

01/04/2021

Recall : Voltage reflection coefficient
 Γ or ρ

$$\Gamma = \frac{V_0^-}{V_0^+} = \frac{Z_L - Z_0}{Z_L + Z_0}$$

Z_L is complex
 $\therefore \Gamma$ " " "

$$\frac{I_0^-}{I_0^+} = -\frac{V_0^-}{V_0^+} = -\Gamma$$

change of phase by 180°

$$Z_L = Z_0 \left(\frac{1 + \Gamma}{1 - \Gamma} \right)$$

1. Matched load (perfect matched)

$$Z_L = Z_0 \Rightarrow \Gamma = \frac{Z_L - Z_0}{Z_L + Z_0} = 0$$

Z_0 \rightarrow Z_0

0% reflection

X 2. Short-circuited line

$$Z_L = 0 \Rightarrow \Gamma = -1 = 1 \angle 180^\circ$$



100% reflection
with change of phase by 180°
w.r.t. incident wave

X 3. Open-circuited line

$$Z_L = \infty \Rightarrow \Gamma = 1 \rightarrow 100\% \text{ reflection}$$

Z_0 \rightarrow o.c.

with no change of phase

Ex: 50 Ω line terminated in a 75 Ω load

$\rightarrow (Z_0 = 50 \Omega)$

$$\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{75 - 50}{75 + 50} = \frac{25}{125} = \frac{1}{5} = 0.2$$

$= 20\%$

Application:

TDR (Time Domain Reflectometry)

\rightarrow measured reflected signal



$$v = \frac{3 \times 10^8 \text{ m/s}}{\sqrt{\epsilon_r}}$$

$$t = \text{measured}$$

$$\text{distance} = v \times t$$

$$\Gamma = |\Gamma| e^{j\theta_r} = |\Gamma| \angle \theta_r$$

↙
magnitude
of ref. coeff.

↘ angle of reflection
coefficient

$$-1 \leq \Gamma \leq 1$$

$$0 \leq |\Gamma| \leq 1$$

0% to 100%

$$x + jy \quad \text{or} \quad R \angle \theta$$

$$x = R \cos \theta$$

$$y = R \sin \theta$$

$$R = \sqrt{x^2 + y^2}$$

$$\theta = \tan^{-1} \left(\frac{y}{x} \right)$$

Complex
nos.

Example: A $100\ \Omega$ transmission line is connected to a load consisting of $50\ \Omega$ resistor in series with a $10\ \text{pF}$ capacitor. Find reflection coefficient for $100\ \text{MHz}$ signal

Sol: $Z_0 = 100\ \Omega$
 $f = 100\ \text{MHz} \Rightarrow \omega = 2\pi f = 2\pi \times 10^8\ \text{Hz}$
 $Z_L = 50\ \Omega$ resistor in series with a capacitor of $10\ \text{pF}$
 $(10 \times 10^{-12}\ \text{F})$
 $Z_L = R_L + jX_C$
 $= R_L - \frac{j}{\omega C} = 50 - \frac{j}{2\pi \times 10^8}$
 $= 50 - j159\ \Omega$

$$\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{50 - j159 - 50}{50 - j159 + 50}$$

$$= x + jy$$

RLO

$$= -0.76 e$$

$$+j119.3^\circ$$

$$= 0.76 e^{+j119.3^\circ} = j180^\circ$$

$$= +0.76 e^{-j60.7^\circ}$$

$$= +0.76 \angle -60.7^\circ$$

$$|\Gamma|_{\text{or}} \downarrow |\Gamma| = 0.76 = 76\% \text{ reflection}$$

$$R = \sqrt{x^2 + y^2}$$

$$\theta = \tan^{-1}\left(\frac{y}{x}\right)$$

Show that $|\Gamma| = 1$ for purely reactive load

purely reactive $\Rightarrow R = 0$

$$X = X_L \text{ or } X_C$$

\downarrow
inductive

\downarrow
capacitive
load

Impedance

$\leftarrow Z = 5 + j40 \Omega$

\hookrightarrow inductive load

$$Z = +j40 \Omega$$

\hookrightarrow purely inductive load

$$Z = 20 - j30 \Omega$$

\hookrightarrow capacitive load

$$Z = -j30 \Omega$$

\hookrightarrow purely capacitive load

Let Z_L be purely inductive wave

$$\Rightarrow Z_L = jX_L$$

$$\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{jX_L - Z_0}{jX_L + Z_0}$$

$$= \frac{-(Z_0 - jX_L)}{Z_0 + jX_L} = \frac{-\sqrt{Z_0^2 + X_L^2} e^{-j\theta}}{\sqrt{Z_0^2 + X_L^2} e^{j\theta}},$$

$$\Gamma = -e^{-j2\theta} \text{ where } \theta = \tan^{-1}\left(\frac{X_L}{Z_0}\right)$$

$$\therefore |\Gamma| = |e^{-j2\theta}| = \left[(e^{-j2\theta}) (e^{-j2\theta})^* \right]^{1/2}$$

$$\Rightarrow \boxed{|\Gamma| = 1}$$

complex conjugate

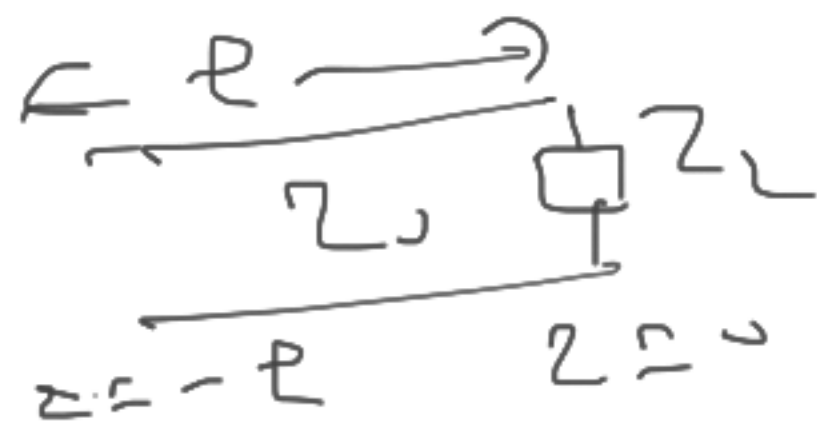
STANDING WAVES

Assume line
to be lossless, i.e., $\alpha = 0 \Rightarrow \gamma = \alpha + j\beta = j\beta$

For this, we recall

$$\textcircled{9} \text{ or } \textcircled{A} : V_0^+ e^{-j\beta z} + V_0^- e^{+j\beta z}$$

$$\textcircled{10} \text{ or } \textcircled{B} : \frac{V_0^+}{Z_0} e^{-j\beta z} - \frac{V_0^-}{Z_0} e^{j\beta z}$$



Using $\frac{V_0^-}{V_0^+} = \Gamma \Rightarrow \underline{V_0^- = \Gamma V_0^+}$

$$\therefore \textcircled{A} : V(z) = V_0^+ (e^{-j\beta z} + \Gamma e^{j\beta z})$$

$$\textcircled{B} : I(z) = \frac{V_0^+}{Z_0} (e^{-j\beta z} + \Gamma e^{j\beta z})$$

$$|V(z)| = [V(z) \cdot V^*(z)]^{1/2}$$

complex conjugate

$$= \left[\left\{ V_0^+ (e^{-j\beta z} + \Gamma e^{j\beta z}) \right\} \cdot \left\{ (V_0^+)^* (e^{j\beta z} + \Gamma e^{-j\beta z}) \right\} \right]^{1/2}$$

$$= \left[\left\{ V_0^+ (e^{-j\beta z} + |\Gamma| e^{j\theta_r} e^{j\beta z}) \right\} \cdot \left\{ (V_0^+)^* (e^{j\beta z} + |\Gamma| e^{-j\theta_r} e^{-j\beta z}) \right\} \right]^{1/2}$$

$$[\therefore \Gamma = |\Gamma| e^{j\theta_r}]$$

$$\Rightarrow |V(z)| = |V_0^+| \left[1 + |r|^2 + |r| e^{j(2\beta z + \theta_r)} + e^{-j(2\beta z - \theta_r)} \right]^{\frac{1}{2}}$$

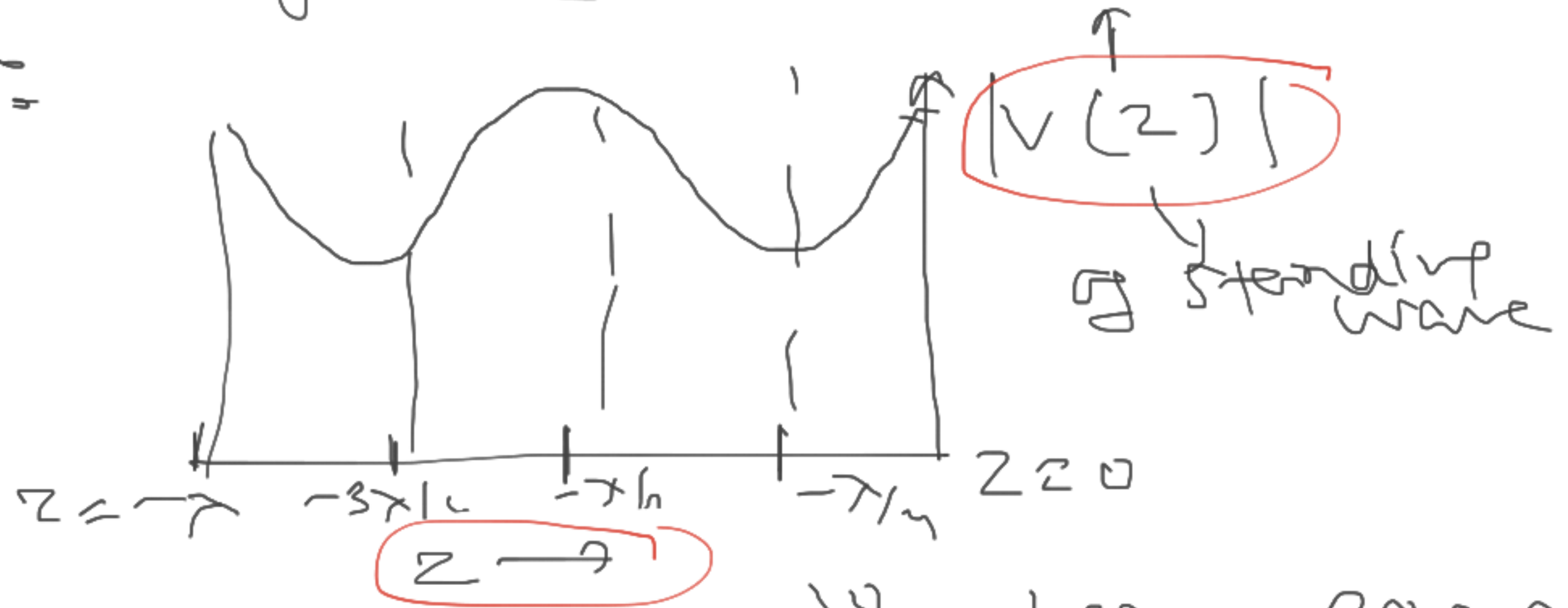
$$\Rightarrow |V(z)| = V_0^+ \left[1 + |r|^2 + 2|r| \cos(2\beta z + \theta_r) \right]^{\frac{1}{2}}$$

$$\left[e^{jx} + e^{-jx} = 2 \cos x \right] \quad \text{--- (c)}$$

Similarly, we can derive for $I(z)$

$$\text{Here, } \beta = \frac{2\pi}{\lambda}$$

The variation of $|V(z)|/|I(z)|$ as a function of z (position on transmission line) is:



At 1 GHz , $\lambda = \frac{c}{f} = \frac{3 \times 10^{10} \text{ cm/sec}}{1 \times 10^9} = \underline{\underline{30 \text{ cm}}}$

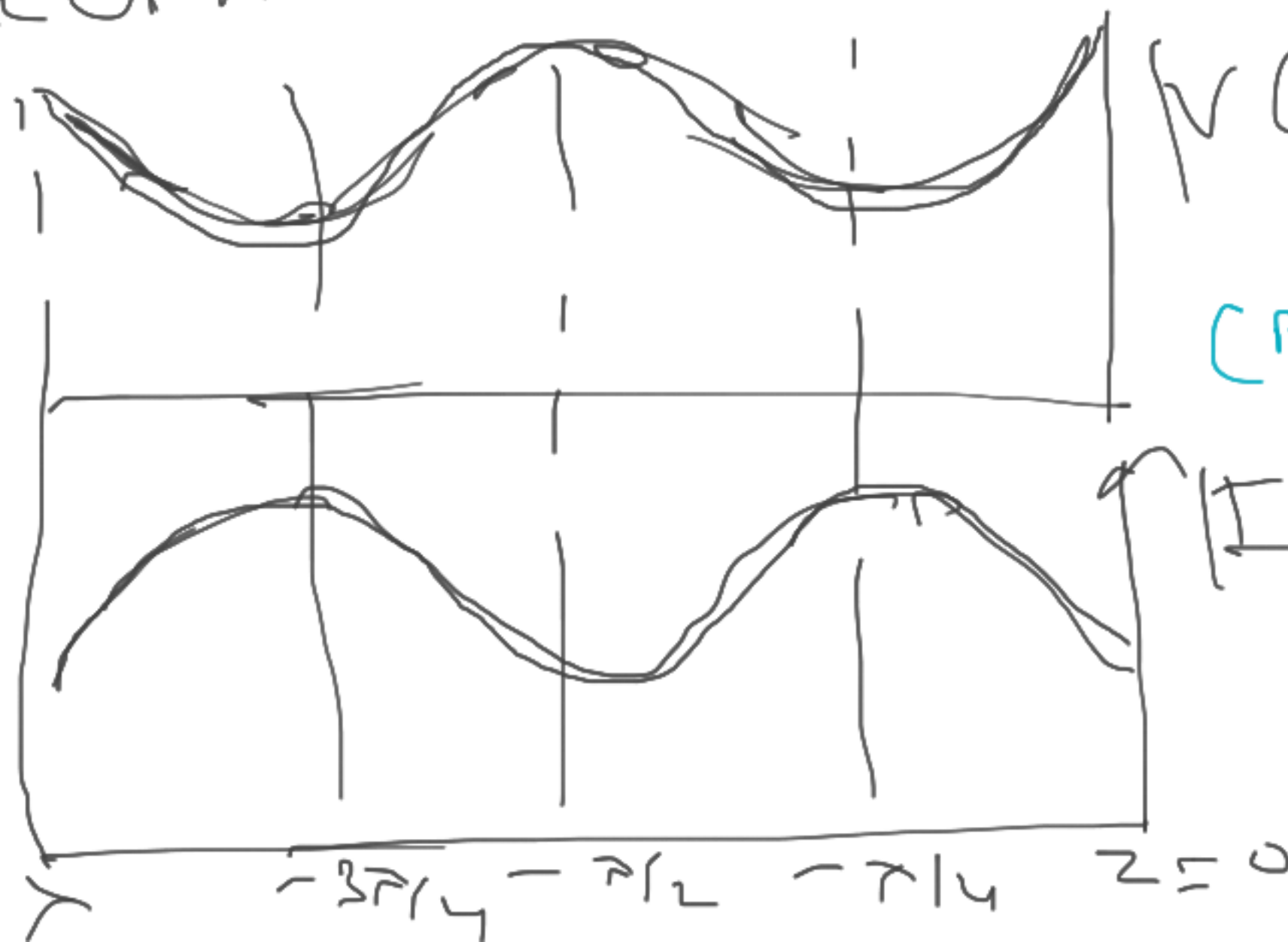
(1 GHz)

Electrical length λ at 1 GHz
 $\lambda/2 = 15 \text{ cm} \Rightarrow$ electrical length $= \frac{\lambda}{2}$ at 1 GHz

If free 24 Hz, $\lambda = 15 \text{ cm}$
 $\Rightarrow 1 \lambda @ 24 \text{ Hz}$ (for 15 cm)
 $0.5 \lambda @ 24 \text{ Hz}$ (for 7.5 cm)

\Downarrow
 electrical length

Standing wave
 (superposition
 of incident
 & reflected
 waves)
 \rightarrow pure wave



$|V(z)| \Rightarrow$ maximum
 & minimum
 (peak & null
 crest & trough)

$|I(z)| \Rightarrow$ voltage
 maximum
 \Downarrow
 current
 minimum
 & vice versa

Standing wave means positions of maxima & minima always remain same for a particular load

Positions of maxima & minima
& amplitude " " " " " "
for a given load

to be determined

(S.C.,
O.C.,
matched
load
(M.L.)
or
any other
load in
genl.
 $[Z_L = R_L + jX]$)

The amplitude of maxima & minima?

The max. value of standing wave pattern of $|v(z)|$ corresponds to position on line at which incident & reflected waves are in phase.

[incident \rightarrow forward travelling wave
reflected \rightarrow backward travelling wave]

$$\text{i.e., } (2\beta z + \theta_r) = 2n\pi$$



or, $2\beta z_{\max} + \theta_r = 2n\pi$

$n = 0, 1, 2, 3, \dots$

$$\therefore |v(z)|_{\max} = |v_0^+| [1 + |r|^2 + 2|r|(1)]^{\frac{1}{2}}$$

from
Eqn (C)

$$= |v_0^+| [(1 + |r|)^2]^{\frac{1}{2}}$$

$$|v(z)|_{\max} = |v_0^+| [1 + |r|]$$

m.l.
if $|r| \approx 0$, $|v(z)|_{\max} = |v_0^+|$

if $|r| \approx 1$, $|v(z)|_{\max} = 2|v_0^+|$

if $|r| \approx 0.3$, $|v(z)|_{\max} = |v_0^+| [1 + 0.3]$

s.r.c.
or
o.c