaning of a **node**: it is any position at which the robot remains static.

$$f(x, u) \approx f(x_0, u_0) + \frac{\partial f}{\partial x}(x - x_0) + \frac{\partial f}{\partial u}(u - u_0) + \text{HOT}$$

HOT = high-order terms.

(x_0, u_0) are an expansion point.

Now let's introduce new variables e and v that represent the distances from the expansion point:

$$e = x - x_0$$

$$\dot{e} = \dot{x}$$

$$v = u - u_0$$

Then we can rewrite the Taylor expansion:

$$\dot{e} \approx \frac{\partial f}{\partial x}e + \frac{\partial f}{\partial u}v + \text{HOT}$$

$$\dot{e} \approx Ae + Bv + \text{HOT}$$

Let's drop the high-order term and get an approximation. And this approximation is called linearization.

$$\dot{e} = Ae + Bv$$

In this context, (x_0, u_0) is a linearization point.

This type of linearization is proved to provide the best possible linear model for the given system.

Taylor expansion along a trajectory.

Now let's consider a non-linear dynamical system:

$$\dot{x} = f(x, u)$$

and a trajectory $x_0 = f(x_0, u_0)$. Note that now x_0 is not a point - it is a whole trajectory

$$f(x, u) \approx f(x_0, u_0) + \frac{\partial f}{\partial x}(x - x_0) + \frac{\partial f}{\partial u}(u - u_0) + \text{HOT}$$

We can denote $\dot{e} = \dot{x} - \dot{x}_0 = f(x, u) - f(x_0, u_0)$.

The rest stays the same: $e = x - x_0, v = u - u_0$

$$\dot{e} \approx Ae + Bv + \text{HOT}$$

Let's drop HOT and obtain linearization:

$$\dot{e} = Ae + Bv$$

Basically, nothing changes between expansion around a node and expansion along a trajectory as long as we introduce the change of variables described above. The change of variables is slightly different, but original function and the local approximation behave in the same way in the region of the linearization point.

So, can we linearize around each and any point?

- 1) If it is a node - yes.
- 2) If we want to linearize around some other point - yes, but the change of variables would entail slightly different results.

While we had:

$$e = x - x_0, \dot{e} = \dot{x},$$

now \dot{e} is the difference between the derivative of the state of our non-linear system and derivative of the state of our trajectory distance from the trajectory linearization.

The meaning of the variables changes slightly, but the mathematical expression is the exact same expression.

Affine expansion

The other way to obtain linearization, without change of variables is as follows.

$$f(x, u) \approx f(x_0, u_0) + A(x - x_0) + B(u - u_0)$$

Denoting

$$f(x_0, u_0) - Ax_0 - Bu_0 = c$$

$$\dot{x} = Ax + Bu + c$$

c makes it not a linear model, but affine, which means it has a constant term.

It can be a constant in the case of a node, and a function of time in the case of expansion along the trajectory.

Often we choose u to compensate c , so u will also be affine in this case.

12.2 Manipulator equations

Frequently, in robotics we deal with the following equation when describing a system:

$$H\ddot{q} + C\dot{q} + g = \tau$$

which is called a **manipulator equation**

However, cars, underwater robots are usually described by the other equations - Euler or Lagrangian equations.

Let's derive linearization for the manipulator equation.

Begin by proposing new variables:

$$x = q - \vec{q}_0, \dot{x} = \dot{q} - \dot{\vec{q}}_0$$

$$u = \tau - \tau_0$$

Points around which we linearize are denoted from equation:

Let's introduce

$$\phi(\dot{q}, q, t) = H^{-1}(\tau - C\dot{q} - g)$$

13 Lyapunov theory

Stability is not defined only for linear systems, but for nonlinear systems as well.

There exist a small neighbourhood. Every solution that starts from this neighbourhood will asymptotically approach the same solution.

Asymptotic stability criteria:

Autonomous dynamic system $\dot{x} = f(x)$ is asymptotically stable if there exists a scalar function $V = V(x) > 0$.

Note that computing $\dot{V}(x)$ comes along with computing \dot{x} . We can think of $V(x)$ as energy (pseudo-energy).

Asymptotic stability means that the system converges, and marginal stability means that the system does not diverge.

Asymptotic stability

The system is called asymptotically stable if there exists a function $V > 0$ such that $\dot{V} < 0$, except for $V = 0, \dot{V} = 0$.

Marginal stability

The system $\dot{x} = f(x)$ is stable in the sense of Lyapunov if there exists $V > 0$ such that $\dot{V} \leq 0$.

Lyapunov function

A function $V > 0$ in this case is called a Lyapunov function.

Example 1 Consider the following system:

$$\dot{x} = -x$$

Let's introduce a function $V = x^2 > 0$ for all $x \neq 0$. $\dot{V} = 2x \cdot \dot{x} = 2x(-x) = -2x^2 < 0$. V satisfies the Lyapunov criteria, so the system is (asymptotically) stable.

Example 2 Consider the equation of the pendulum:

$$\ddot{q} = -\dot{q} - \sin(q)$$

13.1 LaSalle's Principle

The system is called stable if

LaSalle's principle allows us to prove asymptotic stability even for $\dot{V}(x) \leq 0$ only for the trivial solution.

13.2 Linear case

Lyapunov theory applies for both nonlinear and linear systems. For linear systems the following feature exist:

For a system $\dot{x} = Ax$, we can always choose a Lyapunov candidate function in the form:

$$V = x^T S x,$$

where S is positive-definite

$$\dot{V} = \dot{x}^T S x + x^T S \dot{x} = (Ax)^T S x + x^T S A x = x^T A^T S x + x^T S A x = x^T (A^T S + S A) x$$